# FINAL DESIGN NOISE IMPACT ANALYSIS TECHNICAL REPORT



# RESTON AVENUE TO JARRET VALLEY DRIVE A DESIGN-BUILD PROJECT

#### **UPC 99478**

State Project No. 007-029-942 and 007-029-225
Federal Project No. STP-5A01(745) and STP-5A01(790)
Contract ID Number: C00099478DB98

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NOVEMBER 20, 2019 REVISED JANUARY 18, 2022

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#### 1.0 EXECUTIVE SUMMARY

This report describes the details of a final design noise impact assessment completed for the Route 7 Corridor Improvements project (Reston Avenue to Jarret Valley Drive) in Fairfax County, Virginia (**Figure 1**). The noise analysis was conducted in accordance with Federal Highway Administration (FHWA) and Virginia Department of Transportation (VDOT) noise assessment regulations and guidelines. The FHWA regulations are set forth in 23 CFR Part 772. VDOT's revised policy was updated most recently on February 20, 2018.

The scope of the Route 7 Corridor Improvements project involves constructing an additional general purpose through lane for each direction of travel extending 6.9 miles from Reston Avenue to Jarret Valley Drive in Fairfax County. Route 7 will be widened from two lanes to three lanes in each direction, including major intersection improvements. Service drives will be constructed as needed for access to driveways and to complete connections. The project also includes a shared-use path on both sides along the corridor. The project is expected to improve traffic flow and provide immediate congestion relief to the roadway corridor.

The study involved monitoring of existing noise conditions and modeling of 2018 existing conditions and future design year (2040) build condition in the study area with the FHWA-approved computerized Traffic Noise Model. The worst-case noise hour was established for both eastbound and westbound noise receptors using VDOT's ENTRADA traffic modeling software. A total of 1,234 receptors representing 1,234 noise-sensitive sites were modeled within 14 Common Noise Environments (CNEs) in the project study area. These 1,234 modeled sites include 1,092 residential dwellings units, a recreational trail (47 trail units), two cemeteries (25 cemetery grid units), 10 churches, four outdoor nurseries, four picnic areas, 13 playgrounds, four schools, an outdoor sports complex (30 grid units), basketball and volleyball courts, and a community pool (some locations are represented by more than one receptor).

**Table 1** provides a summary of existing and future noise levels and impacts for each CNE in the study area. Impacts are predicted to occur for existing conditions in CNEs A, B, C, D, E, F, G, H, I, J, K, L, and N. Existing noise impacts were predicted at 161 receptors including single-family residential dwelling units, two cemeteries, a recreational trail, a schoolyard, and an athletic field in the study area. The worst-case noise hour existing noise levels ranged from 40 to 73 dBA. The future design year (2040) build condition resulted in noise impacts at the same CNEs impacted under the existing conditions (CNEs A, B, C, D, E, F, G, H, I, J, K, L, and N).

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#### **TABLE 1** SUMMARY OF PREDICTED EXTERIOR NOISE LEVELS FOR THE WORST HOUR

Í			Range of Predicted Exterior Noise Levels and Impacts for the Worst Hour							
ONE	Lord Hos. Bosovietica	Activity Category		Existi	ng	:	2040 Bı	ıild		
CNE	Land Use - Description		Sound Level (dBA)		Number of		l Level BA)	Number of		
			Min	Max	Impacts	Min	Max	Impacts		
	Single-family homes in Cedar Chase development (Cedar Chase Road, Cedar Chase Court), Estates of North Hills (Water Pointe Lane, Water Pointe Circle, and Round Pebble Lane), and Reston Parkway	В	41	66	1	43	67	2		
A	Boyd School Playground; North Pointe Fire Station Picnic table; Great Falls Assisted Living Patio	С	55	59	0	56	61	0		
	Good Shepherd Lutheran Church; The Boyd School – Reston Campus	D	30	32	0	30	33	0		
	Single-family homes in Autumn Wood development (Aidan Run Court, Autumn Mist Lane), Shain Court, Northfalls Court, Bowen Avenue, Loran Court, Loran Road, and Utter- back Store Road	В	49	71	14	52	73	17		
В	Dog Park	С	5	1	0	5	2	0		
	Seneca Hill Animal Hospital, Dranesville Church of the Brethren, MTO Shahmaghsoudi School of Islamic Sufism	D	26	44	0	32	46	0		
	Meadows Farms Nurseries and Landscaping	E	6	2	0	6	5	0		
С	Single-family homes in Wyndham Hills Development (Stones Throw Drive, Fieldview Drive), Bright Pond Lane, Piney Run Meadows Development (Tommye Lane, Meadowlook Court), Bishopsgate Way, Falls Park Estates (Markell Court), Great Falls Crossing (Hunter Gate Way), and Baron Cameron Avenue	В	45	72	16	48	73	21		
	Great Falls Crossing Community Center (Pool, tennis, basketball, picnic area, pavilion, playground)	С	55	64	0	57	65	0		
D	Single-family homes on Utterback Store Road, Great Passage Court, and Great Passage Boulevard	В	48	71	2	50	72	2		
	Nike Park soccer/softball fields	С	50	64	0	54	68	2		
Е	Single-family homes along Great Passage Boulevard, Kettle Pond Lane, Amanda Drive, Riva Ridge Drive, Piney Pond Drive, Mountain Hope Court, Crippen Court, and Springvale Road	В	46	70	10	48	71	16		
F	Single-family homes on Springvale Road, Springvale Court, Van Patten Lane, Colvin Run Road, Colvin Meadows Court, Colvin Meadows Lane, Lees Meadows Court, Robindale Drive, Hessick Court, Locust Hill Drive, and Trotting Horse Lane; Colvin Run Mill; cemetery	В	43	72	24	45	74	28		
	Unnamed Cemetery, Colvin Run Mill	С	59	72	3	61	74	4		
	Meadows Farms Nurseries and Landscaping; Hills Nursery	E	65	68	0	68	70	0		



#### TABLE 1 (CONTINUED)

ı			Range of Predicted Exterior Noise Levels and Impacts for the Worst Hour								
CNE	Land Has Description	Activity		Existin	ng	2	2040 Bı	ıild			
CNE	Land Use - Description	Category	Sound Level (dBA)		Number of		l Level BA)	Number of			
			Min	Max	Impacts	Min	Max	Impacts			
G	Single-family homes on Water Falls Lane, Dunn Meadows Court, Cobble Pond Way, Dunn Meadows Road, Delta Glenn Court, Newkirk Court, Mill Wheel Lane, Colvin Forest Lane, Scenic View Terrace, Grapes Farm Way, Carpers Farm Court, Middleton Ridge Road, Middleton Court, Difficult Run Court, Tweed Court, and Beulah Road	В	42	72	38	45	74	46			
	Capital Church Picnic Area, Beulah Dental, Chesterbrook Academy Preschool playground	С	61	65	0	65	69	1			
	Capital Church; Chesterbrook Academy Preschool	D	32	45	0	36	48	0			
н	Single-family homes on Trotting Horse Lane, Fairpine Lane, Forestville Drive, Farmingdale Court, Vernon Drive, Lyons Street, Kenmore Drive, and Towlston Road	В	47	73	14	48	75	15			
''	The Eastern Ridge School outdoor activity area	С	61	73	3	65	77	5			
	The Eastern Ridge School	D	3	4	0	3	8	0			
	Single-family homes on Beulah Road, Deramus Farm Court, Atwood Road, Robnel Place, Stokley Way, Vanetta Lane, Kilby Glen Drive, and Towlston Road	В	44	71	10	49	74	13			
'	Picnic area at the Fairfax County Fire Station 42	С	5	0	0	5	3	0			
	Wolf Trap Nursery	E	6	8	0	7	0	0			
	Single-family homes on Towlston Road, Schuman Court, and Windsor Meadows Lane	В	48	69	2	51	70	2			
J	Andrew Chapel Cemetery	С	56	73	6	58	73	8			
	St. Athanasius Roman Catholic Church	D	4	2	0	4	4	0			
	Trap Road, Lucky Estates Drive, Timberwolf Court, Trailridge Court, Wolftrap Run Road, and Route 7	В	45	68	3	48	70	5			
К	Andrew Chapel playground, Jills House playground, McLean Bible Church playground	С	50	62	0	51	63	0			
	Andrew Chapel United Methodist Church, Bethel Baptist Church, Jills House, McClean Bible Church	D	35	37	0	35	40	0			
L	Single-family residences on Route 7, Dreamweaver Court, Royal Estates Drive, Old Tolson Mill Road, Brook Road, Gal- lant Green Drive, Gunnell Court, Woodside Drive, and Lew- insville Road	В	41	71	5	43	73	6			
	Providence Baptist Church playground and volleyball Court	С	57	62	0	61	65	0			
	Providence Baptist Church, St Thomas Episcopal Church/ McLean Preschool	D	36	37	0	37	38	0			



TABLE 1 (CONTINUED)

			Range of Predicted Exterior Noise Levels and Impacts for the Worst Hour							
CNIE	Land Has Description	Activity		Existi	ng	:	2040 Bı	ild		
CNE	Land Use - Description	Category	Sound Level (dBA)		Number of		l Level BA)	Number of		
			Min	Max	Impacts	Min	Max	Impacts		
М	Single-family residences on Route 7, Mirador Place, Prestwould Place, Woodhurst Boulevard, and Mayhurst Boulevard	В	47	62	0	51	65	0		
N	Single-family residences on Laurel Hill Road, Glenridge Court, Old Ash Grove, Stanbridge Place, Carrington Ridge Lane, Broadstone Place, and Jarret Valley Drive	В	43	70	1	48 73		11		
	Berea Church of Christ	D	32 0 33		0					
F/G	Cross County Trail	С	56	72	7	58	73	18		
	Total Impacted Dwellings				159			222		

The widening results in an average 3 dBA increase in the acoustical environment over existing conditions. The future design year (2040) build noise levels are predicted to range from 43 to 77 dBA. Future noise impacts were predicted at 222 receptor locations including 184 single-family residential dwelling units, two cemeteries, a recreational trail (18 receptors), two schoolyards, and an athletic field in the study area. Changes in the number of impacted areas from the noise analysis completed during preliminary design were a result of refined noise modeling detail, updated traffic data, refined proposed topography and cut/fill detail, and increased receptor density.

Noise abatement must be considered where noise impact is predicted to occur with the 2040 Build alternative. Noise abatement is evaluated to determine if it is warranted, feasible, and reasonable. **Table 2** summarizes the total length, estimated cost, and benefits that would be provided by the noise barriers that were evaluated in this study. Noise abatement was determined to be feasible and reasonable for the majority of the CNEs (CNE A, B, C, D, E, F, G, H, I J, K, L, and N).

Construction activity may cause intermittent fluctuations in noise levels. During the construction phase of the project, all reasonable measures will be taken to minimize noise impact from these activities.



TABLE 2
SUMMARY OF NOISE BARRIERS EVALUATED IN THIS STUDY

		Marina	luon o oto d			Noise B	arrier Deta	ils	Conform Amond	خ	e?
CNE	Barrier ID	Number of Impacted Receptors	Impacted and Benefitted Receptors	Non-Impacted and Benefitted Receptors	Length (ft)	Average Height Range (ft)	Surface Area (SF)	Cost at \$42/SF	Surface Area/ Benefitted Receptor (SF/BR) <sup>1</sup>	Feasible?	Reasonable?
Α	A1	1	1	4	600	16	9,597	\$403,074	1,919	Υ	N
	A2	1	1	12	1,286	16	20,117	\$844,914	1,547	Υ	Υ
B/D	B1-B5, D1	19	19	49	5,593	15	83,891	\$3,523,422	1,234	Υ	Υ
D/E	D2, E1-E4	18	18	24	4,326	15	64,888	\$2,725,296	1,545	Υ	Υ
С	C1-C2	21	21	47	5,140	15	77,096	\$3,238,032	1,134	Υ	Υ
	F1, F1B, F1C, F2	8	7	3	1,127	13	14,658	\$615,636	1,466	Υ	Υ
F	F3	12	12	14	2,546	16	40,735	\$1,710,870	1,567	Υ	Υ
	F4-F4B	6	6	16	2,210	16	35,352	\$1,484,784	1,607	Ν	
	F5-F9	8	8	17	2,489	22	54,789	\$2,301,138	2,192	Υ	N
	G1-G6	24	24	54	5,350	18	96,303	\$4,044,726	1,234	Υ	Υ
	G8-G9	16	15	13	1,906	14	26,678	\$1,120,476	953	N	
G	G10-G13	20	20	10	2,591	17	44,649	\$1,875,258	1,488	Υ	Υ
	G14-G16	3	3	1	801	16	12,831	\$538,902	3,208	Υ	N
Н	H2-H11	20	18	24	3,901	16	61,772	\$2,594,424	1,470	Υ	Υ
	12	5	5	2	835	13	10,852	\$455,784	1,550	Υ	Υ
	14-6	8	8	4	1,041	16	16,654	\$699,468	1,388	Υ	Υ
J/K	J2-J3, K1-K4	15	14	27	3,094	16	49,494	\$2,078,748	1,207	Υ	Υ
	L1-L5	4	3	1	974	12	11,693	\$491,106	2,923	Υ	N
L	L6-L8	2	2	2	852	12	9,703	\$407,526	2,426	Υ	N
	Existing Barrier N	10	0	1	307	15	4,607	\$193,494	4,607	N	
N	N1-N3 and Existing	10	9	6	1,577	14	23,132	\$971,544	1,542	Υ	Υ
	N4	1	1	0	301	18	5,427	\$227,934	5,427	Υ	N

1 Where Square Feet/Benefitted Receptor (SF/BR) exceeds VDOT's maximum of 1,600, a noise barrier would not be considered cost-reasonable.

Route 7 Widening: Reston Avenue to Jarrett Valley Drive State Project 0007-029-942, 0007-029-225



#### 2.0 INTRODUCTION

#### 2.1 BACKGROUND AND PURPOSE

A final design traffic noise analysis was performed for the Route 7 Corridor Improvements slated from Reston Avenue to Jarret Valley Drive located in Fairfax County, Virginia. All highway noise impact assessment procedures, noise abatement criteria, and documentation are in accordance with the Federal Highway Administration (FHWA) and Virginia Department of Transportation (VDOT) noise assessment regulations and guidelines. FHWA regulations for highway traffic noise for federal-aid highway projects are contained in Title 23 of the United States Code of Federal Regulations Part 772 (23 CFR 772), updated July 13, 2011. The current VDOT State Noise Abatement Policy became effective on July 13, 2011, and was updated on February 20, 2018. The FHWA regulations for mitigation of highway traffic noise in the planning and design of federally aided highway projects contained in 23 CFR 772 state that a "Type I" traffic noise impact analysis is required when there is the addition of through-traffic lanes or ramps in an interchange.

This report documents a summary of the roadway improvements under study, a description of noise terminology, the applicable standards and criteria, the computations of existing and future noise levels, a projection of future noise levels, identification of potential noise impacts, evaluation of measures to mitigate noise impacts, noise abatement, a discussion of construction noise, and information to assist local officials.

#### 2.2 PROJECT DESCRIPTION

The scope of the Route 7 Corridor Improvements project involves constructing an additional general purpose through lane for each direction of travel extending 6.9 miles from Reston Avenue to Jarret Valley Drive in Fairfax County. A "Preliminary Noise Analysis" was completed as part of the EA documentation, and multiple noise barriers were identified as potentially warranted, feasible, and reasonable at that time. This Final Design Noise Impact Analysis Technical Report is being completed consistent with the requirements of the final design details that have been developed.

Route 7 will be widened from two lanes to three lanes in each direction, including major intersection improvements. Service drives will be constructed as needed for access to driveways and to complete connections. The project also includes a shared-use path on both sides along

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the corridor. The project is expected to improve traffic flow and provide immediate congestion relief to the roadway corridor.

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#### 3.0 METHODOLOGY

The Noise Control Act of 1972 gives the United States Environmental Protection Agency (U.S. EPA) the authority to establish noise regulations to control major noise sources, including motor vehicles and construction equipment. Furthermore, the U.S. EPA is required to set noise emission standards for motor vehicles used for interstate commerce and the FHWA is required to enforce the U.S. EPA noise emission standards through the Office of Motor Carrier Safety. The National Environmental Policy Act (NEPA) of 1969 gives broad authority and responsibility to federal agencies to evaluate and mitigate adverse environmental impacts caused by federal actions. FHWA is required to comply with NEPA, including mitigating adverse highway traffic noise effects. The Federal-Aid Highway Act of 1970 mandates FHWA to develop standards for mitigating highway traffic noise. It also requires FHWA to establish traffic noise level criteria for various types of land uses. The Act prohibits FHWA approval of federal aid highway projects unless adequate consideration has been made for noise abatement measures to comply with the standards. FHWA regulations for highway traffic noise for federal-aid highway projects are contained in 23 CFR 772. The regulations contain noise abatement criteria, which represent the maximum acceptable level of highway traffic noise for specific types of land uses. The regulations do not mandate that the abatement criteria be met in all situations but rather require that reasonable and feasible efforts be made to provide noise mitigation when the abatement criteria are approached or exceeded.

The State Noise Abatement Policy was developed to implement the requirements of 23 Code of Federal Regulations (CFR) Part 772 Procedures for Abatement of Highway Traffic Noise and Construction Noise (July 13, 2011), FHWA's Highway Traffic Noise Analysis and Abatement Policy and Guidance (December 2011), and the noise related requirements of The National Environmental Policy Act of 1969. The current VDOT State Noise Abatement Policy became effective on July 13, 2011 and was updated on February 20, 2018.

Noise is generally defined as unwanted or annoying sound. Airborne sound occurs by a rapid fluctuation of air pressure above and below atmospheric pressure. Sound pressure levels are usually measured and expressed in decibels (dB). The decibel scale is logarithmic and expresses the ratio of the sound pressure unit being measured to a standard reference level.

Most sounds occurring in the environment do not consist of a single frequency but rather a broad band of differing frequencies. The intensities of each frequency add to generate sound. Because the human ear does not respond to all frequencies equally, the method commonly used

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to quantify environmental noise consists of evaluating all of the frequencies of a sound according to a weighting system. It has been found that the A-weighted filter on a sound level meter, which includes circuits to differentially measure selected audible frequencies, best approximates the frequency response of the human ear.

Although the A-weighted noise level may adequately indicate the level of environmental noise at any instant in time, community noise levels vary continuously. Most environmental noise includes a conglomeration of noise from distant sources, creating a relatively steady background noise in which no particular source is identifiable. To describe the time-varying character of traffic noise, a statistical noise descriptor called the equivalent hourly sound level, or  $L_{eq(h)}$ , is commonly used.  $L_{eq(h)}$  describes a noise-sensitive receptor's cumulative exposure from all noise-producing events over a one-hour period.

Because decibels are logarithmic units, sound levels cannot be added by ordinary arithmetic means. The following general relationships provide a basic understanding of sound generation and propagation.

- An increase, or decrease, of 10 dB will be perceived by a receptor to be a doubling, or halving, of the sound level.
- Doubling the distance between a highway and receptor will produce a 3 dB sound level decrease.
- A 3 dB sound level increase is barely detectable by the human ear.

#### 3.1 NOISE ABATEMENT CRITERIA

The State Noise Abatement Policy has adopted the Noise Abatement Criteria (NAC) that have been established by FHWA (23 CFR 772) for determining traffic noise impacts for a variety of land uses. The NAC, listed in **Table 3** for various activities, represents the upper limit of acceptable traffic noise conditions and also a balancing of that which may be desirable with that which may be achievable. The NAC applies to areas having regular human use and where lowered noise levels are desired. They do not apply to the entire tract of land on which the activity is based, but only to that portion where the activity takes place. The NAC is given in terms of the hourly, A-weighted, equivalent sound level in decibels (dBA). The noise impact assessment is made using the guidelines listed in **Table 3**. The study area consists of exterior residential (Category B) land use, athletic/recreational fields (Category C), exterior commercial (Category E),

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the interior of public/institutional buildings (Category D), as well as other non-noise-sensitive land uses included in Category F and Category G (undeveloped).

TABLE 3
FHWA NOISE ABATEMENT CRITERIA
HOURLY A-WEIGHTED SOUND LEVEL DECIBELS (Leg(h) IN dBA)

Activity Category	Activity Criteria L <sub>eq(h)</sub>	Evaluation Location	Activity Description
А	57	Exterior	Lands on which serenity and quiet are of extraordinary significance and serve an important public need and where the preservation of those qualities is essential if the area is to continue to serve its intended purpose
B*	67	Exterior	Residential
C*	67	Exterior	Active sport areas, amphitheaters, auditoriums, campgrounds, cemeteries, daycare centers, hospitals, libraries, medical facilities, parks, picnic areas, places of worship, playgrounds, public meeting rooms, public or nonprofit institutional structures, radio studios, recording studios, recreation areas, Section 4(f) sites, schools, television studios, trails, and trail crossings
D	52	Interior	Auditoriums, day care centers, hospitals, libraries, medical facilities, places of worship, public meeting rooms, public or nonprofit institutional structures, radio studios, recording studios, schools, and television studios
E*	72	Exterior	Hotels, motels, offices, restaurants/bars, and other developed lands, properties or activities not included in A-D or F
F			Agriculture, airports, bus yards, emergency services, industrial, logging maintenance facilities, manufacturing, mining, rail yards, retail facilities, shipyards, utilities (water resources, water treatment, electrical), and warehousing
G			Undeveloped lands that are not permitted

Source: 23 CFR Part 772

#### 3.2 DEFINITION OF NOISE IMPACT

Traffic noise impacts occur if either of the following two conditions is met.

 The predicted traffic noise levels (future design year) approach or exceed the NAC, as shown in **Table 3**.

The VDOT State Noise Abatement Policy defines an approach level to be used when determining a traffic noise impact. The "Approach" level has been defined by VDOT as one dBA less than the Noise Abatement Criteria

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Includes undeveloped lands permitted for this activity category

for Activity Categories A to E. For example, for a Category B receptor, 66 dBA would be approaching 67 dBA and would be considered an impact. If design year noise levels "approach or exceed" the NAC, then the activity is impacted and a series of abatement measures must be considered.

 The predicted traffic noise levels are substantially higher than the existing noise levels.

A substantial noise increase has been defined by VDOT when the predicted (future design year) highway traffic noise levels exceed existing noise levels by 10 dBA or more for all noise-sensitive exterior activity categories. For example, if a receptor's existing noise level is 50 dBA and if the future noise level is 60 dBA, then it would be considered an impact. The noise levels of the substantial increase impact do not have to exceed the appropriate NAC. Receptors that satisfy this condition warrant consideration of highway traffic noise abatement.

If a traffic noise impact is identified within the project corridor, then consideration of noise abatement measures is necessary. The final decision on whether or not to provide noise abatement along a project corridor will take into account the feasibility of the design and overall cost weighted against the environmental benefit.

#### 3.3 NOISE PREDICTION MODEL

Since roadway noise levels can be determined accurately through computer modeling techniques for areas that are dominated by road traffic, design year traffic noise calculations have been predicted using the FHWA's Traffic Noise Model (FHWA TNM) Version 2.5, which is the latest approved version. The FHWA TNM® was developed and sponsored by the U.S. Department of Transportation and John A. Volpe National Transportation Systems Center, Acoustics facility. The TNM estimates vehicle noise emissions and resulting noise levels based on reference energy mean emission levels. The existing and proposed alignment (horizontal and vertical) are input into the model, along with the receptor locations, traffic volumes of cars, medium trucks (vehicles with two axles and six tires), heavy trucks, average vehicle speeds, pavement type, and any traffic-control devices. The TNM uses its acoustic algorithms to predict noise levels at the selected receptor locations by taking into account sound propagation variables such as, atmospheric absorption, divergence, intervening ground, barriers, building rows, and sometimes heavy vegetation.

Future build TNM runs were developed by modifying the validated existing condition models to account for the proposed highway widening. Roadway design engineering files and

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future terrain contour files were supplied by Dewberry. The modeling accounted for the variability in the local terrain and included the following parameters that affect the propagation of traffic noise: terrain lines, ground zones, and fixed height barriers to represent buildings. The default ground type used in the modeling was "lawn." The noise model also included a number of "empty" lanes (e.g., roadways without traffic) to represent paved shoulders and side streets.

To fully characterize future noise levels at all noise-sensitive land uses in the study area, noise prediction receivers (also called "receptors" and/or "sites") were added to the measurement sites in the TNM runs. A link to the TNM models is located in Appendix F.

#### 3.4 TRAFFIC DATA

The Environmental Traffic Data, ENTRADA (v.9-2018), Program developed by VDOT standardizes the production of environmental traffic data needed as input for noise analyses. ENTRADA utilizes look-up tables based upon the Highway Capacity Manual (HCM), Special Report 209; NCHRP Reports 365 (187), 387 and 504 (references provided in Section 10.0 of this report); and other nationally and internationally recognized sources to adjust free-flow speeds for different facility types (Freeways, Multi-Lane and Two-Lane Highways, and Urban Streets). It incorporates factors recommended by these documents in order to adjust free-flow speeds based upon number of lanes, access points, lateral clearances, median types, and lane widths.

Traffic volumes in hourly segments for a 24-hour period were provided for Route 7 by Dewberry in ENTRADA format for the 2018 existing conditions and future design year (2040) build conditions. Three roadway zones were established for the Route 7 corridor from west to east to account for variations in traffic volumes/composition:

- Zone one extends from Reston Avenue to Baron Cameron Avenue
- Zone two extends from Baron Cameron Avenue to Lewinsville Road
- Zone three extends from Lewinsville Road to Jarrett Valley Drive

Peak hour traffic (A.M. or P.M.) that corresponded closest to the worst-case noise hour was used for the side roads.



#### 3.4.1 Worst-Case Noise Hour

The traffic data used in the noise analysis must produce sound levels representative of the loudest ("worst noise") hour of the day in the future design year, per FHWA and VDOT policy. In many cases, experience has shown that the peak traffic hour may coincide with the worst noise hour of the day. However, on occasion, conditions such as capacity, effects of traffic on vehicle speed, higher than normal off-peak truck percentages, or unusual hourly traffic distribution may cause the worst noise hour of the day to be different from the peak traffic hour of the day. Due to peak-hour congestion on major commuter routes, the worst noise hour may occur during the off-peak period on such roadways.

Noise levels have been predicted for that hour of the day when the vehicle volume, operating speed, and number of trucks (vehicles with three or more axles) combine to produce the worst noise conditions. According to FHWA guidance, the "worst hourly traffic noise impact" occurs at a time when truck volumes and vehicle speeds are the greatest, typically when traffic is free-flowing and at or near level of service (LOS) C conditions.

The ENTRADA data for the Route 7 corridor was imported into the loudest hour determination spreadsheet developed by VDOT to evaluate the calculated noise levels at test receptors 200 feet from the source. Due to the differing peak traffic periods for Route 7 eastbound and westbound, the loudest hour was identified for the eastbound travel lanes and used for worst-case noise modeling for the sensitive land uses along the eastbound travel lanes. Consequently, to predict an absolute worst-case sound level for the sensitive land uses along the westbound travel lanes, the loudest hour was identified by calculating the westbound peak traffic and using that hour for sound level predictions for the sensitive land uses that are adjacent to the westbound travel lanes. The loudest hours were determined to be 6:00 A.M. for Route 7 eastbound and 3:00 P.M. for Route 7 westbound. Appendix B provides the ENTRADA loudest-hour traffic data summary.



#### 4.0 EXISTING NOISE ENVIRONMENT

#### 4.1 STUDY AREA/COMMON NOISE ENVIRONMENT (CNE) DESCRIPTION

The majority of noise-sensitive land uses in the project study area include single-family residences within an approximate 500-foot corridor adjacent to both the eastbound and westbound lanes of Route 7. Following VDOT and FHWA policies and procedures, the receptors used in the model to represent exterior activity areas at noise-sensitive land uses were grouped into Common Noise Environments (CNEs).

A CNE is defined as a group of receptors within the same Activity Category that are exposed to similar noise sources and levels; traffic volumes, traffic mix, and speed; and topographic features. There are 14 distinct geographic areas within the project area containing noise-sensitive land uses within 500 feet of the construction limits that can be considered similar in acoustical environment. The CNEs within the project area (**Figure 2**) consist of exterior residential (Category B) land use, athletic/recreational fields (Category C), exterior commercial (Category E), interior of public/institutional buildings (Category D), as well as other non-noise-sensitive land uses included in Category F and Category G (undeveloped). The modeled receptors for the analysis were grouped into the following CNEs:

- CNE A is located south of Route 7 between Georgetown Pike and Reston Parkway at the western termini of the project. CNE A extends past the 500ft study buffer towards Georgetown Pike to maintain community continuity. CNE A encompasses noise-sensitive land uses in the Cedar Chase development (Cedar Chase Road, Cedar Chase Court), Reston Parkway, and Estates of North Hills (Water Pointe Lane, Water Pointe Circle, and Round Pebble Lane). CNE A contains 83 modeling-only sites (A1-A83) which represent 77 single-family residential homes, The Boyd School Reston Campus, North Pointe Fire Station, Great Falls Assisted Living, and Good Shepherd Lutheran Church. CNE A also contains two monitoring sites (A1 and A2) which were used for model validation.
- CNE B is located north of Route 7 between Georgetown Pike and Utterback Store Road at the western termini of the project. CNE B encompasses noise-sensitive land uses in the Autumn Wood development (Aidan Run Court, Autumn Mist Lane), Shain Court, Northfalls Court, Bowen Avenue, Loran Court, Loran Road, and Utterback Store Road. CNE B contains 72 modeling-only sites (B1-B72) which represent 67 single-family residences, Seneca Hill Animal Hospital, MTO Shahmaghsoudi School of Islamic Sufism, Dranesville Church of the Brethren, and Meadows Farms



Nurseries and Landscaping. CNE B also contains two monitoring sites (B1 and B2) which were used for model validation.

- CNE C is located south of Route 7 between Reston Parkway and Baron Cameron Avenue and encompasses noise-sensitive land uses in the Wyndham Hills development (Stones Throw Drive, Fieldview Drive), Bright Pond Lane, Piney Run Meadows development (Tommye Lane, Meadowlook Court), Bishopsgate Way, Falls Park Estates (Markell Court), Great Falls Crossing (Hunter Gate Way), and Baron Cameron Avenue. CNE C contains 109 modeling-only sites (C1-C111) which represents 103 single-family residences and Great Falls Crossing Community Center which includes a playground (C-111), pavilion (C-110), basketball court (C-109), picnic area (C-108), swimming pool (C-106), and tennis courts (C-107). CNE C also contains two monitoring sites (C1 and C2) which were used for model validation.
- CNE D is located north of Route 7 between Utterback Store Road and Great Passage Boulevard and encompasses noise-sensitive land uses on Utterback Store Road, Great Passage Court, and Great Passage Boulevard. CNE D contains 41 modeling-only sites (D1-D41) which represent 11 residences and Nike Park soccer and baseball/softball fields.
- CNE E is located north of Route 7 between Great Passage Boulevard and Springvale Road and encompasses noise-sensitive land uses on Great Passage Boulevard, Kettle Pond Lane, Amanda Drive, Riva Ridge Drive, Piney Pond Drive, Mountain Hope Court, Crippen Court, and Springvale Road. CNE E contains 66 modeling-only sites (E1-E66) which represent 66 residences. CNE E also contains one monitoring site (E1) which was used for model validation.
- CNE F is located north of Route 7 between Springvale Road and Trotting Horse Lane in the center part of the project and encompasses noise-sensitive land uses on Springvale Road, Springvale Court, Van Patten Lane, Colvin Run Road, Colvin Meadows Court, Colvin Meadows Lane, Lees Meadows Court, Robindale Drive, Hessick Court, Locust Hill Drive, and Trotting Horse Lane. CNE F contains 164 modeling-only sites (F1-F164) which represent 155 single-family residences, Meadows Farms Nurseries and Landscaping, Colvin Run Mill, and a cemetery. CNE F contains modeling sites for portions of the relocated Cross County Connecter Trail. CNE F also contains four monitoring sites (F1, F2 F3, F4) which were used for model validation.
- CNE G is located south of Route 7 between Baron Cameron Avenue and Beulah Road and encompasses noise-sensitive land uses on Water Falls Lane, Dunn Meadows Court, Cobble Pond Way, Dunn Meadows Road, Delta Glenn Court, Newkirk Court, Mill Wheel Lane, Colvin Forest Lane, Scenic View Terrace, Grapes Farm Way, Carpers Farm Court, Middleton Ridge Road, Middleton Court, Difficult Run Court, Tweed Court, and Beulah Road. CNE G contains 208 modeling-only sites (G1-G208) which

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represent 203 single-family residences, Capital Church, Chesterbrook Academy Preschool, and Beulah Dental. CNE G contains modeling sites for portions of the relocated Cross County Connecter Trail. CNE G also contains three monitoring sites (G1, G2, and G3) which were used for model validation.

- CNE H is located north of Route 7 between Trotting Horse Lane and Towlston Road and encompasses noise-sensitive land uses on Trotting Horse Lane, Fairpine Lane, Forestville Drive, Farmingdale Court, Vernon Drive, Lyons Street, Kenmore Drive, and Towlston Road. CNE H contains 79 modeling-only sites (H1-H79) which represents 72 single-family residences and The Eastern Ridge School. CNE H also contains two monitoring sites (H1 and H2) which were used for model validation.
- CNE I is located south of Route 7 between Beulah Road and Towlston Road and encompasses noise-sensitive land uses on Beulah Road, Deramus Farm Court, Atwood Road, Robnel Place, Stokley Way, Vanetta Lane, Kilby Glen Drive, and Towlston Road. CNE I contains 112 modeling-only sites (I1-I112) which represents 110 single-family residences, Wolf Trap Nursery, and a picnic area at Fairfax County Fire Station 42. CNE I also contains one monitoring site (I-1) which was used for model validation.
- CNE J is located south of Route 7 between Towlson Road and Trap Road and encompasses noise-sensitive land uses on Towlston Road, Schuman Court, and Windsor Meadows Lane. CNE J contains 35 modeling-only sites (J1-J35) which represents 15 single-family residences, St. Athanasius Roman Catholic Church, and Andrew Chapel Cemetery. CNE J also contains one monitoring site (J1) which was used for model validation.
- CNE K is located south of Route 7 between Trap Road and the McLean Bible Church and encompasses noise-sensitive land uses on Trap Road, Lucky Estates Drive, Timberwolf Court, Trailridge Court, Wolftrap Run Road, and Route 7. CNE K contains 39 modeling-only sites (K1-K39) which represents 32 single-family residences, Andrew Chapel Preschool, Bethel Baptist Church, McLean Bible Church, and Jill's House. CNE K also contains one monitoring site (K1) which was used for model validation.
- CNE L is located north of Route 7 between Towlston Road and Lewinsville Road and encompasses noise-sensitive land uses on Route 7, Dreamweaver Court, Royal Estates Drive, Old Tolson Mill Road, Brook Road, Gallant Green Drive, Gunnell Court, Woodside Drive, and Lewinsville Road. CNE L contains 49 modeling-only sites (L1-L49) which represents 45 single-family residences, Providence Baptist Church, and St Thomas Episcopal Church/McLean Preschool. CNE L also contains one monitoring site (L1) which was used for model validation.
- CNE M is located north of Route 7 between Lewinsville Road and the Dulles Toll Road off-ramp at the eastern termini of the project. CNE M encompasses noise-sensitive land uses on Route 7, Mirador Place,

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Prestwould Place, Woodhurst Boulevard, and Mayhurst Boulevard. CNE M contains 52 modeling-only sites (M1-M52) which represents 52 single-family residences. The locations of the receptor sites are shown on *Figure 2-7*. Receptor M-01 is a proposed property acquisition; therefore, no sound level predictions were made for M1 under the Design Year (2040) Build condition. CNE M also contains one monitoring site (M1) which was used for model validation.

CNE N is located south of Route 7 between Laurel Hill Road and Jarrett Valley Drive at the eastern termini of the project. CNE N encompasses noise-sensitive land uses on Laurel Hill Road, Glenridge Court, Old Ash Grove, Stanbridge Place, Carrington Ridge Lane, Broadstone Place, and Jarret Valley Drive. CNE N contains 78 modeling-only sites (N1-N80) which represents 81 residences and Berea Church of Christ. CNE N contains one monitoring site (N1) which was used for model validation. CNE N also contains an existing noise barrier that was erected as part of the Route 7 over Dulles Access Toll Road (DATR) Major Bridge Rehabilitation project (UPC 82135).

#### 4.2 UNDEVELOPED LANDS AND PERMITTED DEVELOPMENTS

Highway traffic noise analyses are (and will be) performed for developed lands as well as undeveloped lands if they are considered "permitted." Undeveloped lands are deemed to be permitted when there is a definite commitment to develop land with an approved specific design of land use activities as evidenced by the issuance of at least one building permit.

In accordance with the *VDOT Traffic Noise Policy*, an undeveloped lot is considered to be planned, designed, and programmed if a building permit has been issued by the local authorities prior to the Date of Public Knowledge for the relevant project. VDOT considers the "Date of Public Knowledge" as the date that the final NEPA approval is made. The NEPA approval date for the project is November 15, 2017. VDOT has no obligation to provide noise mitigation for any undeveloped land that is permitted or constructed after this date.

According to a review of Fairfax County Planning Commission site plan and submission records, there are no new planned or permitted lands or developments (building permits) with noise-sensitive land use within a 500-foot buffer zone as of the NEPA approval date (November 15, 2017). The permitted development that has occurred before the FONSI has been incorporated into this analysis. Please see Appendix H for permitted lands research.



#### 4.3 MONITORING OF EXISTING NOISE LEVELS

A noise monitoring program was conducted within the Route 7 Corridor Improvements study area consistent with FHWA and VDOT recommended procedures. The objectives of the monitoring program were to document existing ambient noise levels in noise-sensitive locations and to provide a means for validation of the traffic noise prediction model.

Short-term noise measurements of 15-minute duration were obtained at 12 locations within the project corridor on November 17, 2015, for the Preliminary Engineering. These measurements were supplemented with 11 locations on March 20, 2019. All monitoring was performed using Metrosonics dB-3080 sound analyzers. One location was omitted from the analysis (G4) since the measurement results were influenced by mowing and mulching activities occurring at neighboring residences. Field calibration of the meters was performed immediately prior to noise monitoring using a Metrosonics cl-304 sound level calibrator. The sound analyzers were post-calibrated subsequent to the measurements using a Metrosonics cl-304 sound level calibrator. All equipment was lab-calibrated on April 26, 2018. This equipment meets all requirements of the American National Standard Specification for Sound Level Meters, ANSI S1.4-1983 (R1990), Type 2. Noise measurements were in the A-weighted scale and reported in decibels (dBA). The data collection procedure involved the Leq measurements in consecutive 30second intervals. This method allows individual time intervals that include noise events unrelated to traffic noise (such as aircraft over flights) to be excluded from consideration. Hourly average noise levels [Leq(h)] were derived at each location from the 15- to 20-minute Leq values. Existing noise measurements were collected under meteorologically acceptable conditions when the pavement was dry and winds were calm or light. Additional data collected at each monitoring location included atmospheric conditions such as wind speed, humidity, and ambient temperature. Monitoring was conducted in accordance with the U.S. Department of Transportation, FHWA "Measurement of Highway-Related Noise," FHWA Report No. FHWA-PD-96-046, May 1996.

Short-term noise monitoring is not a process to determine design year noise impacts or barrier locations. Short-term noise monitoring provides a level of consistency between what is present in real-world situations and how that is represented in the computer noise model. Short-term monitoring does not need to occur within every CNE to validate the computer noise model.

The measured noise levels appear in **Table 4** as equivalent sound levels ( $L_{eq}$ ). The  $L_{eq}$  is a sound-energy average of the fluctuating sound level (in A-weighted decibels, dBA) measured over a specified period of time. **Table 4** provides the site address as well as the date, start time,



and duration of each measurement. The traffic data (vehicle composition and speed) were also recorded during the measurement period. According to VDOT procedure, traffic was grouped into one of three categories: automobiles, medium trucks, and heavy trucks. The traffic data were converted to one-hour traffic data based on the measurement duration for validation of the noise model.

TABLE 4
SHORT-TERM NOISE MONITORING SUMMARY

Site ID	Address	Date	Time Start	Duration (minutes)	Monitored L <sub>eq</sub> (dBA)
A1	11304 Water Pointe Circle	11/17/2015	9:35	15	57
A2	11582 Cedar Chase Road	3/21/2019	10:10	20	56
B1	11119 Loran Road	11/17/2015	9:35	15	63
B2	1063 Autumn Mist Lane	3/21/2019	10:10	20	60
C1	1155 Markell Court	11/17/2015	9:35	15	58
C2	11270 Stones Throw Drive	3/21/2019	10:10	20	56
E1	10805 Piney Pond Drive	11/17/2015	9:35	15	61
F1	10411 Van Pattern Lane	11/17/2015	10:40	15	60
F2	9629 Locust Hill Drive	11/17/2015	10:40	15	60
F3	1220 Colvin Meadows Lane	3/21/2019	11:37	20	56
F4	9911 Hessick Court	3/21/2019	11:37	20	56
G1	1253 Dunn Meadow Court	11/17/2015	10:40	15	64
G2	1293 Colvin Forest Drive	11/17/2015	10:40	15	63
G3	10237 Leesburg Pike	3/21/2019	11:37	20	57
H1	9393 Farmingdale Court	11/17/2015	11:40	15	58
H2	9320 Leesburg Pike	3/21/2019	12:54	20	66
I1	9356 Mildred Court	11/17/2015	11:40	15	63
J1	1308 Trap Road	3/21/2019	12:54	20	57
K1	9105 Lucky Estates Drive	3/21/2019	12:54	20	57
L1	9026 Leesburg Pike	11/17/2015	11:40	15	63
M1	1424 Woodhurst Boulevard	3/21/2019	13:42	20	53
N1	8850 Glenridge Court	11/17/2015	11:40	15	65

The location of each noise monitoring site is indicated with a star symbol on **Figure 2**. Additional noise monitoring data (site sketches, meter printouts, and calibration certificates) are

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located in Appendix A. The monitored  $L_{eq}$  in the study corridor ranged from 53 dBA to 66 dBA. Traffic noise from Route 7 was the dominant source of noise at each of the monitoring locations.

#### 4.4 NOISE MODEL VALIDATION

The noise monitoring data are primarily used to validate the computer model used to predict existing and future levels. Upon measurement of the existing noise levels, a three-dimensional noise model of the existing roadway network was constructed which incorporates all significant terrain features that define the propagation path between the roadway and noise-sensitive receptors. Traffic volumes, composition, and speeds that were observed during the short-term monitoring periods were used as inputs to generate the validation models sound levels. FHWA and VDOT consider a difference of ±3 dBA or less between the measured noise levels and the computer modeled noise levels is considered acceptable. This computer model validation verifies that the sound propagation paths within the model are accurate and that the modeling techniques are correct and ensures that reported changes between the 2018 existing conditions and future design year (2040) conditions are due to changes in traffic or propagation path and not discrepancies between monitoring and modeling techniques.

The model validation was performed for the existing traffic conditions observed and recorded during the measurement period. As these noise measurements were not necessarily obtained during the existing loudest hour, the existing noise levels obtained during the 20-minute short-term monitoring session were not predicted as the project's existing noise levels. Instead, the validated existing conditions TNM noise model was used to generate existing loudest-hour noise levels by using Design Hour Volumes and truck percentages supplied by the traffic engineers as model inputs (refer to Section 5.2).

A summary of the model validation is presented in **Table 5**. Each of the monitored locations was able to be accurately modeled within the acceptable ±3 dBA range. Due to the relatively close proximity of the monitoring locations to Route 7 and absence of other major noise sources, traffic noise was the most dominant component of the acoustic environment at each monitoring location. The project-wide average difference between calculated noise levels and monitored noise levels was 1.7 decibels, which generally shows excellent agreement between monitored and modeled sound levels and suggests confidence in the modeling assumptions.



TABLE 5
COMPUTED VS. MEASURED SOUND LEVELS AT MEASUREMENT SITES

Site ID	CNE	Address	Monitored L <sub>eq</sub> (dBA)	TNM - Computed L <sub>eq</sub> (dBA)	Difference (dBA)
A1	Α	11304 Water Pointe Circle	57.2	58.3	1.1
A2		11582 Cedar Chase Road	56.0	56.8	0.8
B1	В	11119 Loran Road	63.2	64.4	1.2
B2		1063 Autumn Mist Lane	60.2	60.9	0.7
C1	С	1155 Markell Court	58.1	57.2	-0.9
C2		11270 Stones Throw Drive 56.4 59.3		2.9	
E1	Е	10805 Piney Pond Drive	60.7	63.0	2.3
F1		10411 Van Pattern Lane	59.5	60.5	1.0
F2	F	9629 Locust Hill Drive	60.1	62.4	2.3
F3		1220 Colvin Meadows Lane	56.0	58.8	2.8
F4		9911 Hessick Court	56.3	59.3	3.0
G1		1253 Dunn Meadow Court	64.4	64.8	0.4
G2	G	1293 Colvin Forest Drive	63.3	65.6	2.3
G3		10237 Leesburg Pike	56.7	58.6	1.9
H1	Н	9393 Farmingdale Court	58.1	61.1	3.0
H2		9320 Leesburg Pike	65.7	67.4	1.7
I1	I	9356 Mildred Court	63.0	63.2	0.2
J1	J	1308 Trap Road	56.5	59.1	2.6
K1	K	9105 Lucky Estates Drive	57.2	60.2	3.0
L1	L	9026 Leesburg Pike	63.4	66.1	2.7
M1	М	1424 Woodhurst Boulevard	52.5	53.8	1.3
N1	N	8850 Glenridge Court	rt 65.3 65.4		0.1
		Average Diff	ference		1.7
		Standard Deviation	of Difference		1.1

#### 4.5 PREDICTED EXISTING NOISE LEVELS

For calculation of loudest-hour noise levels throughout the study area, 1,234 receiver locations were added to the validated TNM model(s) to provide a comprehensive basis of comparison for the analysis of noise impacts from the existing and future project conditions. Using the appropriate loudest-hour traffic data, existing and future traffic noise levels were predicted for



the measurement sites and the additional receiver locations. The computation methods and predicted noise levels are presented in the next section of this report.

The noise measurements provided valuable information on current noise conditions and the effects of terrain and shielding on sound propagation from the roadway to the nearby residential land uses. However, because existing noise levels are not always measured during the loudest hour of the day, the loudest-hour existing noise levels were computed using the appropriate traffic data as input. The predicted existing noise levels for the loudest hour of the day are then used as the baseline against which probable future noise levels are compared and potential noise impacts assessed.

Of the 1,234 total noise receptor sites (grouped into 14 CNEs), 159 receptor sites (within 13 of the 14 CNEs) are predicted to approach or exceed the NAC for the existing condition worst-case noise hour. For all studied sites, the predicted existing year noise levels range from 45 dBA to 73 dBA. A discussion of the predicted existing noise levels for each of the CNEs is provided below. **Figure 2** presents the locations of all the CNEs and all of their respective modeled receptor sites. Calculated noise levels for all noise-sensitive sites are presented in **Table 7** and discussed below. Due to the amount of data, this table is located in the Data Tables section.

- Existing loudest hour noise levels within CNE A were predicted to range from 41 to 66 dBA. One noise-sensitive sites are predicted to approach or exceed the NAC for the existing condition worst-case noise hour.
- Existing loudest hour noise levels within CNE B were predicted to range from 49 to 71 dBA. There are 14 noise-sensitive sites that are predicted to approach or exceed the NAC for the existing condition worst-case noise hour.
- Existing loudest hour noise levels within CNE C were predicted to range from 45 to 72 dBA. There are 16 noise-sensitive sites that are predicted to approach or exceed the NAC for the existing condition worst-case noise hour.
- Existing loudest hour noise levels within CNE D were predicted to range from 48 to 71 dBA. There are two noise-sensitive sites that are predicted to approach or exceed the NAC for the existing condition worst-case noise hour.
- Existing loudest hour noise levels within CNE E were predicted to range from 46 to 70 dBA. There are 10 noise-sensitive sites that are predicted to approach or exceed the NAC for the existing condition worst-case noise hour.



- Existing loudest hour noise levels within CNE F were predicted to range from 43 to 72 dBA. There are 27 noise-sensitive sites that are predicted to approach or exceed the NAC for the existing condition worst-case noise hour.
- Existing loudest hour noise levels were predicted to range from 42 to 72 dBA within CNE G. There are 38 noise-sensitive sites that are predicted to approach or exceed the NAC for the existing condition worst-case noise hour.
- Existing loudest hour noise levels were predicted to range from 47 to 73 dBA within CNE H. There are 17 noise-sensitive sites that are predicted to approach or exceed the NAC for the existing condition worst-case noise hour.
- Existing loudest hour noise levels were predicted to range from 44 to 71 dBA within CNE I. There are 10 noise-sensitive sites that are predicted to approach or exceed the NAC for the existing condition worst-case noise hour.
- Existing loudest hour noise levels were predicted to range from 48 to 69 dBA within CNE J. There are eight noise-sensitive sites that are predicted to approach or exceed the NAC for the existing condition worst-case noise hour.
- Existing loudest hour noise levels were predicted to range from 45 to 68 dBA within CNE K. Three noise-sensitive sites are predicted to approach or exceed the NAC for the existing condition worst-case noise hour.
- Existing loudest hour noise levels were predicted to range from 41 to 71 dBA within CNE L. There are five noise-sensitive sites that are predicted to approach or exceed the NAC for the existing condition worst-case noise hour.
- Existing loudest hour noise levels were predicted to range from 47 to 62 dBA within CNE M. No noise-sensitive sites are predicted to approach or exceed the NAC for the existing condition worst-case noise hour.
- Existing loudest hour noise levels were predicted to range from 43 to 70 dBA within CNE N. There is one noise-sensitive site predicted to approach or exceed the NAC for the existing condition worst-case noise hour.



#### 5.0 FUTURE NOISE ENVIRONMENT

This section discusses the noise prediction model and traffic data used as input to the noise prediction model and then presents a summary of the predicted noise levels.

#### 5.1 PRESENTATION OF RESULTS

**Table 6** summarizes the range of predicted noise levels by CNE. The table includes a description of each CNE and its land use, the FHWA Activity Category, and the loudest-hour traffic noise levels which are presented in terms of the A-weighted equivalent sound level, or  $L_{eq}$ , in dBA. Loudest-hour noise levels were computed for 2018 existing conditions as well as the future design year (2040) proposed highway widening.

TABLE 6
RANGES OF PREDICTED EXTERIOR NOISE LEVELS FOR THE WORST HOUR

			Range of Predicted Exterior Noise Levels and Impacts for the Worst Hour					
CNE	Land Use- Description	Activity Category	Existing Sound Level (dBA)		Sound Level		Sound	Build I Level BA)
			Min	Max	Min	Max		
	Single-family homes in Cedar Chase development (Cedar Chase Road, Cedar Chase Court), Estates of North Hills (Water Pointe Lane, Water Pointe Circle, and Round Pebble Lane), and Reston Parkway	В	41	66	43	67		
A	Boyd School Playground; North Pointe Fire Station Picnic table; Great Falls Assisted Living Patio	С	55	59	56	61		
	Good Shepherd Lutheran Church; The Boyd School – Reston Campus	D	30	32	30	33		
	Single-family homes in Autumn Wood development (Aidan Run Court, Autumn Mist Lane), Shain Court, Northfalls Court, Bowen Avenue, Loran Court, Loran Road, and Utterback Store Road	В	49	71	52	73		
В	Dog Park	С	5	1	5	2		
	Seneca Hill Animal Hospital, Dranesville Church of the Brethren, MTO Shahmaghsoudi School of Islamic Sufism	D	26	44	32	46		
	Meadows Farms Nurseries and Landscaping	E	6	2	6	5		

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#### **TABLE 6** (CONTINUED)

CNE	Land Use- Description		Range of Predicted Exterior Noise Levels and Impacts for the Worst Hour			
			Existing Sound Level (dBA)		2040 Build Sound Level (dBA)	
		,	Min	Max	Min	Max
С	Single-family homes in Wyndham Hills Development (Stones Throw Drive, Fieldview Drive), Bright Pond Lane, Piney Run Meadows Development (Tommye Lane, Meadowlook Court), Bishopsgate Way, Falls Park Estates (Markell Court), Great Falls Crossing (Hunter Gate Way), and Baron Cameron Avenue	В	45	72	48	73
	Great Falls Crossing Community Center (Pool, tennis, basketball, picnic area, pavilion, playground)	С	55	64	57	65
D	Single-family homes on Utterback Store Road, Great Passage Court, and Great Passage Boulevard	В	48	71	50	72
	Nike Park soccer/softball fields	С	50	64	54	68
Е	Single-family homes along Great Passage Boulevard, Kettle Pond Lane, Amanda Drive, Riva Ridge Drive, Piney Pond Drive, Mountain Hope Court, Crippen Court, and Springvale Road	В	46	70	48	71
F	Single-family homes on Springvale Road, Springvale Court, Van Patten Lane, Colvin Run Road, Colvin Meadows Court, Colvin Meadows Lane, Lees Meadows Court, Robindale Drive, Hessick Court, Locust Hill Drive, and Trotting Horse Lane; Colvin Run Mill; cemetery	В	43	72	45	74
	Unnamed Cemetery, Colvin Run Mill	С	59	72	61	74
	Meadows Farms Nurseries and Landscaping; Hills Nursery	E	65	68	68	70
G	Single-family homes on Water Falls Lane, Dunn Meadows Court, Cobble Pond Way, Dunn Meadows Road, Delta Glenn Court, Newkirk Court, Mill Wheel Lane, Colvin Forest Lane, Scenic View Terrace, Grapes Farm Way, Carpers Farm Court, Middleton Ridge Road, Middleton Court, Difficult Run Court, Tweed Court, and Beulah Road	В	42	72	45	74
	Capital Church Picnic Area, Beulah Dental, Chesterbrook Academy Preschool playground	С	61	65	65	69
	Capital Church; Chesterbrook Academy Preschool	D	32	45	36	48
Н	Single-family homes on Trotting Horse Lane, Fairpine Lane, Forestville Drive, Farmingdale Court, Vernon Drive, Lyons Street, Kenmore Drive, and Towlston Road	В	47	73	48	75
	The Eastern Ridge School outdoor activity area	С	61	73	65	77
	The Eastern Ridge School	D	34		3	38



## TABLE 6 (CONTINUED)

CNE			Range of Predicted Exterior Noise Levels and Impacts for the Worst Hour				
	Land Use- Description	Activity Category	Existing Sound Level (dBA)		(dBA)		
			Min	Max	Min	Max	
I	Single-family homes on Beulah Road, Deramus Farm Court, Atwood Road, Robnel Place, Stokley Way, Vanetta Lane, Kilby Glen Drive, and Towlston Road	В	44	71	49	74	
	Picnic area at the Fairfax County Fire Station 42	С	5	0	5	53	
	Wolf Trap Nursery	Е	68		7	70	
J	Single-family homes on Towlston Road, Schuman Court, and Windsor Meadows Lane	В	48	69	51	70	
	Andrew Chapel Cemetery	С	56	73	58	73	
	St. Athanasius Roman Catholic Church	D	45		47		
	Trap Road, Lucky Estates Drive, Timberwolf Court, Trailridge Court, Wolftrap Run Road, and Route 7	В	45	68	48	70	
К	Andrew Chapel playground, Jills House playground, McLean Bible Church playground	С	50	62	51	63	
	Andrew Chapel United Methodist Church, Bethel Baptist Church, Jills House, McClean Bible Church	D	35	37	35	40	
	Single-family residences on Route 7, Dreamweaver Court, Royal Estates Drive, Old Tolson Mill Road, Brook Road, Gallant Green Drive, Gunnell Court, Woodside Drive, and Lewinsville Road		41	71	43	73	
L	Providence Baptist Church playground and volley ball	С	57	62	61	65	
	Providence Baptist Church, St Thomas Episcopal Church/McLean Preschool		36	37	37	38	
М	Single-family residences on Route 7, Mirador Place, Prestwould Place, Woodhurst Boulevard, and Mayhurst Boulevard	В	47	62	51	65	
N	Single-family residences on Laurel Hill Road, Glenridge Court, Old Ash Grove, Stanbridge Place, Carrington Ridge Lane, Broadstone Place, and Jarret Valley Drive	В	43	70	48	73	
	Berea Church of Christ	D	32		3	33	
F/G	Cross County Trail	С	56 72 58			73	

**Figure 2** provides a location map for the CNEs, noise-sensitive receptors,  $66 \text{ dBA L}_{eq}$  "contour" for the 2040 Build alternative, and potential noise barrier locations. Each receptor is shown in **Figure 2** with a color-coded dot that indicates the status of each receptor according to its 2040 Build noise level.

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Future design year (2040) noise levels are predicted to exceed the NAC within 13 of the 14 CNEs at a total of 222 noise-sensitive receptor sites. For all studied sites, the future design year (2040) exterior noise levels range from 43 dBA to 77 dBA. The increase in noise is attributable to an increase in overall traffic volumes along Route 7 as well as minor alterations in the source/receiver noise propagation path resulting from the construction of the additional travel lane.

- Future design year (2040) noise levels within CNE A are predicted to range from 43 dBA to 67 dBA, with noise levels predicted to approach or exceed the NAC at two noise-sensitive receptor locations. There is a maximum of 4 dBA increase over existing sound levels within CNE A.
- Future design year (2040) noise levels within CNE B are predicted to range from 52 dBA to 73 dBA, with noise levels predicted to approach or exceed the NAC at 17 noise-sensitive receptor locations. There is a maximum of 6 dBA increase over existing sound levels within CNE B.
- Future design year (2040) noise levels within CNE C are predicted to range from 48 dBA to 73 dBA, with noise levels predicted to approach or exceed the NAC at 21 noise-sensitive receptor locations. There is a maximum of 5 dBA increase over existing sound levels within CNE C.
- Future design year (2040) noise levels within CNE D are predicted to range from 50 dBA to 72 dBA, with noise levels predicted to approach or exceed the NAC at four noise-sensitive receptor locations. There is a maximum of 5 dBA increase over existing sound levels within CNE D.
- Future design year (2040) noise levels within CNE E are predicted to range from 48 dBA to 71 dBA, with noise levels predicted to approach or exceed the NAC at 16 noise-sensitive receptor locations. There is a maximum of 4 dBA increase over existing sound levels within CNE E.
- Future design year (2040) noise levels within CNE F are predicted to range from 45 dBA to 74 dBA, with noise levels predicted to approach or exceed the NAC at 32 noise-sensitive receptor locations. There is a maximum of 5 dBA increase over existing sound levels within CNE F.
- Future design year (2040) noise levels within CNE G are predicted to range from 45 dBA to 74 dBA, with noise levels predicted to approach or exceed the NAC at 47 noise-sensitive receptor locations. There is a maximum of 6 dBA increase over existing sound levels within CNE G.
- Future design year (2040) noise levels within CNE H are predicted to range from 48 dBA to 75 dBA, with noise levels predicted to approach or exceed

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- the NAC at 20 noise-sensitive receptor locations. There is a maximum of 7 dBA increase over existing sound levels within CNE H.
- Future design year (2040) noise level within CNE I are predicted to range from 49 dBA to 74 dBA, with noise levels predicted to approach or exceed the NAC at 13 noise-sensitive receptor locations. There is a maximum of 5 dBA increase over existing sound levels within CNE I.
- Future design year (2040) noise levels within CNE J are predicted to range from 51 dBA to 73 dBA, with noise levels predicted to approach or exceed the NAC at 10 noise-sensitive receptor locations. There is a maximum of 6 dBA increase over existing sound levels within CNE J.
- Future design year (2040) noise levels at the athletic fields within CNE K
  are predicted to range from 48 dBA to 70 dBA, with noise levels predicted
  to approach or exceed the NAC at five noise-sensitive receptor location.
  There is a maximum of 7 dBA increase over existing sound levels within
  CNE K.
- Future design year (2040) noise levels within CNE L are predicted to range from 43 dBA to 73 dBA, with noise levels predicted to approach or exceed the NAC at six noise-sensitive receptor locations. There is a maximum of 4 dBA increase over existing sound levels within CNE L.
- Future design year (2040) noise levels within CNE M are predicted to range from 51 dBA to 65 dBA and are not predicted to approach or exceed the NAC at any noise-sensitive receptor location. There is an earth berm constructed between Route 7 and the community, significantly shielding these homes from traffic noise. There is a maximum of 5 dBA increase over existing sound levels within CNE M.
- Future design year (2040) noise levels within CNE N are predicted to range from 48 dBA to 73 dBA, with the noise levels predicted to approach or exceed the NAC at 11 noise-sensitive receptor locations. There is a maximum of 7 dBA increase over existing sound levels within CNE N.

**Table 7** (refer to Data Tables for receptor sound data tables) outlines all of the computed sound levels at all 1,234 of the modeled receptors included in the noise assessment. The noise-impacted sites have been highlighted in red. All impacts result from an approach or exceedance of the NAC. There are no impacts associated with the "substantial increase" impact threshold.

**Table 8** presents a summary of the predicted noise impact for the 2018 existing condition and the future design year (2040) build alternative. The impacts are summarized for the entire study area, separately by FHWA Activity Category.

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### TABLE 8 NOISE IMPACT SUMMARY

	lmnaat	Number of Impacted Units by Land Use and FHWA Activity Category <sup>2</sup>						
Scenario	Impact Type <sup>1</sup>	Residential Exterior (B)	Recreational Exterior (C)	Institutional Interior (D)	Commercial Exterior (E)	Total		
Existing	NAC	140	19	0	0	159		
Build	NAC	184	38	0	0	222		

<sup>1 &</sup>quot;NAC" = Noise levels approach or exceed the FHWA Noise Abatement Criteria (NAC) for applicable Activity Category. 2 The FHWA Activity Category is shown in parenthesis.

**Table 9** presents a summary of the predicted noise impact for the 2018 existing condition and the future design year (2040) build alternative by CNE.

TABLE 9
PREDICTED TRAFFIC NOISE IMPACT BY COMMON NOISE ENVIRONMENT (CNE)

CNE		Activity Category	Range of Predicted Exterior Noise Levels and Impacts for the Worst Hour		
	Land Use - Description		Existing	2040 Build	
			Number of Impacts	Number of Impacts	
А	Single-family homes in Cedar Chase development (Cedar Chase Road, Cedar Chase Court), Estates of North Hills (Water Pointe Lane, Water Pointe Circle, and Round Pebble Lane), and Reston Parkway	В	1	2	
	Boyd School Playground; North Pointe Fire Station Picnic table; Great Falls Assisted Living Patio	С	0	0	
	Good Shepherd Lutheran Church; The Boyd School – Reston Campus	D	0	0	
	Single-family homes in Autumn Wood development (Aidan Run Court, Autumn Mist Lane), Shain Court, Northfalls Court, Bowen Avenue, Loran Court, Loran Road, and Utterback Store Road	В	14	17	
В	Dog Park	С	0	0	
	Seneca Hill Animal Hospital, Dranesville Church of the Brethren, MTO Shahmaghsoudi School of Islamic Sufism	D	0	0	
	Meadows Farms Nurseries and Landscaping	Е	0	0	
С	Single-family homes in Wyndham Hills Development (Stones Throw Drive, Fieldview Drive), Bright Pond Lane, Piney Run Meadows Development (Tommye Lane, Meadowlook Court), Bishopsgate Way, Falls Park Estates (Markell Court), Great Falls Crossing (Hunter Gate Way), and Baron Cameron Avenue	В	16	21	
	Great Falls Crossing Community Center (Pool, tennis, basketball, picnic area, pavilion, playground)	С	0	0	

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# **TABLE 9** (CONTINUED)

		Activity	Range of Predicted Exterior Noise Levels and Impacts for the Worst Hour			
CNE	Land Use - Description	Category	Existing	2040 Build		
			Number of Impacts	Number of Impacts		
D	Single-family homes on Utterback Store Road, Great Passage Court, and Great Passage Boulevard	В	2	2		
	Nike Park soccer/softball fields	С	0	2		
E	Single-family homes along Great Passage Boulevard, Kettle Pond Lane, Amanda Drive, Riva Ridge Drive, Piney Pond Drive, Mountain Hope Court, Crippen Court, and Springvale Road	В	10	16		
F	Single-family homes on Springvale Road, Springvale Court, Van Patten Lane, Colvin Run Road, Colvin Meadows Court, Colvin Meadows Lane, Lees Meadows Court, Robindale Drive, Hessick Court, Locust Hill Drive, and Trotting Horse Lane; Colvin Run Mill; cemetery	В	24	28		
	Unnamed Cemetery, Colvin Run Mill	С	3	4		
	Meadows Farms Nurseries and Landscaping; Hills Nursery	Е	0	0		
G	Single-family homes on Water Falls Lane, Dunn Meadows Court, Cobble Pond Way, Dunn Meadows Road, Delta Glenn Court, Newkirk Court, Mill Wheel Lane, Colvin Forest Lane, Scenic View Terrace, Grapes Farm Way, Carpers Farm Court, Middleton Ridge Road, Middleton Court, Difficult Run Court, Tweed Court, and Beulah Road	В	38	46		
	Capital Church Picnic Area, Beulah Dental, Chesterbrook Academy Preschool playground	С	0	1		
	Capital Church; Chesterbrook Academy Preschool	D	0	0		
Н	Single-family homes on Trotting Horse Lane, Fairpine Lane, Forestville Drive, Farmingdale Court, Vernon Drive, Lyons Street, Kenmore Drive, and Towlston Road	В	14	15		
''	The Eastern Ridge School outdoor activity area	С	3	5		
	The Eastern Ridge School	D	0	0		
	Single-family homes on Beulah Road, Deramus Farm Court, Atwood Road, Robnel Place, Stokley Way, Vanetta Lane, Kilby Glen Drive, and Towlston Road	В	10	13		
'	Picnic area at the Fairfax County Fire Station 42	С	0	0		
	Wolf Trap Nursery	E	0	0		
	Single-family homes on Towlston Road, Schuman Court, and Windsor Meadows Lane	В	2	2		
J	Andrew Chapel Cemetery	С	6	8		
	St. Athanasius Roman Catholic Church	D	0	0		

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# **TABLE 9** (CONTINUED)

		Activity	Range of Predicted Exterior Noise Levels and Impacts for the Worst Hour		
CNE	Land Use - Description	Category	Existing	2040 Build	
			Number of Impacts	Number of Impacts	
	Trap Road, Lucky Estates Drive, Timberwolf Court, Trailridge Court, Wolftrap Run Road, and Route 7	В	3	5	
К	Andrew Chapel playground, Jills House playground, McLean Bible Church playground	С	0	0	
	Andrew Chapel United Methodist Church, Bethel Baptist Church, Jills House, McClean Bible Church	D	0	0	
	Single-family residences on Route 7, Dreamweaver Court, Royal Estates Drive, Old Tolson Mill Road, Brook Road, Gallant Green Drive, Gunnell Court, Woodside Drive, and Lewinsville Road	В	5	6	
L	Providence Baptist Church playground and volley ball	С	0	0	
	Providence Baptist Church, St Thomas Episcopal Church/McLean Preschool	D	0	0	
М	Single-family residences on Route 7, Mirador Place, Prestwould Place, Woodhurst Boulevard, and Mayhurst Boulevard	В	0	0	
N	Single-family residences on Laurel Hill Road, Glenridge Court, Old Ash Grove, Stanbridge Place, Carrington Ridge Lane, Broadstone Place, and Jarret Valley Drive	В	1	11	
	Berea Church of Christ	D	0	0	
F/G	Cross County Trail	С	7	18	
	Total Impacted Dwellings	159	222		

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#### 6.0 NOISE ABATEMENT DETERMINATION

Noise Abatement Determination is a three-phased approach. The first phase of the process is to determine if highway traffic noise abatement consideration is warranted for the affected communities and/or affected receptors. The warranted criterion specifically pertains to traffic noise impacted receptors, defined in Section 5. Since predicted noise levels for the future design year (2040) build condition approach or exceed the NAC and/or meet the substantial increase criterion, in accordance with VDOT's State Noise Abatement Policy, noise abatement considerations are warranted for these impacted noise-sensitive areas. Satisfying the warranted criterion is considered to be the first phase (Phase 1) of the three-phased noise abatement determination. Phases 2 and 3 (determining feasibility and reasonableness) are discussed below. Following completion of all three phases, a determination can be made related to the feasibility and reasonableness of the noise abatement options.

Noise-sensitive sites behind existing noise barriers that are predicted to be impacted by traffic noise under the future design year (2040) build condition are subject to the following evaluation. This is due to the fact that noise barriers posts and foundations are uniquely designed for each noise barrier; as such, retrofitting a noise barrier to address new noise impacts is not possible. This methodology determines if the existing noise barrier is still feasible and reasonable under VDOT's State Noise Abatement Policy, and is as follows:

- Determine the future design year (2040) noise levels with and without the existing noise barrier.
  - If the noise barrier is determined to be feasible and reasonable. then the process shall stop.
  - If the existing barrier is not feasible and/or reasonable, a new feasible barrier shall be evaluated.
    - If the new noise barrier being evaluated is determined to not be feasible and/or not reasonable, the existing noise barrier will be left in place without modification.
    - If the new noise barrier being evaluated is determined to be both feasible and reasonable, the new barrier will be recommended for further consideration.



#### 6.1 ABATEMENT MEASURES EVALUATION

VDOT guidelines recommend a variety of mitigation measures that should be considered in response to transportation-related noise impacts. While noise barriers and/or earth berms are generally the most effective forms of noise mitigation, additional mitigation measures exist which have the potential to provide considerable noise reductions under certain circumstances. Mitigation measures considered for this project include:

- Traffic-Control Measures,
- Alteration of Horizontal and Vertical Alignments,
- Acoustical Insulation of Public-Use and Non-Profit Facilities,
- Acquisition of Buffer Land,
- Construction of Earth Berms, and
- Construction of Noise Barriers.

# **6.1.1 Traffic-Control Measures (TCM)**

Traffic-control measures (such as speed limit restrictions, truck traffic restrictions, and other traffic-control measures that may be considered for the reduction of noise emission levels) are not practical for this project. Reducing speeds will not be an effective noise mitigation measure since a substantial decrease in speed is necessary to provide adequate noise reduction. Typically, a 10-mile-per-hour (mph) reduction in speed will result in only a 2 dBA decrease in noise level, which would not eliminate all impacts and is not perceptible to the typical human ear. Additionally, a reduction in speed is not practical for a limited access highway and would be counterproductive to the project objective of alleviating traffic and reducing congestion.

#### 6.1.2 Alteration of Horizontal and Vertical Alignments

Consistent with the Environmental Assessment documentation, complete realignment of Route 7 either horizontally or vertically is not included in the scope of the project as it would result in significant amounts of right-of-way and easement impacts to the adjacent private properties. Accordingly, the scope of this project is to widen Route 7 through construction of an additional travel lane in each direction in the median of the existing interstate. Minimal vertical profile adjustments are being made to address substandard vertical profile elements, but more drastic

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vertical changes are not feasible or proposed due to the impacts on the travelling public during construction and impacts on private property which would be required. The noise barriers being studied as part of this project have been placed to maximize their benefit to the surrounding properties and developments while also minimizing right-of-way, easement acquisition, and environmental impacts as well as maintaining access to proposed stormwater management facilities.

#### 6.1.3 Acoustical Insulation of Public-Use and Non-Profit Facilities

This noise abatement measure option applies only to public and institutional use buildings. Since no public use or institutional structures are anticipated to have interior noise levels exceeding FHWA's interior NAC, this noise abatement option will not be applied.

# 6.1.4 Acquisition of Buffering Land

The purchase of property for noise barrier construction or the creation of a "buffer zone" to reduce noise impacts is only considered for predominantly unimproved properties because the amount of property required for this option to be effective would create significant additional impacts (e.g., in terms of residential displacements), which were determined to outweigh the benefits of land acquisition.

#### 6.1.5 Construction of Berms/Noise Barriers

Construction of noise barriers can be an effective way to reduce noise levels at areas of outdoor activity. Noise barriers can be wall structures, earthen berms, or a combination of the two. The effectiveness of a noise barrier depends on the distance and elevation difference between roadway and receptor and the available placement location for a barrier. Gaps between overlapping noise barriers also decrease the effectiveness of the barrier, as opposed to a single connected barrier. The barrier's ability to attenuate noise decreases as the gap width increases.

Noise barriers and earth berms are often implemented into the highway design in response to the identified noise impacts. The effectiveness of a free-standing (post and panel) noise barrier and an earth berm of equivalent height are relatively consistent; however, an earth berm is perceived as a more aesthetically pleasing option. In contrast, the use of earth berms is

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not always an option due to the excessive space they require adjacent to the roadway corridor. At a standard slope of 2:1, every one foot in height would require four feet of horizontal width. This requirement becomes more difficult to meet in urban settings where residential properties often abut the proposed roadway corridor. In these situations, implementation of earth berms can require significant property acquisitions to accommodate noise mitigation, and the cost associated with the acquisition of property to construct a berm can significantly increase the total costs to implement this form of noise mitigation and make it unreasonable.

Availability of fill material to construct the berm also needs to be considered. On projects where proposed grading yields excess waste material, earth berms are often cost-effective mitigation options. On balance or borrow projects, the implementation of earth berms is often an expensive solution due to the need to identify, acquire, and transport the material to the project site. Berms were not considered for this project due to right-of-way constraints.

As a general practice, noise barriers are most effective when placed at a relatively high point between the roadway and the impacted noise-sensitive land use. To achieve the greatest benefit from a potential noise barrier, the goal of the barrier should focus on breaking the line of sight (to the greatest degree possible) from the roadway to the receptor. In roadway fill conditions, where the highway is above the natural grade, noise barriers are typically most effective when placed on the edge of the roadway shoulder or on top of the fill slope. In roadway cut conditions, where the roadway is located below the natural grade, barriers are typically most effective when placed at the top of the cut slope. Engineering and safety issues have the potential to alter these typical barrier locations.

The effectiveness of a noise barrier is measured by examining the barrier's capability to reduce future noise levels. Noise reduction is measured by comparing design year pre- and post-barrier noise levels. This difference between unabated and abated noise levels is known as insertion loss (IL).

Additionally, the Noise Policy Code of Virginia (HB 2577, as amended by HB 2025) states:

"Whenever the Commonwealth Transportation Board or the Department plan for or undertake any highway construction or improvement project and such project includes or may include the requirement for the mitigation of traffic noise impacts, first consideration should be given to the use of noise reducing design and low noise pavement materials and techniques in lieu of construction of noise barriers or sound barriers. Vegetative screening, such as the planting of appropriate conifers, in such a design would be utilized to act as a visual screen if visual screening is required."

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This documentation is located in **Appendix D**.

# 6.2 FEASIBILITY, REASONABLENESS, AND DESIGN GOALS

According to FHWA and VDOT guidelines, potential mitigation measures for warranted receptors must also be assessed for feasibility and reasonableness. Noise mitigation is required to be both "feasible" and "reasonable" to be recommended for construction.

# 6.2.1 Feasibility Criterion for Noise Barriers

All receptors that meet the warranted criterion must progress to the "feasible" phase. Phase 2 of the noise abatement criteria requires that both of the following acoustical and engineering conditions be considered. The noise abatement measure is said to be feasible if it meets both of the following criteria.

- At least a 5 dBA highway traffic noise reduction at impacted receptors: According to 23 CFR 772, FHWA requires the highway agency to determine the number of impacted receptors required to achieve at least 5 dBA of reduction. VDOT requires that 50% or more of the impacted receptors experience 5 dBA or more of insertion loss to be feasible.
- The determination that it is possible to design and construct the noise abatement measure: The factors related to the design and construction include safety, barrier height, topography, drainage, utilities, environmental impacts and maintenance of the abatement measure, maintenance access to adjacent properties, and general access to adjacent properties (i.e., arterial widening projects). Topography and environmental impacts, notably the avoidance of jurisdictional wetlands and streams, are required to be considered to ensure the recommended noise barrier improvements can be permitted by the appropriate state and federal agencies (Virginia Department of Environmental Quality and U.S. Army Corps of Engineers, for example). A feasibility determination (e.g., engineering conflicts, sight distance, safety concerns, etc.) has been conducted for all the proposed barriers. There were no feasibility issues noted except for the floodplain impacts noted for Barrier System F4-F4B and Barrier System G8-G9.

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#### 6.2.2 Reasonableness Criterion for Noise Barriers

All receptors that meet the feasibility criterion must progress to the "reasonableness" phase. Phase 3 of the noise abatement criteria requires that all of the following conditions be considered.

- The Viewpoints of the Benefited Receptors: VDOT shall solicit the viewpoints of all benefited receptors (refer to Section 7.1) through certified mailings and obtain enough responses to document a decision as to whether or not there is a desire for the proposed noise abatement measure. Fifty percent (50%) or more of the respondents shall be required to favor the noise abatement measure in determining reasonableness. Community views in and of themselves are not sufficient for a barrier to be found reasonable if one or both of the other two reasonableness criteria are not satisfied.
- Cost-effectiveness: Typically, the limiting factor related to barrier reasonableness is the cost-effectiveness value, where the total surface area of the barrier is divided by the number of benefited receptors receiving at least a 5 dBA reduction in noise level. VDOT's approved cost is based on a maximum square footage of abatement per benefited receptor, a value of 1,600 square feet per benefited receptor (SF/BR).

Where multi-family housing includes balconies at elevations that exceed a 30-foot high barrier or the topography causes receptors to be above the elevation of a 30-foot barrier, these receptors are not assessed for barrier benefits and are not included in the computation of the barrier's reasonableness.

#### 6.2.3 Noise Reduction Design Goals

The design goal is a reasonableness factor indicating a specific reduction in noise levels that VDOT uses to identify that a noise abatement measure effectively reduces noise. The design goal establishes a criterion, selected by VDOT, which noise abatement must achieve. VDOT's noise reduction design goal is defined as a 7 dBA of insertion loss for at least one impacted receptor, meaning that at least one impacted receptor is predicted to achieve a 7 dBA or greater noise reduction with the proposed barrier in place. The design goal is not the same as acoustic feasibility, which defines the minimum level of effectiveness for a noise abatement measure.

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Acoustic feasibility indicates that the noise abatement measure can, at a minimum, achieve a discernible reduction in noise levels.

Noise reduction is measured by comparing the future design year (2040) build condition pre-and post-barrier noise levels. This difference between unabated and abated noise levels is known as "insertion loss" (IL). It is important to optimize the noise barrier design to achieve the most effective noise barrier in terms of both noise reduction (insertion losses) and cost. Although at least a 5 dBA reduction is required to meet the feasibility criteria, the following tiered noise barrier abatement goals are used to govern barrier design and optimization.

- Reduction of future highway traffic noise by 7 dBA at one or more of the impacted receptor sites (required criterion)
- Reduction of future highway traffic noise levels to the low-60-decibel range when practical (desirable)
- Reduction of future highway traffic noise levels to existing noise levels when practical (desirable)

#### 6.3 NOISE ABATEMENT RESULTS

Noise barriers were evaluated for the residences within CNE A, B, C, D, E, F, G, H, I, J, K, L, and N that are predicted to experience noise impacts in the build condition. The barrier locations are shown on the graphics located on **Figures 2A** through **2K**. An overview of the evaluated barrier parameters is shown in **Table 10**. A summary of the evaluated barriers acoustical performance and statistics is described in the following subsections. The detailed sound level results for each receptor are located in **Tables 11** through **30** (refer to Data Tables for sound levels data tables). The acoustical profiles of the recommended noise barriers are located within Appendix C. The Warranted, Feasible, and Reasonable Worksheets were completed for all impacted CNEs are included in Appendix E.

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**TABLE 10** SUMMARY OF POTENTIAL NOISE BARRIERS EVALUATED IN THIS STUDY

		Mumbar	lmnastad			Noise B	arrier Deta	ils	Curfoco Arool		le?
CNE	Barrier ID	Number of Impacted Receptors	Impacted and Benefitted Receptors	tted Recentors		Average Height Range (ft)	Surface Area (SF)	Cost at \$42/SF	Surface Area/ Benefitted Receptor (SF/BR) <sup>1</sup>	Feasible?	Reasonable?
٨	A1	1	1	4	600	16	9,597	\$403,074	1,919	Υ	N
Α	A2	1	1	12	1,286	16	20,117	\$844,914	1,547	Υ	Υ
B/D	B1-B5, D1	19	19	49	5,593	15	83,891	\$3,523,422	1,234	Υ	Υ
D/E	D2, E1-E4	18	18	24	4,326	15	64,888	\$2,725,296	1,545	Υ	Υ
С	C1-C2	21	21	47	5,140	15	77,096	\$3,238,032	1,134	Υ	Υ
	F1, F1B, F1C, F2	8	7	3	1,127	13	14,658	\$615,636	1,466	Υ	Υ
F	F3	12	12	14	2,546	16	40,735	\$1,710,870	1,567	Υ	Υ
	F4-F4B	6	6	16	2,210	16	35,352	\$1,484,784	1,607	N	
	F5-F9	8	8	17	2,489	22	54,789	\$2,301,138	2,192	Υ	N
	G1-G6	24	24	54	5,350	18	96,303	\$4,044,726	1,234	Υ	Υ
G	G8-G9	16	15	13	1,906	14	26,678	\$1,120,476	953	Ν	
l G	G10-G13	20	20	10	2,591	17	44,649	\$1,875,258	1,488	Υ	Υ
	G14-G16	3	3	1	801	16	12,831	\$538,902	3,208	Υ	N
Н	H2-H11	20	18	24	3,901	16	61,772	\$2,594,424	1,470	Υ	Υ
	12	5	5	2	835	13	10,852	\$455,784	1,550	Υ	Υ
'	I4-6	8	8	4	1,041	16	16,654	\$699,468	1,388	Υ	Υ
J/K	J2-J3, K1-K4	15	14	27	3,094	16	49,494	\$2,078,748	1,207	Υ	Υ
	L1-L5	4	3	1	974	12	11,693	\$491,106	2,923	Υ	N
L	L6-L8	2	2	2	852	12	9,703	\$407,526	2,426	Υ	N
	Existing Barrier N	10	0	1	307	15	4,607	\$193,494	4,607	N	
N	N1-N3 and Existing	10	9	6	1,577	14	23,132	\$971,544	1,542	Υ	Υ
	N4	1	1	0	301	18	5,427	\$227,934	5,427	Υ	N

1 Where Square Feet/Benefitted Receptor (SF/BR) exceeds VDOT's maximum of 1,600, a noise barrier would not be considered cost-reasonable.

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#### 6.3.1 CNE A

# Barrier A1

A single noise barrier configuration (Barrier A1) was evaluated for all the CNE A impacted receptors on Cedar Chase Court/Road, extending west of Reston Avenue behind the 7 Eleven Store. **Table 11** (see Data Tables) outlines the performance of the optimized barrier scenario.

The barrier averages 16 feet in height, totals 600 feet in length, and has a total surface area of 9,597 SF benefitting five receptors, equating to 1,919 SF/BR. The barrier provides a noise reduction of 6 to 8 dBA and benefits one impacted receptor as well as four non-impacted receptors. The barrier provides an average noise reduction of 6 dBA to the benefitted receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 100% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier is considered feasible but not reasonable due to a SF/BR calculation above the specified 1,600 SF/BR.

#### **Barrier A2**

A single noise barrier configuration (Barrier A2) was evaluated for all the CNE A impacted receptor on Water Pointe Lane, extending from approximately eastbound Station 1178+00 to Station 1190+00 where it terminates at Reston Parkway. **Table 12** (see Data Tables) outlines the performance of the optimized barrier scenario.

The barrier averages 16 feet in height (13 to 18 feet), totals 1,286 in length, and has a total surface area of 20,117 SF benefitting 13 receptors, equating to 1,547 SF/BR. The barrier provides a noise reduction of 5 to 8 dBA and benefits the one impacted receptor as well as 12 non-impacted receptors. The barrier provides an average noise reduction of 7 dBA to the benefitted receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 100% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier is considered feasible and reasonable pending public involvement.

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# 6.3.2 CNE B

# Barrier System B1-B5 and D1

A six noise barrier configuration (Barrier B1-B5 and D1) was evaluated for all the impacted receptors in CNE B and a portion of CNE D (Nike Park athletic fields; Receptors D-01 through D-30), extending from approximately westbound Station 167+00 to Station 224+75 (Reston Avenue to Nike Park). Breaks in the barriers system are required for two private driveways, the walking path and Utterback Store Road. The barriers were evaluated as system since they were shown to work interdependently. **Table 13** (see Data Tables) outlines the performance of the optimized barrier for both scenarios.

Barriers B2-B5 and D1 average 15 feet in height, total 5,593 feet in length, and have a total surface area of 83,891 SF benefitting 68 receptors, equating to 1,234 SF/BR. The barriers provide a noise reduction of 5 to 14 dBA and benefits 19 of the 19 impacted receptors as well as 49 non-impacted receptors. The barrier system provides an average noise reduction of 7 dBA to the benefitted receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 100% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier system is considered <u>feasible and reasonable</u> pending public involvement.

#### 6.3.3 CNE D/E

#### **Barrier System D2 and E1-E4**

A five noise barrier configuration (Barrier D2 and Barriers E1-E4) was evaluated for all the impacted receptors in CNE E and a portion of CNE D (Great Passage Court; Receptors D-31 through D-41), extending from approximately westbound Station 228+50 to Station 277+00 (Columbia Gas plant to Springvale Road). Breaks in the barrier system are required for Great Passage Boulevard, Amanda Drive, Riva Ridge Drive and a pipeline right-of-way. The barriers were evaluated as a system since they were shown to work interdependently. **Table 14** (see Data Tables) outlines the performance of the optimized barrier scenario.

Barrier D2 and Barriers E1-E4 average 15 feet in height, total 4,326 feet in length, and have a total surface area of 64,888 SF benefitting 42 receptors, equating to 1,545 SF/BR. The

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barriers provide a noise reduction of 5 to 10 dBA and benefits all 18 of the 18 impacted receptors as well as 25 non-impacted receptors. The barrier system provides an average noise reduction of 6 dBA to the benefitted receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 100% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier system is considered **feasible and reasonable** pending public involvement.

#### 6.3.4 CNE C

# **Barrier System C1-C2**

A two noise barrier configuration (Barriers C1–C2) was evaluated for all the impacted receptors in CNE C, extending from approximately eastbound Station 1193+00 to Station 1245+75 (Reston Parkway to Markell Court). A break in the barrier is required at Bishopgate Way. The barriers were evaluated as a system since they were shown to work interdependently. **Table 15** (see Data Tables) outlines the performance of the optimized barrier scenario.

Barriers C1-C2 average 15 feet in height, total 5,140 feet in length, and have a total surface area of 77,096 SF benefitting 68 receptors, equating to 1,134 SF/BR. The barriers provide a noise reduction of 5 to 15 dBA and benefits all 21 impacted receptors as well as 47 non-impacted receptors. The barrier system provides an average noise reduction of 8 dBA to the benefitted receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 100% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier system is considered **feasible and reasonable** pending public involvement.

#### 6.3.5 CNE F

CNE F was divided into four subareas (F1, F1B, F1C, and F2; F-3; F4 and F4B; and F5-F9) to evaluate the noise barriers configurations independently based on their individual acoustical influence zones.

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# Barrier System F1-F1B, F1C, and F2

A four noise barrier configuration (Barriers F1-F1B, F1C, and F2) was evaluated for all the CNE F impacted receptors west of Colvin Run Road W, extending from approximately westbound Station 301+00 to Station 312+75. The noise barrier protects residences along Van Patten Lane, a cemetery along Route 7, and a single-family residence along Route 7. The barrier was required to be split for two driveways into the cemetery as well as a residential driveway. The barriers were evaluated as a system since they were shown to work interdependently. **Table 16** (see Data Tables) outlines the performance of the optimized barrier scenario.

The barriers average 13 feet in height, total 1,127 feet in length, and have a total surface area of 14,658 SF benefitting 10 receptors, equating to 1,466 SF/BR. The barriers provide a noise reduction of 5 to 10 dBA and benefits seven of the eight impacted receptors as well as three non-impacted receptors. The barrier system provides an average noise reduction of 6 dBA to the benefitted receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 88% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier system is considered **feasible and reasonable** pending public involvement.

#### **Barrier F3**

A single noise barrier configuration (Barrier F3) was evaluated for all the CNE F impacted receptors on Colvin Meadows Lane, extending from approximately westbound Station 313+50 to Station 338+80. **Table 17** (see Data Tables) outlines the performance of the optimized barrier scenario.

The barrier averages 16 feet in height, totals 2,546 feet in length, and has a total surface area of 40,735 SF benefitting 26 receptors, equating to 1,567 SF/BR. The barrier provides a noise reduction of 5 to 11 dBA and benefits all 12 impacted receptors as well as 14 non-impacted receptors. The barrier provides an average noise reduction of 8 dBA to the benefitted receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 100% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier is considered feasible and reasonable pending public involvement.



# **Barrier System F4-F4B**

A dual noise barrier configuration (Barrier F4-F4B) was evaluated for all the CNE F impacted receptors near the Clovin Run Mill including trail receptors, extending from approximately westbound Station 346+00 to Station 369+50. A break in the barrier is required at Colvin Run Road. The barriers were evaluated as a system since they were shown to work interdependently. **Table 18** (see Data Tables) outlines the performance of the optimized barrier scenario.

Additional investigations have indicated that this barrier is **not feasible** as a result of floodplain impacts associated with Difficult Run watershed. Barrier System F4-F4B was determined to be not-feasible due to the potential impacts to the 100-year floodplain as a result of construction of these noise barriers. While the bridge over Difficult Run is being raised to accommodate the 25-year storm, the 100-year storm is still projected to overtop Route 7. As the low point on Route 7 is west of the bridge over Difficult Run, construction of noise barrier system F4-F4B would restrict flow during 100-year and larger flow events, potentially resulting in damaging flood impacts upstream of Route 7. Accordingly, the barrier system is deemed "not-feasible" and therefore is not recommended for construction. There are no alternative barrier locations outside the floodplain where a barrier can be constructed to effectively mitigate noise levels.

#### **Barrier System F5-F9**

A five noise barrier configuration (Barrier F5-F9) was evaluated for all the CNE F impacted receptors along Locust Hills Drive, extending from approximately westbound Station 370+00 to Station 397+00. There are three private driveways east of Faulkner Drive that require breaks in the barrier. The barriers were evaluated as a system since they were shown to work interdependently. **Table 19** (see Data Tables) outlines the performance of the optimized barrier scenario.

The barriers average 22 feet in height, total 2,489 feet in length, and have a total surface area of 54,789 SF benefitting 25 receptors, equating to 2,192 SF/BR. The barriers provide a noise reduction of 5 to 12 dBA and benefits all eight impacted receptors as well as 17 non-impacted receptors. The barrier system provides an average noise reduction of 6 dBA to the



benefitted receptors. The barrier is considered <u>feasible but not reasonable</u> due to a SF/BR calculation above the specified 1,600 SF/BR.

Multiple noise barrier height iterations from 10 to 30 feet were analyzed for this portion of CNE F in attempt to design a reasonable barrier. In addition, partial mitigation (i.e., F5-F8, F6-F8, F6-F9) was also analyzed from 10 to 30 feet. A barrier design that met the specified reasonable calculation threshold was not found for any of the alternatives analyzed. The acoustical effectiveness is reduced as a result of the breaks in the barrier coupled with the terrain and distance to the receptors along Locust Hill Drive. The number of non-impacted benefitting receptors as a result of barrier systems analyzed is diminished by flanking noise propagating through the required breaks in the barrier needed for the three private driveways and Faulkner Drive. A matrix of results is located with the CNE F5-F9 Warranted Feasible and Reasonable Worksheets located in Appendix E.

#### 6.3.6 CNE G

CNE G was divided into four subareas (G1-G6, G8-G9, G11-G13, and G14-G16) to evaluate the noise barriers configurations independently based on their individual acoustical influence zones.

#### **Barrier System G1-G6**

A six noise barrier configuration (Barriers G1-G6) was evaluated for all the CNE G impacted receptors between Baron Cameron Road of Colvin Forest Drive, extending from approximately eastbound Station 1280+50 to Station 1338+35. The noise barrier protects residences along Dunn Meadow Road, Dunn Meadow Court, Colvin Forest Drive and three single-family residences that have a private driveway from Route 7. Breaks in the barriers system are required at Delta Gate Court, Colvin Forest Drive and three private driveways. The barriers were evaluated as a system since they were shown to work interdependently. **Table 20** (see Data Tables) outlines the performance of the optimized barrier scenario.

The barriers average 18 feet in height, total 5,350 feet in length, and have a total surface area of 96,303 SF benefitting 78 receptors, equating to 1,235 SF/BR. The barriers provide a noise reduction of 5 to 14 dBA and benefits all 24 impacted receptors as well as 54 non-impacted receptors. The barrier system provides an average noise reduction of 8 dBA to the benefitted



receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 100% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier is considered <u>feasible and reasonable</u> pending public involvement.

#### **Barrier System G8-G9**

A dual noise barrier configuration (Barrier G8-G9) was evaluated for the CNE G impacted receptors representing the Cross County recreational trail that crosses Carpers Farm Way, extending from approximately eastbound Station 1350+00 to Station 1369+250. A break in the barrier is required at Colvin Run Road. The barriers were evaluated as a system since they were shown to work interdependently. **Table 21** (see Data Tables) outlines the performance of the optimized barrier scenario.

Additional investigations have indicated that this barrier is **not feasible** as a result of floodplain impacts associated with Difficult Run watershed. Noise barriers G8 and G9 near Colvin Run and Difficult Run were determined to be not-feasible due to the potential impacts to the 100-year floodplain as a result of construction of these noise barriers. While the bridge over Difficult Run is being raised to accommodate the 25-year storm, the 100-year storm is still projected to overtop Route 7. As the low point on Route 7 is west of the bridge over Difficult Run, construction of barrier system G8-G9 would restrict flow during 100-year and larger flow events, potentially resulting in damaging flood impacts upstream of Route 7. Accordingly, Barrier System G8-G9 is deemed "not-feasible" and therefore is not recommended for construction. All of the impacts are located with the floodplain and alternative offline barrier locations are not feasible.

# **Barrier System G10-G13**

A five noise barrier configuration (Barriers G10-G13) was evaluated for all the CNE G impacted receptors between Serenity Woods Lane and Middleton Ridge Road, extending from approximately eastbound Station 1373+00 to Station 1400+00. The noise barrier was designed to protect residences along Serenity Woods Lane, Middleton Ridge Road, Middleton Court, Difficult Run Court, and Tweed Court. Breaks in the barriers system were required at Serenity Woods Lane, two private driveways and Middleton Ridge Road. The barriers were evaluated as

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a system since they were shown to work interdependently. **Table 22** (see Data Tables) outlines the performance of the optimized barrier scenario.

The barriers average 17 feet in height (13 to 18 feet), total 2,591 feet in length, and have a total surface area of 44,649 SF benefitting 30 receptors, equating to 1,488 SF/BR. The barriers provide a noise reduction of 5 to 13 dBA and benefits at all 20 impacted receptors as well as 10 non-impacted receptors. The barrier system provides an average noise reduction of 8 dBA to the benefitted receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 100% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier configuration is considered **feasible and reasonable** pending public involvement.

# **Barrier System G14-G16**

A three noise barrier configuration (Barriers G14-G16) was evaluated for all the CNE G impacted receptors between Serenity Woods Lane and Middleton Ridge Road, extending from approximately eastbound Station 1407+50 to Station 1414+00. The noise barrier protects a single-family residence (Receptor G-202), the playground at Chesterbrook Academy Preschool (Receptor G-203) – both of which have direct access from Route 7, and a single-family residence with access off of Beulah Road. Breaks in the barrier system are required for two private driveways. The barriers were evaluated as a system since they were shown to work interdependently. **Table 23** (see Data Tables) outlines the performance of the optimized barrier scenario.

The barriers average 16 feet in height, total 801 feet in length, and have a total surface area of 12,831 SF benefitting four receptors, equating to 3,208 SF/BR. The barriers provide a noise reduction of 5 to 7 dBA and benefits at all three impacted receptors as well as one non-impacted receptor. The barrier system provides an average noise reduction of 6 dBA to the benefitted receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 100% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier configuration is considered <u>feasible but not reasonable</u> due to a SF/BR calculation above the specified 1600 SF/BR.

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# 6.3.7 CNE H

# Barrier System H2-H11

A 10 noise barrier configuration (Barriers H2-H11) was evaluated for all the CNE H impacted receptors between Forestville Drive and Towlston Road, extending from approximately eastbound Station 408+00 to Station 452+30. The noise barrier protects residences along Farmingdale Court, Wolf Trap Creek Court, five residences with direct driveway access onto Route 7, and the outdoor recreational area associated with The Eastern Ridge School. Breaks in the barrier system are required at Forestville Drive as well as the residential driveways. The barriers were evaluated as a system since they were shown to work interdependently. **Table 24** (see Data Tables) outlines the performance of the optimized barrier scenario. This barrier impacts overhead utility lines and will require relocating the powerlines to the front yards of the homes that abut Route 7. An additional barrier was evaluated as part of this system west of barrier H2 in an attempt to provide additional attenuation at site H-01, however the barrier provided no additional acoustical benefit and therefore was excluded from the barrier system.

The barriers average 16 feet in height (15 to 16 feet), total 3,901 feet in length, and have a total surface area of 61,772 SF benefitting 42 receptors, equating to 1,470SF/BR. The barriers provide a noise reduction of 5 to 17 dBA and benefits at 18 of 20 impacted receptors as well as 24 non-impacted receptors. The barrier system provides an average noise reduction of 8 dBA to the benefitted receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 90% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier configuration is considered **feasible and reasonable** pending public involvement.

#### 6.3.8 CNE I

#### **Barrier 12**

A single noise barrier configuration (Barrier I2) was evaluated for part of the CNE I impacted receptors on Deramus Farm Court, extending west of Atwood Road. **Table 25** (see Data Tables) outlines the performance of the optimized barrier scenario.

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The barrier averages 13 feet in height, totals 835 feet in length, and has a total surface area of 10,852 SF benefitting seven receptors, equating to 1,550 SF/BR. The barrier provides a noise reduction of 5 to 12 dBA and benefits five impacted receptors as well as two non-impacted receptors. The barrier provides an average noise reduction of 7 dBA to the benefitted receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 100% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier configuration is considered <u>feasible and reasonable</u> pending public involvement.

# **Barrier System I4-I6**

A three noise barrier configuration (Barriers I4-I6) was evaluated for part of the CNE I impacted receptors extending east of Atwood Road to Towlston Road. Breaks in the barrier system are required at Stokley Way and a residential driveway. The barriers were evaluated as a system since they were shown to work interdependently. **Table 26** (see Data Tables) outlines the performance of the optimized barrier scenario.

The barrier averages 16 feet in height, totals 1,041 feet in length, and has a total surface area of 16,654 SF benefitting 12 receptors, equating to 1,388 SF/BR. The barrier provides a noise reduction of 5 to 11 dBA and benefits eight impacted receptors as well as four non-impacted receptors. The barrier provides an average noise reduction of 6 dBA to the benefitted receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 100% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier is considered feasible and reasonable due to a SF/BR calculation above the specified 1,600 SF/BR.

#### 6.3.9 CNE J K

#### **Barrier System J K**

A six noise barrier configuration (Barriers J2-J3 and K1-K4) was evaluated for all the impacted receptors in CNE J, and K extending from approximately eastbound Station 1453+50 to Station 1488+25. Breaks in the barrier systems were required at Trap Road, Lucky Estates Drive and 2 private access driveways. The barriers were evaluated as a system since they were

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shown to work interdependently. **Table 27** (see Data Tables) outlines the performance of the optimized barrier scenario. A barrier was evaluated west of Towlston Road, but provided no acoustical benefit to the impacted site J-01 and was removed from the analysis.

Barrier configuration JK is 16 feet in height, totals 3,094 feet in length, and has a total surface area of 49,494 SF benefitting 41 receptors, equating to 1,207 SF/BR. The barriers provide a noise reduction of 5 to 10 dBA and benefits 14 out of 15 impacted receptors as well as 27 non-impacted receptors. A barrier was evaluated west of Towson Road in an effort to benefit the impacted site J-01. However, the barrier did not provide any acoustical benefits to the site, therefore was eliminated from the barrier system. The barrier system provides an average noise reduction of 6 dBA to the benefitted receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 93% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier configuration is considered <u>feasible and reasonable</u> pending public involvement.

#### 6.3.9 CNE L

CNE L was divided into two subareas (L1-L5 and L6-L8) to evaluate the noise barriers configurations independently based on their individual acoustical influence zones.

#### **Barrier System L1-L5**

A five noise barrier configuration (Barriers L1-L5) was evaluated for impacted Receptors L-01, L-03, L-04, and L-05 in CNE L, extending from approximately westbound Station 463+00 to Station 474+00. The breaks in the barrier system are required for four private driveways. The barriers were evaluated as a system since they were shown to work interdependently. **Table 28** (see Data Tables) outlines the performance of the optimized barrier scenario.

The barriers average 12 in height (11 to 13 feet), are 974 feet in length, and have a total surface area of 11,693 SF benefitting four receptors, equating to 2,923 SF/BR. The barriers provide a noise reduction of 5 to 7 dBA and benefits the three of the four impacted receptors and one non-impacted benefitted receptor. The barrier system provides an average noise reduction of 6 dBA to the benefitted receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 75% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA



design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier is considered **feasible but not reasonable** due to a SF/BR calculation above the specified 1,600 SF/BR.

# **Barrier System L6-L8**

A three noise barrier configuration (Barriers L6-L8) was evaluated for impacted Receptors L-11 and L-12 in CNE L, extending from approximately westbound Station 479+00 to Station 488+00. The breaks in the barrier system were required at two private driveways. The barriers were evaluated as a system since they were shown to work interdependently. **Table 29** (see Data Tables) outlines the performance of the optimized barrier scenario.

The barriers average 12 in height (10 to 12 feet), are 852 feet in length, and have a total surface area of 9,703 SF benefitting four receptors, equating to 2,426 SF/BR. The barriers provide a noise reduction of 5 to 10 dBA and benefit the two impacted receptors and two non-impacted benefitted receptors. The barrier system provides an average noise reduction of 7 dBA to the benefitted receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 100% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier is considered feasible **but not reasonable** due to a SF/BR calculation above the specified 1,600 SF/BR. The barrier is not feasible since it does not provide 5 dBA reduction to 50% of the impacted locations.

#### 6.3.10 CNE N

# **Existing Barrier N**

CNE N contains an existing noise barrier that was constructed as part of the Route 7 over Dulles Access Toll Road (DATR) Major Bridge Rehabilitation project (UPC 82135). This barrier extends from eastbound Station 1523+25 to Station 1526+75 and was designed for noise sensitive sites behind the Stanbridge Place duplexes represented by Receptors N-75 and N-76 in this analysis. Following VDOT's guidance for evaluating existing noise barriers that are not physically impacted, future design year noise levels were evaluated with the existing noise barrier in place. Noise impacts were identified behind the noise barrier, therefore the barrier was

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evaluated for its effectiveness. Design year build noise levels with and without the existing noise barrier were analyzed. **Table 30** (see Data Tables) outlines the performance of the optimized barrier scenario.

The existing sound barrier configuration averages 15 feet in height, totals 307 feet in length, and has a total surface area of 4,607 SF benefitting one non-impacted receptor (church interior), equating to 4,607 SF/BR. The existing barrier does not benefit any impacted sites; therefore, it is considered not feasible. As such, a new barrier system (described below) was evaluated.

# **Barrier System N1-N3 and Existing Barrier**

As previously mentioned, since the existing barrier was not shown to be feasible, a new barrier system was evaluated at this location. The three noise barrier configuration (Barriers N1-N3 and existing Barrier) was evaluated for all the impacted receptors in CNE N, extending from approximately eastbound Station 1508+00 to Station 1526+75 (Laurel Jill Road to Jarrett Valley Drive). The barrier system is split by Laurel Hill Road and Old Ash Grove. The required access openings limit the overall effectiveness of this sound barrier configuration. The barriers were evaluated as a system since they were shown to work interdependently. **Table 31** (see Data Tables) outlines the performance of the optimized barrier scenario.

The barrier system varies from 12 to 15 feet in height (N1 is 12 feet high and N2-N3 are 15 feet high), totals 1,577 feet in length, and has a total surface area of 23,132 SF (including existing barrier) benefitting 15 receptors, equating to 1,542 SF/BR. The barriers provide a noise reduction of 5 to 10 dBA and benefits nine of 10 impacted receptors including the two impacted sites (N-75 and N-79) behind the existing noise barrier. Furthermore, the noise barrier benefits six non-impacted receptors. The barrier system provides an average noise reduction of 7 dBA to the benefitted receptors. The barrier is feasible since it provides at least a 5 dBA reduction to 90% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier configuration is considered <u>feasible and reasonable</u> pending public involvement.



#### **Barrier N4**

A noise barrier configuration N4 was evaluated for the isolated impacted Receptor N-78 in CNE N, extending from Jarret Valley Drive to the on ramp for the DTR. The barrier was evaluated independently from N1-N3 due to its isolation from the remainder of CNE N. **Table 32** (see Data Tables) outlines the performance of the optimized barrier scenario.

Barrier N4 averages 18 feet in height, totals 301 feet in length, and has a total surface area of 5,427 SF benefitting one receptor, equating to 5,427 SF/BR. The barrier provides a noise reduction of 7 dBA and benefits one impacted receptor. The barrier is feasible since it provides at least a 5 dBA reduction to 100% of the impacted locations (greater than 50%). The barrier also meets the 7 dBA design goal since it provides a noise reduction of at least 7 dBA to more than one impacted receptor. The barrier is considered **feasible but not reasonable** due to a SF/BR calculation above the specified 1,600 SF/BR.

A summary of the noise barriers analyzed and determined to be feasible and reasonable is located in **Table 33**.



# TABLE 33 SUMMARY OF FEASIBLE AND REASONABLE NOISE BARRIERS

	Barrier ID	Inser Los (dB	ss	Hei (f		Length Area		Total #	Benefitted Units			Square Foot per	Cost
CNE		Range	Average	Range	Average	(ft)	(SF)	Impacted Units	Impacts	Non- Impacts	Total	Benefitted Receptor	(\$42.00/ft²)
Α	A2	5-8	7	13-18	16	1,286	20,117	1	1	12	13	1,547	\$844,914
B, D	B1-B5 and D1	5-14	7	15	15	5,593	83,891	19	19	49	68	1,234	\$3,523,422
С	C1-C2	5-15	8	15	15	5,140	77,096	21	21	47	68	1,134	\$3,238,032
D, E	D2 and E1-E4	5-10	6	15	15	4,326	64,888	18	18	24	42	1,545	\$2,725,296
F	F1, F1B, F1C, F2	5-10	6	13	13	1,127	14,658	8	7	3	10	1,466	\$615,636
「	F3	5-11	7	16	16	2,546	40,735	12	12	14	26	1,567	\$1,710,870
	G1-G6	5-14	8	18	18	5,350	96,303	24	24	54	78	1,234	\$4,044,726
G	G10-G13	5-13	8	13-18	17	2,591	44,649	20	20	10	30	1,488	\$1,875,258
Н	H2-H11	5-17	8	15-16	16	3,901	61,772	20	18	24	42	1,470	\$2,594,424
I	12	5-12	7	13	13	835	10,852	5	5	2	7	1,550	\$455,784
	14-16	5-11	6	16	16	1,041	16,654	8	8	4	12	1,388	\$699,468
JK	J2-J3, K1-K04	5-10	6	16	16	3,094	49,494	15	14	27	41	1,207	\$2,078,748
N	N1-N3 and Existing Barrier	5-10	7	12-15	14	1,577	23,132	10	9	6	15	1,542	\$971,544

\* Insertion Loss statistics are calculated for all benefitted receptors

Route 7 Widening: Reston Avenue to Jarrett Valley Drive State Project 0007-029-942, 0007-029-225 Federal Project No.: STP-5A01(745) and STP-5A01(790)

ROUTE 7 CORRIDOR IMPROVEMENTS

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# 7.0 PUBLIC INVOLVEMENT/LOCAL OFFICIALS COORDINATION

FHWA and VDOT policies require that VDOT provide certain information to local officials within whose jurisdiction the highway project is located in order to minimize future traffic noise impacts of Type I projects on currently undeveloped lands. (Type I projects involve highway improvements with noise analysis.) This information must include details on noise-compatible land-use planning and noise impact zones for undeveloped lands within the project corridor. The aforementioned details are provided below. Additional information about VDOT's noise abatement program has also been included in this section.

#### 7.1 PUBLIC INVOLVEMENT EFFORTS

This section documents the administration and results of the public preference surveys conducted for the recommended noise barrier systems. Figures 2A through 2K in the project mapping show the summary of the barrier voting, by parcel. Additional public involvement was completed for the residences adjacent to revisions to Noise Barrier G2. Of the five surveys sent to adjoining property owners, 4 were returned in favor of the revised barrier design.

#### **Public Preference Surveys**

Property owners and residents, including tenants, of all properties that would be benefited by the recommended noise barriers were sent survey letters by certified mail. Twenty-one (21) calendar days from the anticipated delivery date is required to provide the recipients ample time to review and respond to the survey. The letters and surveys, from Dewberry, asked the respondents to indicate whether they wished to have the proposed noise barriers constructed or not. In these mailings, barrier details, contact information, a survey form and return envelope were provided to homeowners and residents. The mailings gave the affected property owners/residents an understanding of the proposed barrier and its implications, an opportunity to ask questions, and a formal survey form for expressing their views. Only the owners and residents of those receptor units that will be benefited by the proposed mitigation may vote on whether the proposed noise barrier should be constructed. The owner/resident of each benefited receptor unit shall be entitled to one weighted vote, regardless of the number of owners of that receptor unit unless they are the owners of a rental facility or the developer of lands.



Survey recipients were informed that to register a vote in favor of the barrier, a "YES" survey form would have to be returned. In addition, a non-response does not assume that the survey recipient is in favor of the barrier's construction. The letters and surveys were sent out during the week of January 31, 2020. For this project, 455 certified letters were mailed. The disposition of all certified letters was tracked and retained in the technical files. Eighty-six letters were "returned to sender" and 22 were claimed, though a survey was not received.

# **Survey Responses**

Table 34 provides a summary of the survey responses for each mailer for each Barrier System. The table indicates the number of letters sent and the number of survey forms sent back with responses in favor ("YES"). For this project, 14 certified letters were mailed for Barrier System A2, 59 were sent for Barrier System B1-B5D and D1, 69 were mailed for Barrier System C1 and C2, 46 were sent for Barrier System D2 and E1-E4, 8 were sent for Barrier System F1, F1B, F1C and F2, 27 were sent for Barrier System F3, 83 were sent for Barrier System G1-G6, 36 were sent for Barrier System G10-G13, 47 were sent for Barrier System H2-H11, 8 were sent for Barrier System I2, 14 were sent for Barrier System I4-I6, 28 were sent for Barrier System J2-J3 and K1-K4, 16 were sent for Barrier System N1-N3. A total of 22 responses were received for Barrier C, of these all 22 are in favor of the noise barrier. A total of 11 responses were received for Barrier A2, of these 11 are in favor of the noise barrier and zero are not in favor of the barrier. A total of 41 responses were received for Barrier System B1-B5D and D1 of these 37 are in favor of the noise barrier and four are not in favor of the barrier. A total of 58 responses were received for Barrier System C1 and C2, of these 56 are in favor and two are not in favor of the barrier. A total of 32 responses were received for Barrier System D2 and E1-E4, of these 31 are in favor and one is not in favor of the barrier. A total of six responses were received for Barrier System F1, F1B, F1C, and F2, of these six are in favor and zero are not in favor of the barrier. A total of 24 responses were received for Barrier System F3, of these 24 are in favor and zero are not in favor of the barrier. A total of 54 responses were received for Barrier System G1-G6, of these 53 are in favor and one is not in favor of the barrier. A total of 28 responses were received for Barrier System G10-G13, of these 27 are in favor and one is not in favor of the barrier. A total of 32 responses were received for Barrier System H2-H11, of these 27 are in favor and one is not in favor of the barrier. A total of five responses were received for Barrier System I2, of these five are in favor and zero are not in favor of the barrier. A total of 11 responses were received for Barrier System I4-I6, of these 11 are in favor and zero are not in favor of the barrier. A total of 18



responses were received for Barrier System J2-J3 and K1-K4, of these 12 are in favor and six are not in favor of the barrier. A total of 11 responses were received for Barrier System N1-N3, of these 10 are in favor and one is not in favor of the barrier.

Table 34
SUMMARY OF BARRIER SURVEY LETTERS AND RESPONSES

Barrier Number	Total letter Mailed		onse: "In f barrier"	Non- Responsive	RTS (Return to Sender)	
	Malleu	Yes No		Responsive	Sender)	
Barrier System A2	14	11	0	3	1	
Barrier System B1-B5B and D1	59	37	4	18	8	
Barrier System C1 and C2	69	56	2	11	11	
Barrier System D2 and E1- E4	46	31	1	14	3	
Barrier System F1,F1B,F1C, and F2	8	6	0	2	1	
Barrier System F3	27	24	0	3	3	
Barrier System G1-G6	83	53	1	29	14	
Barrier System G10-G13	36	27	1	8	6	
Barrier System H2-H11	47	30	2	15	6	
Barrier System I2	8	5	0	3	0	
Barrier System I4-I6	14	11	0	3	1	
Barrier System J2-J3 and K1-K4	28	12	6	18	10	
Barrier System N1-N3	16	10	1	5	1	

The survey results were weighted according to section 12.4.1 of the VDOT Highway Traffic Noise Impact Analysis Guidance Manual. A summary of the weighted results are shown in **Table 35** below. The Tables from the Voting Summary worksheet showing the detailed weighted results are located in *Appendix J*.

ROUTE 7 CORRIDOR IMPROVEMENTS

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Table 35
SUMMARY OF BARRIER SURVEY WEIGHTED RESULTS

Barrier Number	% of "Yes" Votes (all votes)	% of "No" Votes (all votes)	# of Outstand- ing Votes (all votes)	% of "Yes" Votes (Re- spondents)	% of "No" Votes (Re- spondents)
Barrier System A2	73.9	0	26.1	100	0
Barrier System B1-B5B and D1	54.9	5.9	39.2	90.3	9.7
Barrier System C1 and C2	83.1	2.5	14.4	97.1	2.9
Barrier System D2 and E1-E4	72.1	1.8	26.1	97.5	2.5
Barrier System F1,F1B,F1C, and F2	54.5	0	45.5	100	0
Barrier System F3	94.1	0	5.9	100	0
Barrier System G1-G6	66.9	1.8	31.3	97.4	2.6
Barrier System G10- G13	83.8	2.3	13.8	97.3	2.7
Barrier System H2-H11	59.2	4.5	36.3	93	7
Barrier System I2	71	0	29	100	0
Barrier System I4-I6	76.9	0	23.1	100	0
Barrier System J2-J3 and K1-K4	28.5	13.9	57.6	67.2	32.8
Barrier System N1-N3	73	4.8	22.2	93.9	6.1

Based on the outcome of the barrier survey letters, Barrier System A2, Barrier System B1-B5B and D1, Barrier System C1 and C2, Barrier System D2 and E1-E4, Barrier System F1, F1B, F1C, and F2, Barrier System F3, Barrier System G1-G6, Barrier System G10-G13, Barrier System H2-H11, Barrier System I2, Barrier System I4-I6, Barrier System J2-J3 and K1-K4, and Barrier System N1-N3 are recommended for construction.



Additional public comments regarding both barrier systems are summarized below. Responses to specific resident questions were addressed by the team and have been included in **Appendix K**.

# BARRIER SYSTEM A2

- This is a great proposal. Thank you.
- Since 1997 the noise has escalated. Not sure how much more after the land expansion can be tolerated. Thank you for considering this noise wall.
- There is currently a wooden fence behind all the properties backing on to Route 7. Will the fence be replaced by the wall?

#### BARRIER SYSTEM B1-B5B AND D1

- I want the noise barrier to blend in the nearby surroundings so it won't look too out of place.

  The height to be as minimal as possible so it won't block too much of the existing view.
- It would be ideal if the above ground utilities (electric, telecom) could be buried as part of wall "B2" construction. If any trees have to be moved it would be ideal if they could be replaced. Thanks for considering our concerns and addressing the noise levels!!
- Adequate lighting along noise barrier needs to be installed
- Wow thank you for doing this survey! We look forward to RT. 7 improvements. Kindly request that you take into consideration the comments attached regarding cross section @ rt 7 Utterback Store Road. Thanks in Advance. Cross walk posts/corner makes a difficult & sharp right on red welcome improved design for better traffic flow.
- Please install as you go instead of at end of project.
- The noise level has increased over the past 2 years. We have been here for almost 30 years and now have to sleep with white noise machine. We welcome the noise barriers.



- It would prevent children, pets and animals crossing RT7 which is much safer. It would also cut down the emergency vehicle noise. I just say there are times when I jump from all the sirens.
- Please let us know when the project will be completed
- Thank you!
- Please see attachments.
- It's great that building a noise barrier, I've been looking forward to it for a long time. After I bought this house years ago, there were big trees on the roadside have been cut down. Being harassed by the loudest noise from cars, trucks, planes and firetrucks stay at the deck and backyard. Prolonged neurasthenia and tinnitus headaches led to a doctor's diagnosis of anxiety last year.
- For our health and fitness, 1) we vote for building noise barrier as soon as possible, because my house is located at a hill; also add extra long wall from another side.
- 2) please plant more ever green trees to replace those have been cut, or we have to apply for some exemption from the property tax to plant those trees by ourselves.
- I agree with the noise barriers on the condition that residential side of the barrier has landscaping
- I live off the street on route 7 and I'm worried more trees will need to be cut down.
- A noise barrier is not necessary to protect our property from excessive noise.
- In order to preserve nature and the scenery of the neighborhood we require to plant trees on the residential side
- There are too few homes close enough to the proposed location for the noise barrier to be needed or effective. Instead the barrier would encroach upon the wooded areas that residents consider part of the beauty of our residential areas. The barrier would require removal of even more beautiful trees, to be replaced by a mile of unsightly concrete. It is an unnecessary expense!

February 22, 2020

Potential Noise Barriers B1-B58 and D1 (Considered for Construction) - **Specifically section B5B**Jennifer Thomas and Craig Curtis at Shirley Contracting Company,

L.J. Muchenje Highway Noise Specialist at VDOT

And



# To Whom It May Concern:

First, I would like to let Craig Curtis, Jennifer Thomas, and L. J. Muchenje know that I appreciate the understanding they've expressed concerning my situation. The proximity and dimensions of the proposed sound wall (listed as section B58), which, if built as planned, will run the entire 365 feet of my

southernmost property line and stand within 35 to 50 feet of that boundary for the majority of that run.

Unfortunately, while the empathy I received was welcomed, what I had hoped for was something
more

substantive. Perhaps alternatives to or possibilities to mitigate the objectionable prospect of this imposing structure that will run the entire length of my property disrupting the attractive natural scenery and destroying the view that enticed me to purchase the property 35 years ago. This, in light of the fact that the proposed sound wall that will apparently be something I'm forced to accept or at the very least have little recourse to prevent other than my sole vote to oppose it, will most likely, according to the real estate agents I've spoken with, have a substantially detrimental effect on my existing property value. While the proposed sound wall may be feasible it should not be considered reasonable, at least in its entirety. This section (85B) of the proposed wall is going to have little or no appreciable noise benefits for the majority of the homeowners voting on whether or not it should be built. Any noise reduction benefit as a result of constructing this portion of the proposed sound wall to the homes within a quarter of a mile, pales in comparison to the negative visual impact, both present and future. In reflection, this section of the barrier should truly be considered independently as it will put an undue burden, financial and aesthetic, on Loran Road homeowners, myself included.

- John Parsons
- Yes to barrier system

#### BARRIER SYSTEM C1 AND C2

- Concerned about wildlife trapped on Route 7 because of the wall. This area has been traditional route for deer/fox etc. to cross route 7. SAD! Can anything be done to protect the wildlife a little better?
- My property has temporary and permanent easements noted on the diagrams is any part of my property going to be purchased by the county?



- Considering the proximity of our property to Route 7 which is less than 80 feet, the traffic noise
  is a major problem with passing of every truck or heavy machine the whole house shakes this is causing
  major stress.
- Great idea since it will reduce noise and increase privacy for my home.
- Will the end of the barrier at Reston Parkway taper downwards or end abruptly at the height of the barrier?
- It's definitely needed!
- The design and the height of the wall does not look nice specifically from the look from inside of the community. As if it is a separation or isolation of some kind. A large concrete wall is not slightly at all.
- Glad to see the residential side will be high enough for sound not to be affecting our house.
   Thank you for caring.
- I live a few feet from the wall and very much want the wall.
- There is a walkway between 11266 and 11268 Stones throw drive I do not see an access to this through the sound barrier. Is this an oversight?
- Yes, it's very important and helpful
- The noise barrier system is a must to have the noise right now is so loud even causes vibrations inside the house.
- Thank you. We are adversely affected by the work that has been done and want the noise barrier.

#### BARRIER SYSTEM D2 AND E1-E4

- Please advice of vote count as soon as possible.
- It will be more than welcome.
- Will lighting be installed to deter the criminal element behind these walls? Previously, car headlights brightened the area, but after these walls are up, it will be very dark.



- Why is there no acceleration lane rom Amanda Drive to West Bound Route 7? There is one currently- well actually there was one prior to all the construction.
- You're asking us to vote on this proposed sound wall without addressing the following- 1 what is the final location of the wall in proximity to the finished roadway? 2 At what elevation does the wall start relative to the finished roadway heights.
- I Feel the wall will be way to high at 15ft! IT will be like being behind a prison wall! NO THANKS!
- We really need this noise barrier.
- PLEASE INSTALL A.S.A.P!!
- Strongly Vote Yes
- The wall as shown at our property is few feet further away from the road than the noise wall on the other side of Great Passage Blvd. My recommendation would be to take the same wall further in the same line as it is on the other side of Great Passage Blvd.
- Please build the noise wall to ensure full privacy and noise reduction for my property. If possible,
   increase the height to 22ft.
- Thanks
- Noise Barrier will help to lower noise to my house. Hope this project is successful. Good Luck!

#### • BARRIER SYSTEM F1, F1B, F1C, AND F2

• We are also concerned about the status of the trees behind the existing fence. We hope we can get them as they also provide noise abatement. Thank you for your efforts.

# Barrier System F3

- The Route 7 corridor improvement project is well planned and well processed we hope the noise reduction wall can also be well installed to function properly as expected i.e. to keep the noise level down and protect our health. Thank you again for the excellent execution of the project.
- Please construct noise wall
- The design looks good and think it will be very beneficial for our property when Rte. 7 is widened



- Our neighborhood is very helpful that a noise wall barrier will improve the quality of life, particularly for those whose property backs directly to route 7. Thank you for sending this survey.
- Given the increase in noise level and the impact that it will have on our property, we had put in a request for the noise barrier. During the public meetings that were held for Route 7 expansion we were told that there will be a noise barrier bordering our property to minimize noise impact. We sincerely hope there is no change in what was conveyed to us during the meetings.
- We definitely need the noise barrier; it is a must.
- Without the barrier our property has potential of losing significant market value.
- The bigger, longer, and thicker the better. It is already very noisy.
- We also concern about our driveway. We've been going to all meetings and still didn't get no answers. Where our mailbox going to be and how entrance be replaced.
- Absolutely needed and desired please!!

# • Barrier System G1-G6

- This is very need and welcomed addition. The noise levels can be unpleasurable.
- The noise wall is necessary!
- Also, the pedestrian tunnel from Colvin Run Park under 7 is not necessary and a waste of tax payer money.
- Thanks so much!
- Why is the decorative side facing traffic and not the property owners?
- The dogwood pattern on the noise barrier should be on the home owners side, since the homeowner has to look at the barrier forever!
- Better yet, put dogwood pattern on both sides of the barrier.
- Plant some trees to replace my trees.



- These barriers are good but ugly looking. In 2000, I spent \$4000 to plant these Cyprus trees for privacy and protection along side Route 7, which are now removed. My humble request is that some trees should be planted along side these barriers inside and outside to cover the barriers. I am 83 years old, limited income, I cannot afford any more trees to be planted. Thank you.
- Might be nice to plant some evergreen trees on property owners' side of wall.
- I feel the sound barrier is absolutely essential. I like the proposed placement near the road as this will abate excessive noise, I'm now hearing on my second floor. Please ensure that the construction of the wall leaves as many existing trees in place, undisturbed. This will not only improve appearance from home side but will also help abate noise coming over the wall.
- Noise Barrier is request due to the increased noise levels and removal of vegetation.
- I would like to see section G6 extend at least 250 more feet to the east of where it is shown to stop in your enclosed renderings. And I would prefer that the color of the noise walls to be a light grey instead of the reddish tint that seems to appear in your enclosed renderings. Thank you very much. If you cant extend it 250 more feet more to the east then could you please extend it at least 100 feet.
- We definitely need noise barriers without it, the area will become unhabitable.
- Probably, too high and will look ugly!
- Yes!
- My husband and I voluntarily manage our community cemetery known as Browns Chapel Cemetery #1 and #2. We are concerned about future parking and ingress egress of commercial lawn care equipment, excavators, vault trucks, hearses, and visitors' access to the cemetery at 10416 Leesburg Pike regarding a potential sound barrier. We have no Right turn lane on the north side of Leesburg Pike. Safety, access and parking are very important issues for us and for our future as a cemetery can someone either call or write me about this matter? Thank you!!
- May not need it in front of the church
- It would be nice if the residential side had the same work at the top as the roadway side since residents have to look at it every day.



# Barrier System G10-G13

- The bigger the barrier, the better.
- We surely want the noise barrier.
- My home will be unhabitable without the noise barrier system. My bedroom is on the route 7
   side and we will not be able to sleep. Please implement it as planned.
- Does the easement is used to back yard will be reestablished as original conditions and plants?
   Based on the studied made what are the current noise levels expected noise levels before and after the noise barrier at my location?
- Note to the design/build team: we have expressed verbally and provided written input at the community meetings that our first floor living area is 8-9 feet above ground level where the noise wall will start. Therefore, the taller 16-17 foot or taller 18ft noise abatement wall height will be necessary to abate noise for first level living at our parcel.

# Barrier System H2-H11

- We vote in favor of the noise barrier wall.
- We are a school with young children who would benefit from the sound and safety of a sound barrier.
- Thank you
- This is the worst idea I have heard since the Trumps wall.
- Waste of money, tax payer money.
- 16-foot wall for a total length of 3,941 feet is ridiculous.
- Simulated ashlar stone doesn't make it better.
- I'm shocked this is under consideration.
- The fact that it planned on 1 side of the road is absurd and pointless.
- Focus your resources on a project that makes sense.
- Jennifer thank you very much for sending us the potential noise barriers H2-H11 (considered for construction) Public input survey questionnaire. We are all grateful appreciated.



- Would you please let us know when this noise wall will be built?
- We all look forward to seeing the noise wall soon.
- Thank you very much again.
- Noise barrier system is essential and the taller it is better to reflect sound off the residences.
   Especially for properties located on elevated/ hill top alongside Route 7.

# Barrier System I2

• The noise barrier system is needed today and most definitely will be needed when route 7 is expanded to 3 lanes in each direction. Currently the noise from Route 7 is very loud when we are in our backyard and inside our house in addition at night time headlights from the cars on route 7 shine into our house and along with the noise is very disruptive. We look forward to the barrier!

# Barrier System I4-I6

- After barrier system is installed at the border of the property land. Please restore the damaged lawn grass near the barrier.
- We'd like the noise barrier implemented.
- How far down from the TM development is the noise barrier?
- The barrier is also important for safety.

# Barrier System J2-J3 and K1-K4

- We only object to the potential K1 section of the barrier. Our property line runs from the corner of Trap Road all the way to the property line of the house East of the Church. The house on the corner of Trap is the Minister's residence and is a part of our overall property. We would support the residents/property owners' decisions with regard to the J and Remaining K sections.
- Thank you all! You're awesome people!
- Please build noise barrier!
- Please go forward



- Thank you
- Completely, 100% want a noise barrier

### Barrier System N1-N3

- Can you please reconsider moving noise barrier "N1" to the same laine as "N2"? East bound traffic noise and the proposed location of "N2" is not optimal for Glenridge Properties. See attached recommended alternative to "N2" wall location, if possible. Thank you for your consideration.
- Because my neighborhood wants it.
- Thank you!
- Because me and my neighbors want it.
- The noise wall is needed there is significant noise already and additional lanes will certainly impact our houses. Please let me know if I can provide additional information.

# 7.2 INFORMATION FOR LOCAL GOVERNMENT OFFICIALS NOISE-COMPATIBLE LAND-USE PLANNING

Sections 12.1 and 12.2 of VDOT's current noise policy outline VDOT's approach to communication with local officials and provides information and resources on highway noise and noise-compatible land-use planning. VDOT's intention is to assist local officials in planning the uses of undeveloped land adjacent to highways to minimize the potential impacts of highway traffic noise.

"Entering the Quiet Zone" is a brochure that provides general information and examples to elected officials, planners, developers, and the general public about the problem of traffic noise and effective responses to it. A link to this brochure on FHWA's website is provided below: <a href="https://www.fhwa.dot.gov/environment/noise/noise\_compatible\_planning/federal\_approach/land\_use/index.cfm">https://www.fhwa.dot.gov/environment/noise/noise\_compatible\_planning/federal\_approach/land\_use/index.cfm</a>.

A wide variety of administrative strategies may be used to minimize or eliminate potential highway noise impacts, thereby preventing the need or desire for costly noise abatement structures such as noise barriers in future years. There are five broad categories of such strategies:



- Zoning,
- Other legal restrictions (subdivision control, building codes, health codes),
- Municipal ownership or control of the land,
- Financial incentives for compatible development, and
- Educational and advisory services.

"The Audible Landscape: A Manual for Highway and Land Use" is a well-written and comprehensive guide addressing these noise-compatible land-use planning strategies, with significant detailed information. This document is available through FHWA's Website at <a href="https://www.fhwa.dot.gov/environment/noise/noise">https://www.fhwa.dot.gov/environment/noise/noise</a> compatible planning/federal approach/audible landscape/index.cfm.

#### 7.3 NOISE IMPACT ZONES IN UNDEVELOPED LAND ALONG THE STUDY CORRIDOR

Also required under the revised 2011 FHWA and VDOT noise policies is information on the noise impact zones adjacent to project roadways in undeveloped lands. To determine these zones, noise levels are computed at various distances from the edge of the project roadways in each of the undeveloped areas of the project study area. Then, the distances from the edge of the roadway to the noise abatement criteria sound levels are determined through interpolation. Distances vary in the project corridor due to changes in traffic volumes, or terrain features. Any noise-sensitive sites within these zones should be considered noise impacted if no barrier is present to reduce sound levels.

Noise level contours are lines of equal noise exposure that typically parallel roadway alignments and are often times useful to local officials in undeveloped corridors. Highway traffic noise is considered a linear noise source and sound levels can drop considerably over distance. The degree that sound levels decrease can vary based on a number of different factors including objects that shield the roadway noise, terrain features and ground cover type (e.g., pavement, grass or snow). The use of noise level contours has become increasingly popular over the last several years, as they have been implemented in planning programs for undeveloped areas with roadway noise influence. Through conscious planning efforts and noise contour generation, municipal officials can restrict future development inside the noise impact zone (i.e., the area within the 66-dBA noise contour). **Figure 2** shows the approximate 66-dBA noise level contours for the study area when considering the proposed improvements and the Design Year (2040)



traffic volumes, speeds and composition. This 66-dBA noise contour can be used to approximate the distance away from Route 7 in which the NAC will be exceeded for an Activity Category B receptor (e.g., the most common receptor).

#### 7.4 **VDOT'S NOISE ABATEMENT PROGRAM**

Information on VDOT's noise abatement program is available on VDOT's Website at http://www.virginiadot.org/projects/pr-noise-walls-about.asp. The site provides information on VDOT's noise program and policies, noise barriers, and a downloadable noise barrier brochure.

Route 7 Widening: Reston Avenue to Jarrett Valley Drive State Project 0007-029-942, 0007-029-225

- 70 -Federal Project No.: STP-5A01(745) and STP-5A01(790)



#### 8.0 CONSTRUCTION NOISE

Throughout the construction of Route 7 project, noise-sensitive land uses that are analyzed for traffic noise impacts are also susceptible to construction noise impacts. Typical highway construction/reconstruction equipment such as loaders, dump trucks, graders, bulldozers, etc. is likely to temporarily elevate noise within the project area. Sensitive receptors within 100 to 200 feet of construction activities may experience varying periods and degrees of noise impacts, with potential noise levels between 75 dBA and 85 dBA, depending on the nature of the construction activity, the type of equipment in use, and the relative nearness to the activity.

VDOT is concerned with noise generated during the construction phase of the proposed project. While the degree of construction noise impact will vary, it is directly related to the types and number of equipment used and the proximity to the noise-sensitive land uses within the project area. Land uses that are sensitive to traffic noise, are also potentially considered to be sensitive to construction noise. Any construction noise impacts that do occur as a result of roadway construction measures are anticipated to be temporary in nature and will cease upon completion of the project construction phase. A method of controlling construction noise is to establish the maximum level of noise that construction operations can generate. In view of this, VDOT has developed and FHWA has approved a specification that establishes construction noise limits. This specification can be found in VDOT's 2016 Road and Bridge Specifications, Section 107.16(b.3), "Noise." The contractor will be required to conform to this specification to reduce the impact of construction noise on the surrounding community.

Construction noise can be minimized by implementing specific measures to help mitigate the noise at the source. The contractor shall exercise proper maintenance procedures for all construction equipment regularly and thoroughly. Replacement of failing or ineffective muffling and exhaust systems, periodic lubrication of moving parts, and properly tuned engines are necessary in order to keep construction equipment noise emissions to a minimum.

The following construction noise related items are included in VDOT's 2016 Road and Bridge Specifications:

• The Contractor's operations shall be performed so that exterior noise levels measured during a noise-sensitive activity shall not exceed 80 decibels. Such noise level measurements shall be taken at a point on the perimeter of the construction limit that is closest to the adjoining property on which a noise-sensitive activity is occurring. A noise-sensitive activity is any activity for which lowered noise levels are essential if the activity is to serve its

ROUTE 7 CORRIDOR IMPROVEMENTS

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intended purpose and not present an unreasonable public nuisance. Such activities include, but are not limited to, those associated with residences, hospitals, nursing homes, churches, schools, libraries, parks, and recreational areas.

- The Department may monitor construction-related noise. If construction noise levels exceed 80 decibels during noise-sensitive activities, the Contractor shall take corrective action before proceeding with operations. The Contractor shall be responsible for costs associated with the abatement of construction noise and the delay of operations attributable to noncompliance with these requirements.
- The Department may prohibit or restrict to certain portions of the project any work that produces objectionable noise between 10 P.M. and 6 A.M. If other hours are established by local ordinance, the local ordinance shall govern.
- Equipment shall in no way be altered so as to result in noise levels that are greater than those produced by the original equipment.
- When feasible, the Contractor shall establish haul routes that direct his vehicles away from developed areas and ensure that noise from hauling operations is kept to a minimum.
- These requirements shall not be applicable if the noise produced by sources other than the Contractor's operation at the point of reception is greater than the noise from the Contractor's operation at the same point.



#### 9.0 LIST OF PREPARERS AND REVIEWERS

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#### 10.0 REFERENCES

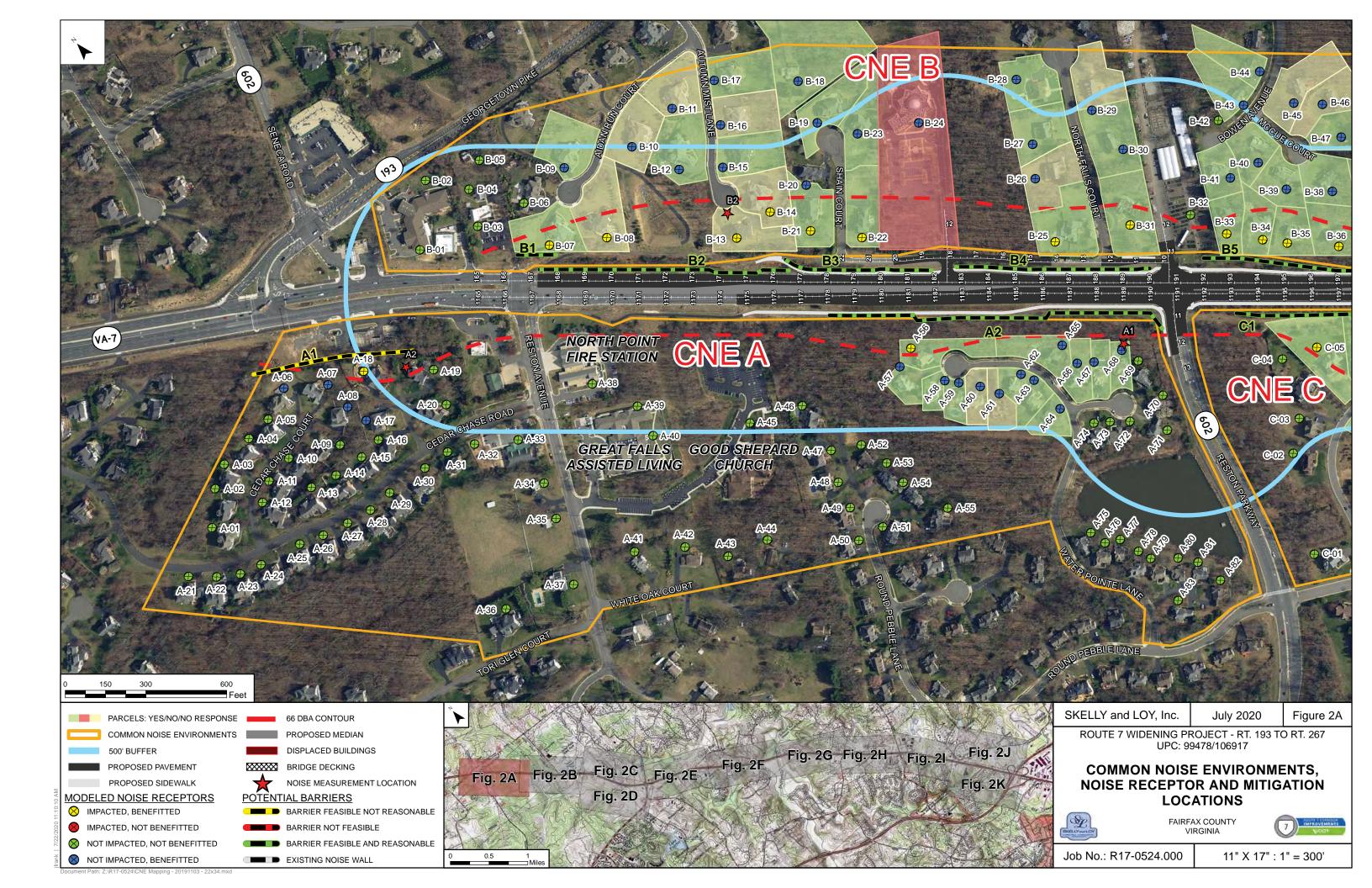
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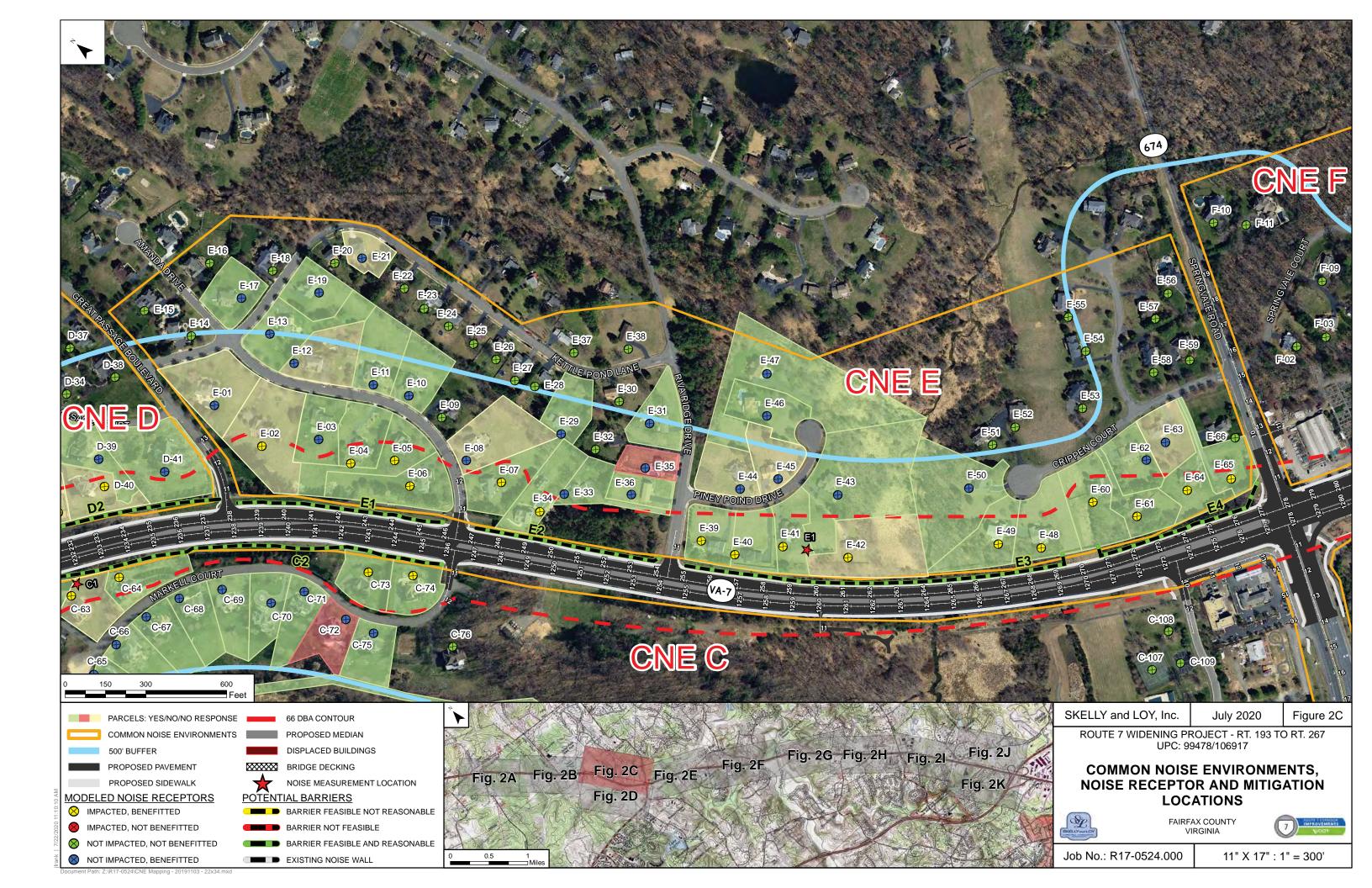
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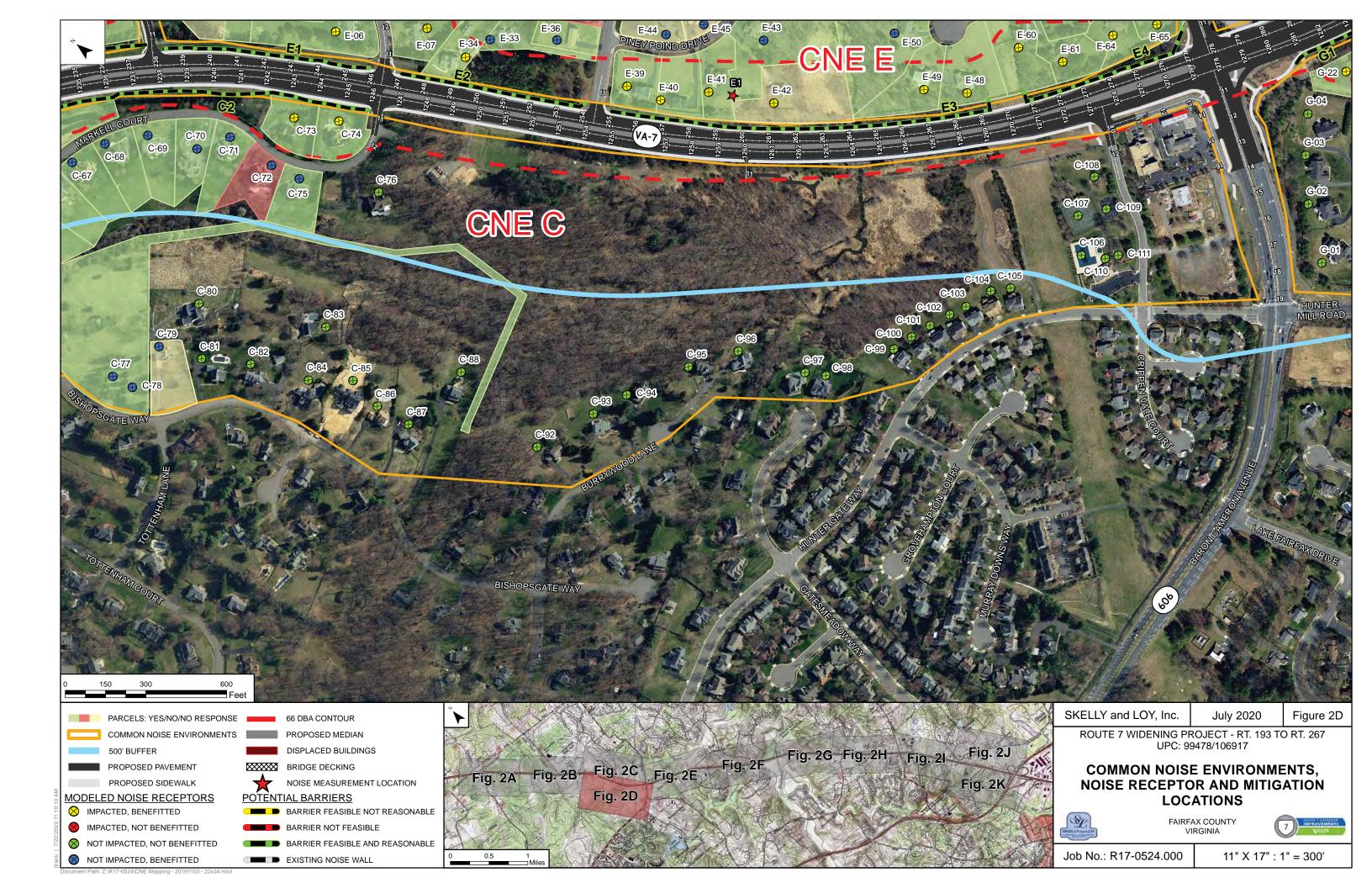


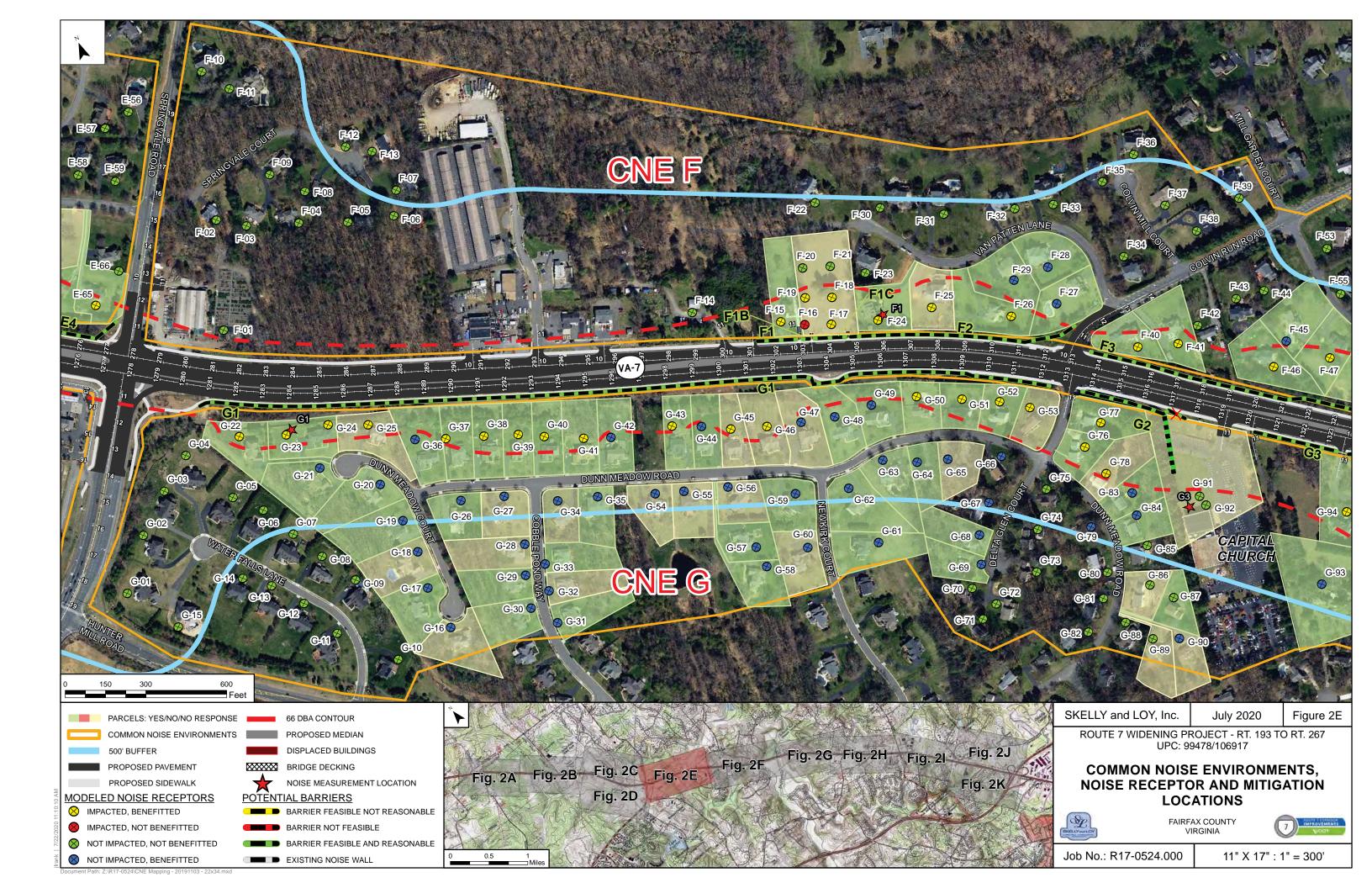
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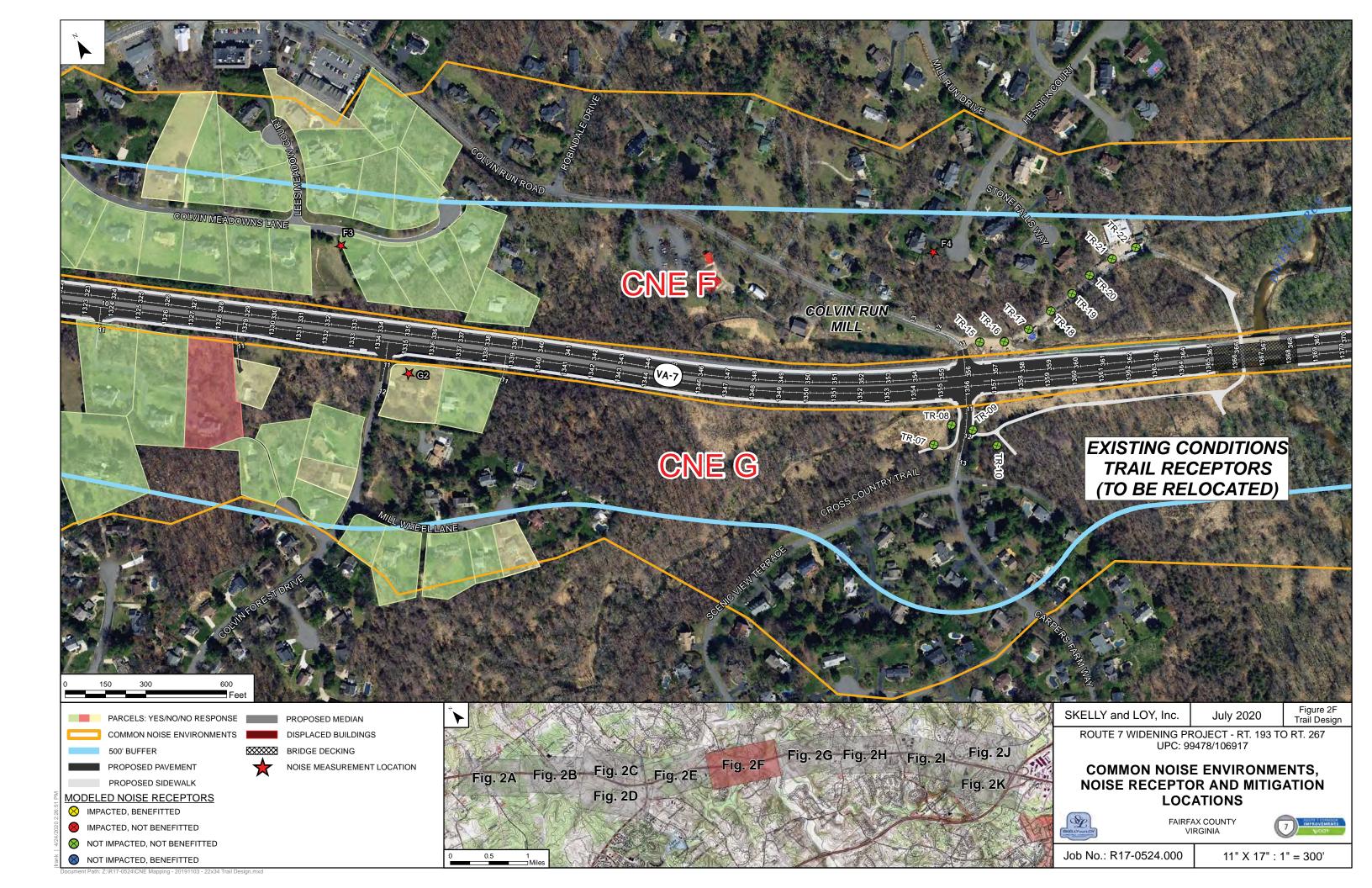


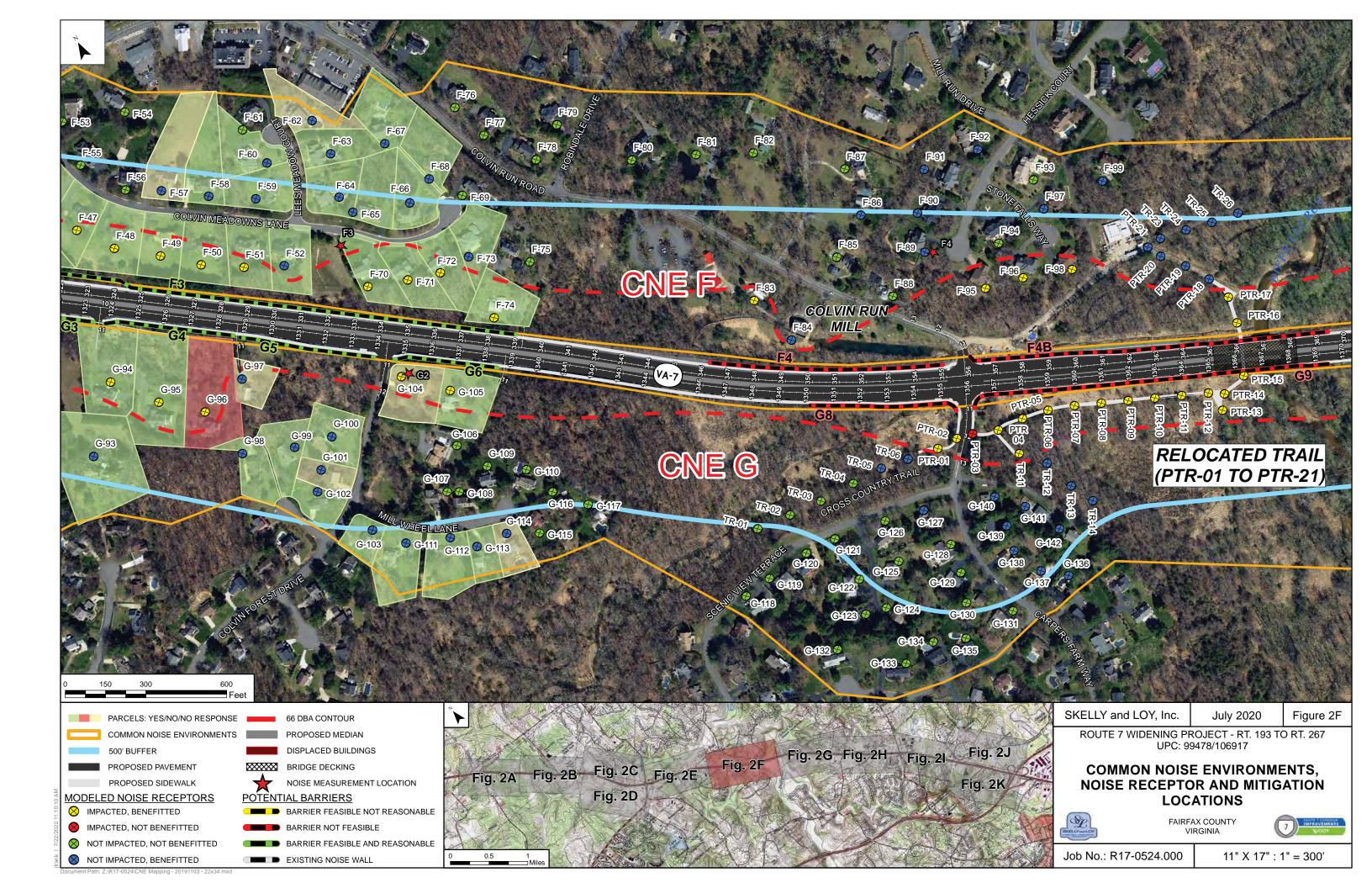


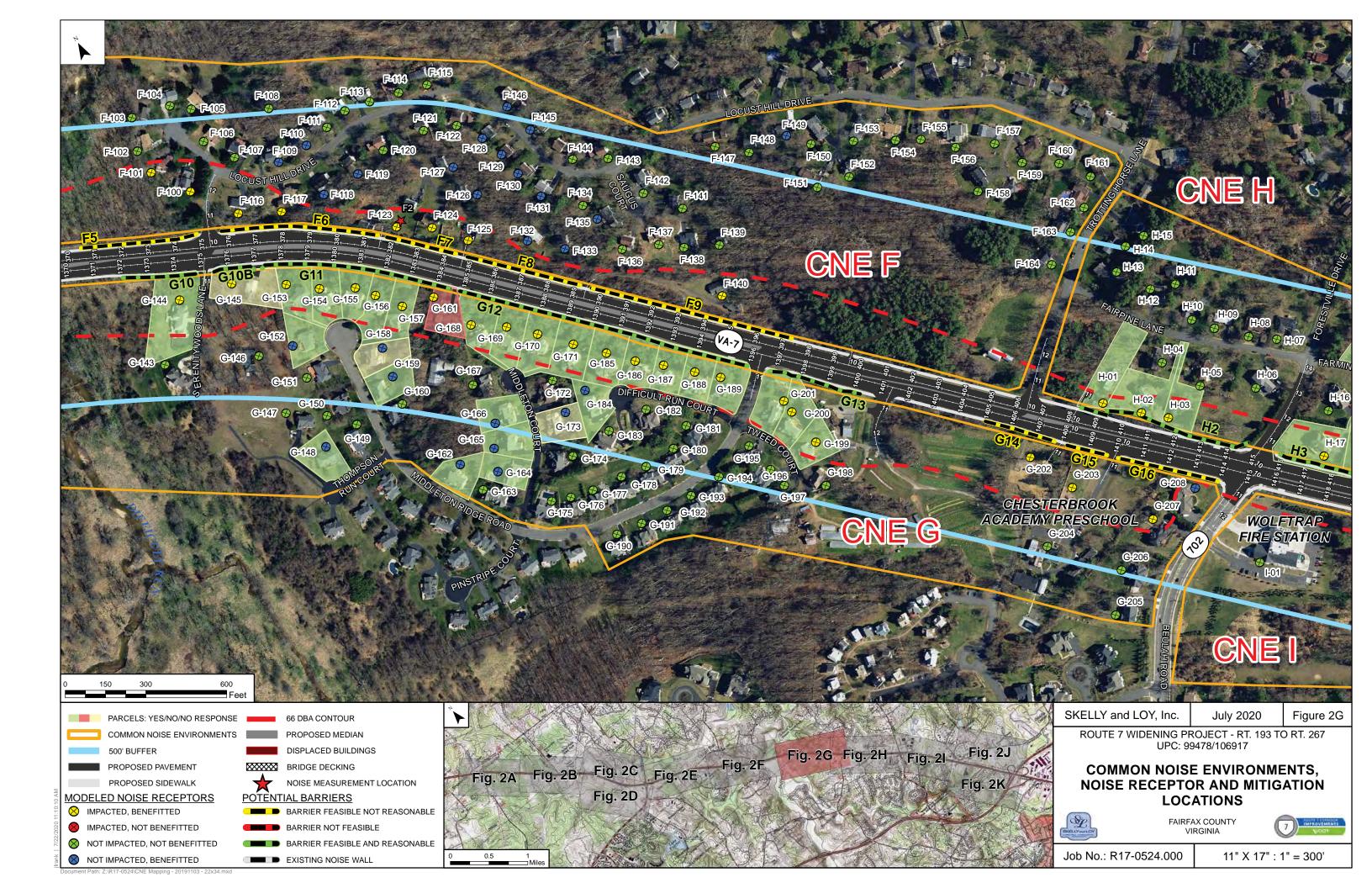


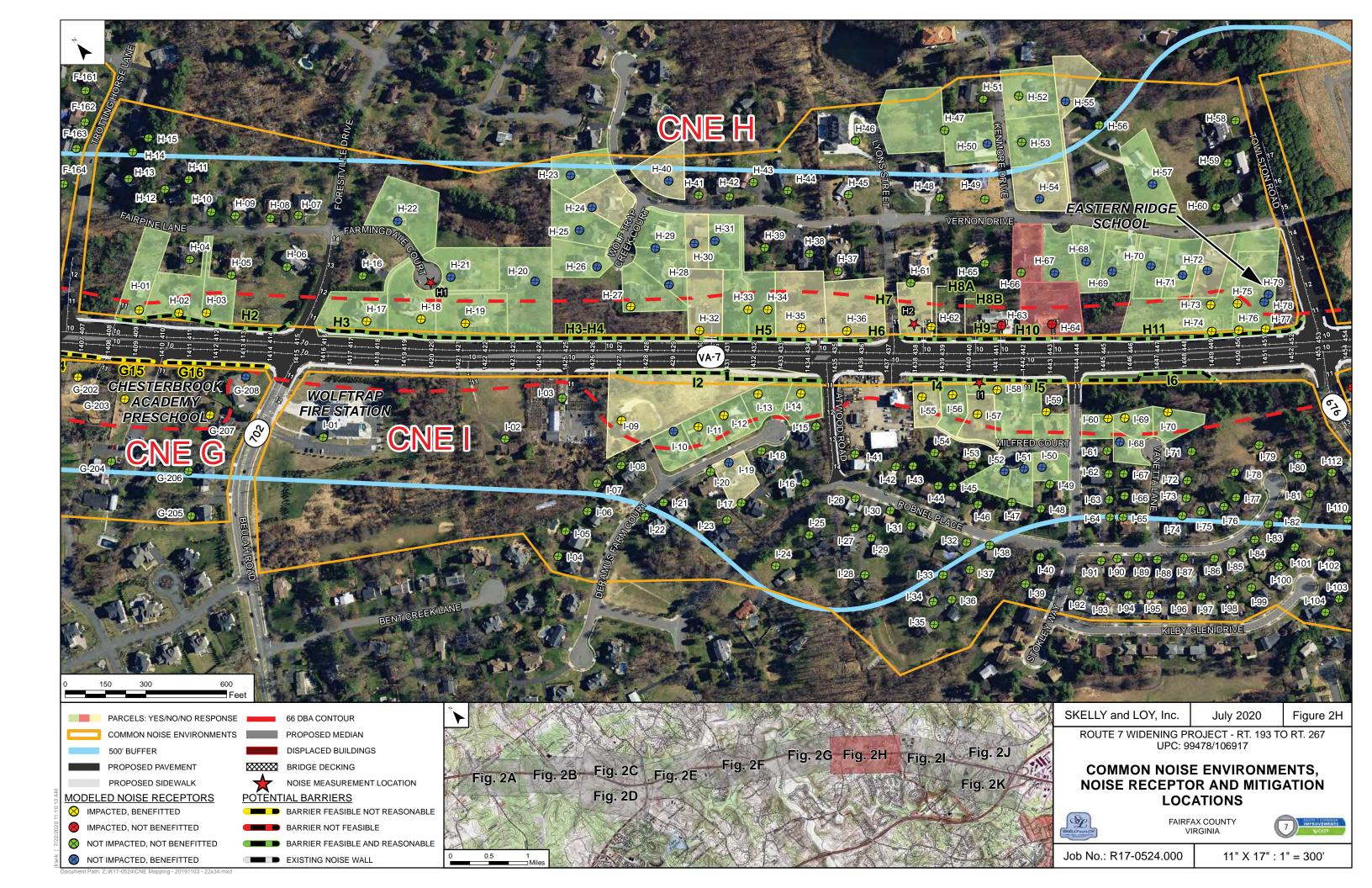


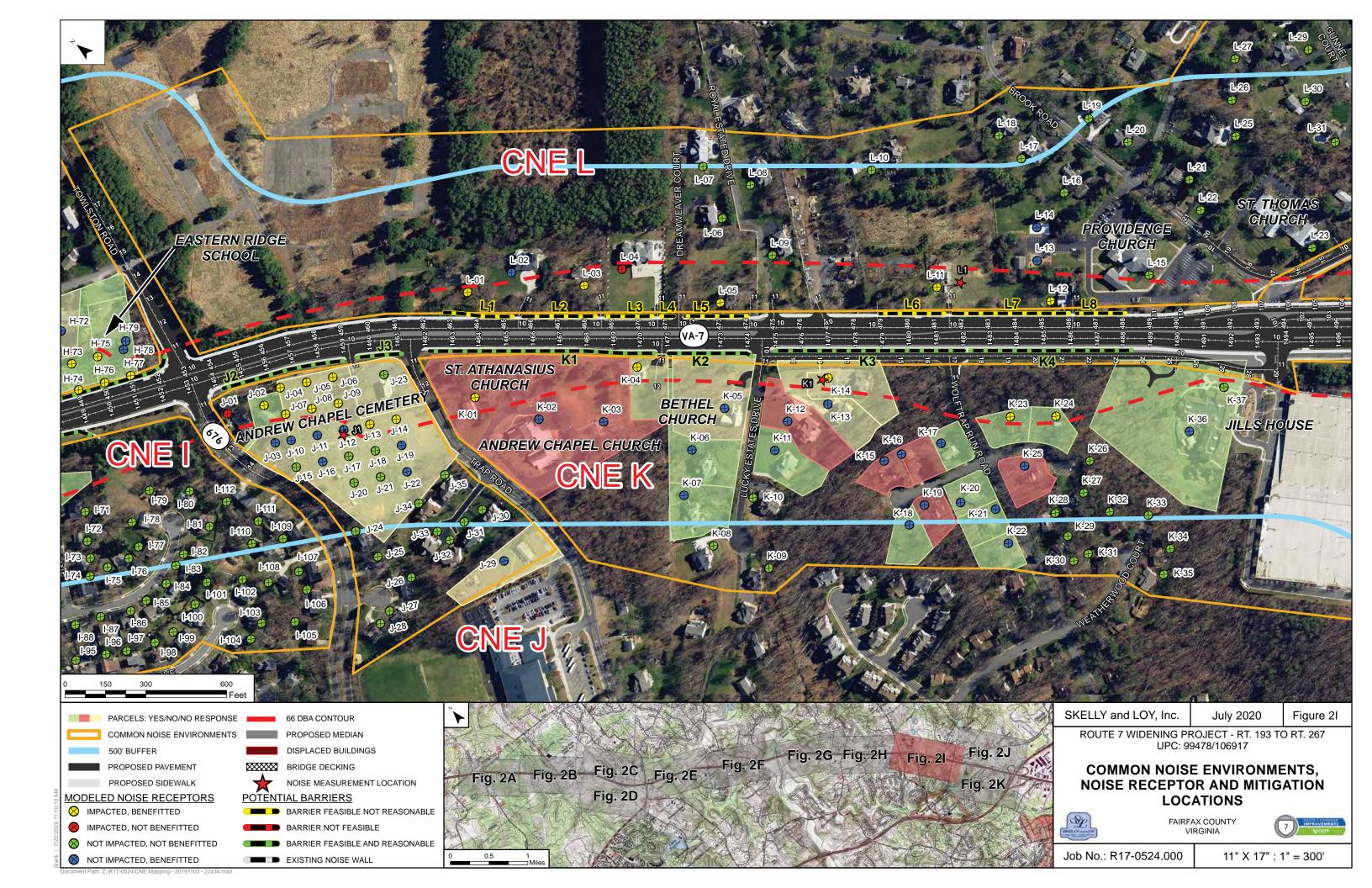


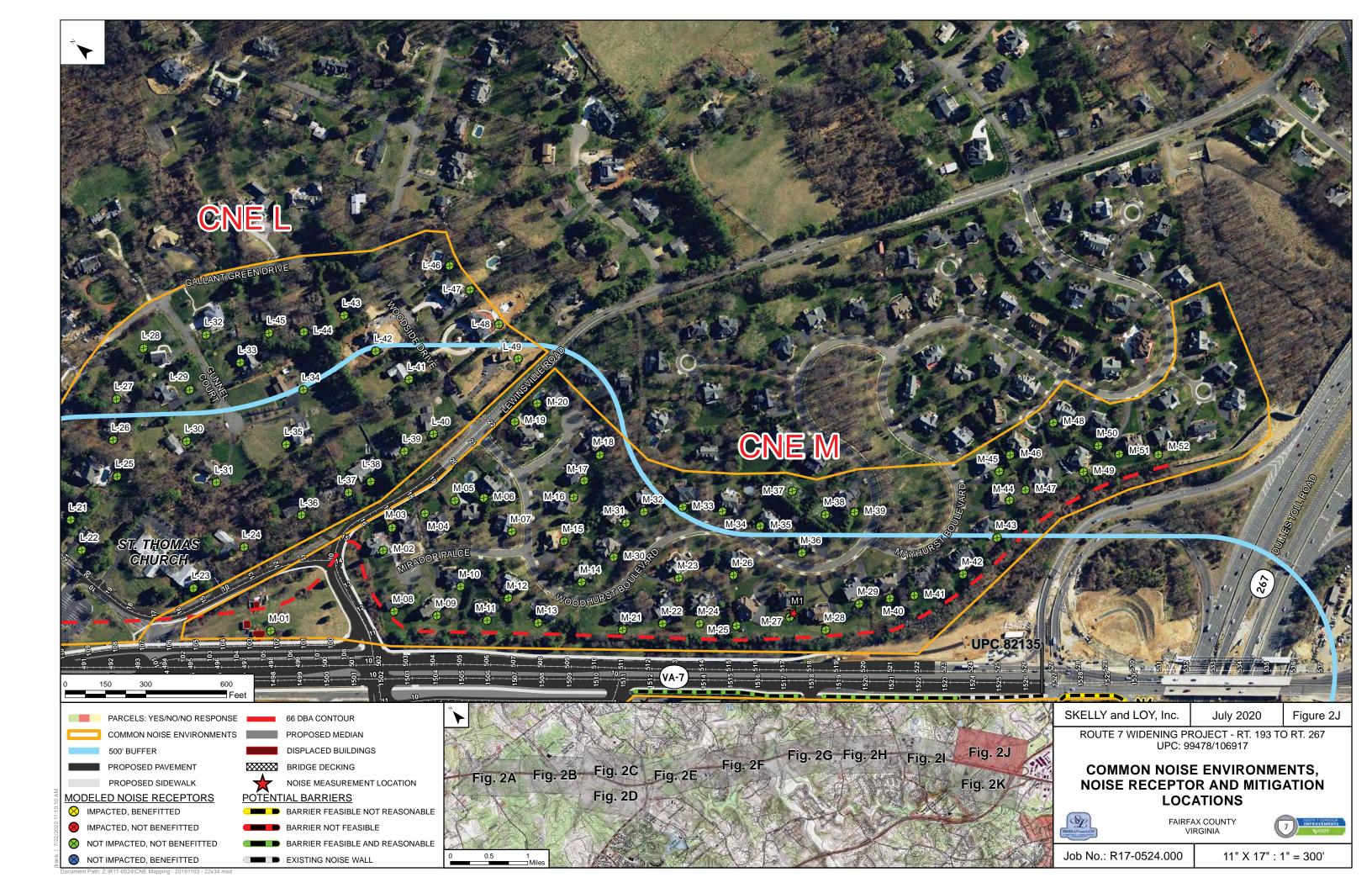


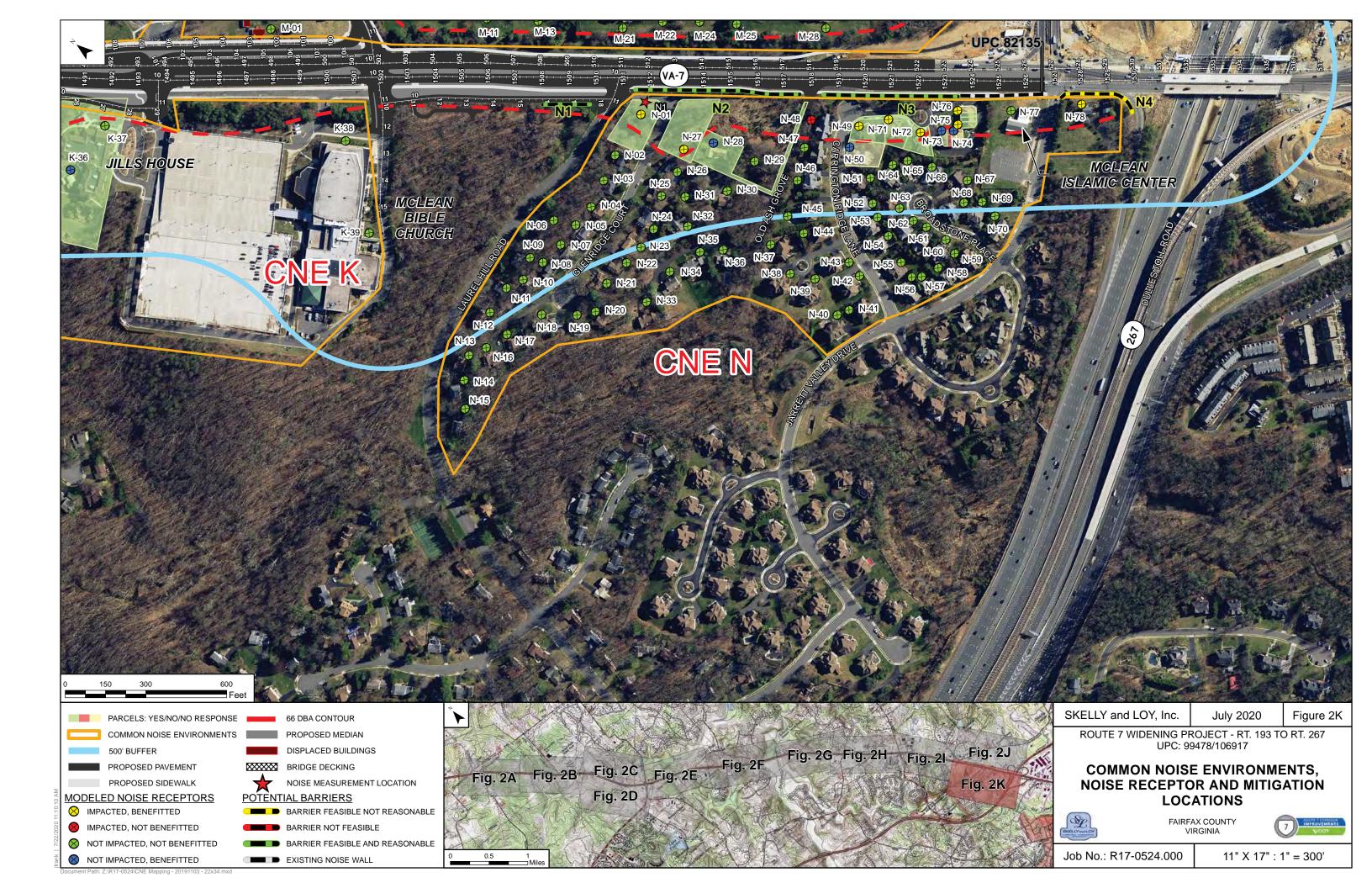












**DATA TABLES** 

		ROUTE 7 EXIS	TABLE 7		EVELS			
CNE	Receptor ID	Address	# of Dwelling Units	Activity Category	Land Use	NAC	Levels (Le	nour Noise q(h) in dBA)
							2018 Existing	2040 Build
	A-01	1080 CEDAR CHASE CT	1	В	Residence	66	50	52
	A-02	1076 CEDAR CHASE CT	1	В	Residence	66	53	55
	A-03	1076 CEDAR CHASE CT	1	В	Residence	66	55	57
	A-04 A-05	1074 CEDAR CHASE CT 1072 CEDAR CHASE CT	1 1	B B	Residence Residence	66 66	61 58	61
	A-06	1070 CEDAR CHASE CT	1	В	Residence	66	62	65
	A-07	1068 CEDAR CHASE CT	1	В	Residence	66	62	63
	A-08	1069 CEDAR CHASE CT	1	В	Residence	66	58	59
	A-09	1071 CEDAR CHASE CT	1	В	Residence	66	53	54
	A-10	1073 CEDAR CHASE CT	1	В	Residence	66	52	56
	A-11	1075 CEDAR CHASE CT	1	В	Residence	66	51	54
	A-12 A-13	11596 CEDAR CHASE RD 11594 CEDAR CHASE RD	1 1	B B	Residence Residence	66 66	50 52	53 53
	A-13 A-14	11592 CEDAR CHASE RD	1	В	Residence	66	53	54
	A-15	11590 CEDAR CHASE RD	1 1	В	Residence	66	54	55
	A-16	11588 CEDAR CHASE RD	1	В	Residence	66	55	56
	A-17	11586 CEDAR CHASE RD	1	В	Residence	66	58	59
	A-18	11584 CEDAR CHASE RD	1	В	Residence	66	66	67
	A-19	11582 CEDAR CHASE RD	1	В	Residence	66	64	65
	A-20	11580 CEDAR CHASE RD	1	В	Residence	66	59	59
	A-21 A-22	11605 CEDAR CHASE RD 11603 CEDAR CHASE RD	1 1	B B	Residence Residence	66 66	49 48	50 50
	A-23	11601 CEDAR CHASE RD	1	В	Residence	66	47	49
	A-24	11599 CEDAR CHASE RD	1	В	Residence	66	47	49
	A-25	11597 CEDAR CHASE RD	1	В	Residence	66	46	48
	A-26	11595 CEDAR CHASE RD	1	В	Residence	66	46	48
	A-27	11593 CEDAR CHASE RD	1	В	Residence	66	47	48
	A-28	11591 CEDAR CHASE RD	1	В	Residence	66	48	50
	A-29	11589 CEDAR CHASE RD	1 1	В	Residence	66	50	51
	A-30 A-31	11585 CEDAR CHASE RD 11585 CEDAR CHASE RD	1	B B	Residence Residence	66 66	52 54	53 56
	A-32	11579 CEDAR CHASE RD	1	С	Playground	66	55	56
	A-33	11579 CEDAR CHASE RD	1	D	School	51	56 (31)	57 (32)
	A-34	1126 RESTON AVE	1	В	Residence	66	52	54
	A-35	1132 RESTON AVE	1	В	Residence	66	51	53
	A-36	11602 TORI GLEN CT	1	В	Residence	66	41	43
	A-37	1138 RESTON AVE	1	В	Residence	66	48	49
	A-38 A-39	1117 RESTON AVE 1121 RESTON AVE	1 1	C	Picnic Area Outdoor Area	66 66	55 59	56 61
	A-40	1121 RESTON AVE	1	C	Patio	66	56	58
l ∢	A-41	11500 WHITE OAK CT	1	В	Residence	66	50	51
CNE	A-42	11498 WHITE OAK CT	1	В	Residence	66	49	51
ᅙ	A-43	11496 WHITE OAK CT	1	В	Residence	66	48	50
	A-44	11494 WHITE OAK CT	1	В	Residence	66	47	50
	A-45	1133 RESTON AVE	1	D	Church	51	57 (32)	58 (33)
	A-46 A-47	1104 ROUND PEBBLE LN 1106 ROUND PEBBLE LN	1 1	B B	Residence Residence	66 66	56 52	58 54
	A-47 A-48	1108 ROUND PEBBLE LN	1	В	Residence	66	50	52
	A-49	1110 ROUND PEBBLE LN	1	В	Residence	66	49	51
	A-50	1112 ROUND PEBBLE LN	1	В	Residence	66	48	50
	A-51	1111 ROUND PEBBLE LN	1	В	Residence	66	47	49
	A-52	1102 ROUND PEBBLE LN	1	В	Residence	66	50	52
	A-53	1100 ROUND PEBBLE LN	1	В	Residence	66	48	50
	A-54 A-55	1100 ROUND PEBBLE LN 1109 ROUND PEBBLE LN	1 1	B B	Residence Residence	66 66	48 46	50 48
	A-55 A-56	1101 WATER POINTE LN	1	В	Residence	66	63	66
	A-57	1100 WATER POINTE LN	1	В	Residence	66	59	61
	A-58	1104 WATER POINTE LN	1	В	Residence	66	57	60
	A-59	1104 WATER POINTE LN	1	В	Residence	66	57	61
	A-60	1106 WATER POINTE LN	1	В	Residence	66	58	61
	A-61	1108 WATER POINTE LN	1	В	Residence	66	55	59
	A-62	1110 WATER POINTE LN	1	В	Residence	66	59	63
	A-63 A-64	1110 WATER POINTE LN 1114 WATER POINTE LN	1 1	B B	Residence Residence	66 66	57 55	60 57
	A-65	1109 WATER POINTE LN	1	В	Residence	66	63	65
	A-66	1113 WATER POINTE LN	1	В	Residence	66	61	63

		ROUTE 7 EXIS	TABLE 7		EVELS			
CNE	Receptor ID	Address	# of Dwelling Units	Activity Category	Land Use	NAC		nour Noise q(h) in dBA)
O			Units			2	2018 Existing	2040 Build
	A-67	11306 WATER POINTE CIR	1	В	Residence	66	61	63
	A-68	11304 WATER POINTE CIR	1	В	Residence	66	61	63
	A-69	11300 WATER POINTE CIR	1	В	Residence	66	60	62
	A-70	11301 WATER POINTE CIR	1	В	Residence	66	61	65
	A-71	11303 WATER POINTE CIR	1	В	Residence	66	59	63
	A-72	11305 WATER POINTE CIR 11307 WATER POINTE CIR	1 1	B B	Residence Residence	66 66	54 53	56 56
	A-73 A-74	11307 WATER POINTE CIR	1	В	Residence	66	53	56
	A-74 A-75	1141 WATER POINTE LN	1	В	Residence	66	50	53
	A-76	1143 WATER POINTE LN	1	В	Residence	66	50	53
	A-77	1145 WATER POINTE LN	1	В	Residence	66	51	54
	A-78	1147 WATER POINTE LN	1	В	Residence	66	51	54
	A-79	1149 WATER POINTE LN	1	В	Residence	66	52	55
	A-80	1151 WATER POINTE LN	1	В	Residence	66	52	55
	A-81	1153 WATER POINTE LN	1	В	Residence	66	53	55
	A-82	1155 WATER POINTE LN	1	В	Residence	66	53	56
	A-83	1157 WATER POINTE LN	1	В	Residence	66	51	54
	B-01	11415 GEORGETOWN PIKE	1	D	Animal Hospital	51	69 (44)	71 (46)
	B-02	11415 GEORGETOWN PIKE	1	С	Dog Park	66	51	52
	B-03	11500 LEESBURG PIKE	1	D	Church	51	63 (38)	67 (42)
	B-04	11502 LEESBURG PIKE	1	В	Residence	66	58	61
	B-05 B-06	11411 GEORGETOWN PIKE 11448 AIDAN RUN CT	1 1	B B	Residence	66 66	55 61	57 63
	B-06 B-07	11448 AIDAN RUN CT	1 1	В	Residence Residence	66	71	73
	B-08	11445 AIDAN RUN CT	1	В	Residence	66	70	72
	B-09	11444 AIDAN RUN CT	1	В	Residence	66	54	56
	B-10	11441 AIDAN RUN CT	1	В	Residence	66	55	57
	B-11	1056 AUTUMN MIST LN	1	В	Residence	66	52	55
	B-12	1058 AUTUMN MIST LN	1	В	Residence	66	58	61
	B-13	1063 AUTUMN MIST LN	1	В	Residence	66	70	72
	B-14	1061 Autumn Mist Ln	1	В	Residence	66	63	66
	B-15	1059 AUTUMN MIST LN	1	В	Residence	66	57	60
	B-16	1057 AUTUMN MIST LN	1	В	Residence	66	53	56
	B-17	1055 AUTUMN MIST LN	1	В	Residence	66	51	54
	B-18	11309 GEORGETOWN PIKE	1	В	Residence	66	49	52
	B-19	1070 SHAIN CT	1	В	Residence	66	54	57
	B-20	1076 SHAIN CT	1 1	B B	Residence	66 66	59	62
	B-21 B-22	1076 SHAIN CT 1075 SHAIN CT	1	В	Residence Residence	66	66 68	69 70
	B-23	1073 SHAIN CT	1	В	Residence	66	54	57
	B-24	11326 LEESBURG PIKE	1	D	School	51	51 (26)	57 (32)
	B-25	1066 NORTHFALLS CT	1	В	Residence	66	67	67
	B-26	1062 NORTHFALLS CT	1	В	Residence	66	57	62
	B-27	1058 NORTHFALLS CT	1	В	Residence	66	55	60
	B-28	1054 NORTHFALLS CT	1	В	Residence	66	50	55
	B-29	1061 NORTHFALLS CT	1	В	Residence	66	53	57
	B-30	1061 NORTHFALLS CT	1	В	Residence	66	55	58
	B-31	1065 NORTHFALLS CT	1	В	Residence	66	64	67
	B-32	11254 LEESBURG PIKE	1	E	Nursery	71	62	65
	B-33	11133 BOWEN AVE	1	В	Residence	66	68	70
	B-34	11131 BOWEN AVE	1	В	Residence	66	67	70
ш	B-35 B-36	1094 MCCUE CT 1096 MCCUE CT	1 1	B B	Residence Residence	66 66	68 70	71 72
CNE	B-36 B-37	1095 MCCUE CT	1	В	Residence	66	63	64
O	B-38	1098 MCCUE CT	1	В	Residence	66	61	63
	B-39	1092 MCCUE CT	1	В	Residence	66	60	62
	B-40	11129 BOWEN AVE	1	В	Residence	66	57	60
	B-41	11135 BOWEN AVE	1	В	Residence	66	59	62
	B-42	11134 BOWEN AVE	1	В	Residence	66	52	54
	B-43	11128 BOWEN AVE	1	В	Residence	66	51	54
	B-44	11126 BOWEN AVE	1	В	Residence	66	51	52
	B-45	11127 BOWEN AVE	1	В	Residence	66	51	54
	B-46	1091 MCCUE CT	1	В	Residence	66	51	53
	B-47	1093 MCCUE CT	1	В	Residence	66	52	55
	B-48	1090 LORAN CT	1	В	Residence	66	53	56
	B-49	1092 LORAN CT	1	В	Residence	66	51	54

1	TABLE 7 ROUTE 7 EXISTING AND FUTURE PREDICTED NOISE LEVELS								
CNE	Receptor ID	Address	# of Dwelling Units	Activity Category	Land Use	NAC	Levels (Le	hour Noise q(h) in dBA)	
							2018 Existing	2040 Build	
	B-50	1094 LORAN CT	1	В	Residence	66	57	59	
	B-51	1096 LORAN CT	1	В	Residence	66	57	59	
	B-52	1098 LORAN CT	1	В	Residence	66	56	58	
	B-53 B-54	11104 LORAN RD 11106 LORAN RD	1 1	B B	Residence	66	59 62	61	
	B-54 B-55	11108 LORAN RD	1 1	В	Residence Residence	66 66	69	71	
	B-56	11110 LORAN RD	1	В	Residence	66	66	68	
	B-57	11112 LORAN RD	1	В	Residence	66	67	71	
	B-58	11111 LORAN RD	1	В	Residence	66	54	57	
	B-59	11113 LORAN RD	1	В	Residence	66	59	62	
	B-60	11115 LORAN RD	1	В	Residence	66	62	65	
	B-61	11117 LORAN RD	1	В	Residence	66	64	67	
	B-62	11119 LORAN RD	1	В	Residence	66	68	71	
	B-63	1124 UTTERBACK STORE RD	1 1	В	Residence	66	61	65	
	B-64	1116 UTTERBACK STORE RD	1 1	B B	Residence	66	56 53	61	
	B-65 B-66	1112 UTTERBACK STORE RD 1108 UTTERBACK STORE RD	1 1	B R	Residence Residence	66 66	53	57 57	
	B-67	1104 UTTERBACK STORE RD	1 1	В	Residence	66	53	57	
	B-68	1100 UTTERBACK STORE RD	1	В	Residence	66	54	57	
	B-69	11101 LORAN RD	1	В	Residence	66	54	57	
	B-70	1097 LORAN CT	1	В	Residence	66	50	54	
	B-71	1093 LORAN CT	1	В	Residence	66	51	54	
	B-72	1088 UTTERBACK STORE RD	1	В	Residence	66	51	54	
	C-01	11300 STONES THROW DR	1	В	Residence	66	54	57	
	C-02	11296 STONES THROW DR	1	В	Residence	66	55	58	
	C-03	11294 STONES THROW DR	1	В	Residence	66	56	60	
	C-04	11292 STONES THROW DR 11290 STONES THROW DR	1 1	B B	Residence	66	62	64	
	C-05 C-06	11288 STONES THROW DR	1 1	В	Residence Residence	66 66	63 64	66 67	
	C-07	11286 STONES THROW DR	1	В	Residence	66	67	69	
	C-08	11284 STONES THROW DR	1 1	В	Residence	66	68	70	
	C-09	11285 STONES THROW DR	1	В	Residence	66	60	62	
	C-10	11287 STONES THROW DR	1	В	Residence	66	58	61	
	C-11	11289 STONES THROW DR	1	В	Residence	66	53	57	
	C-12	1149 FIELDVIEW DR	1	В	Residence	66	49	52	
	C-13	1151 FIELDVIEW DR	1	В	Residence	66	48	52	
	C-14	1153 FIELDVIEW DR	1	В	Residence	66	50	54	
	C-15	1155 FIELDVIEW DR	1	В	Residence	66	51	55	
	C-16	11270 STONES THROW DR	1 1	B B	Residence	66	72	73 72	
	C-17 C-18	11268 STONES THROW DR 11266 STONES THROW DR	1	В	Residence Residence	66 66	69 63	68	
	C-19	11264 STONES THROW DR	1	В	Residence	66	60	65	
	C-20	11262 STONES THROW DR	1	В	Residence	66	57	62	
	C-21	11260 STONES THROW DR	1	В	Residence	66	56	60	
	C-22	11258 STONES THROW DR	1	В	Residence	66	52	56	
	C-23	11256 STONES THROW DR	1	В	Residence	66	48	52	
	C-24	11263 STONES THROW DR	1	В	Residence	66	54	57	
	C-25	11261 STONES THROW DR	1	В	Residence	66	53	56	
	C-26	11259 STONES THROW DR	1	В	Residence	66	51	54	
	C-27	11255 STONES THROW DR	1 1	В	Residence	66	49	52	
	C-28	11257 Stones Throw Dr	1	В	Residence	66	45	48	
	C-29 C-30	11225 BRIGHT POND LN 11217 BRIGHT POND LN	1 1	В В	Residence Residence	66 66	46 46	49 49	
	C-30	11217 BRIGHT POND LN 11211 BRIGHT POND LN	1 1	В	Residence	66	46	49	
	C-32	11205 BRIGHT POND LN	1	В	Residence	66	47	50	
	C-33	11200 BRIGHT POND LN	1	В	Residence	66	49	52	
	C-34	1144 MEADOWLOOK CT	1	В	Residence	66	49	52	
	C-35	1140 MEADOWLOOK CT	1	В	Residence	66	55	58	
	C-36	1141 MEADOWLOOK CT	1	В	Residence	66	61	66	
	C-37	1143 MEADOWLOOK CT	1	В	Residence	66	68	70	
	C-38	1152 MEADOWLOOK CT	1	В	Residence	66	59	61	
	C-39	1158 MEADOWLOOK CT	1	В	Residence	66	55	57	
	C-40	1162 MEADOWLOOK CT	1	В	Residence	66	50	52	
	C-41	1147 MEADOWLOOK CT	1 1	В	Residence	66	71	72	
1	C-42 C-43	1151 MEADOWLOOK CT 1159 MEADOWLOOK CT	1 1	B B	Residence Residence	66 66	68 63	69 65	

		ROUTE 7 EXISTIN	TABLE 7	REDICTED NOISE LE	EVELS			
CNE	Receptor ID	Address	# of Dwelling Units	Activity Category	Land Use	NAC	Levels (Le	nour Noise q(h) in dBA)
							2018 Existing	2040 Build
	C-44	1163 MEADOWLOOK CT	1	В	Residence	66	59	61
	C-45	11116 TOMMYE LN	1	В	Residence	66	60	61
	C-46	11133 TOMMYE LN	1	В	Residence	66	48	50
	C-47 C-48	11129 TOMMYE LN 11125 TOMMYE LN	1	B B	Residence Residence	66 66	45 45	48 48
	C-49	11121 TOMMYE LN	1	В	Residence	66	51	52
	C-50	11117 TOMMYE LN	1	В	Residence	66	52	53
	C-51	11113 TOMMYE LN	1	В	Residence	66	53	55
	C-52	11109 TOMMYE LN	1	В	Residence	66	52	53
١	C-53 C-54	1155 MEADOWLOOK CT 11108 TOMMYE LN	1	B B	Residence	66 66	70 69	71 70
U U	C-54 C-55	11110 TOMMYE LN	1	В	Residence Residence	66	61	61
CNE	C-56	11106 TOMMYE LN	1	В	Residence	66	68	69
	C-57	11102 TOMMYE LN	1	В	Residence	66	61	62
	C-58	11104 TOMMYE LN	1	В	Residence	66	68	69
	C-58B	0	1	В	Residence	66	66	67
	C-59 C-60	1192 BISHOPSGATE WAY 11100 TOMMYE LN	1 1	B B	Residence Residence	66 66	63 57	64 58
	C-60 C-61	1153 MARKELL CT	1	В	Residence	66	71	72
	C-62	1151 MARKELL CT	1	В	Residence	66	56	57
	C-63	1155 MARKELL CT	1	В	Residence	66	65	66
	C-64	1157 MARKELL CT	1	В	Residence	66	68	70
	C-65	1150 MARKELL CT	1	В	Residence	66	55	56
	C-66	1152 MARKELL CT	1	B B	Residence	66	55	57
	C-67 C-68	1154 MARKELL CT 1156 MARKELL CT	1 1	В	Residence Residence	66 66	58 62	60
	C-69	1158 MARKELL CT	1	В	Residence	66	64	65
	C-70	1160 MARKELL CT	1	В	Residence	66	61	63
	C-71	1162 MARKELL CT	1	В	Residence	66	62	64
	C-72	1164 MARKELL CT	1	В	Residence	66	61	63
	C-73 C-74	1163 MARKELL CT	1 1	B B	Residence Residence	66 66	70 70	71 68
	C-74 C-75	1167 MARKELL CT 1166 MARKELL CT	1	В	Residence	66	61	63
	C-76	1170 MARKELL CT	1	В	Residence	66	60	62
	C-77	1201 Bishopsgate Way	1	В	Residence	66	53	54
	C-78	1201 Bishopsgate Way	1	В	Residence	66	52	54
	C-79	1201 BISHOPSGATE WAY	1	В	Residence	66	53	55
	C-80 C-81	1203 BISHOPSGATE WAY 1205 BISHOPSGATE WAY	1 1	B B	Residence Residence	66 66	52 53	55 55
	C-82	1205 BISHOPSGATE WAY	1	В	Residence	66	54	56
	C-83	1209 BISHOPSGATE WAY	1	В	Residence	66	54	56
	C-84	1211 BISHOPSGATE WAY	1	В	Residence	66	53	55
	C-85	1213 BISHOPSGATE WAY	1	В	Residence	66	53	55
	C-86	1215 BISHOPSGATE WAY	1	В	Residence	66	52	54
	C-87 C-88	1217 BISHOPSGATE WAY 1219 BISHOPSGATE WAY	1 1	B B	Residence Residence	66 66	50 51	53 53
	C-00 C-92	11006 BURYWOOD LN	1	В	Residence	66	50	53
	C-93	11004 BURYWOOD LN	1	В	Residence	66	50	52
	C-94	11002 BURYWOOD LN	1	В	Residence	66	52	54
	C-95	11000 BURYWOOD LN	1	В	Residence	66	54	56
	C-96	11001 BURYWOOD LN	1	В	Residence	66	55	57
	C-97 C-98	1286 GATESMEADOW WAY 1284 GATESMEADOW WAY	1 1	B B	Residence Residence	66 66	54 54	56 55
	C-98	10864 HUNTER GATE WAY	1	В	Residence	66	58	59
	C-100	10860 HUNTER GATE WAY	1	В	Residence	66	58	60
	C-101	10858 HUNTER GATE WAY	1	В	Residence	66	58	60
	C-102	10856 Hunter Gate Way	1	В	Residence	66	58	60
	C-103	10854 HUNTER GATE WAY	1	В	Residence	66	59	60
	C-104 C-105	10852 HUNTER GATE WAY 10850 HUNTER GATE WAY	1 1	B B	Residence Residence	66 66	59 59	60 60
	C-105	10846 HUNTER GATE WAY	1	С	Pool	66	56	57
	C-107	10846 HUNTER GATE WAY	1	C	Tennis Court	66	59	60
	C-108	10846 HUNTER GATE WAY	1	С	Picnic Area	66	64	65
	C-109	10846 HUNTER GATE WAY	1	С	Basketball	66	59	60
	C-110	10846 HUNTER GATE WAY	1	С	Pavillion	66	55	57
	C-111	10846 HUNTER GATE WAY	1	С	Playground	66	55	57

		ROUTE 7 EXIST	TABLE 7	REDICTED NOISE LE	EVELS			
CNE	Receptor ID	Address	# of Dwelling Units	Activity Category	Land Use	NAC	Levels (Levels	hour Noise q(h) in dBA)
								2040 Build
	D-01	1149 UTTERBACK STORE RD	1	С	Sports Complex	66	64	68
	D-02	1149 UTTERBACK STORE RD	1	С	Sports Complex	66	62	66
	D-03	1149 UTTERBACK STORE RD	1	С	Sports Complex	66		64
	D-04	1149 UTTERBACK STORE RD	1	С	Sports Complex	66	1	62
	D-05	1149 UTTERBACK STORE RD	1	С	Sports Complex	66		63
	D-06 D-07	1149 UTTERBACK STORE RD 1149 UTTERBACK STORE RD	1 1	C C	Sports Complex Sports Complex			64 62
	D-07	1149 UTTERBACK STORE RD	1	C	Sports Complex	66		61
	D-09	1149 UTTERBACK STORE RD	1 1	C	Sports Complex	66		60
	D-10	1149 UTTERBACK STORE RD	1	C	Sports Complex	66		59
	D-11	1149 UTTERBACK STORE RD	1	С	Sports Complex	66	56	60
	D-12	1149 UTTERBACK STORE RD	1	С	Sports Complex	66	56	60
	D-13	1149 UTTERBACK STORE RD	1	С	Sports Complex	66		61
	D-14	1149 UTTERBACK STORE RD	1	С	Sports Complex	66		58
	D-15	1149 UTTERBACK STORE RD	1	С	Sports Complex	66	-	57
	D-16	1149 UTTERBACK STORE RD	1	С	Sports Complex	66		56
	D-17 D-18	1149 UTTERBACK STORE RD 1149 UTTERBACK STORE RD	1 1	C C	Sports Complex Sports Complex	66 66		57 60
	D-18 D-19	1149 UTTERBACK STORE RD	1	C	Sports Complex	66	1	59
۵	D-19 D-20	1149 UTTERBACK STORE RD	1	C	Sports Complex	66		56
CNE	D-21	1149 UTTERBACK STORE RD	1	C	Sports Complex	66		55
ົວ	D-22	1149 UTTERBACK STORE RD	1	С	Sports Complex	66	50	54
	D-23	1149 UTTERBACK STORE RD	1	С	Sports Complex	66	51	55
	D-24	1149 UTTERBACK STORE RD	1	С	Sports Complex	66	53	58
	D-25	1149 UTTERBACK STORE RD	1	С	Sports Complex	66		62
	D-26	1149 UTTERBACK STORE RD	1	С	Sports Complex	66		63
	D-27	1149 UTTERBACK STORE RD	1	С	Sports Complex	66		59
	D-28 D-29	1149 UTTERBACK STORE RD 1149 UTTERBACK STORE RD	1 1	C C	Sports Complex	66		61 62
	D-29 D-30	1149 UTTERBACK STORE RD	1	С	Sports Complex Sports Complex	66	1	60
	D-30	1054 Hanchel Ter	1	В	Residence	66		72
	D-32	1052 Hanchel Ter	1	В	Residence	66		63
	D-33	1050 Hanchel Ter	1	В	Residence	66	55	57
	D-34	10924 GREAT PASSAGE CT	1	В	Residence	66	53	55
	D-35	10932 GREAT PASSAGE CT	1	В	Residence	66		55
	D-36	10928 GREAT PASSAGE CT	1	В	Residence	66		53
	D-37	1100 GREAT PASSAGE BLVD	1	В	Residence	66		50
	D-38	1104 GREAT PASSAGE BLVD	1	В	Residence	66		55
	D-39 D-40	1051 Hanchel Ter 1051 HANCHEL TER	1 1	B B	Residence Residence			65 70
	D-40 D-41	1108 GREAT PASSAGE BLVD	1	В	Residence	66		63
	E-01	1142 KETTLE POND LN	1	В	Residence	66	<del> </del>	62
	E-02	1112 AMANDA DR	1	В	Residence	66		66
	E-03	1114 AMANDA DR	1	В	Residence	66		63
	E-04	1116 AMANDA DR	1	В	Residence	66	67	69
	E-05	1118 AMANDA DR	1	В	Residence	66	66	67
	E-06	1124 AMANDA DR	1	В	Residence	66	70	71
	E-07	1125 AMANDA DR	1	В	Residence	66	64	66
	E-08	1123 AMANDA DR	1	В	Residence	66	62	64
	E-09	1121 AMANDA DR 1119 AMANDA DR	1 1	B B	Residence Residence	66	59 58	61 59
	E-10 E-11	1119 AMANDA DR 1117 AMANDA DR	1 1	B	Residence Residence	66 66	58 56	59 58
	E-11	1117 AMANDA DR 1115 AMANDA DR	1	В	Residence	66	53	55
	E-13	1146 KETTLE POND LN	1	В	Residence	66	50	53
	E-14	1143 KETTLE POND LN	1	В	Residence	66	52	54
	E-15	1104 AMANDA DR	1	В	Residence	66	49	51
	E-16	1105 AMANDA DR	1	В	Residence	66	46	48
	E-17	1107 AMANDA DR	1	В	Residence	66	50	52
	E-18	1149 KETTLE POND LN	1	В	Residence	66	47	49
	E-19	1148 KETTLE POND LN	1	В	Residence	66	47	49
	E-20	1150 KETTLE POND LN	1	В	Residence	66	46	48
	E-21	1152 KETTLE POND LN	1	В	Residence	66	46	48
	E-22	1154 KETTLE POND LN	1	В	Residence	66	49	51
	E-23 E-24	1156 KETTLE POND LN 1158 KETTLE POND LN	1 1	B B	Residence Residence	66 66	51 52	53 54
	L-24	1160 KETTLE POND LN	1	В	Residence	66	52	55

		ROUTE 7 EXISTI	TABLE 7	PREDICTED NOISE LE	EVELS			
CNE	Receptor ID	Address	# of Dwelling Units	Activity Category	Land Use	NAC	Levels (Le	nour Noise q(h) in dBA)
							2018 Existing	2040 Build
	E-26	1162 KETTLE POND LN	1	В	Residence	66	52	54
	E-27	1164 KETTLE POND LN	1	В	Residence	66	51	54
	E-28	1166 KETTLE POND LN	1	В	Residence	66	49	52
	E-29 E-30	1168 KETTLE POND LN 1170 KETTLE POND LN	1 1	B B	Residence Residence	66 66	53 50	55 50
	E-31	1150 RIVA RIDGE DR	1	В	Residence	66	51	53
	E-32	1152 RIVA RIDGE DR	1	В	Residence	66	55	57
Ш	E-33	1158 RIVA RIDGE DR	1	В	Residence	66	63	65
SNE	E-34	1127 AMANDA DR	1	В	Residence	66	67	68
_	E-35	1154 RIVA RIDGE DR	1	В	Residence	66	56	58
	E-36	1156 RIVA RIDGE DR	1	В	Residence	66	62	64
	E-37	1165 KETTLE POND LN	1	В	Residence	66	48	51
	E-38 E-39	1169 KETTLE POND LN 10809 PINEY POND DR	1 1	B B	Residence Residence	66 66	49 67	50 68
	E-39	10807 PINEY POND DR	1	В	Residence	66	69	70
	E-41	10805 PINEY POND DR	1 1	В	Residence	66	66	68
	E-42	10803 PINEY POND DR	1	В	Residence	66	65	67
	E-43	10801 PINEY POND DR	1	В	Residence	66	57	58
	E-44	10806 PINEY POND DR	1	В	Residence	66	58	60
	E-45	10804 PINEY POND DR	1	В	Residence	66	57	59
	E-46	10802 PINEY POND DR	1	В	Residence	66	50	53
	E-47	10800 PINEY POND DR	1	В	Residence	66	49	52
	E-48 E-49	11715 CRIPPEN CT 11717 CRIPPEN CT	1 1	B B	Residence Residence	66 66	70 70	71 71
	E-49 E-50	11717 CRIPPEN CT	1 1	В	Residence	66	64	65
	E-51	11716 CRIPPEN CT	1 1	В	Residence	66	48	51
	E-52	11714 CRIPPEN CT	1	В	Residence	66	48	51
	E-53	11710 CRIPPEN CT	1	В	Residence	66	50	52
	E-54	1106 MOUNTAIN HOPE CT	1	В	Residence	66	46	49
	E-55	1104 MOUNTAIN HOPE CT	1	В	Residence	66	47	49
	E-56	1105 MOUNTAIN HOPE CT	1 1	В	Residence	66	54	55
	E-57	1103 MOUNTAIN HOPE CT	1	В	Residence	66	52	54
	E-58 E-59	1107 MOUNTAIN HOPE CT 11700 CRIPPEN CT	1 1	B B	Residence Residence	66 66	52 56	54 58
	E-60	11713 CRIPPEN CT	1	В	Residence	66	63	66
	E-61	11711 CRIPPEN CT	1	В	Residence	66	66	69
	E-62	11709 CRIPPEN CT	1	В	Residence	66	55	58
	E-63	11707 CRIPPEN CT	1	В	Residence	66	54	57
	E-64	11705 CRIPPEN CT	1	В	Residence	66	65	68
	E-65	11703 CRIPPEN CT	1	В	Residence	66	64	67
	E-66	11701 CRIPPEN CT	1	В	Residence	66	60	64
	F-01 F-02	10618 LEESBURG PIKE 10613 SPRINGVALE CT	1 1	E B	Nursery Residence	71 66	65 53	68 57
	F-02	10611 SPRINGVALE CT	1	В	Residence	66	55	58
	F-04	10609 SPRINGVALE CT	1	В	Residence	66	53	56
	F-05	10603 SPRINGVALE CT	1	В	Residence	66	53	55
	F-06	10601 SPRINGVALE CT	1	В	Residence	66	51	55
	F-07	10600 SPRINGVALE CT	1	В	Residence	66	51	55
	F-08	10605 SPRINGVALE CT	1	В	Residence	66	51	53
	F-09	10607 SPRINGVALE CT	1	В	Residence	66	49	51
	F-10 F-11	1137 SPRINGVALE RD 1141 SPRINGVALE RD	1 1	B B	Residence Residence	66 66	53 49	55 51
	F-11	10604 Springvale Ct	1	В	Residence	66	49	49
	F-13	10602 SPRINGVALE CT	1 1	В	Residence	66	47	50
	F-14	10500 LEESBURG PIKE	1	E	Nursery	71	68	70
	F-15	10420 LEESBURG PIKE	1	В	Residence	66	70	68
	F-16	10416 LEESBURG PIKE	1	С	Cemetery	66	72	73
	F-17	10416 LEESBURG PIKE	1	С	Cemetery	66	72	74
	F-18	10416 LEESBURG PIKE	1	С	Cemetery	66	65	68
	F-19	10416 LEESBURG PIKE	1	С	Cemetery	66	65	68
	F-20 F-21	10416 LEESBURG PIKE 10416 LEESBURG PIKE	1 1	C C	Cemetery Cemetery	66 66	60 59	62 61
	F-21	10416 VAN PATTEN LN	1	В	Residence	66	52	55
	F-23	10413 VAN PATTEN LN	1	В	Residence	66	55	57
	F-24	10411 VAN PATTEN LN	1	В	Residence	66	71	70
	F-25	10409 VAN PATTEN LN	1	В	Residence	66	68	71

		ROUTE 7 EXIS	TABLE 7	PREDICTED NOISE LE	EVELS			
CNE	Receptor ID	Address	# of Dwelling Units	Activity Category	Land Use	NAC		hour Noise eq(h) in dBA) 2040 Build
							Existing	
	F-26	10407 VAN PATTEN LN	1	В	Residence	66	71	69
	F-27 F-28	10401 VAN PATTEN LN 10403 VAN PATTEN LN	1 1	B B	Residence Residence	66 66	62	62 61
	F-29	10405 VAN PATTEN LN	1	В	Residence	66	61	62
	F-30	10414 VAN PATTEN LN	1	В	Residence	66	48	50
	F-31	10410 VAN PATTEN LN	1	В	Residence	66	49	51
	F-32	10406 VAN PATTEN LN	1	В	Residence	66	52	52
	F-33	10402 VAN PATTEN LN	1	В	Residence	66	51	51
	F-34	10400 VAN PATTEN LN	1	В	Residence	66	54	57
	F-35 F-36	1101 COLVIN MILL CT	1 1	B B	Residence Residence	66 66	49 48	50 49
	F-36	1103 COLVIN MILL CT 1105 COLVIN MILL CT	1	В	Residence	66	48	50
	F-38	1107 COLVIN MILL CT	1	В	Residence	66	53	55
	F-39	1162 MILL GARDEN CT	1	В	Residence	66	51	54
	F-40	10313 COLVIN RUN RD	1	В	Residence	66	69	72
	F-41	10309 COLVIN RUN RD	1	В	Residence	66	66	69
	F-42	10301 COLVIN RUN RD	1	В	Residence	66	59	63
	F-43	1202 COLVIN MEADOWS LN	1	В	Residence	66	56	60
	F-44	1200 COLVIN MEADOWS LN	1	В	Residence	66	55	58
	F-45 F-46	1206 COLVIN MEADOWS LN 1204 COLVIN MEADOWS LN	1 1	B B	Residence	66 66	60 65	64 69
	F-47	1208 COLVIN MEADOWS LN	1	В	Residence Residence	66	62	67
	F-48	1210 COLVIN MEADOWS LN	1	В	Residence	66	68	70
	F-49	1212 COLVIN MEADOWS LN	1	В	Residence	66	69	71
	F-50	1214 COLVIN MEADOWS LN	1	В	Residence	66	70	71
	F-51	1216 COLVIN MEADOWS LN	1	В	Residence	66	69	70
	F-52	1218 COLVIN MEADOWS LN	1	В	Residence	66	65	65
	F-53	1201 COLVIN MEADOWS LN	1	В	Residence	66	49	51
	F-54	1203 COLVIN MEADOWS LN	1	В	Residence	66	48	50
	F-55	1205 COLVIN MEADOWS LN	1	В	Residence	66	52	55
	F-56 F-57	1207 COLVIN MEADOWS LN 1209 COLVIN MEADOWS LN	1 1	B B	Residence Residence	66 66	51 53	54 55
	F-58	1211 COLVIN MEADOWS LN	1	В	Residence	66	54	56
	F-59	1194 LEES MEADOW CT	1	В	Residence	66	54	55
	F-60	1192 LEES MEADOW CT	1	В	Residence	66	52	54
	F-61	1192 LEES MEADOW CT	1	В	Residence	66	48	51
	F-62	1191 LEES MEADOW CT	1	В	Residence	66	50	53
	F-63	1193 LEES MEADOW CT	1	В	Residence	66	52	54
	F-64	1195 LEES MEADOW CT	1	В	Residence	66	54	56
	F-65	1195 LEES MEADOW CT 1225 COLVIN MEADOWS LN	1 1	B B	Residence	66	55 55	57 58
	F-66 F-67	1227 COLVIN MEADOWS LN	1	В	Residence Residence	66 66	55	57
	F-68	1227 COLVIN MEADOWS LN	1	В	Residence	66	54	56
	F-69	1230 Colvin Meadows Ln	1	В	Residence	66	54	57
	F-70	1222 COLVIN MEADOWS LN	1	В	Residence	66	70	70
	F-71	1224 COLVIN MEADOWS LN	1	В	Residence	66	68	70
	F-72	1226 COLVIN MEADOWS LN	1	В	Residence	66	66	68
	F-73	1228 COLVIN MEADOWS LN	1	В	Residence	66	61	64
	F-74 F-75	10124 LEESBURG PIKE 10101 Colvin Run Rd	1 1	B B	Residence	66	71	74 64
	F-75 F-76	10101 Colvin Run Rd 10108 COLVIN RUN RD	1 1	В	Residence Residence	66 66	60 57	56
	F-77	10104 COLVIN RUN RD	1	В	Residence	66	58	55
	F-78	10100 COLVIN RUN RD	1	В	Residence	66	56	55
	F-79	1172 ROBINDALE DR	1	В	Residence	66	53	56
	F-80	10030 COLVIN RUN RD	1	В	Residence	66	53	53
ш	F-81	10026 COLVIN RUN RD	1	В	Residence	66	52	52
CNE	F-82	10020 COLVIN RUN RD	1	В	Residence	66	54	56
ົວ	F-83	10017 COLVIN RUN RD	1	В	Residence	66	66	67
	F-84 F-85	10017 COLVIN RUN RD 10014 COLVIN RUN RD	1 1	C B	Historic Site Residence	66 66	66 59	65 59
	F-86	10014 COLVIN RON RD	1	В	Residence	66	60	62
	F-87	10024 COLVIN RUN RD	1	В	Residence	66	57	59
	F-88	10010 COLVIN RUN RD	1	В	Residence	66	64	65
	F-89	9912 HESSICK CT	1	В	Residence	66	63	65
	F-90	9910 HESSICK CT	1	В	Residence	66	59	61
	F-91	9908 HESSICK CT	1	В	Residence	66	56	58

	TABLE 7 ROUTE 7 EXISTING AND FUTURE PREDICTED NOISE LEVELS							
CNE	Receptor ID	Address	# of Dwelling Units	Activity Category	Land Use	NAC	Levels (Le	nour Noise q(h) in dBA)
							2018 Existing	2040 Build
	F-92	9906 HESSICK CT	1	В	Residence	66	53	56
	F-93	9907 HESSICK CT	1	В	Residence	66	55	58
l -	F-94	1200 STONE FALLS WAY 9911 HESSICK CT	1	В	Residence	66	62	65
l -	F-95 F-96	1204 STONE FALLS WAY	1	B B	Residence Residence	66 66	67 66	69 68
l	F-97	1205 STONE FALLS WAY	1	В	Residence	66	57	60
	F-98	1208 STONE FALLS WAY	1	В	Residence	66	66	67
	F-99	1104 MILL FIELD CT	1	В	Residence	66	61	63
l	F-100	9713 LOCUST HILL DR	1	В	Residence	66	68	69
-	F-101 F-102	9715 LOCUST HILL DR 9719 LOCUST HILL DR	1 1	B B	Residence Residence	66 66	65 63	67 65
	F-102 F-103	9719 LOCUST HILL DR	1	В	Residence	66	61	63
	F-104	9720 LOCUST HILL DR	1	В	Residence	66	54	56
	F-105	9718 LOCUST HILL DR	1	В	Residence	66	54	56
	F-106	9714 LOCUST HILL DR	1	В	Residence	66	59	61
	F-107	9710 LOCUST HILL DR	1	В	Residence	66	60	62
<b>I</b> ⊦	F-108 F-109	9716 LOCUST HILL DR 9708 LOCUST HILL DR	1	B B	Residence	66 66	43 58	45 60
l -	F-109 F-110	9706 LOCUST HILL DR 9706 LOCUST HILL DR	1	В	Residence Residence	66	54	56
l	F-111	9704 LOCUST HILL DR	1	В	Residence	66	53	54
	F-112	9702 LOCUST HILL DR	1	В	Residence	66	52	53
	F-113	9700 LOCUST HILL DR	1	В	Residence	66	51	52
	F-114	9622 LOCUST HILL DR	1	В	Residence	66	50	51
<b>I</b>	F-115	9620 LOCUST HILL DR	1	В	Residence	66	48	50
	F-116 F-117	9711 LOCUST HILL DR 9709 LOCUST HILL DR	1	B B	Residence Residence	66 66	71 70	72 71
	F-117 F-118	9707 LOCUST HILL DR	1	В	Residence	66	61	61
	F-119	9705 LOCUST HILL DR	1	В	Residence	66	58	59
	F-120	9703 LOCUST HILL DR	1	В	Residence	66	55	55
	F-121	9621 LOCUST HILL DR	1	В	Residence	66	51	52
	F-122	9619 LOCUST HILL DR	1	В	Residence	66	50	52
	F-123	9629 LOCUST HILL DR	1	В	Residence	66	72	74
<b>I</b> ⊦	F-124 F-125	9627 LOCUST HILL DR 9720 LEESBURG PIKE	1	<u>В</u> В	Residence Residence	66 66	71 70	73 73
l	F-126	9625 LOCUST HILL DR	1	В	Residence	66	59	60
	F-127	9623 LOCUST HILL DR	1	В	Residence	66	54	56
	F-128	9617 LOCUST HILL DR	1	В	Residence	66	51	53
	F-129	9615 LOCUST HILL DR	1	В	Residence	66	53	54
	F-130	9613 LOCUST HILL DR	1	В	Residence	66	54	55
	F-131 F-132	9611 LOCUST HILL DR 9609 LOCUST HILL DR	1	B B	Residence Residence	66 66	55 65	56 65
	F-133	9607 LOCUST HILL DR	1	В	Residence	66	65	65
	F-134	9605 LOCUST HILL DR	1	В	Residence	66	56	56
	F-135	1202 SAUGUS CT	1	В	Residence	66	57	58
	F-136	1204 SAUGUS CT	1	В	Residence	66	60	61
	F-137	1206 SAUGUS CT	1	В	Residence	66	57	58 57
⊦	F-138 F-139	1207 SAUGUS CT 1205 SAUGUS CT	1 1	<u>В</u> В	Residence Residence	66 66	56 56	57 57
	F-139 F-140	9700 LEESBURG PIKE	1	В	Residence	66	65	66
	F-141	1203 SAUGUS CT	1	В	Residence	66	52	54
	F-142	1201 SAUGUS CT	1	В	Residence	66	53	55
	F-143	9602 LOCUST HILL DR	1	В	Residence	66	52	53
	F-144	9612 LOCUST HILL DR	1	В	Residence	66	51	54
-	F-145 F-146	9614 Locust HIII Dr 9616 Locust HiII Dr	1 1	B B	Residence Residence	66 66	50 49	52 51
-	F-146 F-147	9541 LOCUST HILL DR	1	В	Residence	66	51	53
	F-148	9539 LOCUST HILL DR	1	В	Residence	66	52	55
	F-149	9537 LOCUST HILL DR	1	В	Residence	66	54	56
	F-150	9531 LOCUST HILL DR	1	В	Residence	66	52	55
	F-151	9529 LOCUST HILL DR	1	В	Residence	66	55	59
-	F-152	9527 LOCUST HILL DR	1	В	Residence	66	54	58
<b>I</b> ⊦	F-153 F-154	9525 LOCUST HILL DR 9523 LOCUST HILL DR	1	B B	Residence Residence	66 66	51 51	54 56
⊦	F-155	9515 LOCUST HILL DR	1	В	Residence	66	50	54
-	F-156	9513 LOCUST HILL DR	1	В	Residence	66	50	53
[	F-157	9511 LOCUST HILL DR	1	В	Residence	66	49	53

		ROUTE 7 EXIST	TABLE 7	PREDICTED NOISE LE	EVELS			
CNE	Receptor ID	Address	# of Dwelling Units	Activity Category	Land Use	NAC	Levels (Le	nour Noise q(h) in dBA)
							2018 Existing	2040 Build
	F-158	9509 LOCUST HILL DR	1	В	Residence	66	51	55
	F-159	9505 LOCUST HILL DR	1	В	Residence	66	49	52
	F-160	9503 LOCUST HILL DR	1	В	Residence	66	49	52
	F-161 F-162	9501 LOCUST HILL DR 1212 TROTTING HORSE LN	1 1	B B	Residence Residence	66 66	48 50	51 53
	F-162	1214 TROTTING HORSE LN	1	В	Residence	66	52	55
	F-164	1216 TROTTING HORSE LN	1	В	Residence	66	53	57
	G-01	10691 WATER FALLS LN	1	В	Residence	66	58	62
	G-02	10693 WATER FALLS LN	1	В	Residence	66	60	64
	G-03	10694 WATER FALLS LN	1	В	Residence	66	61	65
	G-04	10692 WATER FALLS LN	1	В	Residence	66	61	65
	G-05 G-06	10690 WATER FALLS LN 10688 WATER FALLS LN	1 1	B B	Residence Residence	66	56 51	60 56
	G-00 G-07	10686 WATER FALLS LN	1	В	Residence	66	49	53
	G-08	10684 WATER FALLS LN	1 1	В	Residence	66	48	51
	G-09	10682 WATER FALLS LN	1	В	Residence	66	47	51
	G-10	10680 WATER FALLS LN	1	В	Residence	66	45	48
	G-11	10681 WATER FALLS LN	1	В	Residence	66	46	49
	G-12	10683 WATER FALLS LN	1	В	Residence	66	47	49
	G-13	10685 WATER FALLS LN	1	В	Residence	66	48	51
	G-14	10687 WATER FALLS LN	1	B B	Residence	66	49	52
	G-15 G-16	10689 WATER FALLS LN 1264 DUNN MEADOW CT	1 1	В	Residence Residence	66 66	49 50	51 53
	G-16 G-17	1262 DUNN MEADOW CT	1	В	Residence	66	50	53
	G-18	1260 DUNN MEADOW CT	1	В	Residence	66	51	54
	G-19	1258 DUNN MEADOW CT	1	В	Residence	66	54	56
	G-20	1256 DUNN MEADOW CT	1	В	Residence	66	57	60
	G-21	1254 DUNN MEADOW CT	1	В	Residence	66	58	60
	G-22	1251 DUNN MEADOW CT	1	В	Residence	66	66	68
	G-23	1253 DUNN MEADOW CT	1	B B	Residence	66	65	68
	G-24 G-25	1253 DUNN MEADOW CT 1255 DUNN MEADOW CT	1 1	В	Residence Residence	66 66	68 71	72 73
	G-26	10523 DUNN MEADOW RD	1	В	Residence	66	56	58
	G-27	10519 DUNN MEADOW RD	1	В	Residence	66	56	59
	G-28	1252 COBBLE POND WAY	1	В	Residence	66	54	57
	G-29	1254 COBBLE POND WAY	1	В	Residence	66	52	55
	G-30	1256 COBBLE POND WAY	1	В	Residence	66	50	52
	G-31	1257 COBBLE POND WAY	1	В	Residence	66	49	51
	G-32	1255 COBBLE POND WAY	1	B B	Residence	66	50 52	53
	G-33 G-34	1253 Cobble Pond Way 10515 DUNN MEADOW RD	1 1	В	Residence Residence	66	57	54 58
	G-35	10513 DUNN MEADOW RD	1	В	Residence	66	59	60
	G-36	10524 DUNN MEADOW RD	1	В	Residence	66	60	63
	G-37	10522 DUNN MEADOW RD	1	В	Residence	66	68	70
	G-38	10520 DUNN MEADOW RD	1	В	Residence	66	66	68
	G-39	10518 DUNN MEADOW RD	1	В	Residence	66	66	68
	G-40	10516 DUNN MEADOW RD	1	В	Residence	66	67	69
	G-41 G-42	10514 DUNN MEADOW RD 10512 DUNN MEADOW RD	1 1	B B	Residence	66	67 65	69 65
	G-42 G-43	10512 DUNN MEADOW RD 10508 DUNN MEADOW RD	1	В	Residence Residence	66	65	66
	G-43	10506 DUNN MEADOW RD	1	В	Residence	66	64	65
	G-45	10500 DUNN MEADOW RD	1	В	Residence	66	66	66
	G-46	10498 DUNN MEADOW RD	1	В	Residence	66	67	69
	G-47	10496 DUNN MEADOW RD	1	В	Residence	66	62	65
	G-48	10410 DUNN MEADOW RD	1	В	Residence	66	60	63
	G-49	10408 DUNN MEADOW RD	1	В	Residence	66	59	65
	G-50	10406 DUNN MEADOW RD	1 1	B B	Residence	66	66 71	69
	G-51 G-52	10404 DUNN MEADOW RD 10402 DUNN MEADOW RD	1	В	Residence Residence	66	71 71	73 73
	G-52 G-53	10402 DUNN MEADOW RD	1	В	Residence	66	69	71
	G-54	10509 DUNN MEADOW RD	1	В	Residence	66	57	58
	G-55	10507 DUNN MEADOW RD	1	В	Residence	66	57	59
	G-56	10501 DUNN MEADOW RD	1	В	Residence	66	57	58
	G-57	10503 DUNN MEADOW RD	1	В	Residence	66	51	53
	G-58	10505 DUNN MEADOW RD	1	В	Residence	66	50	52
I	G-59	10497 DUNN MEADOW RD	1	В	Residence	66	57	59

				DEDIGTED MOIOE LE	\/ELO			
		ROUTE / EXISTIN	IG AND FUTURE P	REDICTED NOISE LE	VELS			
CNE	Receptor	Address	# of Dwelling Units	Activity Category	Land Use	NAC		nour Noise q(h) in dBA)
	ני		Office			_	2018 Existing	2040 Build
	G-60	1290 NEWKIRK CT	1	В	Residence	66	51	53
	G-61 G-62	1291 NEWKIRK CT 10411 DUNN MEADOW RD	1 1	B B	Residence Residence	66 66	47 52	50 55
	G-63	10409 DUNN MEADOW RD	1	В	Residence	66	56	59
	G-64	10405 DUNN MEADOW RD	1	В	Residence	66	56	59
	G-65	10403 DUNN MEADOW RD	1	В	Residence	66	58	60
	G-66	10401 DUNN MEADOW RD	1 1	В	Residence	66	56	60
	G-67 G-68	1212 DELTA GLEN CT 1214 DELTA GLEN CT	1 1	B B	Residence Residence	66 66	52 50	56 53
	G-69	1214 DELTA GLEN CT	1 1	В	Residence	66	48	51
	G-70	1218 DELTA GLEN CT	1	В	Residence	66	46	49
	G-71	1220 DELTA GLEN CT	1	В	Residence	66	45	48
	G-72	1217 DELTA GLEN CT	1 1	В	Residence	66	46	48
	G-73 G-74	1215 DELTA GLEN CT 1213 DELTA GLEN CT	1 1	B B	Residence Residence	66 66	46 50	48 53
	G-75	1211 DELTA GLEN CT	1 1	В	Residence	66	55	59
	G-76	1203 DELTA GLEN CT	1	В	Residence	66	65	68
	G-77	1201 DELTA GLEN CT	1	В	Residence	66	70	72
	G-78	10334 DUNN MEADOW RD	1	В	Residence	66	63	66
	G-79 G-80	10331 DUNN MEADOW RD 10329 DUNN MEADOW RD	1 1	B B	Residence Residence	66 66	53 50	56 52
	G-81	10327 DUNN MEADOW RD	1 1	В	Residence	66	48	50
	G-82	10317 DUNN MEADOW RD	1	В	Residence	66	42	45
	G-83	10332 DUNN MEADOW RD	1	В	Residence	66	62	65
	G-84	10330 DUNN MEADOW RD	1	В	Residence	66	56	61
	G-85	10328 DUNN MEADOW RD	1 1	B B	Residence	66	54	58
	G-86 G-87	10326 DUNN MEADOW RD 10324 DUNN MEADOW RD	1 1	В	Residence Residence	66 66	51 51	55 55
	G-88	10318 DUNN MEADOW RD	1	В	Residence	66	46	49
	G-89	10320 DUNN MEADOW RD	1	В	Residence	66	46	48
	G-90	10322 DUNN MEADOW RD	1	В	Residence	66	47	50
	G-91	10237 LEESBURG PIKE	1 1	D C	Church	51	61 (36)	66 (41)
	G-92 G-93	10237 LEESBURG PIKE 10231 LEESBURG PIKE	1 1	В	Picnic Area Residence	66 66	61 57	65 61
	G-94	10249 LEESBURG PIKE	1	В	Residence	66	66	68
	G-95	10247 LEESBURG PIKE	1	В	Residence	66	65	67
	G-96	10245 LEESBURG PIKE	1	В	Residence	66	64	67
	G-97	10219 LEESBURG PIKE	1 1	B B	Residence	66	61	63 64
	G-98 G-99	10214 CHESTNUT OAK CT 10202 CHESTNUT OAK CT	1 1	В	Residence Residence	66 66	61 58	60
	G-100	1296 COLVIN FOREST DR	1	В	Residence	66	58	61
	G-101	1298 COLVIN FOREST DR	1	В	Residence	66	58	59
	G-102	10200 CHESTNUT OAK CT	1	В	Residence	66	56	59
o l	G-103	1301 COLVIN FOREST DR 1293 COLVIN FOREST DR	1	В	Residence	66	54	57
CNE	G-104 G-105	1293 COLVIN FOREST DR 1295 COLVIN FOREST DR	1 1	B B	Residence Residence	66 66	69 67	70 70
ا ا	G-106	1297 COLVIN FOREST DR	1	В	Residence	66	56	59
	G-107	10112 MILL WHEEL LN	1	В	Residence	66	54	56
	G-108	10110 MILL WHEEL LN	1	В	Residence	66	55	57
	G-109 G-110	10106 MILL WHEEL LN 10100 MILL WHEEL LN	1 1	B B	Residence Residence	66 66	57 56	60
	G-110 G-111	10100 MILL WHEEL LN 10115 MILL WHEEL LN	1 1	В	Residence	66	55	55
	G-112	10111 MILL WHEEL LN	1	В	Residence	66	51	53
	G-113	10109 MILL WHEEL LN	1	В	Residence	66	51	54
	G-114	10107 MILL WHEEL LN	1	В	Residence	66	53	55
	G-115	10105 MILL WHEEL LN	1 1	B B	Residence	66 66	47 55	52 59
	G-116 G-117	10103 MILL WHEEL LN 10101 MILL WHEEL LN	1 1	В	Residence Residence	66	55	59
	G-118	10019 SCENIC VIEW TER	1	В	Residence	66	55	59
	G-119	10017 SCENIC VIEW TER	1	В	Residence	66	56	60
	G-120	10015 SCENIC VIEW TER	1	В	Residence	66	57	61
	G-121	10013 SCENIC VIEW TER	1 1	В	Residence	66	56	60
	G-122 G-123	10011 SCENIC VIEW TER 10009 SCENIC VIEW TER	1 1	B B	Residence Residence	66 66	56 54	60 58
	G-123 G-124	10009 SCENIC VIEW TER	1	В	Residence	66	54	57
	G-125	10005 SCENIC VIEW TER	1	В	Residence	66	55	59

		POLITE 7 EVISTING	TABLE 7	REDICTED NOISE LE	VEI S			
		ROUTE / EXISTING	AND FUTURE P	REDICTED NOISE LE	VELS			
CNE	Receptor	Address	# of Dwelling Units	Activity Category	Land Use	NAC		nour Noise q(h) in dBA)
							2018 Existing	2040 Build
	G-126	10003 SCENIC VIEW TER	1	В	Residence	66	58	62
	G-127	1220 CARPERS FARM WAY	1	В	Residence	66	61	65
	G-128	1222 CARPERS FARM WAY	1	В	Residence	66	58	62
	G-129 G-130	1224 CARPERS FARM WAY 1226 CARPERS FARM WAY	1 1	B B	Residence Residence	66 66	56 55	60 58
	G-131	1228 CARPERS FARM WAY	1	В	Residence	66	54	59
	G-132	10012 CARPERS FARM CT	1	В	Residence	66	57	59
	G-133	10010 CARPERS FARM CT	1	В	Residence	66	55	58
	G-134 G-135	10008 CARPERS FARM CT 10004 CARPERS FARM CT	1	B B	Residence Residence	66 66	55 54	58 57
	G-136	1229 CARPERS FARM WAY	1	В	Residence	66	56	60
	G-137	1227 CARPERS FARM WAY	1	В	Residence	66	58	62
	G-138	1225 CARPERS FARM WAY	1	В	Residence	66	59	63
	G-139	1223 CARPERS FARM WAY	1	В	Residence	66	59	63
	G-140 G-141	1221 CARPERS FARM WAY 1219 CARPERS FARM WAY	1 1	B B	Residence Residence	66 66	61 58	65 63
	G-141 G-142	1217 CARPERS FARM WAY	1	В	Residence	66	56	61
	G-143	1284 SERENITY WOODS LN	1	В	Residence	66	59	63
	G-144	1280 SERENITY WOODS LN	1	В	Residence	66	70	73
	G-145	9801 LEESBURG PIKE	1	В	Residence	66	70	73
	G-146	1283 SERENITY WOODS LN	1	В	Residence	66	52	56
	G-147 G-148	1294 THOMPSON RUN CT 1292 THOMPSON RUN CT	1	B B	Residence Residence	66 66	49 48	52 50
	G-148	1290 THOMPSON RUN CT	1	В	Residence	66	44	47
	G-150	9731 MIDDLETON RIDGE RD	1	В	Residence	66	51	55
	G-151	9733 MIDDLETON RIDGE RD	1	В	Residence	66	53	57
	G-152	9735 MIDDLETON RIDGE RD	1	В	Residence	66	60	62
	G-153 G-154	9737 MIDDLETON RIDGE RD 9739 MIDDLETON RIDGE RD	1 1	B B	Residence Residence	66 66	72 71	73 72
	G-155	9740 MIDDLETON RIDGE RD	1	В	Residence	66	71	73
	G-156	9736 MIDDLETON RIDGE RD	1	В	Residence	66	70	72
	G-157	9734 MIDDLETON RIDGE RD	1	В	Residence	66	67	70
	G-158	9732 MIDDLETON RIDGE RD	1	В	Residence	66	56	59
	G-159 G-160	9730 MIDDLETON RIDGE RD 9728 MIDDLETON RIDGE RD	1 1	B B	Residence Residence	66 66	48 45	52 48
	G-160	9719 LEESBURG PIKE	1	В	Residence	66	71	74
	G-162	9724 MIDDLETON RIDGE RD	1	В	Residence	66	46	49
	G-163	1294 MIDDLETON CT	1	В	Residence	66	42	45
	G-164	1292 MIDDLETON CT	1	В	Residence	66	48	50
	G-165 G-166	1288 MIDDLETON CT 1286 MIDDLETON CT	1	B B	Residence Residence	66 66	49 48	52 50
	G-166	9723 LEESBURG PIKE	1	В	Residence	66	47	52
	G-168	1280 MIDDLETON CT	1	В	Residence	66	63	68
	G-169	1281 MIDDLETON CT	1	В	Residence	66	66	71
	G-170	1283 MIDDLETON CT	1	В	Residence	66	68	71
	G-171	1285 MIDDLETON CT	1	B B	Residence Residence	66 66	67 55	70 58
	G-172 G-173	1287 MIDDLETON CT 1289 MIDDLETON CT	1	В	Residence	66	55 52	58
	G-174	1291 MIDDLETON CT	1	В	Residence	66	50	52
	G-175	1293 MIDDLETON CT	1	В	Residence	66	46	49
	G-176	9716 MIDDLETON RIDGE RD	1	В	Residence	66	45	49
	G-177	9714 MIDDLETON RIDGE RD 9712 MIDDLETON RIDGE RD	1	B B	Residence Residence	66 66	46 46	48 49
	G-178 G-179	9712 MIDDLETON RIDGE RD 9710 MIDDLETON RIDGE RD	1	В	Residence	66	46	52 52
	G-180	9706 MIDDLETON RIDGE RD	1	В	Residence	66	52	56
	G-181	1298 DIFFICULT RUN CT	1	В	Residence	66	58	61
	G-182	1294 DIFFICULT RUN CT	1	В	Residence	66	60	63
	G-183	1290 DIFFICULT RUN CT	1 1	В В	Residence	66	54 59	57 62
	G-184 G-185	1288 DIFFICULT RUN CT 1291 DIFFICULT RUN CT	1 1	B B	Residence Residence	66 66	71	62 74
	G-186	1293 DIFFICULT RUN CT	1	В	Residence	66	71	74
	G-187	1295 DIFFICULT RUN CT	1	В	Residence	66	72	74
	G-188	1297 DIFFICULT RUN CT	1	В	Residence	66	72	74
	G-189	1299 DIFFICULT RUN CT 9713 MIDDLETON RIDGE RD	1 1	B B	Residence	66 66	72 44	74 48
	G-190 G-191	9711 MIDDLETON RIDGE RD 9711 MIDDLETON RIDGE RD	1	В	Residence Residence	66	45	48
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		DOUTE 7 EVICE	TABLE 7	REDICTED NOISE LE	TVEL C			
		ROUTE / EXIST	ING AND FUTURE P	REDICTED NOISE LE	EVELS			
CNE	Receptor	Address	# of Dwelling Units	Activity Category	Land Use	NAC		hour Noise q(h) in dBA)
Ĭ			O.III.O				2018 Existing	2040 Build
	G-192	9709 MIDDLETON RIDGE RD	1	В	Residence	66	48	50
	G-193	9707 MIDDLETON RIDGE RD	1	В	Residence	66	51	54
	G-194	9705 MIDDLETON RIDGE RD	1	В	Residence	66	54	57
	G-195 G-196	1290 TWEED CT 1294 TWEED CT	1 1	B B	Residence	66 66	59 58	62
	G-196 G-197	1294 TWEED CT	1	В	Residence Residence	66	56	61
	G-198	1297 TWEED CT	1	В	Residence	66	59	63
	G-199	1295 TWEED CT	1	В	Residence	66	66	69
	G-200	1293 TWEED CT	1	В	Residence	66	70	72
	G-201	1291 TWEED CT	1	В	Residence	66	70	73
	G-202	9601 LEESBURG PIKE	1	В	Residence	66	69	72
	G-203 G-204	9525 LEESBURG PIKE 9525 LEESBURG PIKE	1 1	C D	Playground Preschool	66 51	65 57 (32)	69 61 (36)
	G-204 G-205	1318 BEULAH RD	1	В	Residence	66	57 (32)	56
	G-206	1314 BEULAH RD	1	В	Residence	66	57	62
	G-207	1310 BEULAH RD	1	В	Residence	66	63	68
	G-208	1300 BEULAH RD	1	D	Medical Center	51	71 (46)	74 (49)
	H-01	9522 LEESBURG PIKE	1	В	Residence	66	71	75
	H-02	9407 FAIRPINE LN	1	В	Residence	66	67	74
	H-03	9405 FAIRPINE LN	1	В	Residence	66	64	68
	H-04 H-05	9409 FAIRPINE LN 9403 FAIRPINE LN	1 1	B B	Residence Residence	66 66	51 55	53 56
	H-06	9401 FAIRPINE LN	1	В	Residence	66	61	62
	H-07	9400 FAIRPINE LN	1	В	Residence	66	55	57
	H-08	9402 FAIRPINE LN	1	В	Residence	66	53	55
	H-09	9404 FAIRPINE LN	1	В	Residence	66	53	56
	H-10	9406 FAIRPINE LN	1	В	Residence	66	53	56
	H-11	9410 FAIRPINE LN	1	В	Residence	66	56	59
	H-12	9410 FAIRPINE LN	1	B B	Residence	66 66	54 53	58
	H-13 H-14	1217 TROTTING HORSE LN 1215 TROTTING HORSE LN	1 1	В	Residence Residence	66	51	55 54
	H-15	1213 TROTTING HORSE LN	1	В	Residence	66	51	55
	H-16	9397 FARMINGDALE CT	1	В	Residence	66	64	64
	H-17	9395 FARMINGDALE CT	1	В	Residence	66	72	74
	H-18	9393 Farmingdale Ct	1	В	Residence	66	72	73
	H-19	9390 FARMINGDALE CT	1	В	Residence	66	67	67
	H-20 H-21	9392 FARMINGDALE CT 9394 FARMINGDALE CT	1 1	B B	Residence Residence	66 66	60 58	60 59
	H-22	9394 FARMINGDALE CT 9396 FARMINGDALE CT	1	В	Residence	66	53	55
	H-23	9428 VERNON DR	1	В	Residence	66	54	56
	H-24	9390 WOLF TRAP CREEK CT	1	В	Residence	66	55	56
	H-25	9392 WOLF TRAP CREEK CT	1	В	Residence	66	60	61
	H-26	9394 WOLF TRAP CREEK CT	1	В	Residence	66	62	62
	H-27	9395 WOLF TRAP CREEK CT	1	В	Residence	66	70	71
	H-28 H-29	9393 WOLF TRAP CREEK CT 9424 VERNON DR	1 1	<u>В</u> В	Residence Residence	66 66	63 58	63
	H-30	9422 VERNON DR 9422 VERNON DR	1	В	Residence	66	59	61
	H-31	9420 VERNON DR	1	В	Residence	66	59	61
	H-32	9412 LEESBURG PIKE	1	В	Residence	66	73	75
	H-33	9418 VERNON DR	1	В	Residence	66	67	70
	H-34	9416 VERNON DR	1	В	Residence	66	67	70
	H-35	9400 LEESBURG PIKE	1 1	<u>В</u> В	Residence	66	72 73	74 74
	H-36 H-37	1306 LYONS ST 9400 VERNON DR	1	В	Residence Residence	66 66	58	60
	H-38	9406 VERNON DR	1	В	Residence	66	58	60
I	H-39	9414 VERNON DR	1	В	Residence	66	58	60
CNE	H-40	9425 VERNON DR	1	В	Residence	66	54	56
ပ	H-41	9423 VERNON DR	1	В	Residence	66	53	55
	H-42	9421 VERNON DR	1	В	Residence	66	52	54
	H-43 H-44	9415 VERNON DR 9407 VERNON DR	1 1	<u>В</u> В	Residence Residence	66 66	52 52	54 54
	H-44 H-45	1272 LYONS ST	1	В	Residence	66	52	54
	H-46	1266 LYONS ST	1	В	Residence	66	50	51
	H-47	1266 KENMORE DR	1	В	Residence	66	50	51
	H-48	1273 LYONS ST	1	В	Residence	66	54	55
	H-49	1272 KENMORE DR	1	В	Residence	66	56	58

		ROUTE 7 EXISTI	TABLE 7	REDICTED NOISE LE	VELS			
CNE	Receptor ID	Address	# of Dwelling Units	Activity Category	Land Use	NAC	Levels (Le	hour Noise q(h) in dBA)
							2018 Existing	2040 Build
	H-50	1266 KENMORE DR	1	В	Residence	66	52	54
	H-51	1260 KENMORE DR	1	В	Residence	66	47	48
	H-52	1261 KENMORE DR	1	В	Residence	66	49	51
	H-53 H-54	1267 KENMORE DR 9240 VERNON DR	1 1	B B	Residence Residence	66 66	54 56	56
	H-54 H-55	9226 VERNON DR	1 1	В	Residence	66	53	58 55
	H-56	9222 VERNON DR	1 1	В	Residence	66	54	56
	H-57	9218 VERNON DR	1	В	Residence	66	57	59
	H-58	1290 TOWLSTON RD	1	В	Residence	66	59	62
	H-59	1292 TOWLSTON RD	1	В	Residence	66	51	53
	H-60	9200 VERNON DR	1	В	Residence	66	53	55
	H-61	9320 LEESBURG PIKE	1	В	Residence	66	62	65
	H-62	9320 LEESBURG PIKE	1	В	Residence	66	72	73
	H-63	9312 LEESBURG PIKE	1	В	Residence	66	72	72
	H-64	9304 LEESBURG PIKE	1 1	B B	Residence	66	<b>71</b> 59	<b>72</b> 59
1	H-65 H-66	9247 VERNON DR 9243 VERNON DR	1 1	B R	Residence Residence	66 66	61	62
	H-67	9239 VERNON DR	1 1	В	Residence	66	61	63
1	H-68	9227 VERNON DR	1 1	В	Residence	66	59	61
	H-69	9225 VERNON DR	1	В	Residence	66	63	65
	H-70	9219 VERNON DR	1	В	Residence	66	58	61
	H-71	9217 VERNON DR	1	В	Residence	66	58	62
	H-72	9215 VERNON DR	1	В	Residence	66	58	62
	H-73	1296 TOWLSTON RD	1	С	Playground	66	64	68
	H-74	9201 Vernon Dr	1	С	Playground	66	73	76
	H-75	9201 VERNON DR	1	С	Playground	66	63	67
	H-76	9201 Vernon Dr	1 1	C C	Playground	66	73 72	76 77
	H-77 H-78	9201 Vernon Dr 9201 VERNON DR	1 1	C	Playground Playground	66 66	61	65
	H-79	9201 VERNON DR	1 1	D	School	51	59 (34)	63 (38)
	I-01	1315 BEULAH RD	1	C	Picnic Area	66	50	53
	I-02	9439 LEESBURG PIKE	1	В	Residence	66	61	64
	I-03	9439 LEESBURG PIKE	1	E	Nursery	71	68	70
	I-04	9472 DERAMUS FARM CT	1	В	Residence	66	51	53
	I-05	9470 DERAMUS FARM CT	1	В	Residence	66	52	54
	I-06	9468 DERAMUS FARM CT	1	В	Residence	66	53	55
	I-07	9466 DERAMUS FARM CT	1	В	Residence	66	55	57
	I-08	9464 DERAMUS FARM CT	1	В	Residence	66	56	58
	I-09 I-10	9462 DERAMUS FARM CT 9460 DERAMUS FARM CT	1 1	B B	Residence Residence	66 66	68 62	70 64
	I-10	9458 DERAMUS FARM CT	1 1	В	Residence	66	66	69
	I-12	9454 DERAMUS FARM CT	1 1	В	Residence	66	68	71
	I-13	9452 DERAMUS FARM CT	1	В	Residence	66	71	74
	I-14	9450 DERAMUS FARM CT	1	В	Residence	66	69	69
1	I-15	9451 DERAMUS FARM CT	1	В	Residence	66	62	64
	I-16	9455 DERAMUS FARM CT	1	В	Residence	66	52	55
	I-17	9457 DERAMUS FARM CT	1	В	Residence	66	50	53
	I-18	9453 DERAMUS FARM CT	1	В	Residence	66	57	60
	I-19	9459 DERAMUS FARM CT	1 1	В	Residence	66	57	60
1	I-20	9461 DERAMUS FARM CT	1 1	B B	Residence	66 66	55 54	59 56
1	I-21 I-22	9463 DERAMUS FARM CT 9465 DERAMUS FARM CT	1 1	В	Residence Residence	66	54	55
1	I-23	9405 DERAMOS PARM CT 9416 ATWOOD RD	1	В	Residence	66	52	55
	I-24	9413 ATWOOD RD	1 1	В	Residence	66	48	51
	I-25	9411 ATWOOD RD	1	В	Residence	66	50	53
1	I-26	9375 ROBNEL PL	1	В	Residence	66	54	58
	I-27	9373 ROBNEL PL	1	В	Residence	66	53	57
1	I-28	9371 ROBNEL PL	1	В	Residence	66	49	52
1	I-29	9369 ROBNEL PL	1	В	Residence	66	52	55
1	I-30	9367 ROBNEL PL	1	В	Residence	66	52	55
1	I-31	9365 Robnel Pl	1 1	В	Residence	66	47	50
	I-32 I-33	9363 ROBNEL PL 9361 ROBNEL PL	1 1	B B	Residence	66 66	50 48	52 51
	I-33	9361 ROBNEL PL 9359 ROBNEL PL	1	В	Residence Residence	66	48	50
	I-35	9359 ROBNEL PL 9357 ROBNEL PL	1 1	В	Residence	66	46	49
			1 1	В	Residence	66		50

		ROUTE 7 EXISTIN	TABLE 7 G AND FUTURE P	REDICTED NOISE LE	VELS			
CNE	Receptor ID	Address	# of Dwelling Units	Activity Category	Land Use	NAC		hour Noise q(h) in dBA) 2040 Build
							Existing	
	I-37	9353 ROBNEL PL	1	В	Residence	66	48	51
	I-38 I-39	9351 ROBNEL PL 1342 STOKLEY WAY	1	B B	Residence Residence	66 66	49 46	52 49
	I-39	1342 STOKLET WAT	1 1	В	Residence	66	50	53
	I-41	9374 ROBNEL PL	1 1	В	Residence	66	53	57
	I-42	9370 ROBNEL PL	1	В	Residence	66	50	54
	I-43	9368 ROBNEL PL	1	В	Residence	66	52	54
	I-44	9366 ROBNEL PL	1	В	Residence	66	50	53
	I-45	9364 ROBNEL PL	1	В	Residence	66	53	55
	I-46	9352 ROBNEL PL	1	В	Residence	66	50	53
	I-47 I-48	9350 ROBNEL PL 1338 STOKLEY WAY	1	B B	Residence Residence	66 66	50 49	53 51
	I-48	1336 STOKLET WAT	1	В	Residence	66	52	54
	I-50	1334 STOKLEY WAY	1 1	В	Residence	66	56	60
	I-51	9353 MILDRED CT	1	В	Residence	66	57	60
	I-52	9355 MILDRED CT	1	В	Residence	66	57	61
	I-53	9357 MILDRED CT	1	В	Residence	66	55	59
	I-54	9359 MILDRED CT	1	В	Residence	66	52	56
_	I-55	9360 MILDRED CT	1	В	Residence	66	70	73
CNE	I-56	9358 MILDRED CT	1	В	Residence	66	70	74
ច	I-57	9356 MILDRED CT	1	В	Residence	66	66	69
	I-58	9352 MILDRED CT	1	В	Residence	66	70 67	73 70
	I-59 I-60	9350 Mildred Ct 1331 STOKLEY WAY	1	B B	Residence Residence	66 66	64	67
	I-61	1333 STOKLEY WAY	1	В	Residence	66	57	60
	I-62	1335 STOKLEY WAY	1 1	В	Residence	66	54	57
	I-63	1337 STOKLEY WAY	1	В	Residence	66	52	55
	I-64	1339 STOKLEY WAY	1	В	Residence	66	52	54
	I-65	9320 ROBNEL PL	1	В	Residence	66	52	55
	I-66	1336 VANETTA LN	1	В	Residence	66	54	57
	I-67	1334 VANETTA LN	1	В	Residence	66	55	58
	I-68	1332 VANETTA LN	1	В	Residence	66	57	61
	I-69	1330 VANETTA LN	1	B B	Residence	66	63	67
	I-70 I-71	1331 VANETTA LN 1333 VANETTA LN	1	В	Residence Residence	66 66	64 59	68 62
	I-72	1335 VANETTA LN	1 1	В	Residence	66	55	59
	I-73	1337 VANETTA LN	1	В	Residence	66	54	57
	I-74	9316 ROBNEL PL	1	В	Residence	66	53	56
	I-75	9314 ROBNEL PL	1	В	Residence	66	54	58
	I-76	9310 ROBNEL PL	1	В	Residence	66	55	58
	I-77	9306 ROBNEL PL	1	В	Residence	66	54	57
	I-78	9304 ROBNEL PL	1	В	Residence	66	56	59
	I-79	9300 ROBNEL PL	1	В	Residence	66	58	61
	I-80 I-81	9301 ROBNEL PL 9303 ROBNEL PL	1	B B	Residence Residence	66 66	57 52	60 55
	I-82	9305 ROBNEL PL 9305 ROBNEL PL	1	В	Residence	66	53	56
	I-83	9307 ROBNEL PL	1	В	Residence	66	53	56
	I-84	9309 ROBNEL PL	1	В	Residence	66	52	55
	I-85	9311 ROBNEL PL	1	В	Residence	66	52	54
	I-86	9313 ROBNEL PL	1	В	Residence	66	51	54
	I-87	9315 ROBNEL PL	1	В	Residence	66	51	54
	I-88	9317 ROBNEL PL	1	В	Residence	66	52	55
	I-89 I-90	9319 ROBNEL PL 9321 ROBNEL PL	1 1	B B	Residence Residence	66 66	52 52	56 55
	I-90	9321 ROBNEL PL 9323 ROBNEL PL	1	В	Residence	66	51	55
	I-91	9318 KILBY GLEN DR	1	В	Residence	66	50	53
	I-93	9316 KILBY GLEN DR	1	В	Residence	66	49	52
	I-94	9314 KILBY GLEN DR	1	В	Residence	66	49	52
	I-95	9312 KILBY GLEN DR	1	В	Residence	66	49	52
	I-96	9310 KILBY GLEN DR	1	В	Residence	66	48	51
	I-97	9308 KILBY GLEN DR	1	В	Residence	66	48	51
	I-98	9306 KILBY GLEN DR	1	В	Residence	66	49	51
	I-99	9302 KILBY GLEN DR	1	В	Residence	66	50	53
	I-100	9300 KILBY GLEN DR	1	B B	Residence	66	50	53 52
	I-101 I-102	9298 KILBY GLEN DR 9296 KILBY GLEN DR	1	В	Residence Residence	66 66	50 50	52

	TABLE 7 ROUTE 7 EXISTING AND FUTURE PREDICTED NOISE LEVELS										
		ROUTE 7 EXISTII	NG AND FUTURE P	REDICTED NOISE LE	VELS						
CNE	Receptor	Address	# of Dwelling Units	Activity Category	Land Use	NAC		hour Noise q(h) in dBA)			
O	וטו		Units			2	2018 Existing	2040 Build			
	I-103	9297 KILBY GLEN DR	1	В	Residence	66	48	52			
	I-104	9299 KILBY GLEN DR	1	В	Residence	66	48	51			
	I-105	1324 TOWLSTON RD	1	В	Residence	66	44	49			
	I-106	1322 TOWLSTON RD 1320 TOWLSTON RD	1 1	В	Residence	66	47	51			
	I-107	1320 TOWLSTON RD	1 1	B B	Residence Residence	66 66	48 47	52 50			
	I-109	1314 TOWLSTON RD	1	В	Residence	66	52	55			
	I-110	1316 TOWLSTON RD	1 1	В	Residence	66	50	53			
	I-111	1316 TOWLSTON RD	1	В	Residence	66	54	57			
	I-112	1310 TOWLSTON RD	1	В	Residence	66	53	56			
	J-01	1301 TOWLSTON RD	1	В	Residence	66	69	70			
	J-02	1303 TOWLSTON RD	1	В	Residence	66	68	67			
	J-03	1305 TOWLSTON RD	1	В	Residence	66	58	59			
	J-04	1308 TRAP RD	1 1	С	Cemetery	66	71	71			
	J-05 J-06	1308 TRAP RD 1308 TRAP RD	1 1	C C	Cemetery Cemetery	66 66	73 73	73 73			
	J-06 J-07	1308 TRAP RD	1	C	Cemetery	66	67	68			
	J-08	1308 TRAP RD	1	C	Cemetery	66	67	69			
	J-09	1308 TRAP RD	1	С	Cemetery	66	67	68			
	J-10	1308 TRAP RD	1	С	Cemetery	66	61	64			
	J-11	1308 TRAP RD	1	С	Cemetery	66	63	65			
	J-12	1308 TRAP RD	1	С	Cemetery	66	63	65			
	J-13	1308 TRAP RD	1	С	Cemetery	66	64	66			
	J-14	1308 TRAP RD	1	С	Cemetery	66	64	66			
	J-15 J-16	1305 TOWLSTON RD 1308 TRAP RD	1 1	C C	Cemetery Cemetery	66 66	58 60	62 62			
l _	J-10 J-17	1308 TRAP RD	1	C	Cemetery	66	60	63			
CNE J	J-17	1308 TRAP RD	1	C	Cemetery	66	60	62			
2	J-19	1308 TRAP RD	1 1	C	Cemetery	66	60	61			
	J-20	1308 TRAP RD	1	С	Cemetery	66	57	59			
	J-21	1308 TRAP RD	1	С	Cemetery	66	56	58			
	J-22	1308 TRAP RD	1	С	Cemetery	66	56	58			
	J-23	9201 LEESBURG PIKE	1	D	Church	51	70 (45)	72 (47)			
	J-24	1319 TOWLSTON RD	1	В	Residence	66	53	59			
	J-25	1321 TOWLSTON RD	1	В	Residence	66	49	53			
	J-26 J-27	1323 SCHUMAN CT 1322 SCHUMAN CT	1 1	B B	Residence Residence	66 66	48 48	51 53			
	J-28	1320 SCHUMAN CT	1	В	Residence	66	49	54			
	J-29	1316 TRAP RD	1 1	В	Residence	66	53	56			
	J-30	9201 WINDSOR MEADOWS LN	1	В	Residence	66	55	57			
	J-31	9203 WINDSOR MEADOWS LN	1	В	Residence	66	52	54			
	J-32	9207 WINDSOR MEADOWS LN	1	В	Residence	66	51	53			
	J-33	9207 WINDSOR MEADOWS LN	1	В	Residence	66	50	53			
	J-34	9202 WINDSOR MEADOWS LN	1	В	Residence	66	51	53			
	J-35	9200 WINDSOR MEADOWS LN	1 1	В	Residence	66	54	57			
	K-01 K-02	1301 TRAP RD 1301 TRAP RD	1 1	B D	Residence Church	66 51	68 60 (35)	70 61 (36)			
	K-02	1301 TRAP RD	1	С	Playground	66	62	63			
	K-03	9105 LEESBURG PIKE	1	В	Residence	66	67	68			
	K-05	9101 LEESBURG PIKE	1	D	Church	51	60 (35)	64 (39)			
	K-06	9118 LUCKY ESTATES DR	1	В	Residence	66	57	59			
	K-07	9122 LUCKY ESTATES DR	1	В	Residence	66	53	55			
	K-08	9126 Lucky Estates Dr	1	В	Residence	66	50	52			
	K-09	9123 LUCKY ESTATES DR	1	В	Residence	66	45	48			
	K-10	9119 LUCKY ESTATES DR	1	В	Residence	66	50	53			
	K-11 K-12	9115 LUCKY ESTATES DR 9109 LUCKY ESTATES DR	1 1	B B	Residence Residence	66 66	57 61	60			
	K-12 K-13	9105 LUCKY ESTATES DR	1 1	В	Residence	66	59	62			
	K-14	9101 LUCKY ESTATES DR	1	В	Residence	66	66	69			
	K-15	9030 TIMBERWOLF CT	1	В	Residence	66	57	59			
	K-16	9028 TIMBERWOLF CT	1	В	Residence	66	58	60			
	K-17	9026 TIMBERWOLF CT	1	В	Residence	66	61	63			
	K-18	9031 TIMBERWOLF CT	1	В	Residence	66	56	59			
<u>×</u>	K-19	9029 TIMBERWOLF CT	1	В	Residence	66	58	61			
S	K-20	1402 WOLFTRAP RUN RD	1	В	Residence	66	56	59			
ı	K-21	1404 WOLFTRAP RUN RD	1	В	Residence	66	55	58			

		ROUTE 7 EXIS	TABLE 7	REDICTED NOISE LE	VELS			
CNE	Receptor ID	Address	# of Dwelling Units	Activity Category	Land Use	NAC	Levels (Le	hour Noise q(h) in dBA)
							2018 Existing	2040 Build
	K-22	1406 WOLFTRAP RUN RD	1	В	Residence	66	53	56
	K-23	9024 TRAILRIDGE CT	1	В	Residence	66	64	67
	K-24	9022 TRAILRIDGE CT	1	В	Residence	66	64	67
	K-25	9023 TRAILRIDGE CT	1	В	Residence	66	58	61
	K-26 K-27	9020 TRAILRIDGE CT	1 1	B B	Residence Residence	66	59 55	62 58
	K-27	9021 TRAILRIDGE CT 1405 WOLFTRAP RUN RD	1	В	Residence	66 66	51	54
	K-28	1407 WOLFTRAP RUN RD	1	В	Residence	66	51	55
	K-30	1409 WOLFTRAP RUN RD	1	В	Residence	66	48	52
	K-31	9024 WEATHERWOOD CT	1	В	Residence	66	47	51
	K-32	1440 LAUREL HILL RD	1	В	Residence	66	52	56
	K-33	9021 WEATHERWOOD CT	1	В	Residence	66	50	54
	K-34	9023 WEATHERWOOD CT	1	В	Residence	66	47	49
	K-35	9025 WEATHERWOOD CT	1	В	Residence	66	46	48
	K-36	9011 LEESBURG PIKE	1	С	Playground	66	53	57
	K-37	9011 LEESBURG PIKE	1	D	School	51	60 (35)	69 (44)
	K-38	8909 LEESBURG PIKE	1	D	Church	51	62 (37)	65(40)
	K-39	8909 LEESBURG PIKE	1	C B	Playground Residence	66	50	51
	L-01 L-02	9120 LEESBURG PIKE 9116 LEESBURG PIKE	1 1	В	Residence	66 66	67 63	69 65
	L-02 L-03	9112 LEESBURG PIKE	1	В	Residence	66	66	69
	L-03	9106 LEESBURG PIKE	1	В	Residence	66	63	66
	L-05	9100 LEESBURG PIKE	1	В	Residence	66	69	72
	L-06	1377 DREAMWEAVER CT	1	В	Residence	66	61	64
	L-07	1355 DREAMWEAVER CT	1	В	Residence	66	54	58
	L-08	1325 ROYAL ESTATES DR	1	В	Residence	66	55	58
	L-09	1327 ROYAL ESTATES DR	1	В	Residence	66	61	65
	L-10	8964 OLD TOLSON MILL RD	1	В	Residence	66	56	60
	L-11	9026 LEESBURG PIKE	1	В	Residence	66	69	71
	L-12	9022 LEESBURG PIKE	1	В	Residence	66	71	73
	L-13	8973 OLD TOLSON MILL RD	1	С	Playground	66	62	65
	L-14	8980 Brook Rd	1	С	Volleyball	66	57	61
	L-15	8980 BROOK RD	1	D	Church	51	61 (36)	63 (38)
	L-16	8970 BROOK RD	1	В	Residence	66	54	58
	L-17	8962 BROOK RD	1	В	Residence	66	53	57
	L-18 L-19	8954 BROOK RD 8965 BROOK RD	1 1	B B	Residence Residence	66 66	52 50	56 53
	L-19 L-20	8916 GALLANT GREEN DR	1	В	Residence	66	51	54
	L-20	8977 BROOK RD	1	В	Residence	66	52	55
	L-22	8983 BROOK RD	1	В	Residence	66	57	60
	L-23	8991 BROOK RD	1	D	Church	51	62 (37)	62 (37)
_	L-24	8991 BROOK RD	1	В	Residence	66	58	59
CNE	L-25	8913 GALLANT GREEN DR	1	В	Residence	66	51	54
ਹ	L-26	8909 GALLANT GREEN DR	1	В	Residence	66	48	52
	L-27	8905 GALLANT GREEN DR	1	В	Residence	66	46	48
	L-28	8901 GALLANT GREEN DR	1	В	Residence	66	44	46
	L-29	1334 GUNNELL CT	1	В	Residence	66	43	44
	L-30	1336 GUNNELL CT	1	В	Residence	66	45	47
	L-31	1342 GUNNELL CT	1	В	Residence	66	47	49
	L-32 L-33	8815 GALLANT GREEN DR 1335 GUNNELL CT	1 1	B B	Residence Residence	66 66	41	43
	L-33	1339 GUNNELL CT	1	В	Residence	66	43	45
	L-34 L-35	1343 GUNNELL CT	1	В	Residence	66	45	46
	L-36	8832 LEWINSVILLE RD	1	В	Residence	66	57	58
	L-37	8826 LEWINSVILLE RD	1	В	Residence	66	57	59
	L-38	8820 LEWINSVILLE RD	1	В	Residence	66	58	61
	L-39	8814 LEWINSVILLE RD	1	В	Residence	66	56	59
	L-40	1388 WOODSIDE DR	1	В	Residence	66	57	60
	L-41	1382 WOODSIDE DR	1	В	Residence	66	45	48
	L-42	1378 WOODSIDE DR	1	В	Residence	66	43	46
	L-43	1374 WOODSIDE DR	1	В	Residence	66	41	43
	L-44	8805 GALLANT GREEN DR	1	В	Residence	66	41	44
	L-45	8809 GALLANT GREEN DR	1	В	Residence	66	42	44
	L-46	1379 WOODSIDE DR	1	В	Residence	66	42	44
	L-47	1379 WOODSIDE DR	1	В	Residence	66	43	45
	L-48	1383 WOODSIDE DR	1	В	Residence	66	50	52

		ROUTE 7 EXIS	TABLE 7	REDICTED NOISE LE	VELS			
CNE	Receptor ID	Address	# of Dwelling Units	Activity Category	Land Use	NAC		nour Noise q(h) in dBA)
)	15		Units			_	2018 Existing	2040 Build
	L-49	1387 WOODSIDE DR	1	В	Residence	66	58	60
	M-01	8934 LEESBURG PIKE	1	В	Residence	66	61	Aquired
	M-02	8808 MIRADOR PL	1	В	Residence	66	57	60
	M-03	8806 MIRADOR PL	1	В	Residence	66	60	62
	M-04	8804 MIRADOR PL	1	В	Residence	66	58	61
	M-05	8802 MIRADOR PL	1	В	Residence	66	56	58
	M-06	1400 WOODHURST BLVD	1	В	Residence	66	53	55
	M-07	8800 MIRADOR PL	1	В	Residence	66	54	57
	M-08 M-09	8809 MIRADOR PL	1 1	B B	Residence	66	60 58	65 62
	M-10	8807 MIRADOR PL 8805 MIRADOR PL	1	В	Residence Residence	66	59	62
	M-10 M-11	8803 MIRADOR PL	1	В	Residence	66	60	63
	M-12	8801 MIRADOR PL	1	В	Residence	66	62	64
	M-13	1406 WOODHURST BLVD	1	В	Residence	66	58	61
	M-14	1407 WOODHURST BLVD	1	В	Residence	66	57	60
	M-15	1405 WOODHURST BLVD	1	В	Residence	66	53	56
	M-16	1403 WOODHURST BLVD	1	В	Residence	66	51	54
1	M-17	8805 PRESTWOULD PL	1	В	Residence	66	49	52
	M-18	8801 PRESTWOULD PL	1	В	Residence	66	48	51
	M-19	1401 WOODHURST BLVD	1	В	Residence	66	60	62
	M-20	8800 PRESTWOULD PL	1	В	Residence	66	58	61
	M-21	1408 WOODHURST BLVD	1	В	Residence	66	61	63
	M-22	1410 WOODHURST BLVD	1	В	Residence	66	59	61
	M-23	1412 WOODHURST BLVD	1	В	Residence	66	54	57
	M-24	1418 WOODHURST BLVD	1	В	Residence	66	59	61
I≥	M-25	1424 WOODHURST BLVD	1	В	Residence	66	62	64
CNE M	M-26	1420 WOODHURST BLVD	1	В	Residence	66	52	55
ົວ	M-27	1426 WOODHURST BLVD	1	В	Residence	66	59	61
	M-28	1428 WOODHURST BLVD	1	В	Residence	66	59	62
	M-29	1430 WOODHURST BLVD	1	В	Residence	66	59	61
	M-30	1411 WOODHURST BLVD	1	В	Residence	66	54	57
	M-31	1413 WOODHURST BLVD	1	В	Residence	66	51	54
	M-32	1415 WOODHURST BLVD	1	В	Residence	66	52	55
	M-33	1417 WOODHURST BLVD	1	В	Residence	66	52	55
	M-34	1421 WOODHURST BLVD	1	В	Residence	66	51	54
	M-35	1423 WOODHURST BLVD	1	В	Residence	66	51	54
	M-36	1427 WOODHURST BLVD	1	В	Residence	66	52	55
	M-37	1431 WOODHURST BLVD	1	В	Residence	66	48	51
	M-38	1429 WOODHURST BLVD	1	В	Residence	66	48	51
	M-39	1429 WOODHURST BLVD 1477 MAYHURST BLVD	1	В	Residence	66	50	54
	M-40		1	В	Residence	66	61	64
	M-41 M-42	1475 MAYHURST BLVD 1473 MAYHURST BLVD	1 1	B B	Residence	66 66	62 60	65 63
1	M-43	1473 MAYHURST BLVD	1	В	Residence Residence	66	59	63
1	M-44	1469 MAYHURST BLVD	1	В	Residence	66	58	62
1	M-45	1467 MAYHURST BLVD	1	В	Residence	66	52	57
1	M-46	1441 MAYHURST BLVD	1	В	Residence	66	52	55
	M-47	1439 MAYHURST BLVD	1	В	Residence	66	56	60
	M-48	1435 MAYHURST BLVD	1	В	Residence	66	47	52
1	M-49	1437 MAYHURST BLVD	1	В	Residence	66	61	65
1	M-50	1433 MAYHURST BLVD	1	В	Residence	66	57	61
1	M-51	1431 MAYHURST BLVD	1	В	Residence	66	61	65
	M-52	1429 MAYHURST BLVD	1	В	Residence	66	62	65
	N-01	8850 GLENRIDGE CT	1	В	Residence	66	65	67
	N-02	8852 GLENRIDGE CT	1	В	Residence	66	60	63
1	N-03	8854 GLENRIDGE CT	1	В	Residence	66	58	61
1	N-04	8856 GLENRIDGE CT	1	В	Residence	66	56	59
1	N-05	8858 GLENRIDGE CT	1	В	Residence	66	55	58
1	N-06	1427 LAUREL HILL RD	1	В	Residence	66	54	56
	N-07	8860 GLENRIDGE CT	1	В	Residence	66	54	57
	N-08	8862 GLENRIDGE CT	1	В	Residence	66	53	56
1	N-09	1429 LAUREL HILL RD	1	В	Residence	66	50	52
1	N-10	8864 GLENRIDGE CT	1	В	Residence	66	52	54
1	N-11	1431 LAUREL HILL RD	1	В	Residence	66	49	51
	N-12	1433 LAUREL HILL RD	1	В	Residence	66	48	50
l	N-13	1435 LAUREL HILL RD	1	В	Residence	66	46	50

		ROUTE 7 EXIST	TABLE 7	PREDICTED NOISE LE	VELS			
CNE	Receptor ID	Address	# of Dwelling Units	Activity Category	Land Use	NAC	Levels (Le	nour Noise q(h) in dBA)
							2018 Existing	2040 Build
	N-14	1437 LAUREL HILL RD	1	В	Residence	66	46	49
	N-15	1439 LAUREL HILL RD	1	В	Residence	66	44	48
	N-16	8866 GLENRIDGE CT	1	В	Residence	66	50	53
	N-17 N-18	8868 GLENRIDGE CT 8869 GLENRIDGE CT	1 1	B B	Residence Residence	66 66	51 50	54 53
	N-19	8867 GLENRIDGE CT	1	В	Residence	66	52	55
	N-20	8865 GLENRIDGE CT	1	В	Residence	66	51	54
	N-21	8863 GLENRIDGE CT	1	В	Residence	66	49	54
	N-22	8861 GLENRIDGE CT	1	В	Residence	66	50	54
	N-23	8859 GLENRIDGE CT	1	В	Residence	66	46	52
	N-24	8857 GLENRIDGE CT	1	В	Residence	66	48	53
	N-25	8855 GLENRIDGE CT	1	В	Residence	66	54	57
	N-26	8853 GLENRIDGE CT	1	В	Residence	66	56	59
	N-27 N-28	8851 GLENRIDGE CT 1484 OLD ASH GRV	1 1	B B	Residence Residence	66 66	64 61	66 64
	N-29	1482 OLD ASH GRV	1	В	Residence	66	56	60
	N-30	1488 OLD ASH GRV	1 1	В	Residence	66	47	51
	N-31	1486 OLD ASH GRV	1	В	Residence	66	53	57
	N-32	1492 OLD ASH GRV	1	В	Residence	66	47	53
	N-33	1498 OLD ASH GRV	1	В	Residence	66	43	49
	N-34	1496 OLD ASH GRV	1	В	Residence	66	44	49
	N-35	1494 OLD ASH GRV	1	В	Residence	66	45	50
	N-36	1490 OLD ASH GRV	1	В	Residence	66	45	50
	N-37	1440 CARRINGTON RIDGE LN	1	В	Residence	66	47	51
z	N-38 N-39	1442 CARRINGTON RIDGE LN	1 1	B B	Residence Residence	66 66	45 47	50 52
CNE N	N-39 N-40	1444 CARRINGTON RIDGE LN 8826 JARRETT VALLEY DR	1	В	Residence	66	47	50
ပ	N-41	8826 JARRETT VALLEY DR	1	В	Residence	66	46	53
	N-42	1448 CARRINGTON RIDGE LN	1	В	Residence	66	46	52
	N-43	1446 CARRINGTON RIDGE LN	1	В	Residence	66	47	52
	N-44	1438 CARRINGTON RIDGE LN	1	В	Residence	66	49	54
	N-45	1436 CARRINGTON RIDGE LN	1	В	Residence	66	49	54
	N-46	1434 CARRINGTON RIDGE LN	1	В	Residence	66	57	60
	N-47	1432 CARRINGTON RIDGE LN	1	В	Residence	66	60	64
	N-48 N-49	1430 CARRINGTON RIDGE LN 1433 CARRINGTON RIDGE LN	1 1	B B	Residence	66 66	64	69 67
	N-49 N-50	1433 CARRINGTON RIDGE LN 1433 CARRINGTON RIDGE LN	1 1	В	Residence Residence	66	56	61
	N-51	1435 CARRINGTON RIDGE LN	1	В	Residence	66	48	53
	N-52	1437 CARRINGTON RIDGE LN	1	В	Residence	66	47	52
	N-53	1439 CARRINGTON RIDGE LN	1	В	Residence	66	46	51
	N-54	1447 CARRINGTON RIDGE LN	1	В	Residence	66	45	51
	N-55	1449 CARRINGTON RIDGE LN	1	В	Residence	66	45	50
	N-56	8820 JARRETT VALLEY DR	1	В	Residence	66	45	49
1	N-57	8818 JARRETT VALLEY DR	1	В	Residence	66	46	50
1	N-58	8816 JARRETT VALLEY DR	1	В	Residence	66	45	50
	N-59 N-60	8814 JARRETT VALLEY DR 1492 BROADSTONE PL	1 1	B B	Residence Residence	66 66	47 52	52 57
	N-60 N-61	1492 BROADSTONE PL 1490 BROADSTONE PL	1	В	Residence	66	52	56
	N-62	1488 BROADSTONE PL	1	В	Residence	66	52	56
1	N-63	1486 BROADSTONE PL	1	В	Residence	66	51	56
1	N-64	1484 BROADSTONE PL	1	В	Residence	66	50	54
1	N-65	1485 BROADSTONE PL	1	В	Residence	66	52	57
1	N-66	1487 BROADSTONE PL	1	В	Residence	66	52	56
1	N-67	1489 BROADSTONE PL	1	В	Residence	66	54	59
1	N-68	1491 BROADSTONE PL	1	В	Residence	66	53	58
1	N-69	1493 BROADSTONE PL	1 1	В	Residence	66	57	61
1	N-70 N-71	8810 JARRETT VALLEY DR 1404 STANBRIDGE PL	1 1	B B	Residence Residence	66 66	57 63	61 68
	N-71 N-72	1404 STANBRIDGE PL 1487 BROADSTONE PL	1	В	Residence	66	61	66
	N-72 N-73	1409 Stanbridge PI	2	В	Residence	66	59	65
1	N-74	1415 Stanbridge PI	2	В	Residence	66	59	65
	N-75	0	2	В	Residence	66	61	68
	N-76	0	2	В	Residence	66	65	72
	N-77	8800 JARRETT VALLEY DR	1	D	Church	51	57 (32)	66 (41)
	N-78	8801 JARRETT VALLEY DR	1	В	Residence	66	70	73
	PTR-01	9900 Leesburg Pike	1	С	Trail	66	_	66

			TABLE 7		. (E. 0			
		ROUTE / EXISTING	AND FUTURE P	REDICTED NOISE LE	VELS		Laudanti	hann Natas
CNE	Receptor	Address	# of Dwelling Units	Activity Category	Land Use	NAC		nour Noise q(h) in dBA)
J			Office				2018 Existing	2040 Build
	PTR-02	9900 Leesburg Pike	1	С	Trail	66		70
	PTR-03	9900 Leesburg Pike	1	С	Trail	66		70
	PTR-04	9900 Leesburg Pike	1	С	Trail	66		70
	PTR-05	9900 Leesburg Pike	1	С	Trail	66	P	71
	PTR-06	9900 Leesburg Pike	1	С	Trail	66	r	71
	PTR-07	9900 Leesburg Pike	1	С	Trail	66	0	71
l _	PTR-08	9900 Leesburg Pike	1	С	Trail	66	р • о	71
īai	PTR-09	9900 Leesburg Pike	1	С	Trail	66	s	70
Proposed Trail	PTR-10	9900 Leesburg Pike	1	С	Trail	66	e	69
Se	PTR-11	9900 Leesburg Pike	1	С	Trail	66	d	69
&	PTR-12	9900 Leesburg Pike	1	С	Trail	66	_	69
Ϋ́	PTR-13	9900 Leesburg Pike	1	С	Trail	66	l t	68
	PTR-14	9900 Leesburg Pike	1	С	Trail	66	ì	70
	PTR-15	9900 Leesburg Pike	1	С	Trail	66	a	73
	PTR-16	9900 LEESBURG PIKE	1	С	Trail	66	. i	70
	PTR-17	9900 LEESBURG PIKE	1	С	Trail	66	<u> </u>	67
	PTR-18	9900 LEESBURG PIKE	1	С	Trail	66	_	65
	PTR-19	9900 LEESBURG PIKE	1	С	Trail	66		64
	PTR-20	9900 LEESBURG PIKE	1	С	Trail	66	_	63
	PTR-21	9900 LEESBURG PIKE	1	С	Trail	66		65
	TR-01	9900 Leesburg Pike	1	С	Trail	66	56	58
	TR-02	9900 Leesburg Pike	1	С	Trail	66	57	60
	TR-03	9900 Leesburg Pike	1	С	Trail	66	58	60
	TR-04	9900 Leesburg Pike	1	С	Trail	66	60	62
	TR-05	9900 Leesburg Pike	1	С	Trail	66	62	63
	TR-06	9900 Leesburg Pike	1	С	Trail	66	63	64
	TR-07	9900 Leesburg Pike	1	С	Trail	66	64	
	TR-08	9900 Leesburg Pike	1	С	Trail	66	67	relocated
	TR-09	9900 Leesburg Pike	1	С	Trail	66	66	trail
	TR-10	9900 Leesburg Pike	1	С	Trail	66	63	
I≡	TR-11	9900 Leesburg Pike	1	С	Trail	66	62	67
Existing Trail	TR-12	9900 Leesburg Pike	1	С	Trail	66	61	65
ng	TR-13	9900 Leesburg Pike	1	С	Trail	66	59	63
isti	TR-14	9900 Leesburg Pike	1	С	Trail	66	58	62
Ä	TR-15	9900 Leesburg Pike	1	С	Trail	66	72	-
	TR-16	9900 LEESBURG PIKE	1	С	Trail	66	72	1
	TR-17	9900 LEESBURG PIKE	1	С	Trail	66	70	
	TR-18	9900 LEESBURG PIKE	1	С	Trail	66	68	relocated
	TR-19	9900 LEESBURG PIKE	1	С	Trail	66	66	trail
	TR-20	9900 Leesburg Pike	1	С	Trail	66	64	4
	TR-21	9900 LEESBURG PIKE	1	С	Trail	66	63	
	TR-22	9900 LEESBURG PIKE	1	С	Trail	66	62	
	TR-23	9900 LEESBURG PIKE	1	С	Trail	66	60	63
	TR-24	9900 LEESBURG PIKE	1	С	Trail	66	61	63
	TR-25	9900 LEESBURG PIKE	1	С	Trail	66	60	63
	TR-26	9900 LEESBURG PIKE	1	С	Trail	66	60	62

		TABLE 11		
	CNE A- BARRIER A	1 OPTIMIZED I	BARRIER RESULTS	
Receptor ID	# of Dwelling /Recreational Units	2040 Loudes	t Hour Predicted Future I dBA	Noise Levels Leq(h) in
		No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)
		Barrier A1		
A-01	1	52	52	0
A-02	1	55	55	0
A-03	1	57	57	2
A-04	1	61	60	1
A-05	1	60	59	1
A-06	1	65	58	6
A-07	1	63	55	8
A-08	1	59	53	6
A-09	1	54	51	3
A-10	1	56	55	1
A-11	1	54	54	0
A-12	1	53	53	0
A-13	1	53	52	2
A-14	1	54	52	2
A-15	1	55	53	3
A-16	1	56	53	3
A-17	1	59	55	5
A-18	1	67	60	7
A-19	1	65	64	1
A-20	1	59	59	1
A-21	1	50	50	0
A-22	1	50	50	0
A-23	1	49	48	1
A-24	1	49	49	0
A-25	1	48	47	1
A-26	1	48	47	1
A-27	1	48	47	1
A-28	1	50	49	1
A-29	1	51	50	1
A-30	1	53	53	1
A-31	1	56	55	1
A-32	1	56	56	0
A-33	1	57 (32)	56.6 (31.6)	0
*	Insertion Loss	` ,	nay be different due to roui	nding
66		Indicates noise in	mpact (NAC only)	
5			t a 5 dBA benefit	

		TABLE 12				
	CNE A- BARRIER A	A2 OPTIMIZED E	BARRIER RESULTS			
Receptor ID	# of Dwelling /Recreational Units	2040 Loudes	Noise Levels Leq(h) in			
· ·	· ·	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)		
		Barrier A2				
A-56	1	66	59	6		
A-57	1	61	56	5		
A-58	1	60	53	7		
A-59	1	61	53	8		
A-60	1	61	53	8		
A-61	1	59	51	8		
A-62	1	63	55	8		
A-63	1	60	53	7		
A-64	1	57	52	5		
A-65	1	65	57	7		
A-66	1	63	58	6		
A-67	1	63	58	6		
A-68	1	63	58	6		
A-69	1	62	59	3		
A-70	1	65	64	1		
A-71	1	63	62	1		
A-72	1	56	54	2		
A-73	1	56	53	3		
A-74	1	56	52	3		
*	Insertion Loss	(IL) sound levels n	nay be different due to rou	nding		
66	Indicates noise impact (NAC only)					
5		Indicates at leas	t a 5 dBA benefit			

	CNE B- BARRIER B1-B6	TABLE 13	ZED BADDIED DESIII	Te
			t Hour Predicted Future dBA	
Receptor ID	# of Dwelling /Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)
	Bi	arrier B1-B5 and		
B-01	<u></u>	71 (46)	72 (46)	0
B-02	 1	52.3	52	0
B-03	 1	67 (42)	65 (40)	2
B-04	 1	61	60	1
B-05	 1	57	56	1
B-06	 1	63	61	2
B-07	 1	73	65	8
B-08	 1	72	64	8
B-09	 1	56	51	6
B-10	 1	57	51	6
B-11	 1	55	49	6
B-12		61	52	8
B-12		72	62	10
B-13	<u>'</u> 1	66	58	9
B-15		60	52	8
B-16		56	49	7
B-17		54	48	6
B-18	<u>'</u> 1	52	47	5
B-18	1	57	52	5
B-19 B-20	1	62	55	7
B-20 B-21	1 1			
		69	61	8
B-22	1	70	63	7
B-23	1	57	53	5
B-24	1	57 (32)	52 (27)	5
B-25	1	67	58	8
B-26	1	62	55	8
B-27	1	60	53	7
B-28	1	55	50	6
B-29	1	57	51	6
B-30	11	58	53	5
B-31	1	67	61	6
B-32	1	65	62	3
B-33	1	70	64	6
B-34	1	70	61	10
B-35	1	71	60	11
B-36	1	72	59	12
B-37	1	64	55	8
B-38	1	63	54	9
B-39	1	62	55	7
B-40	1	60	54	6
B-41	1	62	56	5
B-42	1	54	51	4
B-43	1	54	49	5
B-44	1	52	47	5
B-45	1	54	47	7
B-46	1	53	46	7
B-47	1	55	47	7
B-48	1	56	48	8
B-49	1	54	48	6
B-50	1	59	50	9
B-51	 1	59	52	7
B-52	 1	58	52	6

	CNE B- BARRIER B1-B6	and D1 OPTIMI	ZED BARRIER RESULT	rs
Receptor ID	# of Dwelling /Recreational Units	2040 Loudes	t Hour Predicted Future I dBA	Noise Levels Leq(h)
Keceptor ID	# 01 Dwelling /Necreational office	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)
	В	arrier B1-B5 and	D1	
B-53	1	61	53	8
B-54	1	63	53	10
B-55	 1	71	57	14
B-56	1	68	60	7
B-57	1	71	62	9
B-58	1	57	52	5
B-59	 1	62	56	6
B-60	 1	65	58	7
B-61	 1	67	60	7
B-62	 1	71	62	 8
B-63	 1	65	61	4
B-64		61	57	4
B-65	1	57	55	2
B-66		57	55	2
B-67	 1	57	55	2
B-68	 1	57	55	2
B-69		57	53	4
B-70		54	49	5
B-71		54	49	5
B-72	<u>'</u> 1	54	52	2
D-01		68	63	5
D-02		66	60	6
D-02		64	59	6
D-03		62	57	5
D-04 D-05		63	59	4
D-06	<u>'</u> 1	64	60	4
D-07		62	58	4
D-08		61	57	4
D-09	<u>.</u> 1	60	56	5
D-09		59	54	5
D-10		60	56	4
D-11	1	60	57	3
D-12 D-13	1	61	60	<u></u>
D-13 D-14	1 1	58	55	3
D-14 D-15		57	53	4
D-13		56	52	4
D-10 D-17		57	55	3
D-17 D-18	1	60	59	
D-18	1	59	57	1
D-19 D-20		56	54	3
D-20 D-21		55	52	4
D-21 D-22	1 1	54	51	3
D-22 D-23		55	53	2
D-23	1	58	57	1
D-24 D-25	1 1	62	56	6
D-25 D-26	1 1	63	57	6
D-26 D-27	1 1	59	54	5
D-27 D-28	1 1	61	55	<u> </u>
D-28 D-29			55	
	1	62	57	6
D-30	1	60	J 54	5

		TABLE 13						
CNE B- BARRIER B1-B6 and D1 OPTIMIZED BARRIER RESULTS								
Receptor ID	# of Dwelling /Recreational Units	2040 Loudest Hour Predicted Future Noise Levels Leq(h						
		No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)				
	Bar	rier B1-B5 and	D1					
66	Indicates noise impact (NAC only)							
5		Indicates at leas	t a 5 dBA benefit					

		TABLE 14			
	CNE D/E- BARRIER D2 and	E1-E4 OPTII	MIZED BARRIER RE	SULTS	
Receptor ID	# of Dwelling /Recreational Units	2040 Loudest Hour Predicted Future Noise Levels Leq(h) in dBA			
recopiol 15		No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	
	Barr	ier D2 and E1	-E4		
E-01	1	62	57	5	
E-02	1	66	60	6	
E-03	1	63	57	6	
E-04	1	69	60	8	
E-05	1	67	60	8	
E-06	1	71	62	9	
E-07	1	66	60	5	
E-08	1	64	59	5	
E-09	1	61	56	4	
E-10	1	59	55	5	
E-11	1	58	53	5	
E-12	1	55	51	5	
E-13	1	53	49	5	
E-14	1	54	50	4	
E-15	1	51	48	3	
E-16	1	48	44	4	
E-17	1	52	48	4	
E-18	1	49	46	3	
E-19	1	49	45	5	
E-20	1	48	44	4	
E-21	1	48	43	5	
E-22	1	51	47	3	
E-23	1	53	49	4	
E-24	1	54	50	4	
E-25	1	55	51	4	
E-26	1	54	51	4	
E-27	1	54	50	4	
E-28	1	52	48	4	
E-29	1	55	51	5	
E-30	1	50	47	4	
E-31	1	53	48	5	
E-32	1	57	53	4	
E-33	1	65	57	7	
E-34	1	68	59	9	
E-35	1	58	52	7	
E-36	1	64	58	6	
E-37	 1	51	47	3	
E-38	 1	50	46	4	
E-39	1	68	63	5	
E-40	1	70	60	10	
E-41	1	68	59	9	
E-42	1	67	58	9	
L-4Z	I	O1	l 30	9	

	TABLE 14						
	CNE D/E- BARRIER D2 and E1-E4 OPTIMIZED BARRIER RESULTS						
Receptor ID	# of Dwelling /Recreational Units	2040 Loudest Hour Predicted Future Noise Levels Leq(h) in dBA					
		No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)			
E-43	1	58	52	6			
E-44	1	60	56	5			
E-45	1	59	54	5			
E-46	1	53	48	5			
E-47	1	52	47	5			
E-48	1	71	62	9			
E-49	1	71	62	10			
E-50	1	65	58	7			
E-51	1	51	47	4			
E-52	1	51	47	3			
E-53	1	52	49	2			
E-54	1	49	47	2			
E-55	1	49	46	3			
E-56	1	55	55	0			
E-57	1	54	53	1			
E-58	1	54	53	1			
E-59	1	58	58	1			
E-60	1	66	61	5			
E-61	1	69	61	8			
E-62	1	58	52	6			
E-63	1	57	52	5			
E-64	1	68	60	8			
E-65	1	67	62	5			
E-66	1	64	63	0			
D-31	1	72	64	8			
D-32	1	63	62	2			
D-33	1	57	55	1			
D-34	1	55	52	3			
D-35	1	55	54	1			
D-36	1	53	51	2			
D-37	1	50	47	4			
D-38	1	55	51	4			
D-39	1	65	60	6			
D-40	1	70	65	5			
D-41	1	63	57	6			
*	Insertion Loss (IL) s	ound levels m	nay be different due to	rounding			

Indicates noise impact (NAC only)

Indicates at least a 5 dBA benefit

66 5

	TABLE 15 CNE C- BARRIER C1-C2 OPTIMIZED BARRIER RESULTS				
Receptor ID	# of Dwelling		dicted Future Noise Level	s Leq(h) in dBA	
Receptor ID	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	
		Barrier C1-C2			
C-01	1	57	57	1	
C-02	1	58	57	1	
C-03	1	60	59	1	
C-04	1	64	62	2	
C-05	1	66	61	5	
C-06	1	67	59	9	
C-07	1	69	59	10	
C-08	1	70	56	14	
C-09	1	62	52	10	
C-10	1	61	52	9	
C-11	1	57	51	6	
C-12	1	52	49	3	
C-13	1	52	47	5	
C-14	1	54	48	6	
C-15	1	55	49	6	
C-16	1	73	58	15	
C-17	1	72	59	13	
C-18	1	68	58	10	
C-19	1	65	55	10	
C-20	1	62	54	8	
C-21	1	60	53	7	
C-22	1	56	50	7	
C-23	1	52	46	6	
C-24	1	57	49	8	
C-25	1	56	49	7	
C-26	1	54	47	7	
C-27	1	52	45	7	
C-28	1	48	43	6	
C-29	1	49	44	5	
C-30	1	49	45	4	
C-31	1	49	45	4	
C-32	1	50	45	5	
C-33	1	52	47	5	
C-34	1	52	47	5	
C-35	1	58	51	7	
C-36	1	66	57	9	
C-37	1	70	61	8	
C-38	1	61	53	8	
C-39	1	57	49	7	
C-40	1	52	47	5	
C-41	1	72	60	11	
C-42	1	69	58	12	
C-43	1	65	54	10	
C-44	1	61	51	9	
C-45	1	61	52	9	
C-46	1	50	46	4	
C-46	1	48	44	4	
C-47	1	48	44	4	
C-46	1	52	48	5	
C-50	1	53	48	5	
C-50 C-51	1	55	48	7	
C-52	1	53	48	5	
U-5Z	1	_ ეა	40	5	

	TABLE 15 CNE C- BARRIER C1-C2 OPTIMIZED BARRIER RESULTS					
Receptor ID	# of Dwelling	2040 Loudest Hour Predicted Future Noise Levels		Leq(h) in dBA		
Neceptor ID	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)		
		Barrier C1-C2				
C-53	1	71	58	14		
C-54	1	70	57	12		
C-55	1	61	53	8		
C-56	1	69	58	12		
C-57	1	62	54	8		
C-58	1	69	60	9		
C-58B	1	67	60	7		
C-59	1	64	59	5		
C-60	1	58	54	5		
C-61	1	72	67	6		
C-62	1	57	53	4		
C-63	1	66	59	7		
C-64	1	70	60	9		
C-65	1	56	50	6		
C-66	1	57	51	6		
C-67	1	60	52	8		
C-68	1	63	54	9		
C-69	1	65	55	10		
C-70	1	63	56	7		
C-71	1	64	57	8		
C-72	1	63	57	7		
C-73	1	71	60	11		
C-74	1	68	60	8		
C-75	1	63	57	6		
C-76	1	62	60	2		
C-77	1	54	49	5		
C-78	1	54	49	5		
C-79	1	55	50	5		
C-80	1	55	51	4		
C-81	1	55	51	4		
C-82	1	56	52	4		
C-83	1	56	53	3		
C-84	1	55	53	2		
C-85	1	55	53	2		
C-86	1	54	53	2		
C-87	1	53	51	2		
C-88	1	53	52	1		
*	Ins	Insertion Loss (IL) sound levels may be different due to rounding				
66		Indicates noise	e impact (NAC only)			
5		Indicates at lea	ast a 5 dBA benefit			

	TABLE 16						
	CNE F-BARRIER F1-F1B-F1C-F2 OPTIMIZED BARRIER RESULTS						
Receptor ID	# of Dwelling	# of Dwelling 2040 Loudest Hour Pred		Leq(h) in dBA			
•	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)			
		Barrier F1-F1B-F1C-F2					
F-15	1	68	64	5			
F-16	1	73	69	4			
F-17	1	74	68	6			
F-18	1	68	63	5			
F-19	1	68	63	5			
F-20	1	62	61	1			
F-21	1	61	57	4			
F-22	1	55	53	1			
F-23	1	57	53	3			
F-24	1	70	62	8			
F-25	1	71	61	10			
F-26	1	69	59	10			
F-27	1	62	57	5			
F-28	1	61	55	5			
F-29	1	62	55	6			
F-30	1	50	49	2			
F-31	1	51	49	3			
F-32	1	52	49	3			
F-33	1	51	49	2			
F-34	1	57	56	1			
F-35	1	50	49	2			
F-36	1	49	47	2			
F-37	1	50	48	1			
F-38	1	55	55	0			
F-39	1	54	54	0			
*	Insertion Loss (IL) sound levels may be different due to rounding						
66		Indicates noise i	impact (NAC only)				
5		Indicates at leas	st a 5 dBA benefit				

	TABLE 17					
	CNE F- BARRIER F3 OPTIMIZED BARRIER RESULTS					
Receptor ID	# of Dwelling	2040 Loudest Hour Predicted Future Noise Levels		s Leq(h) in dBA		
	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)		
		Barrier F3				
F-40	1	72	64	8		
F-41	1	69	63	7		
F-42	1	63	59	4		
F-43	1	60	58	2		
F-44	1	58	56	2		
F-45	1	64	58	6		
F-46	1	69	58	11		
F-47	1	67	61	6		
F-48	1	70	64	6		
F-49	1	71	62	9		
F-50	1	71	61	10		
F-51	1	70	60	10		
F-52	1	65	58	7		
F-53	1	51	50	1		
F-54	1	50	47	3		
F-55	1	55	52	3		
F-56	1	54	50	4		
F-57	1	55	51	5		
F-58	1	56	51	5		
F-59	1	55	49	6		
F-60	1	54	48	6		
F-61	1	51	46	4		
F-62	1	53	48	5		
F-63	1	54	49	5		
F-64	1	56	50	6		
F-65	1	57	50	7		
F-66	1	58	52	6		
F-67	1	57	51	6		
F-68	1	56	51	5		
F-69	1	57	53	4		
F-70	1	70	61	9		
F-71	1	70	63	7		
F-72	1	68	62	7		
F-73	1	64	59	5		
F-74	1	74	67	8		
F-75	1	64	62	2		
*	Insertion Loss (IL) sound levels may be different due to rounding					
66		Indicates noise in	mpact (NAC only)			
5		Indicates at leas	t a 5 dBA benefit	<u> </u>		

		TABLE 18					
	CNE F- BARRIER F4-F4B OPTIMIZED BARRIER RESULTS						
Receptor ID	# of Dwelling	2040 Loudest Hour P	redicted Future Noise Level	s Leq(h) in dBA			
	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)			
		Barrier F4-F4B					
F-83	1	67	62	5			
F-84	1	65	58	8			
F-85	1	59	55	4			
F-86	1	62	57	5			
F-87	1	59	54	4			
F-88	1	65	61	4			
F-89	1	65	61	5			
F-90	1	61	55	6			
F-91	1	58	53	5			
F-92	1	56	51	5			
F-93	1	58	54	4			
F-94	1	65	60	4			
F-95	1	69	64	5			
F-96	1	68	62	6			
F-97	1	60	55	5			
F-98	1	67	60	7			
F-99	1	63	57	6			
PTR-16	1	70	58	12			
PTR-17	1	67	58	9			
PTR-18	1	65	58	7			
PTR-19	1	64	56	8			
PTR-20	1	63	56	8			
PTR-21	1	65	56	8			
TR-23	1	63	56	7			
TR-24	1	63	57	6			
TR-25	1	63	57	6			
TR-26	1	62	57	5			
*	Ins	Insertion Loss (IL) sound levels may be different due to rounding					
66		Indicates noise	e impact (NAC only)				
5		Indicates at le	ast a 5 dBA benefit				

	TABLE 19 CNE F- BARRIER F5-F9 OPTIMIZED BARRIER RESULTS					
Receptor ID	# of Dwelling		dicted Future Noise Levels	s Leq(h) in dBA		
Receptor ID	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)		
		Barrier F5-F9				
F-100	1	69	64	5		
F-101	1	67	62	5		
F-102	1	65	61	4		
F-103	1	63	60	3		
F-104	1	56	53	3		
F-105	1	56	52	4		
F-106	1	61	57	4		
F-107	1	62	58	4		
F-108	1	45	43	2		
F-109	1	60	55	5		
F-110	1	56	51	5		
F-111	1	54	50	4		
F-112	1	53	49	4		
F-113	1	52	48	4		
F-114	1	51	48	3		
F-115	1	50	46	3		
F-116	1	72	65	8		
F-117	1	71	60	12		
F-118	1	61	56	5		
F-119	1	59	54	5		
F-120	1	55	51	4		
F-121	1 1	52	49	3		
F-122	1	52	47	4		
F-123	1	74	66	8		
F-124	1 1	73	63	10		
F-125	1	73	68	5		
F-126	1	60	53	7		
F-127	1	56	51	5		
F-127 F-128	1	53	47	5		
F-128	1	54	48	7		
F-130	1	55	49	7		
F-131	1	56	50	6		
F-131	1	65	56	9		
F-132	1	65	58	7		
F-134	1	56	52	4		
F-135	1	58	53	5		
F-136	1	61	57	4		
F-137	1	58	55	4		
F-137	1	57	54	3		
F-138 F-139	1	57	54	4		
F-139 F-140	1	66	60	6		
		54	51			
F-141	1			4		
F-142	1	55 53	52 49	3		
F-143	1	53 54	50	4		
F-144	1		47	4		
F-145	1	52		5		
F-146	1	51	46	5		
F-147	1	53	49	4		
F-148	1	55	51	4		
F-149	1	56	52	5		
F-150	1	55	51	4		
F-151	1	59	56	3		

	TABLE 19 CNE F- BARRIER F5-F9 OPTIMIZED BARRIER RESULTS					
Receptor ID	# of Dwelling	2040 Loudest Hour P	redicted Future Noise Levels	Leq(h) in dBA		
receptor 15	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)		
		Barrier F5-F9				
F-152	1	58	55	3		
F-153	1	54	50	4		
F-154	1	56	54	2		
F-155	1	54	52	2		
F-156	1	53	51	2		
F-157	1	53	51	2		
F-158	1	55	53	2		
F-159	1	52	52	1		
F-160	1	52	51	1		
F-161	1	51	50	1		
F-162	1	53	53	1		
F-163	1	55	54	1		
F-164	1	57	57	0		
*	Ins	Insertion Loss (IL) sound levels may be different due to rounding				
66		Indicates noise impact (NAC only)				
5		Indicates at le	ast a 5 dBA benefit	·		

TABLE 20 CNE G- BARRIER G1-G6 OPTIMIZED BARRIER RESULTS				
Receptor ID	# of Dwelling	2040 Loudest Hour Pro	edicted Future Noise Leve	ls Leq(h) in dBA
	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA
		Barrier G1-G6		
G-01	1	62	62	0
G-02	1	64	64	0
G-03	1	65	64	1
G-04	1	65	63	2
G-05	1	60	57	3
G-06	1	56	54	3
G-07	1	53	51	2
G-08	1	51	49	2
G-09	1	51	48	2
G-10	1	48	45	3
G-11	1	49	47	2
G-12	1	49	48	2
G-13	1	51	49	2
G-14	1	52	51	2
G-15	1	51	50	1
G-16	1	53	47	6
G-17	1	53	48	5
G-18	1	54	49	5
G-19	1	56	51	6
G-20	1	60	53	7
G-21	1	60	54	6
G-22	1	68	60	7
G-23	1	68	57	10
G-24	1	72	59	13
G-25	1	73	61	12
G-26	1	58	52	6
G-27	1	59	51	8
G-28	1	57	47	9
G-29	1	55	46	9
G-30	1	52	45	8
G-31	1	51	44	7
G-32	1	53	45	8
G-33	1	54	46	8
G-34	1	58	50	8
G-35	1	60	50	9
G-36	1	63	56	7
G-37	1	70	58	12
G-38	1	68	58	11
G-39	1	68	58	11
G-40	1	69	57	13
G-41	1	69	55	14
G-42	1	65	54	11
G-43	1	66	55	11
G-44	1	65	55	11
G-45	1	66	55	10
G-46	1	69	56	13
G-47	1	65	56	9
G-48	1	63	55	8
G-49	1	65	57	8
G-50	1	69	59	11
G-51	1	73	65	8
	1	73	65	8

	TABLE 20 CNE G- BARRIER G1-G6 OPTIMIZED BARRIER RESULTS					
Receptor ID	# of Dwelling	2040 Loudest Hour Pre	dicted Future Noise Leve	ls Leq(h) in dBA		
Receptor 15	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)		
		Barrier G1-G6				
G-53	1	71	66	6		
G-54	1	58	50	9		
G-55	1	59	50	9		
G-56	1	58	50	8		
G-57	1	53	45	7		
G-58	1	52	45	7		
G-59	1	59	50	8		
G-60	1	53	46	7		
G-61	1	50	44	6		
G-62	1	55	49	6		
G-63	1	59	51	8		
G-64	1	59	51	8		
G-65	1	60	53	7		
G-66	1	60	56	5		
G-67	1	56	51	5		
G-68	1	53	48	5		
G-69	1	51	46	5		
G-70	1	49	45	4		
G-71	1	48	44	4		
G-72	1	48	44	4		
G-73	1	48	45	3		
G-74	1	53	49	4		
G-75	1	59	55	3		
G-76	1	68	61	7		
G-77	1	72	65	7		
G-78	1	66	58	8		
G-79	1	56	51	5		
G-80	1	52	49	4		
G-81	1	50	47	3		
G-82	1	45	42	3		
G-83	1	65	59	6		
G-84	1	61	56	5		
G-85	1	58	55	4		
G-86	1	55	52	3		
G-87	1	55	52	4		
G-88	1	49	46	3		
G-89	1	48	45	4		
G-90	1	50	45	5		
G-91	1	66 (41)	63 (38)	3		
G-92	1	65	62	3		
G-93	1	61	56	5		
G-94	1	68	61	7		
G-95	1	67	60	7		
G-96	1	67	59	8		
G-97	1	63	56	7		
G-98	1	64	56	8		
G-99	1	60	52	7		
G-100	1	61	54	7		
G-101	1	59	52	8		
G-102	1	59	52	7		
G-103	1	57	51	6		
G-104	1	70	66	5		

	TABLE 20				
	CNE G- BARRIE	R G1-G6 OPTIMIZED B	ARRIER RESULTS		
Receptor ID	# of Dwelling	2040 Loudest Hour P	redicted Future Noise Levels	Leq(h) in dBA	
,	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	
		Barrier G1-G6			
G-105	1	70	62	8	
G-106	1	59	55	3	
G-107	1	56	52	4	
G-108	1	57	54	3	
G-109	1	60	57	3	
G-110	1	61	58	3	
G-111	1	55	50	5	
G-112	1	53	48	5	
G-113	1	54	48	6	
G-114	1	55	51	5	
G-115	1	52	50	2	
G-116	1	59	56	3	
G-117	1	56	53	3	
*	Insertion Loss (IL) sound levels may be different due to rounding				
66		Indicates noise impact (NAC only)			
5		Indicates at le	ast a 5 dBA benefit		

	TABLE 21 CNE G- BARRIER G8-G9 OPTIMIZED BARRIER RESULTS					
D ( ) ID	# of Dwelling		edicted Future Noise Levels	Leq(h) in dBA		
Receptor ID	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)		
		Barrier G8-G9				
G-118	1	59	57	2		
G-119	1	60	58	2		
G-120	1	61	58	2		
G-121	1	60	57	3		
G-122	1	60	55	4		
G-123	1	58	54	4		
G-124	1	57	55	3		
G-125	1	59	55	4		
G-126	1	62	58	4		
G-127	1	65	60	5		
G-128	1	62	58	4		
G-129	1	60	57	3		
G-130	1	58	56	3		
G-131	1	59	57	2		
G-132	1	59	57	3		
G-133	1	58	55	3		
G-134	1	58	55	3		
G-135	1	57	55	3		
G-136	1	60	55	5		
G-137	1	62	56	5		
G-138	1	63	58	5		
G-139	1	63	58	6		
G-140	1	65	60	6		
G-141	1	63	58	6		
G-142	1	61	55	6		
PTR-01	1	66	61	5		
PTR-02	1	70 70	65	5		
PTR-03	1		66	4		
PTR-04	1 1	70 71	61 61	9		
PTR-05	1	71	60	10		
PTR-06 PTR-07	1	71	61	10		
PTR-07	1	71	61	10		
PTR-09	1	70	61	8		
PTR-10	1	69	59	10		
PTR-11	1	69	59	10		
PTR-12	1	69	59	10		
PTR-13	1	68	58	10		
PTR-14	1	70	59	11		
PTR-15	1	73	57	16		
TR-01	1	58	57	1		
TR-02	1	60	58	2		
TR-03	1	60	58	2		
TR-04	1	62	59	3		
TR-05	1	63	59	5		
TR-06	1	64	59	5		
TR-11	1	67	59	8		
TR-12	1	65	57	8		
TR-13	1	63	56	8		
TR-14	1	62	55	7		
*	Ins	ertion Loss (IL) sound levels r	nay be different due to round	ling		

TABLE 21						
CNE G- BARRIER G8-G9 OPTIMIZED BARRIER RESULTS						
Receptor ID	# of Dwelling	2040 Loudest Hour Predicted Future Noise Levels Leq(h) in dBA			# of Dwelling 2040 Loudest Hour Predicted Future Noise Levels	
recopiol 15	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)		
		Barrier G8-G9				
66		Indicates noise impact (NAC only)				
5		Indicates at least a 5 dBA benefit				

	TABLE 22 CNE G- BARRIER G11-G13 OPTIMIZED BARRIER RESULTS					
Receptor ID	# of Dwelling		dicted Future Noise Level	s Leq(h) in dBA		
Receptor in	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)		
		Barrier G11-G13				
G-143	1	63	60	3		
G-144	1	73	67	6		
G-145	1	73	67	6		
G-146	1	56	52	4		
G-147	1	52	48	4		
G-148	1	50	45	5		
G-149	1	47	44	3		
G-150	1	55	52	3		
G-151	1	57	53	4		
G-152	1	62	58	5		
G-153	1	73	64	10		
G-154	1	72	60	12		
G-155	1	73	60	13		
G-156	1	72	59	13		
G-157	1	70	60	10		
G-158	1	59	53	6		
G-159	1	52	47	5		
G-160	1	48	45	4		
G-161	1	74	63	11		
G-162	1	49	44	6		
G-163	1	45	42	3		
G-164	1	50	46	5		
G-165	1	52	46	6		
G-166	1	50	45	5		
G-167	1	52	48	4		
G-168	1	68	59	9		
G-169	1	71	60	11		
G-170	1	71	60	11		
G-171	1	70	59	11		
G-172	1	58	55	4		
G-173	1	55	48	7		
G-174	1	52	50	3		
G-175	1	49	47	3		
G-176	1	49	46	3		
G-177	1	48	46	3		
G-178	1	49	47	2		
G-179	1	52	50	2		
G-180	1	56	53	3		
G-181	1	61	58	3		
G-182	1	63	59	4		
G-183	1	57	54	3		
G-184	1	62	57	5		
G-185	1	74	64	10		
G-186	1	74	65	9		
G-187	1	74	65	9		
G-188	1	74	66	9		
G-189	1	74	68	6		
G-190	1	48	47	1		
G-190 G-191	1	48	47	1		
G-191 G-192	1	50	49	2		
G-193	1	54	52	2		
G-193	1	57	55	3		
0-194						

	CNE G- BARRIEF	TABLE 22 R G11-G13 OPTIMIZED BA	ARRIER RESULTS		
Receptor ID	# of Dwelling			Leq(h) in dBA	
Receptor ib	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	
		Barrier G11-G13			
G-195	1	62	59	4	
G-196	1	61	57	4	
G-197	1	60	56	4	
G-198	1	63	60	3	
G-199	1	69	64	5	
G-200	1	72	66	6	
G-201	1	73	67	6	
*	Ins	Insertion Loss (IL) sound levels may be different due to rounding			
66		Indicates noise ir	mpact (NAC only)		
5		Indicates at leas	t a 5 dBA benefit		

	CNE G- BARRIEF	TABLE 23 R G14-G16 OPTIMIZED BA	ARRIER RESULTS		
Receptor ID	# of Dwelling	2040 Loudest Hour Predicted Future Noise Levels		Leq(h) in dBA	
Receptor ID	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	
	_	Barrier G14-G16			
G-202	1	72	67	5	
G-203	1	69	63	6	
G-204	1	61 (36)	58 (33)	3	
G-205	1	56	53	3	
G-206	1	62	58	4	
G-207	1	68	62	6	
G-208	1	74 (49)	66 (41)	7	
*	Ins	Insertion Loss (IL) sound levels may be different due to rounding			
66		Indicates noise in	mpact (NAC only)		
5		Indicates at leas	t a 5 dBA benefit		

TABLE 24 CNE H - BARRIER H2-H11 OPTIMIZED BARRIER RESULTS							
Receptor ID	# of Dwelling	2040 Loudest Hour Pro	edicted Future Noise Leve	ls Leq(h) in dBA			
recopior is	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dB/			
Barrier H2-H11							
H-01	1	75	61	14			
H-02	1	74	60	14			
H-03	1	68	59	9			
H-04	1	53	50	3			
H-05	1	56	53	3			
H-06	1	62	59	3			
H-07	1	57	53	4			
H-08	1	55	52	4			
H-09	1	56	54	2			
H-10	1	56	54	1			
H-11	1	59	58	1			
H-12	1	58	57	1			
H-13	1	55	55	1			
H-14	1	54	54	1			
H-15	1	55	54	1			
H-16	1	64	61	4			
H-17	1	74	63	12			
H-18	1	73	61	12			
H-19	1	67	57	10			
H-20	1	60	53	7			
H-21	1	59	53	6			
H-22	1	55	50	5			
H-23	1	56	49	7			
H-24	1	56	49	7			
H-25	1	61	52	10			
H-26	1	62	54	8			
H-27	1	71	60	11			
H-28	1	63	56	7			
H-29	1	60	54	7			
H-30	1	61	56	6			
H-31	1	61	56	5			
H-32	1	75	69	5			
H-33	1	70	63	8			
H-34	1	70	63	8			
H-35	1	74	68	6			
H-36	1	74	66	8			
H-37	1	60	57	3			
H-38	1	60	57	3			
H-39	1	60	56	4			
H-40	1	56	50	6			
H-41	1	55	51	4			
H-42	1	54	51	4			
H-43	1	54	51	3			
H-44	1	54	51	4			
H-45	1	54	51	3			
H-46	1	51	48	3			
H-47	1	51	47	4			
H-48	1	55	52	4			
H-49	1	58	53	4			
H-50	1	54	49	5			
H-51	1	48	45	4			
H-52	1	51	47	4			

		TABLE 24					
	CNE H - BARRIER H2-H11 OPTIMIZED BARRIER RESULTS						
Receptor ID	# of Dwelling	2040 Loudest Hour Predicted Future Noise Level		s Leq(h) in dBA			
	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)			
		Barrier H2-H11					
H-53	1	56	52	4			
H-54	1	58	53	5			
H-55	1	55	51	5			
H-56	1	56	52	4			
H-57	1	59	54	5			
H-58	1	62	61	0			
H-59	1	53	52	2			
H-60	1	55	53	2			
H-61	1	65	61	3			
H-62	1	73	68	5			
H-63	1	72	69	4			
H-64	1	72	68	4			
H-65	1	59	55	3			
H-66	1	62	58	4			
H-67	1	63	58	5			
H-68	1	61	56	5			
H-69	1	65	59	7			
H-70	1	61	56	5			
H-71	1	62	56	6			
H-72	1	62	55	6			
H-73	1	68	59	9			
H-74	1	76	59	17			
H-75	1	67	58	9			
H-76	1	76	60	17			
H-77	1	77	59	17			
H-78	1	65	58	7			
H-79	1	63 (38)	58 (33)	5			
*	Ins	ertion Loss (IL) sound levels n	nay be different due to roun	ding			
66		Indicates noise ir	mpact (NAC only)				
5		Indicates at leas	t a 5 dBA benefit				

	ONE 1 DADD	TABLE 25	DIED DEGILI TO		
	CNE I- BARR	IER I2 OPTIMIZED BAR	RIER RESULTS		
Receptor ID	# of Dwelling	2040 Loudest Hour P	redicted Future Noise Level	s Leq(h) in dBA	
	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	
		Barrier I2			
I-01	1	53	53	0	
I-02	1	64	64	0	
I-03	1	70	70	1	
I-04	1	53	52	1	
I-05	1	54	52	2	
I-06	1	55	53	2	
I-07	1	57	54	2	
I-08	1	58	55	3	
I-09	1	70	65	5	
I-10	1	64	57	7	
I-11	1	69	60	9	
I-12	1	71	62	9	
I-13	1	74	62	12	
I-14	1	69	64	5	
I-15	1	64	62	2	
I-16	1	55	53	2	
I-17	1	53	50	3	
I-18	1	60	56	4	
I-19	1	60	55	5	
I-20	1	59	55	3	
I-21	1	56	53	4	
I-22	1	55	51	4	
I-23	1	55	51	4	
*	Ins	Insertion Loss (IL) sound levels may be different due to rounding			
66		Indicates noise	e impact (NAC only)		
5		Indicates at le	ast a 5 dBA benefit		

	TABLE 26 CNE I- BARRIER I4-16 OPTIMIZED BARRIER RESULTS					
Receptor ID	# of Dwelling		dicted Future Noise Level	s Leq(h) in dBA		
Receptor ID	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)		
		Barrier I4-I6				
I-24	1	51	51	0		
I-25	1	53	52	0		
I-26	1	58	58	0		
I-27	1	57	56	0		
I-28	1	52	51	1		
I-29	1	55	55	1		
I-30	1	55	54	1		
I-31	1	50	49	1		
I-32	1	52	51	2		
I-33	1	51	50	2		
I-34	1	50	49	2		
I-35	1	49	48	1		
I-36	1	50	49	2		
I-37	1	51	50	2		
I-38	1	52	50	2		
I-39	1	49	47	2		
I-40	1	53	50	3		
I-41	1	57	57	0		
I-42	1	54	50	3		
I-43	1	54	51	4		
I-44	1	53	52	2		
I-45	1	55	53	2		
I-46	1	53	51	2		
I-47	1	53	50	3		
I-48	1	51	49	2		
I-49	1	54	50	4		
I-50	1	60	55	5		
I-51	1	60	55	5		
I-52	1	61	55	5		
I-53	1	59	55	4		
I-54	1	56	54	2		
I-55	1	73	68	6		
I-56	1	74	64	10		
I-57	1	69	60	9		
I-58	1	73	62	11		
I-59	1	70	64	5		
I-60	1	67	63	5		
I-61	1	60	56	4		
I-62	1	57	53	4		
I-63	1	55	51	4		
I-64	1	54	51	4		
I-65	1	55	51	4		
I-66	1	57	53	4		
I-67	1	58	54	4		
I-68	1	61	57	5		
I-69	1	67	61	5		
I-70	1	68	63	5		
I-71	1	62	60	2		
I-72 I-73	1	59 57	57 55	2 2		
	1	56	55 55	2 2		
1-74	1 1		56			
I-75	1	58	00	1		

	CNE I- BARRII	TABLE 26 ER I4-I6 OPTIMIZED BAI	RRIER RESULTS	
Receptor ID	# of Dwelling		redicted Future Noise Level	s Leq(h) in dBA
Receptor is	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)
		Barrier I4-I6		
I-76	1	58	57	1
I-77	1	57	56	1
I-78	1	59	58	1
I-79	1	61	61	1
I-80	1	60	60	0
I-81	1	55	55	0
I-82	1	56	55	1
I-83	1	56	55	0
I-84	1	55	55	1
I-85	1	54	54	1
I-86	1	54	53	1
I-87	1	54	52	2
I-88	1	55	52	3
I-89	1	56	53	3
I-90	1	55	52	3
I-91	1	55	52	3
I-92	1	53	50	3
I-93	1	52	50	2
I-94	1	52	50	2
I-95	1	52	50	2
I-96	1	51	50	1
I-97	1	51	50	1
I-98	1	51	51	1
I-99	1	53	52	1
I-100	1	53	53	1
I-101	1	52	52	0
I-102	1	52	52	0
I-103	1	52	51	0
I-104	1	51	50	0
I-105	1	49	49	0
I-106	1	51	51	0
I-107	1	52	52	0
I-108	1	50	50	0
I-109	1	55	55	0
I-110	1	53	53	0
I-111	1	57	57	0
I-112	1	56	56	0
*	Ins	ertion Loss (IL) sound levels	may be different due to rour	nding
66		Indicates noise	impact (NAC only)	
5		Indicates at lea	ast a 5 dBA benefit	

	TABLE 27 CNE I- BARRIER J2-J3 and K1-K4 OPTIMIZED BARRIER RESULTS					
	# of Dwelling		dicted Future Noise Level	s Leq(h) in dBA		
Receptor ID	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)		
		Barrier J2-J3 and K1-K4				
J-01	1	70	67	2		
J-02	1	67	60	7		
J-03	1	59	52	7		
J-04	1	71	61	9		
J-05	1	73	63	10		
J-06	1	73	66	7		
J-07	1	68	60	8		
J-08	1	69	62	7		
J-09	1	68	63	5		
J-10	1	64	57	7		
J-11	1	65	59	6		
J-12	1	65	61	5		
J-13	1	66	61	5		
J-14	1	66	61	5		
J-15	1	62	60	2		
J-16	1	62	58	5		
J-17	1	63	59	4		
J-18	1	62	58	4		
J-19	1	61	56	5		
J-20	1	59	56	3		
J-21	1	58	54	4		
J-22	1	58	53	5		
J-23	1	72 (47)	66(41)	6		
J-24	1	59	58	0		
J-25	1	53	52	1		
J-26	1	51	49	2		
J-27	1	53	53	1		
J-28	1	54	54	1		
J-29	1	56	51	5		
J-30	1	57	53	4		
J-31	1	54	50	4		
J-32	1	53	50	4		
J-33	1	53	49	3		
J-34	1	53	49	4		
J-35	1	57	53	4		
K-01	1	70	62	8		
K-02	1	61 (36)	54 (29)	7		
K-03	1	63	56	7		
K-04	1	68	62	6		
K-05	1	64 (39)	56(31)	8		
K-06	1	59	54	5		
K-07	1 .	55	50	5		
K-08	1	52	48	4		
K-09	1 1	48	43	4		
K-10	1	53	49	4		
K-11	1	60	55	6		
K-12	1	64	58	6		
K-13	1	62	56	6		
K-14	1	69	61	8 7		
K-15	1	59	52 53			
K-16	1 1	60	53 55	7		
K-17		63	55	8		

		TABLE 27					
	CNE I- BARRIER J2-J3 and K1-K4 OPTIMIZED BARRIER RESULTS						
Receptor ID	# of Dwelling /Recreational Units	2040 Loudest Hour P	redicted Future Noise Levels	Leq(h) in dBA			
	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)			
		Barrier J2-J3 and K1-K4	4				
K-18	1	59	52	8			
K-19	1	61	53	7			
K-20	1	59	52	8			
K-21	1	58	52	7			
K-22	1	56	52	5			
K-23	1	67	58	8			
K-24	1	67	61	6			
K-25	1	61	55	6			
K-26	1	62	59	3			
K-27	1	58	56	2			
K-28	1	54	51	3			
K-29	1	55	54	2			
K-30	1	52	51	1			
K-31	1	51	51	1			
K-32	1	56	55	2			
K-33	1	54	53	1			
K-34	1	49	48	1			
K-35	1	48	47	1			
K-36	1	57	50	7			
K-37	1	69 (44)	68(43)	1			
K-38	1	65(40)	65(40)	0			
K-39	1	51	51	0			
*	Insertion Loss (IL) sound levels may be different due to rounding						
66		Indicates noise	e impact (NAC only)				
5		Indicates at le	ast a 5 dBA benefit				

	CNF I - BARRIE	TABLE 28 ER L1-L5 OPTIMIZED BA	ARRIER RESULTS		
Becomton ID	# of Dwelling		redicted Future Noise Levels	Leq(h) in dBA	
Receptor ID	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	
		Barrier L1-L5			
L-01	1	69	63	7	
L-02	1	65	60	5	
L-03	1	69	63	6	
L-04	1	66	62	4 6	
L-05	1	72	66		
L-06	1	64	62	2	
L-07	1	58	56	2	
L-08	1	58	57	1	
L-09	1	65	65	1	
*	Ins	ertion Loss (IL) sound levels	may be different due to rounc	ling	
66		Indicates noise	impact (NAC only)		
5		Indicates at lea	ast a 5 dBA benefit		

		TABLE 29						
	CNE L- BARRIE	R L6-L8 OPTIMIZED BA	ARRIER RESULTS					
Receptor ID	# of Dwelling	2040 Loudest Hour P	redicted Future Noise Levels	Leq(h) in dBA				
	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)				
		Barrier L6-L8						
L-10	1	60	58	1				
L-11	1	71	66	5				
L-12	1	73	62	10				
L-13	1	65	57	8				
L-14	1	61	56	5				
L-15	1	63 (38)	63 (38)	0				
L-16	1	58	54	4				
L-17	1	57	54	3				
L-18	1	56	53	3				
*	Ins	Insertion Loss (IL) sound levels may be different due to rounding						
66		Indicates noise	impact (NAC only)					
5		Indicates at lea	ast a 5 dBA benefit	<u> </u>				

	CNF N. Existing	TABLE 30 BARRIER OPTIMIZED BA	ARRIER RESULTS	
Pagartar ID	# of Dwelling		dicted Future Noise Levels	Leq(h) in dBA
Receptor ID	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)
		Existing Barrier		
N-01	1	67	67	0
N-02	1	63	63	0
N-03	1	61	61	0
N-04	1	59	59	0
N-05	1	58	58	0
N-06	1	56	56	0
N-07	1	57	57	0
N-08	1	56	56	0
N-09	1	52	52	0
N-10	1	54	54	0
N-11	1	51	51	0
N-12	1	50	50	0
N-13	1	50	50	0
N-14	1	49	49	0
N-15	1	48	48	0
N-16	1	53	53	0
N-17	1	54	54	0
N-18	1	53	53	0
N-19	1	55	55	0
N-20	1	54	54	0
N-21	1	54	54	0
N-22	1	54	54	0
N-23	1	52	52	0
N-24	1	53	53	0
N-25	1 1	57	57	0
N-26	1	59	59	0
N-27	1	66	66	0
N-28	1	64	64	0
N-29	1	60	60	0
N-30	1	51	51	0
N-31	1	57	57	0
N-32	1	53	53	0
N-33	1	49	49	0
N-34	1	49	49	0
N-35	1	50	50	0
N-36	1	50	50	0
N-37	1	51	51	0
N-38	1	50	50	0
N-39	1	52	52	0
N-40	1	50	50	0
N-41	1	53	52	0
N-41 N-42	1 1	52	52	
				0
N-43	1	52	52	0
N-44 N-45	1	54 54	54 54	0
	1			0
N-46	1	60	60	0
N-47	1	64	64	0
N-48	1	69	69	0
N-49	1	67	67	0
N-50	1 1	61	61	0
N-51	1	53	53	0
N-52	1	52	52	0

		TABLE 30			
	CNE N- Existing	BARRIER OPTIMIZED B	ARRIER RESULTS		
Receptor ID	# of Dwelling	2040 Loudest Hour Pro	40 Loudest Hour Predicted Future Noise Levels		
	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	
		Existing Barrier			
N-53	1	51	51	0	
N-54	1	51	50	0	
N-55	1	50	49	0	
N-56	1	49	49	0	
N-57	1	50	50	1	
N-58	1	50	50	0	
N-59	1	52	52	1	
N-60	1	57	56	1	
N-61	1	56	56	0	
N-62	1	56	56	0	
N-63	1	56	56	0	
N-64	1	54	54	0	
N-65	1	57	57	0	
N-66	1	56	56	0	
N-67	1	59	58	2	
N-68	1	58	57	1	
N-69	1	61	60	1	
N-70	1	61	61	1	
N-71	1	68	68	0	
N-72	1	66	66	0	
N-73	2	65	64	1	
N-74	2	65	63	2	
N-75	2	68	65	3	
N-76	2	72	68	4	
N-77	1	66 (41)	58 (33)	8	
*	Ins	ertion Loss (IL) sound levels	may be different due to round	ding	
66		Indicates noise i	mpact (NAC only)		
5		Indicates at leas	st a 5 dBA benefit		

	CNE N. RAPRIER N1.	TABLE 31 N3 & EXISTING OPTIMIZE	EN BARRIER RESULTS	
Receptor ID	# of Dwelling		dicted Future Noise Levels	Leq(h) in dBA
Receptor ib	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)
	_	Barrier N1-N3 & Existing		
N-01	1	67	63	5
N-02	1	63	61	2
N-03	1	61	59	1
N-04	1	59	58	1
N-05	1	58	57	1
N-06	1	56	55	1
N-07	1	57	56	1
N-08	1	56	55	1
N-09	1	52	51	1
N-10	1	54	53	1
N-11	1	51	50	1
N-12	1	50	49	1
N-13	1	50	49	1
N-14	1	49	49	1
N-15	1	48	48	0
N-16	1	53	52	1
N-17	1	54	53	1
N-18	1	53	52	1
N-19	1	55	54	1
N-20	1	54	53	1
N-21	1	54	52	1
N-22	1	54	53	1
N-23	1	52	50	1
N-24	1	53	51	2
N-25	1	57	54	3
N-26	1	59	55	4
N-27	1	66	60	6
N-28	1	64	58	6
N-29	1	60	55	4
N-30	1	51	49	2
N-31	1	57	53	4
N-32	1	53	51	2
N-33	1	49	47	1
N-34	1	49	48	1
N-35	1	50	48	2
N-36	1	50	50	1
N-37	1	51	48	3
N-38	1	50	49	2
N-39	1	52	51	1
N-40	1	50	49	1
N-41	1	53	52	1
N-42	1	52	51	1
N-43	1	52	51	2
N-44	1	54	52	2
N-45	1	54	52	2
N-46	1	60	57	3
N-47	1	64	60	4
N-48	1	69	65	3
N-49	1	67	60	8
N-50	1	61	56	5
N-51	1	53	52	2
N-52	1	52	51	1
	<u> </u>	<u> </u>	·	

		TABLE 31			
	CNE N- BARRIER N1-	N3 & EXISTING OPTIMIZ	ED BARRIER RESULTS		
Receptor ID	# of Dwelling	2040 Loudest Hour Pro	edicted Future Noise Levels	Leq(h) in dBA	
	/Recreational Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	
		Barrier N1-N3 & Existing			
N-53	1	51	50	2	
N-54	1	51	49	2	
N-55	1	50	48	2	
N-56	1	49	48	2	
N-57	1	50	49	2	
N-58	1	50	49	2	
N-59	1	52	51	1	
N-60	1	57	55	1	
N-61	1	56	55	1	
N-62	1	56	55	1	
N-63	1	56	55	1	
N-64	1	54	53	1	
N-65	1	57	56	1	
N-66	1	56	56	1	
N-67	1	59	57	2	
N-68	1	58	56	2	
N-69	1	61	60	1	
N-70	1	61	61	1	
N-71	1	68	59	9	
N-72	1	66	58	8	
N-73	2	65	59	6	
N-74	2	65	58	6	
N-75	2	68	60	7	
N-76	2	72	62	10	
N-77	1	66 (41)	58 (33)	8	
*	Ins	ertion Loss (IL) sound levels	may be different due to round	ding	
66		Indicates noise	impact (NAC only)		
5		Indicates at leas	st a 5 dBA benefit		

		TABLE 32						
	CNE N- BARRIE	R N1-N3 OPTIMIZED BA	RRIER RESULTS					
Receptor ID	# of Dwelling	2040 Loudest Hour Pre	dicted Future Noise Levels	Leq(h) in dBA				
recoptor 15	/Recreational Units	ecreational Units  No Barrier With Barrier (dBA)		Insertion Loss (IL)* (dBA)				
		Barrier N1-N3						
N-78	1	73	66	7				
*	Inso	Insertion Loss (IL) sound levels may be different due to rounding						
66		Indicates noise impact (NAC only)						
5		Indicates at least a 5 dBA benefit						

**APPENDICES** 

APPENDIX A - NOISE MEASUREMENT DATA

62.3

60.2

60.8

63.6

60.7

60.3

62.1

63.1

**19** 10:19:00 AM

**20** 10:19:30 AM

**33** 10:26:00 AM

**34** 10:26:30 AM

**35** 10:27:00 AM

**36** 10:27:30 AM

**37** 10:28:00 AM

**38** 10:28:30 AM

**39** 10:29:00 AM

**40** 10:29:30 AM

Site #	B2	Description :	1063 Autumn N	/list Lane	
Done By:					Atmospheric
Done By.	EJA, ERZ				Data
Meter:	<b>&gt;</b>	2			Wind Speed
					<u>(mph)</u>
Monitoring	Data:				6mph
_	Date	3/20/19			Temp. (°F)
	Start Time	10:10AM			
	End Time	10:30AM			51
	Duration	20min.			
	Leq (dBA)	60.2			Humidity (%)
Traffic Date	a: 20 Minute				28
Trame bata	Roadway	Leesburg Pike	Reston PKWY		
	Direction	WB EB	NB SB		
	Traffic Total:	346 493	73 114		
	Cars	322 474	71 107		
	MT	14 13	2 6		
	HT	10 6	1		



Skelly and Loy inc.



Occasional Air plane fly overs that also did not dominate the noise environment

Lav (dBA) Num Lav (dBA) Num Lav (dBA) Num Lav (dBA) Time Time Time Time 10:10:00 AM 62.5 **21** 10:20:00 AM 62.2 2 10:10:30 AM 59.6 **22** 10:20:30 AM 58.7 42 3 10:11:00 AM 61.7 **23** 10:21:00 AM 43 60.4 63 4 10:11:30 AM 62 **24** 10:21:30 AM 62.8 44 64 5 10:12:00 AM 62.2 **25** 10:22:00 AM 58.4 45 65 **26** 10:22:30 AM 6 10:12:30 AM 59.8 53.1 46 66 7 10:13:00 AM 58.8 **27** 10:23:00 AM 56.1 47 67 8 10:13:30 AM 62.6 **28** 10:23:30 AM 48 68 60.4 9 10:14:00 AM 61.8 **29** 10:24:00 AM 57.3 49 69 **10** 10:14:30 AM **30** 10:24:30 AM 54.3 50 70 60.5 **11** 10:15:00 AM 59.7 **31** 10:25:00 AM 54.7 51 71 **12** 10:15:30 AM **32** 10:25:30 AM 72 62.2 59.6 52

53

54

55

56

57

58

59

60

73

74

75

76

77

78

79

80

59.7

52

54.5

56.5

57.2

54.2

57.2

60.1

**Description:** 11582 Cedar Chase Rd Site # A2 Atmospheric Done By: EJA, ERZ Data Wind Speed Meter: (mph) 6mph Monitoring Data: Date 3/20/19 Temp. (°F) **Start Time** 10:10AM **End Time** 10:30AM 51 Duration 20min. Leq (dBA) Humidity (%) 56.0 28 Traffic Data: 20 Minute Roadway Leesburg Pike Reston PKWY WB EB NB SB Direction

Site Data: Site Surface: Grass Grade: Pavement Type: Average

73 114

71 107

6

346

322

14

10

493

474

13

6

Traffic Total:

Cars

MT

HT

Skelly and Loy inc.



Periodic construction noises: did not dominate the noise environment.

Occasional Air plane fly overs that also did not dominate the noise environment



Num	Time	Lav (dBA)	Num	Time	Lav (dBA)	Num	Time	Lav (dBA)	Num	Time	Lav (dBA)
1	10:10:00 AM	58.1	21	10:20:00 AM	57.2	41			61		
2	10:10:30 AM	56.3	22	10:20:30 AM	52.4	42			62		
3	10:11:00 AM	59.1	23	10:21:00 AM	54.2	43			63		
4	10:11:30 AM	56.3	24	10:21:30 AM	55.5	44			64		
5	10:12:00 AM	55.9	25	10:22:00 AM	59.4	45			65		
6	10:12:30 AM	52.2	26	10:22:30 AM	54.6	46			66		
7	10:13:00 AM	57.3	27	10:23:00 AM	53.8	47			67		
8	10:13:30 AM	57.8	28	10:23:30 AM	59.6	48			68		
9	10:14:00 AM	57.1	29	10:24:00 AM	54.7	49			69		
10	10:14:30 AM	54.1	30	10:24:30 AM	48.9	50			70		
11	10:15:00 AM	53.8	31	10:25:00 AM	52.4	51			71		
12	10:15:30 AM	56.6	32	10:25:30 AM	58.9	52			72		
13	10:16:00 AM	56.2	33	10:26:00 AM	56.4	53			73		
14	10:16:30 AM	52.6	34	10:26:30 AM	50.9	54			74		
15	10:17:00 AM	56.5	35	10:27:00 AM	52.8	55			75		
16	10:17:30 AM	57.7	36	10:27:30 AM	55	56			76		
17	10:18:00 AM	55.4	37	10:28:00 AM	57.2	57			77		
18	10:18:30 AM	55.3	38	10:28:30 AM	53	58	•		78		
19	10:19:00 AM	54.3	39	10:29:00 AM	55.1	59			79		
20	10:19:30 AM	55.5	40	10:29:30 AM	56.2	60			80		

Site #	C2	Description:	11270 Stones Throw Dr	
Done By:	EJA, ERZ			Atmospheric Data
Meter:	<b></b>	3		Wind Speed (mph)
Monitoring	Data:			6mph
	Date	3/20/19		Temp. (°F)
	Start Time End Time Duration	10:10AM 10:30AM 20min.		51
	Leq (dBA)	56.4		Humidity (%)
Traffic Data	a: <b>20 Minute</b> Roadway	Leesburg Pike	Reston PKWY	28
	Direction	WB EB	NB SB	
	Traffic Total:	346 493	73 114	
	Cars	322 474	71 107	
	MT HT	14 13 10 6	2 6	
Site Data:	Site Surface:	Grass Grade:	Pavement Type:	Average

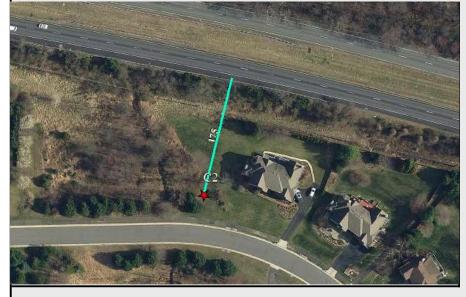


**Notes:** Periodic construction noises: did not dominate the noise environment.

Occasional Air plane fly overs that also did not dominate the noise environment

Rather quiet could hear birds chirping over road noise.

Neighbor had an electric predator noise maker to keep birds off porch that would go off periodically.



Num	Time	Lav (dBA)	Num	Time	Lav (dBA)	Num	Time	Lav (dBA)	Num	Time	Lav (dBA)
1	10:10:00 AM	54.7	21	10:20:00 AM	53.8	41			61		
2	10:10:30 AM	54.9	22	10:20:30 AM	55.3	42			62		
3	10:11:00 AM	54.9	23	10:21:00 AM	54	43			63		
4	10:11:30 AM	59.4	24	10:21:30 AM	56.1	44			64		
5	10:12:00 AM	55.5	25	10:22:00 AM	56.6	45			65		
6	10:12:30 AM	53.7	26	10:22:30 AM	55.3	46			66		
7	10:13:00 AM	54.9	27	10:23:00 AM	50.9	47			67		
8	10:13:30 AM	56.1	28	10:23:30 AM	53.7	48			68		
9	10:14:00 AM	59	29	10:24:00 AM	59.9	49			69		
10	10:14:30 AM	55.6	30	10:24:30 AM	60.2	50			70		
11	10:15:00 AM	53.1	31	10:25:00 AM	54.6	51			71		
12	10:15:30 AM	55.1	32	10:25:30 AM	60.1	52			72		
13	10:16:00 AM	57.8	33	10:26:00 AM	60	53			73		
14	10:16:30 AM	55.4	34	10:26:30 AM	55.2	54			74		
15	10:17:00 AM	50.4	35	10:27:00 AM	51.1	55			75		
16	10:17:30 AM	56	36	10:27:30 AM	59.2	56			76		
17	10:18:00 AM	57	37	10:28:00 AM	56.8	57			77		
18	10:18:30 AM	53.2	38	10:28:30 AM	54.5	58	•		78		
19	10:19:00 AM	57.8	39	10:29:00 AM	53.3	59			79		
20	10:19:30 AM	56.9	40	10:29:30 AM	56.7	60			80		

Site #	F3	Descrip	tion :	1222	Colvin M	leadows	Ln		
Done By:	EJA, ERZ								spheric ata
Meter:			2					Wind	Speed ph)
Monitoring	Data:								5
	Date	3/2	20/19					Tem	p. (°F)
	Start Time	11:3	37 AM						
	End Time		7 AM					5	53
	Duration	20	min						
	Leq (dBA)	5	6.0					Humic	dity (%)
Traffic Date	a: 20 Minute							2	27
Traine Batt	Roadway	Ro	ute 7	Colvi	n Run	Carper	s Farm		
	Direction	EB	WB	NB	SB	NB	SB		
	Traffic Total:	562	403	36	24	9	10		
	Cars	541	376	34	20	9	10		
	MT	16	17	2	4				
	HT	5	10						

Pavement Type:

Average

Site Data: Site Surface: Grass Grade:





Num	Time	Lav (dBA)	Num	Time	Lav (dBA)	Num	Time	Lav (dBA)	Num	Time	Lav (dBA)
1	11:37:00 AM	49.3	21	11:47:00 AM	52.7	41			61		
2	11:37:30 AM	57.9	22	11:47:30 AM	56.9	42			62		
3	11:38:00 AM	58	23	11:48:00 AM	60.2	43			63		
4	11:38:30 AM	60.3	24	11:48:30 AM	58.7	44			64		
5	11:39:00 AM	49.2	25	11:49:00 AM	56.3	45			65		
6	11:39:30 AM	51.7	26	11:49:30 AM	55.5	46			66		
7	11:40:00 AM	57.3	27	11:50:00 AM	55.6	47			67		
8	11:40:30 AM	58.3	28	11:50:30 AM	53.7	48			68		
9	11:41:00 AM	54.2	29	11:51:00 AM	50.5	49			69		
10	11:41:30 AM	56.1	30	11:51:30 AM	55.1	50			70		
11	11:42:00 AM	57.8	31	11:52:00 AM	56.8	51			71		
12	11:42:30 AM	56.6	32	11:52:30 AM	52.9	52			72		
13	11:43:00 AM	49.9	33	11:53:00 AM	50.7	53			73		
14	11:43:30 AM	59.1	34	11:53:30 AM	54	54			74		
15	11:44:00 AM	58	35	11:54:00 AM	54.4	55			75		
16	11:44:30 AM	50.4	36	11:54:30 AM	55.1	56			76		
17	11:45:00 AM	53.4	37	11:55:00 AM	52.3	57			77		
18	11:45:30 AM	55.8	38	11:55:30 AM	56.6	58			78		
19	11:46:00 AM	53.7	39	11:56:00 AM	56.8	59			79		
20	11:46:30 AM	55	40	11:56:30 AM	57.3	60			80		

Average

Site #	F4	Description:	9912 Hessick	Court	
Done By:	EJA, ERZ				Atmospheric Data
Meter:	<b></b>	3			Wind Speed (mph)
Monitoring	Date Start Time End Time Duration Leq (dBA)	3/20/19 11:37 AM 11:57 AM 20min 56.3	Cohin Dun		5 <u>Temp. (°F)</u> 53 <u>Humidity (%)</u> 27
	Roadway Direction Traffic Total: Cars MT HT	Route 7  EB WB  562 403  541 376  16 17  5 10	NB   SB   36   24   34   20   2   4	Carpers Farm	

Site Data: Site Surface: Grass Grade: Pavement Type:





Num	Time	Lav (dBA)	Num	Time	Lav (dBA)	Num	Time	Lav (dBA)	Num	Time	Lav (dBA)
1	11:37:00 AM	55.7	21	11:47:00 AM	58.9	41			61		
2	11:37:30 AM	57.8	22	11:47:30 AM	55.9	42			62		
3	11:38:00 AM	56.5	23	11:48:00 AM	57.6	43			63		
4	11:38:30 AM	52	24	11:48:30 AM	53	44			64		
5	11:39:00 AM	55.2	25	11:49:00 AM	58.6	45			65		
6	11:39:30 AM	58.1	26	11:49:30 AM	58.9	46			66		
7	11:40:00 AM	56.3	27	11:50:00 AM	54.3	47			67		
8	11:40:30 AM	57.7	28	11:50:30 AM	53.9	48			68		
9	11:41:00 AM	56.5	29	11:51:00 AM	56.4	49			69		
10	11:41:30 AM	58.1	30	11:51:30 AM	55.1	50			70		
11	11:42:00 AM	53	31	11:52:00 AM	51.3	51			71		
12	11:42:30 AM	53.9	32	11:52:30 AM	50.1	52			72		
13	11:43:00 AM	60.4	33	11:53:00 AM	55.8	53			73		
14	11:43:30 AM	57.3	34	11:53:30 AM	57.1	54			74		
15	11:44:00 AM	55.1	35	11:54:00 AM	54.6	55			75		
16	11:44:30 AM	54.5	36	11:54:30 AM	53.2	56			76		
17	11:45:00 AM	53.6	37	11:55:00 AM	57.5	57			77		
18	11:45:30 AM	53.9	38	11:55:30 AM	57.1	58	•		78		
19	11:46:00 AM	56.9	39	11:56:00 AM	59.4	59			79		
20	11:46:30 AM	56	40	11:56:30 AM	51.8	60			80		

Description: 1282 Middleton Court Site # G4 Atmospheric Done By: EJA, ERZ Data Wind Speed Meter: (mph) 5 Monitoring Data: 3/20/19 Date Temp. (°F) **Start Time** 11:37 AM **End Time** 11:57 AM 53 20min Duration Humidity (%) Leq (dBA) 59.9 27 Traffic Data: 20 Minute Roadway Route 7 Colvin Run Carpers Farm EB NB SB Direction WB SB 9 10 Traffic Total: 562 403 36 24 Cars 541 376 34 20 9 10

Site Data: Site Surface: Grass Grade: Pavement Type: Average

2

17

10

16

5

MT

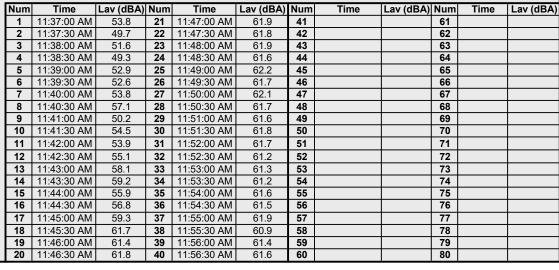
HT

Skelly and Loy inc.



Highway slightly audible (not a very loud area)

#### THIS SITE WAS OMITTED FROM VALIDATION DUE TO NON HIGHWAY NOISE CONTRIBUTIONS





					110411
Site #	G3	Description :	10237 Leesbu	ırg Pike	
Done By:	EJA, ERZ				Atmospheric Data
Meter:		1			Wind Speed (mph)
Monitoring	Data: Date Start Time End Time Duration	3/20/19 11:37 AM 11:57 AM 20min		<u> </u>	5 <u>Temp. (°F)</u> 53
	Leq (dBA)	56.7			Humidity (%)
Traffic Data	a: 20 Minute Roadway	Route 7	Colvin Run	Carpers Farm	27
	Direction Traffic Total: Cars MT HT	EB WB 562 403 541 376 16 17 5 10	NB SB 36 24 34 20 2 4	NB SB 9 10 9 10	
Site Data:	Site Surface:	Grass Grade:	F	Pavement Type:	Average





Num	Time	Lav (dBA)	Num	Time	Lav (dBA)	Num	Time	Lav (dBA)	Num	Time	Lav (dBA)
1	11:37:00 AM	49.5	21	11:47:00 AM	53.2	41			61		
2	11:37:30 AM	57.4	22	11:47:30 AM	54.8	42			62		
3	11:38:00 AM	57.5	23	11:48:00 AM	58.6	43			63		
4	11:38:30 AM	60	24	11:48:30 AM	60.1	44			64		
5	11:39:00 AM	55.1	25	11:49:00 AM	59.9	45			65		
6	11:39:30 AM	53.5	26	11:49:30 AM	53.3	46			66		
7	11:40:00 AM	57.8	27	11:50:00 AM	55.5	47			67		
8	11:40:30 AM	57.1	28	11:50:30 AM	56	48			68		
9	11:41:00 AM	56.4	29	11:51:00 AM	49.2	49			69		
10	11:41:30 AM	49.8	30	11:51:30 AM	54.9	50			70		
11	11:42:00 AM	60.2	31	11:52:00 AM	58.4	51			71		
12	11:42:30 AM	58.5	32	11:52:30 AM	58.2	52			72		
13	11:43:00 AM	53.4	33	11:53:00 AM	52.7	53			73		
14	11:43:30 AM	56	34	11:53:30 AM	50.2	54			74		
15	11:44:00 AM	58.6	35	11:54:00 AM	56.3	55			75		
16	11:44:30 AM	52	36	11:54:30 AM	56.9	56			76		
17	11:45:00 AM	54.8	37	11:55:00 AM	55.5	57			77		
18	11:45:30 AM	56.3	38	11:55:30 AM	58.2	58			78		
19	11:46:00 AM	56.3	39	11:56:00 AM	58.7	59			79		
20	11:46:30 AM	55.6	40	11:56:30 AM	58.6	60			80		

#### **Route 7 Field Data Sheets Description:** 9320 Leesburg Pike Site # H2 Atmospheric Done By:

EJA, ERZ Meter:

Monitoring Data:

Date Start Time **End Time** Duration

1:14 PM 20min Leq (dBA) 65.7

3/20/19

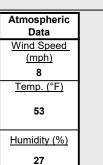
12:54 PM

Traffic Data: 20 Minute Roadway

Direction Traffic Total: Cars MT HT

Ro	oute 7	_S.		
EB	WB	-	NB	S
495	523	]	68	3
472	505		68	2
19	17			4
4	1			

EB	WB	NB	SB	
495	523	68	32	
472	505	68	28	
19	17		4	
4	1			



NB	SB	
17	41	
17	41	



Skel	lv a	nd I	Lov	inc.

<b>*</b>				
u.	\$ 7 - 8 -			
		O COMMON COMPRISACION C	and the second	
		A part of the		
Notes:	Marie Comment			

ım						-	Time	Lav (dBA)	_	Time	Lav (dBA)
1	12:54:00 PM	73.8	21	1:04:00 PM	63.6	41			61		
2	12:54:30 PM	72	22	1:04:30 PM	64.7	42			62		
3	12:55:00 PM	60.2	23	1:05:00 PM	62.2	43			63		
4	12:55:30 PM	63.5	24	1:05:30 PM	65.6	44			64		
5	12:56:00 PM	64.8	25	1:06:00 PM	63	45			65		
ô	12:56:30 PM	63.8	26	1:06:30 PM	60.9	46			66		
7	12:57:00 PM	65.6	27	1:07:00 PM	62.7	47			67		
3	12:57:30 PM	68.5	28	1:07:30 PM	63.7	48			68		
9	12:58:00 PM	64.8	29	1:08:00 PM	64.6	49			69		
0	12:58:30 PM	62.7	30	1:08:30 PM	66.5	50			70		
1	12:59:00 PM	66.1	31	1:09:00 PM	63.1	51			71		
2	12:59:30 PM	63.1	32	1:09:30 PM	67	52			72		
3	1:00:00 PM	64.8	33	1:10:00 PM	65.6	53			73		
4	1:00:30 PM	65.8	34	1:10:30 PM	64.1	54			74		
5	1:01:00 PM	64.7	35	1:11:00 PM	63.9	55			75		
6	1:01:30 PM	59.3	36	1:11:30 PM	64.8	56			76		
7	1:02:00 PM	66.3	37	1:12:00 PM	62.9	57			77		
8	1:02:30 PM	65	38	1:12:30 PM	64.2	58			78		
9	1:03:00 PM	64	39	1:13:00 PM	63.9	59			79		
0	1:03:30 PM	65.9	40	1:13:30 PM	64.2	60			80		
	2 2 3 3 1 5 6 7 7 3 3 4 5 6 7 7 8 8 9	1 12:54:00 PM 2 12:54:30 PM 3 12:55:00 PM 4 12:55:30 PM 5 12:56:00 PM 6 12:56:30 PM 7 12:57:00 PM 8 12:57:30 PM 9 12:58:00 PM 12:58:30 PM 12:58:30 PM 12:59:30 PM 12:59:30 PM 12:59:30 PM 12:59:30 PM 100:30 PM 100:30 PM 100:30 PM 100:30 PM 100:30 PM 100:30 PM 100:30 PM 100:30 PM 100:30 PM	1 12:54:00 PM 73.8 2 12:54:30 PM 72 3 12:55:00 PM 60.2 4 12:55:30 PM 63.5 5 12:56:00 PM 64.8 6 12:56:30 PM 63.8 7 12:57:00 PM 65.6 8 12:57:30 PM 68.5 9 12:57:30 PM 62.7 1 12:59:00 PM 64.8 1 12:59:00 PM 66.1 2 12:59:30 PM 63.1 3 1:00:00 PM 64.8 4 1:00:30 PM 65.8 5 1:01:00 PM 64.8 6 1:01:30 PM 65.8 7 1:02:00 PM 66.3 8 1:02:30 PM 65.9 9 1:03:00 PM 65	1 12:54:00 PM 73.8 21 2 12:54:30 PM 72 22 3 12:55:00 PM 60.2 23 4 12:55:30 PM 63.5 24 5 12:56:00 PM 64.8 25 6 12:56:30 PM 63.8 26 7 12:57:00 PM 65.6 27 3 12:57:30 PM 68.5 28 9 12:58:30 PM 64.8 29 1 12:58:30 PM 62.7 30 1 12:59:00 PM 66.1 31 1 12:59:30 PM 63.1 32 2 12:59:30 PM 64.8 33 4 1:00:30 PM 64.8 33 4 1:00:30 PM 65.8 34 5 1:01:00 PM 64.7 35 6 1:01:30 PM 59.3 36 7 1:02:00 PM 66.3 37 8 1:02:30 PM 65 38 9 1:03:00 PM 65	1         12:54:00 PM         73.8         21         1:04:00 PM           2         12:54:30 PM         72         22         1:04:30 PM           3         12:55:00 PM         60.2         23         1:05:00 PM           4         12:55:30 PM         63.5         24         1:05:30 PM           5         12:56:00 PM         64.8         25         1:06:00 PM           6         12:56:30 PM         63.8         26         1:06:30 PM           7         12:57:30 PM         65.6         27         1:07:00 PM           8         12:57:30 PM         68.5         28         1:07:30 PM           9         12:58:00 PM         64.8         29         1:08:00 PM           0         12:58:30 PM         62.7         30         1:08:30 PM           1         12:59:00 PM         66.1         31         1:09:00 PM           2         12:59:30 PM         63.1         32         1:09:30 PM           3         1:00:00 PM         64.8         33         1:10:00 PM           4         1:00:30 PM         65.8         34         1:10:30 PM           5         1:01:00 PM         64.7         35         1:11:00 PM	1         12:54:00 PM         73.8         21         1:04:00 PM         63.6           2         12:54:30 PM         72         22         1:04:30 PM         64.7           3         12:55:00 PM         60.2         23         1:05:00 PM         62.2           4         12:55:30 PM         63.5         24         1:05:30 PM         65.6           5         12:56:00 PM         64.8         25         1:06:00 PM         63           6         12:56:30 PM         63.8         26         1:06:30 PM         60.9           7         12:57:00 PM         65.6         27         1:07:00 PM         62.7           3         12:57:30 PM         68.5         28         1:07:30 PM         63.7           9         12:58:30 PM         62.7         30         1:08:30 PM         64.6           0         12:59:30 PM         66.1         31         1:09:00 PM         63.1           2         12:59:30 PM         63.1         32         1:09:30 PM         67           3         1:00:00 PM         64.8         33         1:10:00 PM         65.6           4         1:00:30 PM         65.8         34         1:10:30 PM         64.1<	1         12:54:00 PM         73.8         21         1:04:00 PM         63.6         41           2         12:54:30 PM         72         22         1:04:30 PM         64.7         42           3         12:55:00 PM         60.2         23         1:05:00 PM         62.2         43           4         12:55:30 PM         63.5         24         1:05:30 PM         65.6         44           5         12:56:00 PM         64.8         25         1:06:00 PM         63         45           6         12:56:30 PM         63.8         26         1:06:30 PM         60.9         46           7         12:57:00 PM         65.6         27         1:07:00 PM         62.7         47           8         12:57:30 PM         68.5         28         1:07:30 PM         63.7         48           9         12:58:30 PM         62.7         30         1:08:30 PM         64.6         49           0         12:59:30 PM         66.1         31         1:09:00 PM         63.1         51           1         12:59:30 PM         63.1         32         1:09:30 PM         67         52           3         1:00:00 PM         64.8	1       12:54:00 PM       73.8       21       1:04:00 PM       63.6       41         2       12:54:30 PM       72       22       1:04:30 PM       64.7       42         3       12:55:00 PM       60.2       23       1:05:00 PM       62.2       43         4       12:55:30 PM       63.5       24       1:05:30 PM       65.6       44         5       12:56:00 PM       64.8       25       1:06:00 PM       63       45         6       12:56:30 PM       63.8       26       1:06:30 PM       60.9       46         7       12:57:00 PM       65.6       27       1:07:00 PM       62.7       47         3       12:57:30 PM       68.5       28       1:07:30 PM       63.7       48         9       12:58:00 PM       64.8       29       1:08:00 PM       64.6       49         0       12:59:30 PM       66.1       31       1:09:00 PM       63.5       50         1       12:59:30 PM       63.1       32       1:09:30 PM       67       52         3       1:00:00 PM       64.8       33       1:10:00 PM       65.6       53         4       1:00:30 PM <td< th=""><th>1 12:54:00 PM 73.8 21 1:04:00 PM 63.6 41 2 12:54:30 PM 72 22 1:04:30 PM 64.7 42 3 12:55:00 PM 60.2 23 1:05:00 PM 62.2 43 4 12:55:30 PM 63.5 24 1:05:30 PM 65.6 44 5 12:56:00 PM 64.8 25 1:06:00 PM 63 45 6 12:56:30 PM 63.8 26 1:06:30 PM 60.9 46 7 12:57:00 PM 65.6 27 1:07:00 PM 62.7 47 8 12:57:30 PM 68.5 28 1:07:30 PM 63.7 48 9 12:58:30 PM 64.8 29 1:08:00 PM 64.6 49 0 12:58:30 PM 62.7 30 1:08:30 PM 66.5 50 1 12:59:00 PM 66.1 31 1:09:00 PM 63.1 51 1 12:59:00 PM 64.8 33 1:10:00 PM 67 5 1:01:00 PM 64.8 33 1:10:00 PM 64.1 54 5 1:01:30 PM 65.8 34 1:10:30 PM 64.8 56 7 1:02:00 PM 66.3 37 1:12:00 PM 64.8 56 7 1:02:00 PM 66.3 37 1:12:00 PM 64.8 56 9 1:03:00 PM 66.3 37 1:12:00 PM 64.8 56 9 1:03:00 PM 66.3 37 1:12:00 PM 64.8 56 9 1:03:00 PM 66.3 37 1:12:00 PM 64.2 58 9 1:03:00 PM 64.2 58</th><th>1       12:54:00 PM       73.8       21       1:04:00 PM       63.6       41       61         2       12:54:30 PM       72       22       1:04:30 PM       64.7       42       62         3       12:55:00 PM       60.2       23       1:05:00 PM       62.2       43       63         4       12:55:30 PM       63.5       24       1:05:30 PM       65.6       44       64         5       12:56:00 PM       64.8       25       1:06:00 PM       63       45       65         6       12:56:30 PM       63.8       26       1:06:30 PM       60.9       46       66         7       12:57:00 PM       65.6       27       1:07:00 PM       62.7       47       67         8       12:57:30 PM       68.5       28       1:07:30 PM       63.7       48       68         9       12:58:30 PM       64.8       29       1:08:30 PM       66.5       50       70         12:59:30 PM       66.1       31       1:09:00 PM       66.5       50       70         12:59:30 PM       66.1       31       1:09:00 PM       67       52       72         3       1:00:00 PM       <td< th=""><th>1       12:54:00 PM       73.8       21       1:04:00 PM       63.6       41       61         2       12:54:30 PM       72       22       1:04:30 PM       64.7       42       62         3       12:55:00 PM       60.2       23       1:05:00 PM       62.2       43       63         4       12:55:30 PM       63.5       24       1:05:30 PM       65.6       44       64         5       12:56:00 PM       64.8       25       1:06:00 PM       63       45       65         6       12:56:30 PM       63.8       26       1:06:30 PM       60.9       46       66         7       12:57:00 PM       65.6       27       1:07:00 PM       62.7       47       67         3       12:57:30 PM       68.5       28       1:07:30 PM       63.7       48       68         9       12:58:30 PM       64.8       29       1:08:00 PM       64.6       49       69         0       12:58:30 PM       62.7       30       1:08:30 PM       66.5       50       70         1       12:59:30 PM       66.1       31       1:09:00 PM       63.1       51       71         1</th></td<></th></td<>	1 12:54:00 PM 73.8 21 1:04:00 PM 63.6 41 2 12:54:30 PM 72 22 1:04:30 PM 64.7 42 3 12:55:00 PM 60.2 23 1:05:00 PM 62.2 43 4 12:55:30 PM 63.5 24 1:05:30 PM 65.6 44 5 12:56:00 PM 64.8 25 1:06:00 PM 63 45 6 12:56:30 PM 63.8 26 1:06:30 PM 60.9 46 7 12:57:00 PM 65.6 27 1:07:00 PM 62.7 47 8 12:57:30 PM 68.5 28 1:07:30 PM 63.7 48 9 12:58:30 PM 64.8 29 1:08:00 PM 64.6 49 0 12:58:30 PM 62.7 30 1:08:30 PM 66.5 50 1 12:59:00 PM 66.1 31 1:09:00 PM 63.1 51 1 12:59:00 PM 64.8 33 1:10:00 PM 67 5 1:01:00 PM 64.8 33 1:10:00 PM 64.1 54 5 1:01:30 PM 65.8 34 1:10:30 PM 64.8 56 7 1:02:00 PM 66.3 37 1:12:00 PM 64.8 56 7 1:02:00 PM 66.3 37 1:12:00 PM 64.8 56 9 1:03:00 PM 66.3 37 1:12:00 PM 64.8 56 9 1:03:00 PM 66.3 37 1:12:00 PM 64.8 56 9 1:03:00 PM 66.3 37 1:12:00 PM 64.2 58 9 1:03:00 PM 64.2 58	1       12:54:00 PM       73.8       21       1:04:00 PM       63.6       41       61         2       12:54:30 PM       72       22       1:04:30 PM       64.7       42       62         3       12:55:00 PM       60.2       23       1:05:00 PM       62.2       43       63         4       12:55:30 PM       63.5       24       1:05:30 PM       65.6       44       64         5       12:56:00 PM       64.8       25       1:06:00 PM       63       45       65         6       12:56:30 PM       63.8       26       1:06:30 PM       60.9       46       66         7       12:57:00 PM       65.6       27       1:07:00 PM       62.7       47       67         8       12:57:30 PM       68.5       28       1:07:30 PM       63.7       48       68         9       12:58:30 PM       64.8       29       1:08:30 PM       66.5       50       70         12:59:30 PM       66.1       31       1:09:00 PM       66.5       50       70         12:59:30 PM       66.1       31       1:09:00 PM       67       52       72         3       1:00:00 PM <td< th=""><th>1       12:54:00 PM       73.8       21       1:04:00 PM       63.6       41       61         2       12:54:30 PM       72       22       1:04:30 PM       64.7       42       62         3       12:55:00 PM       60.2       23       1:05:00 PM       62.2       43       63         4       12:55:30 PM       63.5       24       1:05:30 PM       65.6       44       64         5       12:56:00 PM       64.8       25       1:06:00 PM       63       45       65         6       12:56:30 PM       63.8       26       1:06:30 PM       60.9       46       66         7       12:57:00 PM       65.6       27       1:07:00 PM       62.7       47       67         3       12:57:30 PM       68.5       28       1:07:30 PM       63.7       48       68         9       12:58:30 PM       64.8       29       1:08:00 PM       64.6       49       69         0       12:58:30 PM       62.7       30       1:08:30 PM       66.5       50       70         1       12:59:30 PM       66.1       31       1:09:00 PM       63.1       51       71         1</th></td<>	1       12:54:00 PM       73.8       21       1:04:00 PM       63.6       41       61         2       12:54:30 PM       72       22       1:04:30 PM       64.7       42       62         3       12:55:00 PM       60.2       23       1:05:00 PM       62.2       43       63         4       12:55:30 PM       63.5       24       1:05:30 PM       65.6       44       64         5       12:56:00 PM       64.8       25       1:06:00 PM       63       45       65         6       12:56:30 PM       63.8       26       1:06:30 PM       60.9       46       66         7       12:57:00 PM       65.6       27       1:07:00 PM       62.7       47       67         3       12:57:30 PM       68.5       28       1:07:30 PM       63.7       48       68         9       12:58:30 PM       64.8       29       1:08:00 PM       64.6       49       69         0       12:58:30 PM       62.7       30       1:08:30 PM       66.5       50       70         1       12:59:30 PM       66.1       31       1:09:00 PM       63.1       51       71         1

Site #	M1	Description:	1426 Woodhurst Blvd	
Done By:	EJA, ERZ			Atmospheric Data
Meter:	<b></b>	1		Wind Speed (mph)
Monitoring	Data:			8
<b>_</b>	Date	3/20/19		Temp. (°F)
	Start Time	1:42 PM		
	End Time	2:02 PM		53
	Duration	20 min		
	Leq (dBA)	52.5		Humidity (%)
Traffic Data	a: 20 Minute			27
	Roadway	Route 7	Lewinsville	
	Direction	EB WB	NB SB	
	Traffic Total:	430 507	91 111	
	Cars	401 478	86 105	

Site Data: Site Surface: Grass Grade: Pavement Type: Average



Site is quiet, terrain feature (berm) and a privacy fence around 8ft tall on berm reduce road noise.



Num	Time	Lav (dBA)	Num	Time	Lav (dBA)	Num	Time	Lav (	dBA)	Num	Time	Lav	(dBA)
1	1:42:00 PM	53.3	21	1:52:00 PM	49.8	41		,		61			
2	1:42:30 PM	50.2	22	1:52:30 PM	51.4	42				62			
3	1:43:00 PM	50.2	23	1:53:00 PM	53.7	43				63			
4	1:43:30 PM	48.3	24	1:53:30 PM	50.3	44				64			
5	1:44:00 PM	52.6	25	1:54:00 PM	48.4	45				65			
6	1:44:30 PM	51.6	26	1:54:30 PM	48.1	46				66			
7	1:45:00 PM	50.8	27	1:55:00 PM	48	47				67			
8	1:45:30 PM	48	28	1:55:30 PM	47.4	48				68			
9	1:46:00 PM	48.2	29	1:56:00 PM	53.1	49				69			
10	1:46:30 PM	49.7	30	1:56:30 PM	52.2	50				70			
11	1:47:00 PM	53.5	31	1:57:00 PM	50.3	51				71			
12	1:47:30 PM	55.5	32	1:57:30 PM	50	52				72			
13	1:48:00 PM	56.4	33	1:58:00 PM	48.6	53				73			
14	1:48:30 PM	52.1	34	1:58:30 PM	50	54				74			
15	1:49:00 PM	55.7	35	1:59:00 PM	55.1	55				75			
16	1:49:30 PM	50.5	36	1:59:30 PM	52.9	56				76			
17	1:50:00 PM	55.5	37	2:00:00 PM	50	57				77			
18	1:50:30 PM	56.7	38	2:00:30 PM	49.6	58				78			
19	1:51:00 PM	56.6	39	2:01:00 PM	49.3	59				79			
20	1:51:30 PM	49.4	40	2:01:30 PM	56.8	60				80			

Site #	K1	Descri	ption :	9101	Lucky E	states Dr	ive		
Done By:	EJA, ERZ							Atmos Da	
Meter:	<b></b>		3					Wind S (mr	
Monitoring	Data:							8	
J	Date		20/19					Temp	. (°F)
	Start Time End Time Duration	1:1	54 PM 4 PM Omin		_			53	3
	Leq (dBA)	5	7.2					<u>Humidi</u>	ty (%)
Traffic Data	a: <b>20 Minute</b> Roadway	Ro	ute 7	S. To	wlston	N. To	wlston	27	7
	Direction Traffic Total: Cars MT HT	EB 495 472 19 4	WB 523 505 17 1	NB 68 68	SB 32 28 4	NB 17 17	SB 41 41		
Site Data:	Site Surface:	Grass	Grade:		l F	avemen	t Type:	Avera	ge





Num	Time	Lav (dBA)	Num	Time	Lav (dBA)	Num	Time	Lav	(dBA)	Num	Time	Lav (dBA)
1	12:54:00 PM	59.4	21	1:04:00 PM	, ,	41			. ,	61		,
2	12:54:30 PM	53.6	22	1:04:30 PM	58.1	42				62		
3	12:55:00 PM	58.3	23	1:05:00 PM	55.7	43				63		
4	12:55:30 PM	58	24	1:05:30 PM	56.3	44				64		
5	12:56:00 PM	57.7	25	1:06:00 PM	57.2	45				65		
6	12:56:30 PM	55.5	26	1:06:30 PM	54.5	46				66		
7	12:57:00 PM	56.7	27	1:07:00 PM	55.6	47				67		
8	12:57:30 PM	58.2	28	1:07:30 PM	57.3	48				68		
9	12:58:00 PM	58.5	29	1:08:00 PM	53.9	49				69		
10	12:58:30 PM	49.4	30	1:08:30 PM	50.6	50				70		
11	12:59:00 PM	56.1	31	1:09:00 PM	60.7	51				71		
12	12:59:30 PM	56.7	32	1:09:30 PM	59.3	52				72		
13	1:00:00 PM	57.4	33	1:10:00 PM	58	53				73		
14	1:00:30 PM	51.1	34	1:10:30 PM	57.2	54				74		
15	1:01:00 PM	57.2	35	1:11:00 PM	54.7	55				75		
16	1:01:30 PM	60.5	36	1:11:30 PM	57.6	56				76		
17	1:02:00 PM	57.4	37	1:12:00 PM	58.4	57				77		
18	1:02:30 PM	51.7	38	1:12:30 PM	53.7	58				78		
19	1:03:00 PM	59.2	39	1:13:00 PM	57.9	59				79		
20	1:03:30 PM	59.4	40	1:13:30 PM	58.2	60				80		

Site #	J1	Descrip	otion :	1308	Trap Ro	ad			
Done By:	EJA, ERZ								spheric ata
Meter:	<b></b>		2						Speed ph)
Monitoring	Data:								8
	Date	3/2	20/19					Tem	o. (°F)
	Start Time		54 PM						
	End Time		4 PM					5	53
	Duration	20	)min						
	Leq (dBA)	5	6.5					<u>Humic</u>	lity (%)
Traffic Date	a:_20 Minute							2	27
ITAIIIC DAL	Roadway	Ro	ute 7	S. To	wlston	N. To	wlston		
	Direction	EB	WB	NB	SB	NB	SB		
	Traffic Total:	495	523	68	32	17	41		
	Cars	472	505	68	28	17	41		
	MT	19	17		4				
	HT	4	1						

Pavement Type:

Average

Site Data: Site Surface: Grass Grade:



	- C	
		Contract of the Contract of th
		TRAP ROAD
Pop.		OAD

Num	Time	Lav (dBA)	Num	Time	Lav (dBA)	Num	Time	Lav (d	BA)	Num	Time	Lav (dB	A)
1	12:54:00 PM	61.7	21	1:04:00 PM	55.7	41				61			
2	12:54:30 PM	58.4	22	1:04:30 PM	49.6	42				62			
3	12:55:00 PM	57.6	23	1:05:00 PM	54	43				63			
4	12:55:30 PM	56.7	24	1:05:30 PM	55.5	44				64			
5	12:56:00 PM	54.4	25	1:06:00 PM	54.3	45				65			
6	12:56:30 PM	60.2	26	1:06:30 PM	50.9	46				66			
7	12:57:00 PM	61.6	27	1:07:00 PM	51.3	47				67			
8	12:57:30 PM	59.3	28	1:07:30 PM	52.7	48				68			
9	12:58:00 PM	61.4	29	1:08:00 PM	54.3	49				69			
10	12:58:30 PM	61.7	30	1:08:30 PM	56.4	50				70			
11	12:59:00 PM	52.2	31	1:09:00 PM	57.3	51				71			
12	12:59:30 PM	55.1	32	1:09:30 PM	56.1	52				72			
13	1:00:00 PM	52.9	33	1:10:00 PM	55.1	53				73			
14	1:00:30 PM	50	34	1:10:30 PM	52.3	54				74			
15	1:01:00 PM	54.4	35	1:11:00 PM	53.2	55				75			
16	1:01:30 PM	55.1	36	1:11:30 PM	55.6	56				76			
17	1:02:00 PM	53.8	37	1:12:00 PM	54.6	57				77			
18	1:02:30 PM	51.4	38	1:12:30 PM	52.3	58				78			
19	1:03:00 PM	56.7	39	1:13:00 PM	54.9	59				79			
20	1:03:30 PM	54.6	40	1:13:30 PM	56	60				80		·	

******* Filename Test Locat Employee N Employee N Department	******* ion ame umber 1003 Autum	***********MON1VA 7ERZ, EJAENV n Mist Lane	*****	*****	*****
Calibrator Calibrator ******	Type Cal. Date ******	  ******	*****	*****	*****
METROSONIC REPORT PRI	S db-3080 NTED ON 03	V1.20 SERIAL /21/19 at 15:36	# 5093 :07		
User ID: _					
LOGGING ST TOTAL LOGG LOGGING ST TOTAL INTE INTERVAL L	ARTED ING TIME OPPED RVALS ENGTH	.03/20/19 at 09 .0 DAYS 01:01:2 .03/20/19 at 10 0.123 .00:00:30	:41:00 4 :42:24		
AUTO STOP. CLOCK SYNC RESPONSE R FILTER	 H ATE	.NO .YES .SLOW .A WT.			
PRE-TEST C PRE-TEST C POST-TEST CUTOFF USE	ALIBRATION ALIBRATION CALIBRATIO D FOR TIME	TIME03/20/ RANGE41.0 T N NOT DONE HISTORY Lav	19 AT 09:3 O 141.0 dB NONE	9:10	
<<< SUMMAR	Y REPORT F	OR TEST NUMBER	1 OF 1 >>>		

EXCHANGE R ATE......

.....

CUTOFFS...

CEILING...

...3dB

...115dB

... 80dB 90dB

DOSE CRITE	RION LEVEL	90dB					
DOSE CRITE	RION LENGT	H 8 HOURS					
Lav	60.	4dB					
Lav ( 80).	41.	0dB					
Lav ( 90).	41.	0dB					
SEL	96.	OdB					
TWA	51.	6dB					
TWA (80).	41.	OdB					
TWA ( 90).	41.	OdB					
Lmax	70.	6dB 03/20/19 a	t 09:48:15				
Lpk	70. UNDER	RANGE	109.48.13				
TIME OVER	115dB00	:00:00.00					
THVIL OVER	1130500	.00.00.00					
DOSE ( 80)		0.00%					
PROJ. DOSE	( 80)	0.00%					
DOSE ( 90)		0.00%					
PROJ. DOSE	( 90)	0.00%					
<<< TIME H	ISTORY REP	ORT FOR TEST NU	MBER 1 OF	1>>>			
TINAC	Lave	Lanav	اساد	1/10 0\	1/00.0)		
TIME	Lav	Lmax	Lpk	L(10.0)	L(99.9)		
	dBA	Lmax dBA	Lpk dBC	L(10.0) dBA	L(99.9) dBA		
3/20/2019	dBA )	dBA	dBC		dBA	<b>E</b> 2	E40E40.0
3/20/2019 9:41:00	dBA ) ) 57.4	dBA 62	dBC UNDER		dBA		549540.9
3/20/2019 9:41:00 9:41:30	dBA ) ) 57.4 ) 55.8	dBA 62 60.1	dBC UNDER UNDER	dBA	dBA 60 57	51	380189.4
3/20/2019 9:41:00 9:41:30 9:42:00	dBA ) 57.4 ) 55.8 ) 60.1	dBA 62 60.1 61.8	dBC UNDER UNDER UNDER	dBA	dBA 60 57 61	51 57	380189.4 1023293
3/20/2019 9:41:00 9:41:30 9:42:00 9:42:30	dBA 57.4 55.8 60.1 60.1	dBA 62 60.1 61.8 62	UNDER UNDER UNDER UNDER UNDER	dBA	dBA 60 57 61 61	51 57 58	380189.4 1023293 1023293
3/20/2019 9:41:00 9:41:30 9:42:00 9:42:30 9:43:00	dBA ) 57.4 ) 55.8 ) 60.1 ) 60.1 ) 58.9	62 60.1 61.8 62 60.3	UNDER UNDER UNDER UNDER UNDER UNDER	dBA	dBA  60 57 61 61 60	51 57 58 57	380189.4 1023293 1023293 776247.1
3/20/2019 9:41:00 9:41:30 9:42:00 9:42:30 9:43:00 9:43:30	dBA 57.4 55.8 60.1 60.1 58.9 60.9	dBA 62 60.1 61.8 62 60.3 62.7	UNDER UNDER UNDER UNDER UNDER UNDER UNDER UNDER	dBA	dBA  60 57 61 61 60 62	51 57 58 57 59	380189.4 1023293 1023293 776247.1 1230269
3/20/2019 9:41:00 9:41:30 9:42:00 9:42:30 9:43:30 9:43:30	dBA 57.4 55.8 60.1 60.1 58.9 60.9 61.7	dBA  62 60.1 61.8 62 60.3 62.7 63.6	UNDER UNDER UNDER UNDER UNDER UNDER UNDER UNDER UNDER	dBA	dBA  60 57 61 61 60 62 63	51 57 58 57 59	380189.4 1023293 1023293 776247.1 1230269 1479108
3/20/2019 9:41:00 9:41:30 9:42:00 9:42:30 9:43:00 9:43:30 9:44:00	dBA 57.4 55.8 60.1 60.1 58.9 60.9 61.7	dBA  62 60.1 61.8 62 60.3 62.7 63.6 66.9	UNDER	dBA	dBA  60 57 61 61 60 62 63 66	51 57 58 57 59 59	380189.4 1023293 1023293 776247.1 1230269 1479108 2187762
3/20/2019 9:41:00 9:41:30 9:42:00 9:42:30 9:43:30 9:43:30 9:44:00 9:44:30	dBA  57.4  55.8  60.1  60.1  58.9  60.9  61.7  63.4	dBA  62 60.1 61.8 62 60.3 62.7 63.6 66.9 59.7	UNDER	dBA	dBA  60 57 61 61 60 62 63 66 59	51 57 58 57 59 59 59	380189.4 1023293 1023293 776247.1 1230269 1479108 2187762 691831
3/20/2019 9:41:00 9:41:30 9:42:00 9:42:30 9:43:00 9:43:30 9:44:00 9:44:30 9:45:30	dBA  57.4  55.8  60.1  60.1  58.9  60.9  61.7  63.4  58.4  59.2	dBA  62 60.1 61.8 62 60.3 62.7 63.6 66.9 59.7 62.8	UNDER	dBA	dBA  60 57 61 61 60 62 63 66 59 61	51 57 58 57 59 59 59 57	380189.4 1023293 1023293 776247.1 1230269 1479108 2187762 691831 831763.8
3/20/2019 9:41:00 9:41:30 9:42:00 9:42:30 9:43:30 9:43:30 9:44:30 9:44:30 9:45:00 9:45:30	dBA  57.4  55.8  60.1  60.1  60.9  61.7  63.4  58.4  59.2  61.1	dBA  62 60.1 61.8 62 60.3 62.7 63.6 66.9 59.7 62.8 62	UNDER	dBA	dBA  60 57 61 61 60 62 63 66 59 61 61	51 57 58 57 59 59 59 57 57	380189.4 1023293 1023293 776247.1 1230269 1479108 2187762 691831 831763.8 1288250
3/20/2019 9:41:00 9:41:30 9:42:30 9:42:30 9:43:30 9:44:00 9:44:30 9:45:00 9:45:30 9:46:00	dBA  57.4  55.8  60.1  60.1  58.9  60.9  61.7  63.4  59.2  61.1  63.6	dBA  62 60.1 61.8 62 60.3 62.7 63.6 66.9 59.7 62.8 62 65.6	UNDER	dBA	dBA  60 57 61 61 60 62 63 66 59 61 61 61	51 57 58 57 59 59 57 57 57 60	380189.4 1023293 1023293 776247.1 1230269 1479108 2187762 691831 831763.8 1288250 2290868
3/20/2019 9:41:00 9:41:30 9:42:00 9:42:30 9:43:30 9:43:30 9:44:30 9:45:30 9:45:30 9:46:30 9:47:00	dBA  57.4  55.8  60.1  60.1  60.9  61.7  63.4  59.2  61.1  63.6  61.8	dBA  62 60.1 61.8 62 60.3 62.7 63.6 66.9 59.7 62.8 62 65.6 68	UNDER	dBA	dBA  60 57 61 61 60 62 63 66 59 61 61 61 65 64	51 57 58 57 59 59 59 57 57 59 60 59	380189.4 1023293 1023293 776247.1 1230269 1479108 2187762 691831 831763.8 1288250 2290868 1513561
3/20/2019 9:41:00 9:41:30 9:42:30 9:42:30 9:43:30 9:43:30 9:44:00 9:45:00 9:45:30 9:46:00 9:46:30 9:47:30	dBA  57.4  55.8  60.1  60.1  60.9  61.7  63.4  59.2  61.1  63.6  61.8  63.3	dBA  62 60.1 61.8 62 60.3 62.7 63.6 66.9 59.7 62.8 62 65.6 68 65.6	UNDER	dBA	dBA  60 57 61 61 60 62 63 66 59 61 61 65 64	51 57 58 57 59 59 57 57 59 60 59 62	380189.4 1023293 1023293 776247.1 1230269 1479108 2187762 691831 831763.8 1288250 2290868 1513561 2137962
3/20/2019 9:41:00 9:41:30 9:42:00 9:42:30 9:43:30 9:43:30 9:44:30 9:45:30 9:45:30 9:46:30 9:47:00	dBA  57.4  55.8  60.1  60.1  60.1  60.9  61.7  63.4  59.2  61.1  63.6  61.8  63.3  65.1	dBA  62 60.1 61.8 62 60.3 62.7 63.6 66.9 59.7 62.8 62 65.6 68 65.6 70.6	UNDER	dBA	dBA  60 57 61 61 60 62 63 66 59 61 61 65 64 64	51 57 58 57 59 59 59 57 57 59 60 59	380189.4 1023293 1023293 776247.1 1230269 1479108 2187762 691831 831763.8 1288250 2290868 1513561 2137962 3235937
3/20/2019 9:41:00 9:41:30 9:42:00 9:42:30 9:43:30 9:43:30 9:44:30 9:44:30 9:45:00 9:45:30 9:46:00 9:47:30 9:47:30 9:48:00	dBA  57.4  55.8  60.1  60.1  58.9  60.9  61.7  63.4  59.2  61.1  63.6  61.8  63.3  65.1  61.6	dBA  62 60.1 61.8 62 60.3 62.7 63.6 66.9 59.7 62.8 62 65.6 68 65.6 70.6 62.9	UNDER	dBA	dBA  60 57 61 61 60 62 63 66 59 61 61 65 64 64 67 62	51 57 58 57 59 59 57 57 59 60 59 62 62	380189.4 1023293 1023293 776247.1 1230269 1479108 2187762 691831 831763.8 1288250 2290868 1513561 2137962 3235937 1445440
3/20/2019 9:41:00 9:41:30 9:42:30 9:42:30 9:43:30 9:43:30 9:44:00 9:45:00 9:45:30 9:46:30 9:47:30 9:48:30 9:48:30 9:49:00	dBA  57.4  55.8  60.1  60.1  60.9  61.7  63.4  59.2  61.1  63.6  61.8  63.3  65.1  60.6	dBA  62 60.1 61.8 62 60.3 62.7 63.6 66.9 59.7 62.8 62 65.6 68 65.6 70.6 62.9 61.8	UNDER	dBA	dBA  60 57 61 61 60 62 63 66 59 61 61 65 64 64 67 62 60	51 57 58 57 59 59 57 57 59 60 59 62 62 60 58	380189.4 1023293 1023293 776247.1 1230269 1479108 2187762 691831 831763.8 1288250 2290868 1513561 2137962 3235937 1445440 10000000
3/20/2019 9:41:00 9:41:30 9:42:00 9:42:30 9:43:30 9:43:30 9:44:30 9:44:30 9:45:00 9:45:30 9:46:00 9:47:30 9:47:30 9:48:00	dBA  57.4  55.8  60.1  60.1  60.9  61.7  63.4  58.4  60.9  61.1  63.6  61.8  63.3  65.1  60.6  60.6  60.6	62 60.1 61.8 62 60.3 62.7 63.6 66.9 59.7 62.8 62 65.6 68 65.6 70.6 62.9 61.8	UNDER	dBA	dBA  60 57 61 61 60 62 63 66 59 61 61 65 64 64 67 62	51 57 58 57 59 59 57 57 59 60 59 62 62 60	380189.4 1023293 1023293 776247.1 1230269 1479108 2187762 691831 831763.8 1288250 2290868 1513561 2137962 3235937 1445440

62 UNDER

61

59 1202264

9:50:30

60.8

9:51:00	62.1	63.3 UNDER	63	60 1621810
9:51:30	62.7	64.5 UNDER	63	61 1862087
9:52:00	62.9	66.8 UNDER	65	59 1949845
9:52:30	59.4	60.2 UNDER	60	58 870963.6
9:53:00	59.9	61.4 UNDER	61	58 977237.2
9:53:30	61.5	62.4 UNDER	61	60 1412538
9:54:00	63.4	66.8 UNDER	65	61 2187762
9:54:30	60.5	62.9 UNDER	60	59 1122018
9:55:00	61.9	65.2 UNDER	64	59 1548817
9:55:30	61	62.4 UNDER	62	59 1258925
9:56:00	61.2	63.5 UNDER	62	59 1318257
9:56:30	63.1	66 UNDER	65	60 2041738
9:57:00	62.4	67.2 UNDER	64	59 1737801
9:57:30	60.9	61.9 UNDER	61	60 1230269
9:58:00	60.7	62.8 UNDER	61	59 1174898
9:58:30	61.5	62.9 UNDER	62	58 1412538
9:59:00	61.8	65.6 UNDER	63	59 1513561
9:59:30	61.4	63.8 UNDER	62	60 1380384
10:00:00	60.6	61.6 UNDER	61	59 1148154
10:00:30	61	63.2 UNDER	62	59 1258925
10:01:00	61.4	65.6 UNDER	64	59 1380384
10:01:30	60.1	65.3 UNDER	62	58 1023293
10:02:00	62.2	63.6 UNDER	63	61 1659587
10:02:30	60.2	61.2 UNDER	60	59 1047129
10:03:00	60.8	62.1 UNDER	61	59 1202264
10:03:30	60.7	62 UNDER	61	59 1174898
10:04:00	60.4	62.5 UNDER	61	58 1096478
10:04:30	59.9	61.3 UNDER	60	58 977237.2
10:05:00	61.6	64.9 UNDER	64	59 1445440
10:05:30	63.3	66.6 UNDER	65	59 2137962
10:06:00	61.3	62.5 UNDER	62	59 1348963
10:06:30	61.8	62.8 UNDER	62	60 1513561
10:07:00	61.9	63.7 UNDER	62	59 1548817
10:07:30	62.3	63.4 UNDER	63	60 1698244
10:08:00	59.9	61.8 UNDER	61	57 977237.2
10:08:30	58.5	59.4 UNDER	58	57 707945.8
10:09:00	60.6	62.5 UNDER	62	58 1148154
10:09:30	61.7	62.7 UNDER	62	60 1479108
10:10:00	62.5	64.1 UNDER	63	60 1778279
10:10:30	59.6	60.9 UNDER	60	58 912010.8
10:11:00	61.7	63.7 UNDER	63	58 1479108
10:11:30	62	65.4 UNDER	64	60 1584893
10:12:00	62.2	63 UNDER	62	60 1659587
10:12:30	59.8	61.2 UNDER	60	58 954992.6
10:12:00	58.8	60.7 UNDER	59	57 758577.6
10:13:30	62.6	65.3 UNDER	64	60 1819701
10.10.00	02.0	SSIS SINDLIN	<b>0</b> 1	30 1013701

10:14:00	61.8	64.1 UNDER	63	59	1513561
10:14:30	60.5	61.4 UNDER	61	58	1122018
10:15:00	59.7	61.2 UNDER	60	57	933254.3
10:15:30	62.2	64 UNDER	63	60	1659587
10:16:00	62.3	64.1 UNDER	63	60	1698244
10:16:30	60.2	61.2 UNDER	61	58	1047129
10:17:00	60.8	62.1 UNDER	61	59	1202264
10:17:30	63.6	68.5 UNDER	66	60	2290868
10:18:00	60.7	61.6 UNDER	61	59	1174898
10:18:30	60.3	62 UNDER	61	57	1071519
10:19:00	62.1	64.3 UNDER	63	60	1621810
10:19:30	63.1	66.5 UNDER	65	60	2041738
10:20:00	62.2	63.6 UNDER	63	60	1659587
10:20:30	58.7	60.4 UNDER	60	57	741310.2
10:21:00	60.4	62.4 UNDER	61	57	1096478
10:21:30	62.8	63.9 UNDER	63	59	1905461
10:22:00	58.4	61.4 UNDER	59	54	691831
10:22:30	53.1	57.2 UNDER	56	47	204173.8
10:23:00	56.1	60 UNDER	58	51	407380.3
10:23:30	60.4	66 UNDER	65	52	1096478
10:24:00	57.3	59.2 UNDER	58	54	537031.8
10:24:30	54.3	60.4 UNDER	59	46	269153.5
10:25:00	54.7	57.9 UNDER	56	47	295120.9
10:25:30	59.6	62.4 UNDER	61	54	912010.8
10:26:00	59.7	62 UNDER	61	55	933254.3
10:26:30	52	56.6 UNDER	55	45	158489.3
10:27:00	54.5	56.5 UNDER	56	49	281838.3
10:27:30	56.5	59.4 UNDER	58	53	446683.6

10:28:00	57.2	59.7 UNDER	57	55	524807.5
10:28:30	54.2	59.7 UNDER	57	47	263026.8
10:29:00	57.2	59.8 UNDER	59	54	524807.5
10:29:30	60.1	62.1 UNDER	61	56	1023293
10:30:00	59.7	63.3 UNDER	61	54	933254.3
10:30:30	57.8	64.8 UNDER	61	49	602559.6
10:31:00	53.4	57.6 UNDER	56	50	218776.2
10:31:30	60	62.5 UNDER	61	56	1000000
10:32:00	58.4	61.8 UNDER	61	49	691831
10:32:30	49	53.2 UNDER	51	45	79432.82
10:33:00	55.8	59.4 UNDER	59	46	380189.4
10:33:30	59	62.1 UNDER	61	54	794328.2
10:34:00	54.3	59.1 UNDER	56	52	269153.5
10:34:30	49.1	53.7 UNDER	53	43	81283.05
10:35:00	54.4	58.7 UNDER	58	43	275422.9
10:35:30	62.1	66.4 UNDER	65	54	1621810
10:36:00	61.5	66.4 UNDER	63	57	1412538
10:36:30	56.7	61.2 UNDER	60	53	467735.1
10:37:00	53.7	56.9 UNDER	56	48	234422.9
10:37:30	58.8	63 UNDER	62	55	758577.6
10:38:00	55.7	59.6 UNDER	58	51	371535.2
10:38:30	51.6	56.4 UNDER	56	45	144544
10:39:00	55.9	60.4 UNDER	59	46	389045.1
10:39:30	59	60.8 UNDER	60	56	794328.2
10:40:00	57.3	59.9 UNDER	59	50	537031.8
10:40:30	49	52.6 UNDER	51	46	79432.82
10:41:00	52.3	55.4 UNDER	54	46	169824.4
10:41:30	58.4	61.9 UNDER	61	52	691831
10:42:00	61.4	63.2 UNDER	62	57	1380384

******** Filename Test Locat Employee N Employee N Department	******** ion ame umber 11582 Cdar	**************************************	*****	*****	*****
Calibrator Calibrator ******	Type Cal. Date ******	  *******	*****	******	*****
METROSONIC REPORT PRI	S db-3080 NTED ON 03	V1.12 SERIAL /21/19 at 15:37	# 3895 :30		
User ID: _					
LOGGING ST TOTAL LOGG LOGGING ST TOTAL INTE INTERVAL L	ARTED ING TIME OPPED RVALS ENGTH	.03/20/19 at 09 .0 DAYS 01:09:3 .03/20/19 at 10 0.14 .00:00:30	:27:00 5 :36:35		
AUTO STOP. CLOCK SYNC RESPONSE R FILTER	 H ATE	.NO .YES .SLOW .A WT.			
PRE-TEST C PRE-TEST C POST-TEST CUTOFF USE	ALIBRATION ALIBRATION CALIBRATIO D FOR TIME	TIME03/20/ RANGE40.1 T N NOT DONE HISTORY Lav	19 AT 09:2 O 140.1 dB NONE	4:41	
<<< SUMMAR	Y REPORT F	OR TEST NUMBER	1 OF 1 >>>		

EXCHANGE R ATE...... ...3dB

CUTOFFS... ....... ... 80dB 90dB CEILING... ...... ....115dB

DOSE CRITE DOSE CRITE	RION LEVEL RION LENGT		
Lav Lav ( 80). Lav ( 90). SEL	40. 40.	OdB 1dB 1dB 1dB	
TWA TWA ( 80). TWA ( 90).	40.	7dB 1dB 1dB	
Lmax Lpk TIME OVER	UNDER	RANGE	36:33
DOSE ( 80) PROJ. DOSE DOSE ( 90) PROJ. DOSE		0.00% 0.00% 0.00% 0.00%	

<<< TIME H	ISTORY REP	ORT FOR TEST NU	MBER 1 OF	1 >>>
>>>	IDIONI NEI		INIDEILTOI	1///

<<< TIME H	ISTORY REP	ORT FOR TEST NU	MBER 1 OF	1>>>			
	Lav dBA	Lmax dBA	Lpk dBC	L(10.0) dBA	L(99.9) dBA		
3/20/2019		<b>42</b> 7.		<b>4.2.</b> 1	<b>3.2</b> 7.		
9:27:00	54.2	60.6	UNDER		55.1	51.1	263026.8
9:27:30	57.4	59	UNDER		58.1	55.1	549540.9
9:28:00	55.9	59.2	UNDER		58.1	52.1	389045.1
9:28:30	54.4	56.6	UNDER		55.1	52.1	275422.9
9:29:00	55.6	57.4	UNDER		57.1	54.1	363078.1
9:29:30	57.8	59.6	UNDER		59.1	55.1	602559.6
9:30:00	56.7	60.6	UNDER		59.1	50.1	467735.1
9:30:30	51.5	54.6	UNDER		52.1	49.1	141253.8
9:31:00	56.6	57.8	UNDER		57.1	54.1	457088.2
9:31:30	55.5	56.5	UNDER		56.1	54.1	354813.4
9:32:00	55	56.7	UNDER		56.1	53.1	316227.8
9:32:30	54.4	57	UNDER		56.1	52.1	275422.9
9:33:00	55.8	58.3	UNDER		57.1	53.1	380189.4
9:33:30	56.5	58.2	UNDER		57.1	53.1	446683.6
9:34:00	53.2	55.1	UNDER		54.1	51.1	208929.6
9:34:30	53.4	55	UNDER		54.1	51.1	218776.2
9:35:00	54.7	56.2	UNDER		56.1	52.1	295120.9
9:35:30	55.6	56.6	UNDER		56.1	52.1	363078.1
9:36:00	57.5	59	UNDER		58.1	56.1	562341.3
9:36:30	59.5	64.1	UNDER		63.1	53.1	891250.9

9:3	7:00	54.7	56.2	UNDER	55.1	52.1	295120.9
9:3	7:30	52	55.8	UNDER	55.1	49.1	158489.3
9:38	8:00	52.8	56.6	UNDER	55.1	50.1	190546.1
9:38	8:30	55.7	58.2	UNDER	57.1	51.1	371535.2
	9:00	53.9		UNDER	56.1	51.1	245470.9
	9:30	57.5		UNDER	59.1	55.1	562341.3
	0:00	56.8		UNDER	57.1	54.1	478630.1
	0:30	56.4		UNDER	57.1	54.1	436515.8
	1:00	52.9		UNDER	54.1	49.1	194984.5
	1:30	50.7		UNDER	53.1	49.1	117489.8
	2:00	53.4		UNDER	54.1	51.1	218776.2
	2:30	54.3		UNDER	55.1	52.1	269153.5
	3:00	55.8		UNDER	58.1	52.1	380189.4
	3:30	56.6		UNDER	58.1	55.1	457088.2
	4:00	56.3		UNDER	57.1	55.1	426579.5
	4:30	56.3		UNDER	58.1	50.1	426579.5
	5:00	51.3		UNDER	53.1	48.1	134896.3
	5:30	52.1		UNDER	53.1	50.1	162181
	6:00	56.7		UNDER	57.1	53.1	467735.1
	6:30	57.2		UNDER	59.1	52.1	524807.5
	7:00	56.5		UNDER	59.1	52.1	446683.6
	7:30 7:30	57.2		UNDER	58.1	55.1	524807.5
	8:00	59		UNDER	61.1	55.1	794328.2
	8:30	55.9		UNDER	59.1	51.1	389045.1
	9:00	54.4		UNDER	55.1	51.1	275422.9
	9:30	55.6		UNDER	57.1	53.1	363078.1
	0:00	55.2		UNDER	56.1	53.1	331131.1
	0:30	55.1		UNDER	56.1	53.1	323593.7
	1:00	56.5		UNDER	57.1	55.1	446683.6
	1:30	56.8		UNDER	58.1	54.1	478630.1
	2:00	54.6		UNDER	56.1		288403.2
	2:30	52.4		UNDER	53.1	50.1	173780.1
	3:00	54.4		UNDER	56.1	50.1	275422.9
	3:30	57.2		UNDER	60.1	54.1	524807.5
	4:00	58.8		UNDER	59.1	55.1	758577.6
	4:30	53.8		UNDER	55.1	52.1	239883.3
	5:00	54.3		UNDER	55.1	52.1	269153.5
	5:30	54.9		UNDER	57.1	51.1	309029.5
	6:00	55.9		UNDER	58.1	51.1	389045.1
	6:30	56.1		UNDER	58.1	52.1	407380.3
	7:00	55.5		UNDER	56.1	53.1	354813.4
	7:30 7:30	56.2		UNDER	56.1	55.1	416869.4
	8:00	55.6		UNDER	56.1	54.1	363078.1
	8:30	55.9		UNDER	57.1	53.1	389045.1
	9:00	57.1		UNDER	59.1	53.1	512861.4
	9:30	53.7		UNDER	55.1	51.1	234422.9
10:00		55.9		UNDER	56.1	53.1	389045.1
10.00		23.3	٥,	J.15211		55.1	3030 13.1

10:00:30	53.1	54.6 UNDER	54.1	51.1	204173.8
10:01:00	54.8	56.2 UNDER	55.1	53.1	301995.2
10:01:30	58.6	67.8 UNDER	63.1	51.1	724436
10:02:00	56	57.8 UNDER	57.1	53.1	398107.2
10:02:30	54.3	57 UNDER	55.1	50.1	269153.5
10:03:00	53.7	56.2 UNDER	55.1	51.1	234422.9
10:03:30	53.1	54.6 UNDER	54.1	51.1	204173.8
10:04:00	54.2	55 UNDER	54.1	53.1	263026.8
10:04:30	52.4	53.8 UNDER	53.1	50.1	173780.1
10:05:00	54.4	58.2 UNDER	56.1	51.1	275422.9
10:05:30	56.4	58.3 UNDER	58.1	53.1	436515.8
10:06:00	54.2	56.2 UNDER	55.1	52.1	263026.8
10:06:30	57.6	62.2 UNDER	60.1	52.1	575439.9
10:07:00	55.2	57 UNDER	57.1	52.1	331131.1
10:07:30	56.5	57.4 UNDER	57.1	55.1	446683.6
10:08:00	54.5	56.7 UNDER	56.1	52.1	281838.3
10:08:30	55.9	61.8 UNDER	60.1	50.1	389045.1
10:09:00	56.1	57.6 UNDER	57.1	54.1	407380.3
10:09:30	56.2	58.2 UNDER	57.1	54.1	416869.4
10:10:00	58.1	59.6 UNDER	59.1	55.1	645654.2
10:10:30	56.3	63.8 UNDER	57.1	53.1	426579.5
10:11:00	59.1	64.2 UNDER	61.1	56.1	812830.5
10:11:30	56.3	58.6 UNDER	57.1	54.1	426579.5
10:12:00	55.9	57 UNDER	56.1	53.1	389045.1
10:12:30	52.2	54.2 UNDER	53.1	51.1	165958.7
10:13:00	57.3	63.8 UNDER	61.1	51.1	537031.8
10:13:30	57.8	60.5 UNDER	59.1	56.1	602559.6

10:14:00	57.1	59 UNDER	58.1	56.1 512861.4
10:14:30	54.1	56.6 UNDER	56.1	50.1 257039.6
10:15:00	53.8	56.6 UNDER	56.1	50.1 239883.3
10:15:30	56.6	58.6 UNDER	57.1	55.1 457088.2
10:16:00	56.2	57.4 UNDER	56.1	54.1 416869.4
10:16:30	52.6	54.8 UNDER	54.1	49.1 181970.1
10:17:00	56.5	57.8 UNDER	57.1	54.1 446683.6
10:17:30	57.7	59.3 UNDER	58.1	55.1 588843.7
10:18:00	55.4	57 UNDER	56.1	53.1 346736.9
10:18:30	55.3	58.2 UNDER	57.1	51.1 338844.2
10:19:00	54.3	55.4 UNDER	55.1	53.1 269153.5
10:19:30	55.5	58.2 UNDER	57.1	53.1 354813.4
10:20:00	57.2	59.8 UNDER	59.1	52.1 524807.5
10:20:30	52.4	53.8 UNDER	53.1	50.1 173780.1
10:21:00	54.2	56 UNDER	55.1	51.1 263026.8
10:21:30	55.5	57.7 UNDER	57.1	51.1 354813.4
10:22:00	59.4	66.2 UNDER	65.1	50.1 870963.6
10:22:30	54.6	60.6 UNDER	59.1	49.1 288403.2
10:23:00	53.8	56.6 UNDER	55.1	50.1 239883.3
10:23:30	59.6	62.6 UNDER	62.1	56.1 912010.8
10:24:00	54.7	57.4 UNDER	56.1	50.1 295120.9
10:24:30	48.9	50.7 UNDER	49.1	47.1 77624.71
10:25:00	52.4	54.2 UNDER	53.1	49.1 173780.1
10:25:30	58.9	61.8 UNDER	61.1	53.1 776247.1
10:26:00	56.4	57.4 UNDER	57.1	53.1 436515.8
10:26:30	50.9	53.8 UNDER	52.1	49.1 123026.9
10:27:00	52.8	54.6 UNDER	54.1	51.1 190546.1
10:27:30	55	56.6 UNDER	56.1	53.1 316227.8
10:28:00	57.2	58.4 UNDER	58.1	53.1 524807.5
10:28:30	53	59.4 UNDER	56.1	49.1 199526.2
10:29:00	55.1	57.6 UNDER	57.1	50.1 323593.7
10:29:30	56.2	61.4 UNDER	59.1	53.1 416869.4
10:30:00	54	55 UNDER	54.1	53.1 251188.6
10:30:30	57.3	63 UNDER	60.1	51.1 537031.8
10:30:30	54.8	57.8 UNDER	57.1	51.1 301995.2
10:31:30	56.5	58.1 UNDER	57.1 57.1	54.1 446683.6
10:31:30	53.5	54.6 UNDER	54.1	52.1 223872.1
10:32:30	49.8	51.9 UNDER	51.1	48.1 95499.26
		58.6 UNDER		
10:33:00	55.6 55.2	58.2 UNDER	58.1	
10:33:30	55.2 53.6		57.1 54.1	52.1 331131.1
10:34:00	53.6	55.4 UNDER	54.1	50.1 229086.8
10:34:30	48.9	50.6 UNDER	49.1	47.1 77624.71
10:35:00	51.2	54 UNDER	53.1	48.1 131825.7
10:35:30	63	69.8 UNDER	68.1	53.1 1995262
10:36:00	62.3	69 UNDER	66.1	55.1 1698244
10:36:30	70	74.4 UNDER	73.1	56.1 10000000

******** Filename Test Locat Employee N Employee N Department	******** ion ame umber 11270 Ston	**************************************	******	*****	*****
Calibrator Calibrator ******	Type Cal. Date ******	 ********	*****	******	******
METROSONIC REPORT PRI	S db-3080 NTED ON 03	V1.12 SERIAL /21/19 at 15:37	# 3897 :45		
User ID: _					
LOGGING ST	ARTED	.03/20/19 at 09	:56:30		
TOTAL LOGG LOGGING ST	ING TIME OPPED	.0 DAYS 00:52:2 .03/20/19 at 10	:48:50	)	
TOTAL INTE	RVALS ENGTH	0.105			
AUTO STOP. CLOCK SYNC RESPONSE R FILTER	 H ATE	.NO .YES .SLOW .A WT.			
PRE-TEST C PRE-TEST C	ALIBRATION ALIBRATION	TIME03/20/ RANGE39.9 T	19 AT 09:2 O 139.9 dB	1:29	)
POST-TEST CUTOFF USE	CALIBRATIO D FOR TIME	N NOT DONE HISTORY Lav	NONE		
<<< SUMMAR	Y REPORT F	OR TEST NUMBER	1 OF 1 >>>		
EXCHANGE R	ATE	3dB			

... 80dB 90dB

...115dB

CUTOFFS...

CEILING...

.....

DOSE CRITE	RION LEVEL	90dB	
DOSE CRITE	RION LENGT	H 8 HOURS	
Lav	56.	4dB	
Lav ( 80).	39.	9dB	
Lav ( 90).	39.	9dB	
SEL	91.	3dB	
TWA	46.	8dB	
TWA (80).	39.	9dB	
TWA ( 90).	39.	9dB	
Lmax	68.	8dB 03/20/19 a	t 09:56:37
Lpk	UNDER	RANGE	
TIME OVER	115dB00	:00:00.00	
DOSE ( 80)		0.00%	
PROJ. DOSE	( 80)	0.00%	,
DOSE ( 90)		0.00%	
PROJ. DOSE	( 90)	0.00%	
<<< TIME H	ISTORY REP	ORT FOR TEST NU	MBER 1 OF

MBER 1 OF 1 >>>

					. (40.0)			
TIME	Lav	Lmax		Lpk	L(10.0)	L(99	-	
	dBA	dBA		dBC	dBA	dBA		
3/20/20	019							
9:56	5:30	58.4	68.8	UNDER		62.9	48.9	691831
9:57	<b>'</b> :00	52.8	56.7	UNDER		55.9	49.9	9 190546.1
9:57	<b>'</b> :30	56.3	68.4	UNDER		57.9	47.9	9 426579.5
9:58	3:00	57.2	59.6	UNDER		59.9	55.9	524807.5
9:58	3:30	58.3	61.7	UNDER		60.9	55.9	676083
9:59	9:00	57.5	60.8	UNDER		59.9	45.9	562341.3
9:59	9:30	56.9	66	UNDER		61.9	43.9	9 489778.8
10:00	0:00	54.6	61.2	UNDER		58.9	48.9	9 288403.2
10:00	):30	54.2	60.8	UNDER		58.9	43.9	9 263026.8
10:01	:00	57.1	63.2	UNDER		60.9	52.9	512861.4
10:01	:30	55.5	59.3	UNDER		58.9	50.9	354813.4
10:02	2:00	51.1	54.9	UNDER		54.9	44.9	128825
10:02	2:30	46.6	51.9	UNDER		49.9	43.9	9 45708.82
10:03	3:00	58.1	62	UNDER		60.9	52.9	9 645654.2
10:03	3:30	55.7	56.8	UNDER		56.9	54.9	9 371535.2
10:04	1:00	56.7	67.6	UNDER		59.9	51.9	9 467735.1
10:04	l:30	54.2	61.8	UNDER		60.9	47.9	9 263026.8
10:05	5:00	47.7	51.7	UNDER		49.9	44.9	58884.37
10:05	5:30	51.7	56.4	UNDER		54.9	48.9	9 147910.8
10:06	5:00	58.2	61.6	UNDER		60.9	54.9	660693.4

10:06:30	57.7	60.8 UNDER	60.9	54.9	588843.7
10:07:00	53	57.6 UNDER	56.9	46.9	199526.2
10:07:30	52.8	58.2 UNDER	55.9	45.9	190546.1
10:08:00	57.9	60.9 UNDER	60.9	50.9	616595
10:08:30	55.9	57.6 UNDER	57.9	52.9	389045.1
10:09:00	53.5	56.7 UNDER	55.9	50.9	223872.1
10:09:30	55.9	61 UNDER	59.9	50.9	389045.1
10:10:00	54.7	59.6 UNDER	56.9	50.9	295120.9
10:10:30	54.9	60.4 UNDER	59.9	47.9	309029.5
10:11:00	54.9	58.1 UNDER	56.9	50.9	309029.5
10:11:30	59.4	62 UNDER	61.9	55.9	870963.6
10:12:00	55.5	58.8 UNDER	57.9	50.9	354813.4
10:12:30	53.7	56.6 UNDER	56.9	48.9	234422.9
10:13:00	54.9	61.2 UNDER	59.9	48.9	309029.5
10:13:30	56.1	58.4 UNDER	57.9	50.9	407380.3
10:14:00	59	65.8 UNDER	64.9	52.9	794328.2
10:14:30	55.6	65.6 UNDER	59.9	44.9	363078.1
10:15:00	53.1	56.4 UNDER	56.9	44.9	204173.8
10:15:30	55.1	57.9 UNDER	57.9	51.9	323593.7
10:16:00	57.8	62.6 UNDER	61.9	54.9	602559.6
10:16:30	55.4	59.6 UNDER	58.9	50.9	346736.9
10:17:00	50.4	53.6 UNDER	52.9	47.9	109647.8
10:17:30	56	60.8 UNDER	58.9	51.9	398107.2
10:17:30	57	61.6 UNDER	60.9	51.9	501187.2
10:18:30	53.2	55.7 UNDER	55.9	50.9	208929.6
10:18:30	57.8	60.4 UNDER	59.9	54.9	602559.6
10:19:30	56.9	59.5 UNDER	58.9	55.9	489778.8
10:19:30	53.8	56 UNDER	55.9	50.9	239883.3
10:20:30	55.3	59.2 UNDER	58.9	51.9	338844.2
10:20:30	53.3 54	57.4 UNDER	57.9	46.9	251188.6
					407380.3
10:21:30	56.1	59.2 UNDER	58.9		
10:22:00	56.6	58.2 UNDER	57.9	54.9	457088.2
10:22:30	55.3	61.2 UNDER	59.9	49.9	338844.2
10:23:00	50.9	55.9 UNDER	53.9	45.9 46.0	123026.9
10:23:30	53.7	59.6 UNDER	56.9	46.9	234422.9
10:24:00	59.9	66 UNDER	63.9	54.9	977237.2
10:24:30	60.2	67.8 UNDER	66.9	53.9	1047129
10:25:00	54.6	58.2 UNDER	57.9	50.9	288403.2
10:25:30	60.1	66 UNDER	63.9	54.9	1023293
10:26:00	60	65.8 UNDER	64.9	52.9	1000000
10:26:30	55.2	65 UNDER	56.9	47.9	331131.1
10:27:00	51.1	53.6 UNDER	53.9	44.9	128825
10:27:30	59.2	63.2 UNDER	62.9	53.9	831763.8
10:28:00	56.8	60.4 UNDER	59.9	52.9	478630.1
10:28:30	54.5	56 UNDER	55.9	52.9	281838.3
10:29:00	53.3	55.6 UNDER	55.9	51.9	213796.2

10:29:30	56.7	59 UNDER	58.9	54.9	467735.1
10:30:00	57	61.7 UNDER	60.9	51.9	501187.2
10:30:30	54.1	56.8 UNDER	55.9	48.9	257039.6
10:31:00	50.2	57.2 UNDER	54.9	45.9	104712.9
10:31:30	57.6	61.2 UNDER	59.9	49.9	575439.9
10:32:00	59.2	63.6 UNDER	62.9	50.9	831763.8
10:32:30	56.8	61.6 UNDER	60.9	52.9	478630.1
10:33:00	50.2	54.3 UNDER	53.9	44.9	104712.9
10:33:30	50.5	55.8 UNDER	54.9	42.9	112201.8
10:34:00	58.7	65 UNDER	62.9	54.9	741310.2
10:34:30	52.7	55.8 UNDER	54.9	44.9	186208.7
10:35:00	52.3	58 UNDER	56.9	44.9	169824.4
10:35:30	61.2	66.7 UNDER	64.9	54.9	1318257
10:36:00	57.1	60.8 UNDER	60.9	53.9	512861.4
10:36:30	52.4	56.8 UNDER	55.9	44.9	173780.1
10:37:00	55.9	59.9 UNDER	58.9	46.9	389045.1
10:37:30	55.2	58 UNDER	57.9	50.9	331131.1
10:38:00	54.6	58.4 UNDER	57.9	48.9	288403.2
10:38:30	58.6	61.5 UNDER	60.9	53.9	724436
10:39:00	55.9	62.3 UNDER	58.9	50.9	389045.1
10:39:30	56.9	63.2 UNDER	60.9	52.9	489778.8
10:40:00	57	60 UNDER	58.9	52.9	501187.2
10:40:30	52.4	56 UNDER	55.9	45.9	173780.1
10:41:00	52.6	58 UNDER	56.9	48.9	181970.1
10:41:30	59	62.9 UNDER	62.9	49.9	794328.2
10:42:00	60.1	65.7 UNDER	64.9	55.9	1023293
10:42:30	56.6	60.4 UNDER	59.9	53.9	457088.2
10:43:00	53.2	60 UNDER	57.9	49.9	208929.6

10:43:30	59.2	67.2 UNDER	65.9	48.9	831763.8
10:44:00	58.9	66.8 UNDER	62.9	52.9	776247.1
10:44:30	54.8	60 UNDER	59.9	46.9	301995.2
10:45:00	50.3	55.6 UNDER	52.9	46.9	107151.9
10:45:30	59.6	67.6 UNDER	63.9	49.9	912010.8
10:46:00	52.6	55.3 UNDER	54.9	48.9	181970.1
10:46:30	57.7	63.6 UNDER	60.9	53.9	588843.7
10:47:00	55.8	62 UNDER	60.9	47.9	380189.4
10:47:30	57.8	66.1 UNDER	63.9	43.9	602559.6
10:48:00	56.3	58.6 UNDER	57.9	54.9	426579.5
10:48:30	60	66.9 UNDER	61.9	56.9	1000000

******* Filename Test Locat Employee N Employee N Department	******** ion ame umber 1220 Colvi	***********MON5VA 7ERZ, EJAENV n Meadows Ln	******	******	*****
Calibrator Calibrator ******	Type Cal. Date ******	  ******	******	*****	*****
METROSONIC REPORT PRI	S db-3080 NTED ON 03	V1.20 SERIAL /21/19 at 15:38	# 5093 :00		
User ID: _					
LOGGING ST TOTAL LOGG LOGGING ST TOTAL INTE INTERVAL L AUTO STOP. CLOCK SYNC RESPONSE R	ARTED ING TIME OPPED RVALS ENGTH H	.03/20/19 at 11 .0 DAYS 01:00:0 .03/20/19 at 12 0.121 .00:00:30 .NO .YES	:08:00 5 :08:05		
PRE-TEST C PRE-TEST C POST-TEST CUTOFF USE	ALIBRATION ALIBRATION CALIBRATIO D FOR TIME	.A WT. TIME03/20/ RANGE41.0 T N NOT DONE HISTORY Lav	19 AT 09:3 O 141.0 dB NONE	9:10	)
<<< SUMMAR		OR TEST NUMBER	1 OF 1 >>>		
EXCHANGE R	ATE	3dB			

... 80dB 90dB

...115dB

CUTOFFS...

CEILING...

.....

DOSE CRITE	RION LEVEL	90dB					
DOSE CRITE	RION LENGT	H 8 HOURS					
Lav	56.	8dB					
Lav ( 80).	41.	0dB					
Lav ( 90).	41.	0dB					
SEL	92.	3dB					
TWA	47.	8dB					
TWA ( 80).	41.	0dB					
TWA ( 90).	41.	0dB					
( 5 5 7 .	=.						
Lmax	76.	0dB 03/20/19 a	t 12:05:55				
Lpk	UNDER	RANGE					
TIME OVER	115dB00	:00:00.00					
DOSE ( 80)		0.00%					
PROJ. DOSE	( 80)	0.00%					
DOSE ( 90)		0.00%					
PROJ. DOSE	( 90)	0.00%					
T NOJ. DOJE	( 50)	0.0070					
<<< TIME H	ISTORY REP	ORT FOR TEST NU	MBER 1 OF	1 >>>			
TIME	Lav	Lmax	Lnk	L(10.0)	L(99.9)		
THVIE	dBA	dBA	Lpk dBC	dBA	dBA		
3/20/2019	UDA	UDA	ubc	UDA	ubA		
11:08:00	52.3	56.9	UNDER		54	50	169824.4
11:08:30	51.4		UNDER		53	46	138038.4
11:09:00	51.9		UNDER		54	47	154881.7
11:09:30	54.2		UNDER		57	48	263026.8
11:10:00	54.5		UNDER		56	48	281838.3
11:10:30	56		UNDER		57	53	398107.2
11:11:00	54.1	58.5	UNDER		56	50	257039.6
11:11:30	59.6	64.9	UNDER		64	53	912010.8
11:12:00	58.4	62.4	UNDER		61	51	691831
11:12:30	54.4	56.4	UNDER		56	51	275422.9
11:13:00	49.7	53.9	UNDER		52	47	93325.43
11:13:30	58.9	62.4	UNDER		61	49	776247.1
11:14:00	57.9	63.3	UNDER		62	51	616595
11:14:30	58.4	64.9	UNDER		63	49	691831
11:15:00	52.8	61.7	UNDER		56	48	190546.1
11:15:30	53.5	56.5	UNDER		55	46	223872.1
11:16:00	58.7	60.9	UNDER		60	54	741310.2
11:16:30	57.1	62	UNDER		60	46	512861.4
11:16:30 11:17:00	57.1 52.2		UNDER UNDER		60 55	46 44	512861.4 165958.7

61.3 UNDER

60

48 478630.1

11:17:30

56.8

11:18:00	55.3	57.6 UNDER	57	46	338844.2
11:18:30	53.8	56.5 UNDER	55	51	239883.3
11:19:00	51.2	56.6 UNDER	55	45	131825.7
11:19:30	55.2	58.4 UNDER	57	49	331131.1
11:20:00	58.1	62.1 UNDER	61	55	645654.2
11:20:30	53.6	57.2 UNDER	55	47	229086.8
11:21:00	53.2	58 UNDER	56	50	208929.6
11:21:30	54.5	59.2 UNDER	57	45	281838.3
11:22:00	57.5	63.3 UNDER	60	48	562341.3
11:22:30	57.8	62.9 UNDER	60	48	602559.6
11:23:00	49.8	52.8 UNDER	51	47	95499.26
11:23:30	56.4	58.9 UNDER	58	50	436515.8
11:24:00	56.2	58.6 UNDER	58	51	416869.4
11:24:30	60.4	66.4 UNDER	65	53	1096478
11:25:00	52.9	58.9 UNDER	57	47	194984.5
11:25:30	55.7	58.4 UNDER	57	49	371535.2
11:26:00	58.2	63.6 UNDER	62	50	660693.4
11:26:30	57.2	63.2 UNDER	60	50	524807.5
11:27:00	49.3	51.6 UNDER	51	43	85113.8
11:27:30	55	61.6 UNDER	59	43	316227.8
11:28:00	55.5	58 UNDER	57	46	354813.4
11:28:30	59.5	64.5 UNDER	62	53	891250.9
11:29:00	52.1	56.2 UNDER	54	48	162181
11:29:30	55.7	60 UNDER	59	50	371535.2
11:30:00	58	60 UNDER	58	56	630957.3
11:30:30	55.1	58.5 UNDER	58	47	323593.7
11:31:00	50.2	55.2 UNDER	54	44	104712.9
11:31:30	58.2	65.2 UNDER	61	47	660693.4
11:32:00	59.1	64 UNDER	62	47	812830.5
11:32:30	53.2	57.7 UNDER	55	50	208929.6
11:33:00	53.3	56.6 UNDER	56	50	213796.2
11:33:30	53.4	55.6 UNDER	55	46	218776.2
11:34:00	55.9	59.2 UNDER	58	51	389045.1
11:34:30	55.8	58.8 UNDER	58	49	380189.4
11:35:00	52.6	59.1 UNDER	58	45	181970.1
11:35:30	57.3	58.8 UNDER	58	54	537031.8
11:36:00	58.4	63.3 UNDER	62	54	691831
11:36:30	54.9	61.4 UNDER	57	50	309029.5
11:37:00	49.3	54.1 UNDER	52	44	85113.8
11:37:30	57.9	63.9 UNDER	62	46	616595
11:38:00	58	62 UNDER	59	55	630957.3
11:38:30	60.3	66.4 UNDER	63	51	1071519
11:39:00	49.2	51.2 UNDER	50	45	83176.38
11:39:30	51.7	57.8 UNDER	56	44	147910.8
11:40:00	57.3	60.1 UNDER	59	54	537031.8
11:40:30	58.3	61.2 UNDER	60	53	676083

11:41:00	54.2	59.9 UNDER	57	46	263026.8
11:41:30	56.1	62.1 UNDER	60	47	407380.3
11:42:00	57.8	62.4 UNDER	60	54	602559.6
11:42:30	56.6	62.3 UNDER	60	49	457088.2
11:43:00	49.9	53.2 UNDER	52	47	97723.72
11:43:30	59.1	64.1 UNDER	62	49	812830.5
11:44:00	58	63.3 UNDER	61	47	630957.3
11:44:30	50.4	57.7 UNDER	55	44	109647.8
11:45:00	53.4	57.9 UNDER	57	46	218776.2
11:45:30	55.8	58.8 UNDER	58	49	380189.4
11:46:00	53.7	57.2 UNDER	56	50	234422.9
11:46:30	55	57.3 UNDER	56	49	316227.8
11:47:00	52.7	56.9 UNDER	55	46	186208.7
11:47:30	56.9	66.8 UNDER	58	51	489778.8
11:48:00	60.2	66.9 UNDER	66	52	1047129
11:48:30	58.7	64.4 UNDER	63	53	741310.2
11:49:00	56.3	63.7 UNDER	58	51	426579.5
11:49:30	55.5	58.1 UNDER	57	46	354813.4
11:50:00	55.6	58.5 UNDER	58	49	363078.1
11:50:30	53.7	57.2 UNDER	56	48	234422.9
11:51:00	50.5	55 UNDER	54	44	112201.8
11:51:30	55.1	59.3 UNDER	58	50	323593.7
11:52:00	56.8	62.5 UNDER	62	49	478630.1
11:52:30	52.9	56.3 UNDER	55	48	194984.5
11:53:00	50.7	55 UNDER	53	47	117489.8
11:53:30	54	58 UNDER	57	48	251188.6
11:54:00	54.4	56.9 UNDER	56	48	275422.9
11:54:30	55.1	58.5 UNDER	57	45	323593.7

11:55:00	52.3	56.8 UNDER	54	46	169824.4
11:55:30	56.6	61 UNDER	59	49	457088.2
11:56:00	56.8	60.9 UNDER	60	52	478630.1
11:56:30	57.3	62.4 UNDER	61	50	537031.8
11:57:00	49.6	54.4 UNDER	53	46	91201.08
11:57:30	55.9	58.2 UNDER	57	49	389045.1
11:58:00	58.8	66.1 UNDER	62	49	758577.6
11:58:30	57.9	62.9 UNDER	62	48	616595
11:59:00	52.8	56.2 UNDER	54	48	190546.1
11:59:30	48.2	54 UNDER	52	43	66069.34
12:00:00	56.3	58.8 UNDER	58	54	426579.5
12:00:30	54.8	57.6 UNDER	57	48	301995.2
12:01:00	50.8	54.6 UNDER	54	47	120226.4
12:01:30	55.8	60.1 UNDER	59	51	380189.4
12:02:00	56	58.5 UNDER	58	49	398107.2
12:02:30	57	60.9 UNDER	60	53	501187.2
12:03:00	55.7	61.8 UNDER	60	46	371535.2
12:03:30	54.5	58 UNDER	56	48	281838.3
12:04:00	59.6	63.3 UNDER	62	55	912010.8
12:04:30	57.5	59.6 UNDER	59	52	562341.3
12:05:00	52.9	54 UNDER	53	51	194984.5
12:05:30	67.9	76 UNDER	72	52	6165950
12:06:00	59.5	68.9 UNDER	63	52	891250.9
12:06:30	66.1	74.5 UNDER	72	49	4073803
12:07:00	50.2	57.2 UNDER	50	47	104712.9
12:07:30	58.7	62.9 UNDER	62	54	741310.2
12:08:00	56.6	61 UNDER	57	55	457088.2

******** Filename Test Locat Employee N Employee N Department	******** ion ame umber 9911 Hessi	**************************************	*****	*****	******
Calibrator Calibrator ******	Type Cal. Date ******	 ********	*****	*****	*****
METROSONIC REPORT PRI	S db-3080 NTED ON 03	V1.12 SERIAL /21/19 at 15:38	# 3897 :13		
User ID: _					
LOGGING ST TOTAL LOGG LOGGING ST TOTAL INTE INTERVAL L	ARTED ING TIME OPPED RVALS ENGTH	.03/20/19 at 11 .0 DAYS 00:48:1 .03/20/19 at 12 0.97 .00:00:30	:15:00 1 :03:11		
CLOCK SYNC RESPONSE R FILTER	H ATE	.YES .SLOW .A WT.			
PRE-TEST C PRE-TEST C POST-TEST CUTOFF USE	ALIBRATION ALIBRATION CALIBRATIO D FOR TIME	TIME03/20/ RANGE39.9 T N NOT DONE HISTORY Lav	19 AT 09:2 O 139.9 dB NONE	1:29	
<<< SUMMAR	Y REPORT F	OR TEST NUMBER	1 OF 1 >>>		
EXCHANGE R	ATE	3dB			

CUTOFFS...

CEILING...

.....

... 80dB 90dB

...115dB

DOSE CRITE	RION LEVEL	90dB
DOSE CRITE	RION LENGT	H 8 HOURS
Lav		5dB
Lav ( 80).	39.	9dB
Lav ( 90).	39.	9dB
SEL	91.	OdB
TWA	46.	5dB
TWA ( 80).	39.	9dB
TWA ( 90).	39.	9dB
Lmax	65.	9dB 03/20/19 a t 11:26:04
Lpk	UNDER	RANGE
TIME OVER	115dB00	:00:00.00
DOSE ( 80)		0.00%
PROJ. DOSE	( 80)	0.00%
DOSE ( 90)		0.00%
PROJ. DOSE	( 90)	0.00%

NN THEFT ISLUMENCE ON FLOOR INC. INDENTED A 1777	<<< TIME H	ISTORY REP	ORT FOR TEST NU	MBER 1 OF	1 >>>
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TIME	Lav		nax	Lpk	L(10.0)	L(99.9)		
- 1 1	dBA	dB	3A	dBC	dBA	dBA		
3/20/20								
11:15:	00	56.5	57.8	UNDER	5	57.9	55.9	446683.6
11:15:	30	58	60.7	UNDER	6	50.9	56.9	630957.3
11:16:	00	57.1	60	UNDER	5	9.9	52.9	512861.4
11:16:	30	59	64.8	UNDER	6	3.9	51.9	794328.2
11:17:	00	56.2	60.4	UNDER	5	9.9	53.9	416869.4
11:17:	30	56.8	58.2	UNDER	5	57.9	54.9	478630.1
11:18:	00	53.4	57.2	UNDER	5	55.9	50.9	218776.2
11:18:	30	54.5	57.8	UNDER	5	57.9	49.9	281838.3
11:19:	00	59	60.8	UNDER	6	60.9	57.9	794328.2
11:19:	30	58.1	60.3	UNDER	5	9.9	55.9	645654.2
11:20:	00	52.6	55.7	UNDER	5	64.9	50.9	181970.1
11:20:		52	55.6	UNDER		64.9	48.9	158489.3
11:21:		55.6	57.2	UNDER		6.9	52.9	363078.1
11:21:	30	58.8	61.2	UNDER		60.9	56.9	758577.6
11:22:		55.5		UNDER		8.9	51.9	354813.4
11:22:		53.3		UNDER		66.9	48.9	213796.2
11:23:		58.6		UNDER		50.9	55.9	724436
11:23:		56.5		UNDER		58.9	51.9	446683.6
11:24:		57.5		UNDER		60.9	51.9	562341.3
		57.5 54		UNDER		66.9		251188.6
11:24:	<b>3</b> 0	<b>54</b>	٥/.٥	UNDER		ひ.フ	49.9	₹21100'£

11:25:00	58.3	60 UNDER	59.9	56.9	676083
11:25:30	59.9	62.2 UNDER	61.9	57.9	977237.2
11:26:00	59.1	65.9 UNDER	64.9	49.9	812830.5
11:26:30	49.9	53.2 UNDER	52.9	48.9	97723.72
11:27:00	57	59.6 UNDER	59.9	53.9	501187.2
11:27:30	56.4	57.6 UNDER	57.9	55.9	436515.8
11:28:00	57.8	61.6 UNDER	60.9	51.9	602559.6
11:28:30	54	57.5 UNDER	57.9	49.9	251188.6
11:29:00	58.7	59.9 UNDER	59.9	56.9	741310.2
11:29:30	58.6	61.1 UNDER	59.9	57.9	724436
11:30:00	57.3	59.4 UNDER	59.9	50.9	537031.8
11:30:30	55.5	60 UNDER	59.9	50.9	354813.4
11:31:00	56.5	59.4 UNDER	58.9	54.9	446683.6
11:31:30	56.4	58.8 UNDER	58.9	53.9	436515.8
11:32:00	53.3	55.6 UNDER	54.9	50.9	213796.2
11:32:30	54.6	59.5 UNDER	56.9	51.9	288403.2
11:33:00	56.3	57.8 UNDER	57.9	55.9	426579.5
11:33:30	57.8	59.5 UNDER	59.9	55.9	602559.6
11:34:00	56.6	58.2 UNDER	58.9	51.9	457088.2
11:34:30	52.3	56.2 UNDER	55.9	48.9	169824.4
11:35:00	55.2	56.8 UNDER	56.9	53.9	331131.1
11:35:30	57.4	60.3 UNDER	59.9	55.9	549540.9
11:36:00	57	59.6 UNDER	58.9	51.9	501187.2
11:36:30	51.9	56.4 UNDER	56.9	47.9	154881.7
11:37:00	55.7	59.6 UNDER	58.9	52.9	371535.2
11:37:30	57.8	60.8 UNDER	59.9	55.9	602559.6
11:38:00	56.5	60 UNDER	57.9	51.9	446683.6
11:38:30	52	56.6 UNDER	54.9	48.9	158489.3
11:39:00	55.2	58 UNDER	57.9	52.9	331131.1
11:39:30	58.1	58.8 UNDER	58.9	56.9	645654.2
11:40:00	56.3	57.8 UNDER	57.9		426579.5
11:40:30	57.7	60.8 UNDER	60.9	52.9	588843.7
11:41:00	56.5	59.2 UNDER	58.9	53.9	446683.6
11:41:30	58.1	60.4 UNDER	59.9	55.9	645654.2
11:42:00	53	58.8 UNDER	56.9	47.9	199526.2
11:42:30	53.9	59.2 UNDER	57.9	47.9	245470.9
11:42:30	60.4	61.6 UNDER	61.9	59.9	1096478
11:43:30	57.3	61.2 UNDER	59.9	51.9	537031.8
11:44:00	55.1	58 UNDER	57.9	51.9	323593.7
11:44:30	54.5	58.4 UNDER	57.9	50.9	281838.3
11:44:30	53.6	56.9 UNDER	56.9	47.9	229086.8
11:45:30	53.9	57.5 UNDER	56.9	47.9 51.0	245470.9
11:46:00	56.9	60.7 UNDER	58.9	51.9	489778.8
11:46:30	56	62.5 UNDER	61.9	48.9	398107.2
11:47:00	58.9	60.4 UNDER	59.9 56.0	56.9	776247.1
11:47:30	55.9	57.5 UNDER	56.9	54.9	389045.1

11:48:00	57.6	61.1 UNDER	60.9	53.9	575439.9
11:48:30	53	56.6 UNDER	55.9	50.9	199526.2
11:49:00	58.6	60.4 UNDER	59.9	56.9	724436
11:49:30	58.9	60.2 UNDER	60.9	57.9	776247.1
11:50:00	54.3	59.9 UNDER	57.9	47.9	269153.5
11:50:30	53.9	57.6 UNDER	57.9	48.9	245470.9
11:51:00	56.4	57.7 UNDER	57.9	54.9	436515.8
11:51:30	55.1	58.4 UNDER	58.9	48.9	323593.7
11:52:00	51.3	54.6 UNDER	53.9	48.9	134896.3
11:52:30	50.1	54.4 UNDER	53.9	47.9	102329.3
11:53:00	55.8	57.3 UNDER	56.9	53.9	380189.4
11:53:30	57.1	59 UNDER	58.9	54.9	512861.4
11:54:00	54.6	58 UNDER	57.9	46.9	288403.2
11:54:30	53.2	57.1 UNDER	56.9	46.9	208929.6
11:55:00	57.5	59.2 UNDER	58.9	54.9	562341.3
11:55:30	57.1	59.6 UNDER	58.9	53.9	512861.4
11:56:00	59.4	63.1 UNDER	61.9	50.9	870963.6
11:56:30	51.8	58 UNDER	54.9	48.9	151356.1
11:57:00	59	61.6 UNDER	60.9	56.9	794328.2
11:57:30	56.7	60 UNDER	59.9	53.9	467735.1
11:58:00	55	59.2 UNDER	58.9	50.9	316227.8
11:58:30	54.2	56.4 UNDER	56.9	49.9	263026.8
11:59:00	56.2	59.8 UNDER	59.9	51.9	416869.4
11:59:30	57.1	60.4 UNDER	59.9	53.9	512861.4
12:00:00	53.2	56.4 UNDER	55.9	48.9	208929.6
12:00:30	54.1	58.2 UNDER	56.9	48.9	257039.6
12:01:00	55.1	60.5 UNDER	56.9	52.9	323593.7
12:01:30	57.5	60.8 UNDER	59.9	52.9	562341.3

12:02:00	55.9	58.7 UNDER	57.9	52.9 389045.1
12:02:30	55.1	58.8 UNDER	56.9	51.9 323593.7
12:03:00	59.4	65.1 UNDER	59.9	56.9 870963.6

******** Filename Test Locat Employee N Employee N Department	******** ion ame umber 1282 Middl	************MON7VA 7ERZ, EJAENV eton Ct	*****	*****	*****
Calibrator Calibrator ******	Type Cal. Date ******	  *******	*****	*****	*****
METROSONIC REPORT PRI	S db-3080 NTED ON 03	V1.20 SERIAL /21/19 at 15:38	# 4618 :28		
User ID: _					
LOGGING ST TOTAL LOGG LOGGING ST TOTAL INTE INTERVAL L AUTO STOP. CLOCK SYNC RESPONSE R	ARTED ING TIME OPPED RVALS ENGTH H	.03/20/19 at 11 .0 DAYS 00:46:0 .03/20/19 at 12 0.93 .00:00:30 .NO .YES	:30:00 9 :16:09		
FILTER		.SLOW .A WT.			
PRE-TEST C PRE-TEST C	ALIBRATION ALIBRATION	TIME03/20/ RANGE40.0 T	19 AT 11:2 O 140.0 dB	7:24	
POST-TEST POST-TEST CUTOFF USE	CALIBRATIO CALIBRATIO D FOR TIME	N TIME03/20/ N RANGE40.1 HISTORY Lav	19 AT 13:4 TO 140.1 NONE	3:22	

EXCHANGE R ATE...... ....3dB

CUTOFFS... ....... ... 80dB 90dB

<>< SUMMAR Y REPORT F OR TEST NUMBER 1 OF 1 >>>

CEILING DOSE CRITE	RION LEVEL	115dB 90dB					
DOSE CRITE	RION LENGT	H 8 HOURS					
Lav	59.	3dB					
Lav ( 80).	40.	0dB					
Lav ( 90).	40.	0dB					
SEL	93.	6dB					
TWA	49.	1dB					
TWA ( 80).	40.	OdB					
TWA ( 90).	40.	OdB					
Lmax	69.	0dB 03/20/19 a	t 12:16:08				
Lpk	UNDER	RANGE					
TIME OVER	115dB00	:00:00.00					
DOSE ( 80)		0.0	0%				
PROJ. DOSE	( 80)	0.0	0%				
DOSE ( 90)		0.0	0%				
PROJ. DOSE	( 90)	0.0	0%				
<<< TIME H	ISTORY REP	ORT FOR TEST N	U MBER 1 OF	1>>>			
TIME	Lav	Lmax	Lpk	L(10.0)	L(99.9)		
	dBA	dBA	dBC	dBA	dBA		
3/20/201	9						
11:30:0	0 55.9	9 6	0.3 UNDER		58	53	389045.1
11:30:3	0 55						0000.0.1
11:31:0	0 55.2	2 5	9.1 UNDER		57		331131.1
			9.1 UNDER 3.5 UNDER			52	
11:31:3	0 51.9	9 5			57	52	331131.1
11:31:3 11:32:0	0 51.9 0 51.7	9 5 2 5	3.5 UNDER		57 53	52 49	331131.1 154881.7
	0 51.9 0 51.7 0 55.4	9 5 2 5 4 6	3.5 UNDER 7.8 UNDER		57 53 52	52 49 47	331131.1 154881.7 131825.7
11:32:0	0 51.9 0 51.0 0 55.0 0 55.0	9 5 2 5 4 6 6 6	3.5 UNDER 7.8 UNDER 1.9 UNDER		57 53 52 59	52 49 47 47	331131.1 154881.7 131825.7 346736.9
11:32:0 11:32:3	0 51.9 0 51.0 0 55.4 0 55.0 0 51.3	9 5 2 5 4 6 6 6 8 5	3.5 UNDER 7.8 UNDER 1.9 UNDER 1.5 UNDER		57 53 52 59 58	52 49 47 47 50	331131.1 154881.7 131825.7 346736.9 363078.1
11:32:0 11:32:3 11:33:0	0 51.9 0 51.0 0 55.4 0 55.0 0 51.3 0 51.3	5 2 5 4 6 6 6 8 5 4	3.5 UNDER 7.8 UNDER 1.9 UNDER 1.5 UNDER 2.9 UNDER		57 53 52 59 58 52	52 49 47 47 50 50	331131.1 154881.7 131825.7 346736.9 363078.1 151356.1
11:32:0 11:32:3 11:33:0 11:33:3	0 51.9 0 51.0 0 55.4 0 55.0 0 51.8 0 51.8	5 2 4 6 6 6 8 5 4 5	3.5 UNDER 7.8 UNDER 1.9 UNDER 1.5 UNDER 2.9 UNDER 3.3 UNDER		57 53 52 59 58 52 52	52 49 47 47 50 50	331131.1 154881.7 131825.7 346736.9 363078.1 151356.1 138038.4
11:32:0 11:32:3 11:33:0 11:33:3 11:34:0	0 51.9 0 51.0 0 55.4 0 55.6 0 51.8 0 51.6 0 50.3	5 2 5 4 6 6 6 8 5 4 5 8 5	3.5 UNDER 7.8 UNDER 1.9 UNDER 1.5 UNDER 2.9 UNDER 3.3 UNDER		57 53 52 59 58 52 52	52 49 47 47 50 50 50 49	331131.1 154881.7 131825.7 346736.9 363078.1 151356.1 138038.4 120226.4
11:32:0 11:32:3 11:33:0 11:33:3 11:34:0 11:34:3	0 51.9 0 51.0 0 55.0 0 55.0 0 51.0 0 51.0 0 51.0 0 51.0	5 2 4 6 6 8 5 4 5 4 5 4 5	3.5 UNDER 7.8 UNDER 1.9 UNDER 1.5 UNDER 2.9 UNDER 3.3 UNDER 1.6 UNDER		57 53 52 59 58 52 52 51	52 49 47 47 50 50 50 49	331131.1 154881.7 131825.7 346736.9 363078.1 151356.1 138038.4 120226.4 138038.4 660693.4 208929.6
11:32:0 11:32:3 11:33:0 11:33:3 11:34:0 11:34:3 11:35:0 11:35:3	0 51.9 0 51.9 0 55.4 0 55.4 0 55.6 0 51.6 0 51.6 0 50.8 0 53.6 0 53.6	5 2 4 6 6 8 5 4 5 8 5 4 5 6 6 8 5 4 5 7	3.5 UNDER 7.8 UNDER 1.9 UNDER 1.5 UNDER 2.9 UNDER 3.3 UNDER 1.6 UNDER 3.1 UNDER 0.8 UNDER 6.8 UNDER		57 53 52 59 58 52 52 51 52 60 54 50	52 49 47 47 50 50 49 49 53 49 47	331131.1 154881.7 131825.7 346736.9 363078.1 151356.1 138038.4 120226.4 138038.4 660693.4 208929.6 93325.43
11:32:0 11:32:3 11:33:0 11:33:3 11:34:0 11:34:3 11:35:0	0 51.9 0 51.9 0 55.0 0 55.0 0 51.8 0 51.8 0 51.8 0 53.0 0 549.0 0 51.8	5 2 4 6 6 8 8 5 4 5 8 5 4 5 6 6 8 5 7 5 5 5 7	3.5 UNDER 7.8 UNDER 1.9 UNDER 1.5 UNDER 2.9 UNDER 3.3 UNDER 1.6 UNDER 3.1 UNDER 0.8 UNDER		57 53 52 59 58 52 52 51 52 60 54	52 49 47 47 50 50 49 49 53 49	331131.1 154881.7 131825.7 346736.9 363078.1 151356.1 138038.4 120226.4 138038.4 660693.4 208929.6

55.9 UNDER

56.2 UNDER

50.3 UNDER

46 93325.43

47

48

144544

85113.8

52

54

49

11:37:30

11:38:00

11:38:30

49.7

51.6

49.3

11:39:00	52.9	55 UNDER	54	48	194984.5
11:39:30	52.6	54.7 UNDER	54	50	181970.1
11:40:00	53.8	60.3 UNDER	56	50	239883.3
11:40:30	57.1	61.3 UNDER	59	51	512861.4
11:41:00	50.2	53.5 UNDER	51	48	104712.9
11:41:30	54.5	56.3 UNDER	55	49	281838.3
11:42:00	53.9	56.2 UNDER	55	52	245470.9
11:42:30	55.1	58.1 UNDER	57	51	323593.7
11:43:00	58.1	59.5 UNDER	58	57	645654.2
11:43:30	59.2	65.1 UNDER	62	54	831763.8
11:44:00	55.9	57.9 UNDER	56	54	389045.1
11:44:30	56.8	58.5 UNDER	58	54	478630.1
11:45:00	59.3	62.6 UNDER	60	57	851138
11:45:30	61.7	63.1 UNDER	62	60	1479108
11:46:00	61.4	63 UNDER	62	60	1380384
11:46:30	61.8	63.1 UNDER	62	60	1513561
11:47:00	61.9	63.1 UNDER	62	60	1548817
11:47:30	61.8	63.9 UNDER	62	59	1513561
11:48:00	61.9	63.4 UNDER	62	60	1548817
11:48:30	61.6	62.9 UNDER	62	60	1445440
11:49:00	62.2	64.5 UNDER	63	60	1659587
11:49:30	61.7	63.1 UNDER	62	60	1479108
11:50:00	62.1	64.3 UNDER	63	60	1621810
11:50:30	61.7	63.7 UNDER	62	59	1479108
11:51:00	61.6	63.1 UNDER	62	60	1445440
11:51:30	61.8	63.9 UNDER	62	60	1513561
11:52:00	61.7	63.4 UNDER	62	59	1479108
11:52:30	61.2	62.9 UNDER	62	59	1318257
11:53:00	61.3	63 UNDER	62	60	1348963
11:53:30	61.2	63.1 UNDER	62	59	1318257
11:54:00	61.6	62.9 UNDER	62	60	1445440
11:54:30	61.5	63.5 UNDER	62	59	1412538
11:55:00	61.9	64 UNDER	62	60	1548817
11:55:30	60.9	62.5 UNDER	61	59	1230269
11:56:00	61.4	63.1 UNDER	62	60	1380384
11:56:30	61.6	63.3 UNDER	62	60	1445440
11:57:00	61	62.5 UNDER	62	59	1258925
11:57:30	61.3	62.3 UNDER	62	59	1348963
11:58:00	61	62.3 UNDER	61	60	1258925
11:58:30	60.7	62.9 UNDER	61	58	1174898
11:59:00	60.9	62.1 UNDER	61	59	1230269
11:59:30	61.3	63.7 UNDER	62	60	1348963
12:00:00	61.2	63.5 UNDER	62	59	1318257
12:00:30	61.4	62.9 UNDER	62	60	1380384
12:01:00	61.5	63.9 UNDER	63	59	1412538
12:01:30	60.9	62.2 UNDER	61	59	1230269

12:02:00	61.1	62.3 UNDER	61	60	1288250
12:02:30	60.4	61.9 UNDER	61	58	1096478
12:03:00	61	63.1 UNDER	62	58	1258925
12:03:30	60.7	62.3 UNDER	61	58	1174898
12:04:00	60.6	63.3 UNDER	62	58	1148154
12:04:30	59.3	61.3 UNDER	60	58	851138
12:05:00	59.3	61.3 UNDER	60	58	851138
12:05:30	59	59.7 UNDER	59	58	794328.2
12:06:00	59.3	59.9 UNDER	59	58	851138
12:06:30	59.1	59.9 UNDER	59	57	812830.5
12:07:00	60.6	62.3 UNDER	61	58	1148154
12:07:30	59.7	62.3 UNDER	61	58	933254.3
12:08:00	58.7	59.7 UNDER	59	57	741310.2
12:08:30	60.1	61.3 UNDER	61	58	1023293
12:09:00	59.6	61.3 UNDER	60	57	912010.8
12:09:30	59.9	61.7 UNDER	60	58	977237.2
12:10:00	58.4	60.1 UNDER	59	56	691831
12:10:30	58.2	60.7 UNDER	59	56	660693.4
12:11:00	57.8	60.5 UNDER	59	56	602559.6
12:11:30	59.3	61.3 UNDER	60	58	851138
12:12:00	60.6	62.9 UNDER	61	59	1148154
12:12:30	56.1	59.9 UNDER	59	50	407380.3
12:13:00	51	54.9 UNDER	51	48	125892.5
12:13:30	51.9	57.2 UNDER	54	48	154881.7
12:14:00	54.8	58.3 UNDER	56	50	301995.2
12:14:30	56.1	58.3 UNDER	57	53	407380.3
12:15:00	56.2	59.5 UNDER	58	53	416869.4
12:15:30	56.4	59.7 UNDER	59	53	436515.8
12:16:00	58.8	69 UNDER	57	55	758577.6

******** Filename Test Locat Employee N Employee N Department	******** ion ame umber 10237 Lees	***********MON9VA 7ERZ, EJAENV burg Pike	*****	******	******
Calibrator Calibrator ******	Type Cal. Date ******	 ********	*****	*****	******
METROSONIC REPORT PRI	S db-3080 NTED ON 03	V1.12 SERIAL /21/19 at 15:38	# 3895 :50		
User ID: _					
LOGGING ST TOTAL LOGG	ARTED ING TIME	.03/20/19 at 11 .0 DAYS 01:12:1	:00:00		
LOGGING ST TOTAL INTE INTERVAL L	OPPED RVALS ENGTH	.03/20/19 at 12 0.145 .00:00:30	:12:13		
AUTO STOP. CLOCK SYNC RESPONSE R FILTER	 H ATE	.NO .YES .SLOW .A WT.			
PRE-TEST C PRE-TEST C POST-TEST CUTOFF USE	ALIBRATION ALIBRATION CALIBRATIO D FOR TIME	TIME03/20/ RANGE40.1 T N NOT DONE HISTORY Lav	19 AT 09:2 O 140.1 dB NONE	4:41	
<<< SUMMAR	Y REPORT F	OR TEST NUMBER	1 OF 1 >>>		

CUTOFFS... ....... ... 80dB 90dB CEILING... ...... ....115dB

...3dB

EXCHANGE R ATE......

DOSE CRITE	RION LEVEL	90dB	
DOSE CRITE	RION LENGT	H 8 HOURS	
Lav		8dB	
Lav ( 80).	40.	1dB	
Lav ( 90).	40.	1dB	
SEL	93.	1dB	
	48.	7dB	
TWA ( 80).		1dB	
TWA ( 90).	40.	1dB	
		8dB 03/20/19 a	t 12:04:02
•	UNDER		
TIME OVER	115dB00	:00:00.00	
DOCE ( 80)		0.000	,
DOSE (80)		0.00%	
PROJ. DOSE	` '	0.00% 0.00%	
DOSE (90)			
PROJ. DOSE	( 90)	0.00%	)
<<< TIMF H	ISTORY REP	ORT FOR TEST NU	MBFR 1 OF
		2111 211 122 110	

<<< TIME H	ISTORY REP	ORT FOR TEST NU	MBER 1 OF	1 >>>

TIME	Lav dBA	Lmax dBA		Lpk dBC	L(10.0) dBA	L(99.9 dBA	9)	
3/20/20		UDA		ubc	UDA	UDA		
11:00:		57.9	60.6	UNDER		59.1	55.1	616595
11:00:		58.7		UNDER		59.1	57.1	741310.2
11:01:		57.1		UNDER		59.1	49.1	512861.4
11:01:	30	51.2	54.6	UNDER		53.1	48.1	131825.7
11:02:	00	56	58.6	UNDER		58.1	50.1	398107.2
11:02:	30	53.5	56.3	UNDER		55.1	48.1	223872.1
11:03:	00	53.9	59.9	UNDER		57.1	47.1	245470.9
11:03:	30	57.4	60.6	UNDER		59.1	54.1	549540.9
11:04:	00	57.7	61	UNDER		60.1	52.1	588843.7
11:04:	30	56.8	61.8	UNDER		60.1	53.1	478630.1
11:05:	00	54.9	58.6	UNDER		57.1	50.1	309029.5
11:05:	30	51.9	53.8	UNDER		53.1	49.1	154881.7
11:06:	00	56.7	59.7	UNDER		59.1	51.1	467735.1
11:06:	30	59.1	63.8	UNDER		61.1	56.1	812830.5
11:07:	00	58.9	62	UNDER		60.1	56.1	776247.1
11:07:	30	59.2	60.7	UNDER		60.1	57.1	831763.8
11:08:	00	56.6	59.6	UNDER		59.1	50.1	457088.2
11:08:	30	55.6	60.3	UNDER		59.1	49.1	363078.1
11:09:	00	53.9	56.2	UNDER		55.1	50.1	245470.9
11:09:	30	53	57.3	UNDER		55.1	48.1	199526.2

11:10:00	55.3	57.8 UNDER	57.1	52.1	338844.2
11:10:30	58.8	60.6 UNDER	59.1	56.1	758577.6
11:11:00	59.7	62.2 UNDER	61.1	55.1	933254.3
11:11:30	56	59.8 UNDER	58.1	52.1	398107.2
11:12:00	58.6	61.4 UNDER	61.1	55.1	724436
11:12:30	55.9	57.4 UNDER	57.1	54.1	389045.1
11:13:00	56.8	59.1 UNDER	58.1	54.1	478630.1
11:13:30	57.5	61.4 UNDER	60.1	51.1	562341.3
11:14:00	60.9	64.6 UNDER	63.1	57.1	1230269
11:14:30	57	63 UNDER	58.1	55.1	501187.2
11:15:00	58.4	61 UNDER	60.1	50.1	691831
11:15:30	53	58.5 UNDER	56.1	47.1	199526.2
11:16:00	58.2	60.2 UNDER	59.1	56.1	660693.4
11:16:30	57.2	60.3 UNDER	58.1	55.1	524807.5
11:17:00	56.4	60.2 UNDER	59.1	52.1	436515.8
11:17:30	54.5	59.4 UNDER	57.1	48.1	281838.3
11:17:50	57.9	59.8 UNDER	58.1	56.1	616595
11:18:30	54.9	58.5 UNDER	57.1	47.1	309029.5
11:19:00	50.2	54.8 UNDER	52.1	46.1	104712.9
11:19:30	54	56.6 UNDER	56.1	49.1	251188.6
11:20:00	56.3	61.1 UNDER	58.1	53.1	426579.5
11:20:30	56.3	58.6 UNDER	57.1	55.1	426579.5
11:21:00	55.6	58.3 UNDER	57.1 57.1	49.1	363078.1
11:21:30	54.3	59.2 UNDER	58.1	49.1	269153.5
11:22:00	57.3	59.9 UNDER	58.1	55.1	537031.8
11:22:30	57.3 57.7	59 UNDER	58.1	55.1	588843.7
11:22:30	51.9	57.3 UNDER	56.1	47.1	154881.7
11:23:30	52.4	54.6 UNDER	53.1	47.1	173780.1
11:24:00	60.8	67.3 UNDER	64.1	54.1	1202264
11:24:30	58.5	59.4 UNDER	59.1	57.1	707945.8
11:25:00	59.8	63.8 UNDER	62.1		954992.6
11:25:30	55.5	58.6 UNDER	58.1	50.1	354813.4
11:26:00	59.7	61.1 UNDER	60.1		933254.3
11:26:30	58.2	62.2 UNDER	61.1	54.1	660693.4
11:27:00	52.5	57 UNDER	55.1	46.1	177827.9
11:27:30	50.4	57 UNDER	55.1	45.1	109647.8
11:28:00	58.9	60.7 UNDER	60.1	55.1	776247.1
11:28:30	59.5	60.6 UNDER	60.1		891250.9
11:29:00	56.9	62.2 UNDER	60.1	50.1	489778.8
11:29:30	55.4	57.6 UNDER	57.1	53.1	346736.9
11:30:00	57.8	60.2 UNDER	59.1	55.1	602559.6
11:30:30	54.7	57 UNDER	56.1	50.1	295120.9
11:31:00	53.2	57 UNDER	56.1		208929.6
11:31:30	57	61.8 UNDER	61.1	49.1	501187.2
11:32:00	59.3	63 UNDER	61.1	57.1	851138
11:32:30	57.9	60.8 UNDER	59.1	55.1	616595
11:33:00	57.3	60.4 UNDER	59.1	51.1	537031.8

11:33:30	55.3	57.4 UNDER	57.1	51.1 338844.2
11:34:00	53.6	58.2 UNDER	55.1	51.1 229086.8
11:34:30	55.3	58.1 UNDER	57.1	53.1 338844.2
11:35:00	57.1	58.9 UNDER	58.1	55.1 512861.4
11:35:30	56.5	59.6 UNDER	57.1	54.1 446683.6
11:36:00	57	58.9 UNDER	58.1	54.1 501187.2
11:36:30	54.6	59.7 UNDER	57.1	49.1 288403.2
11:37:00	49.5	52.8 UNDER	52.1	43.1 89125.09
11:37:30	57.4	60.7 UNDER	60.1	45.1 549540.9
11:38:00	57.5	60.2 UNDER	58.1	56.1 562341.3
11:38:30	60	65.4 UNDER	61.1	56.1 1000000
11:39:00	55.1	62.7 UNDER	58.1	47.1 323593.7
11:39:30	53.5	56.6 UNDER	56.1	46.1 223872.1
11:40:00	57.8	62.2 UNDER	61.1	54.1 602559.6
11:40:30	57.1	58.6 UNDER	57.1	55.1 512861.4
11:41:00	56.4	60.2 UNDER	58.1	49.1 436515.8
11:41:30	49.8	51.4 UNDER	50.1	48.1 95499.26
11:42:00	60.2	62.5 UNDER	61.1	50.1 1047129
11:42:30	58.5	61 UNDER	60.1	53.1 707945.8
11:43:00	53.4	56.2 UNDER	54.1	51.1 218776.2
11:43:30	56	58.8 UNDER	58.1	53.1 398107.2
11:44:00	58.6	60.6 UNDER	59.1	55.1 724436
11:44:30	52	56.2 UNDER	53.1	47.1 158489.3
11:45:00	54.8	58.5 UNDER	57.1	47.1 301995.2
11:45:30	56.3	57.4 UNDER	57.1	54.1 426579.5
11:46:00	56.3	59 UNDER	58.1	52.1 426579.5
11:46:30	55.6	57.4 UNDER	57.1	53.1 363078.1

11:47:00	53.2	56.9 UNDER	55.1	49.1 208929.6
11:47:30	54.8	57.4 UNDER	56.1	52.1 301995.2
11:48:00	58.6	59.9 UNDER	59.1	56.1 724436
11:48:30	60.1	61.9 UNDER	61.1	57.1 1023293
11:49:00	59.9	64.1 UNDER	63.1	53.1 977237.2
11:49:30	53.3	55.4 UNDER	54.1	51.1 213796.2
11:50:00	55.5	57.5 UNDER	57.1	53.1 354813.4
11:50:30	56	57.8 UNDER	57.1	51.1 398107.2
11:51:00	49.2	51.7 UNDER	51.1	45.1 83176.38
11:51:30	54.9	57.8 UNDER	57.1	49.1 309029.5
11:52:00	58.4	59.8 UNDER	59.1	56.1 691831
11:52:30	58.2	60.6 UNDER	59.1	56.1 660693.4
11:53:00	52.7	56.2 UNDER	55.1	49.1 186208.7
11:53:30	50.2	53.1 UNDER	51.1	47.1 104712.9
11:54:00	56.3	57.8 UNDER	57.1	53.1 426579.5
11:54:30	56.9	59.4 UNDER	58.1	54.1 489778.8
11:55:00	55.5	56.6 UNDER	55.1	54.1 354813.4
11:55:30	58.2	61 UNDER	60.1	55.1 660693.4
11:56:00	58.7	61.3 UNDER	60.1	55.1 741310.2
11:56:30	58.6	60.8 UNDER	60.1	54.1 724436
11:57:00	51.4	55 UNDER	53.1	47.1 138038.4
11:57:30	54	57.3 UNDER	56.1	48.1 251188.6
11:58:00	58.3	59.4 UNDER	59.1	55.1 676083
11:58:30	60.1	62.2 UNDER	61.1	57.1 1023293
11:59:00	51.8	57.4 UNDER	55.1	46.1 151356.1
11:59:30	48	50.6 UNDER	49.1	45.1 63095.73
12:00:00	55.4	57.5 UNDER	57.1	47.1 346736.9
12:00:30	55.1	57 UNDER	56.1	52.1 323593.7
12:01:00	55.5	57.4 UNDER	57.1	52.1 354813.4
12:01:30	56.5	62.4 UNDER	61.1	47.1 446683.6
12:02:00	56.9	59.8 UNDER	58.1	53.1 489778.8
12:02:30	56.3	58.2 UNDER	57.1	53.1 426579.5
12:03:00	48.6	54.2 UNDER	53.1	44.1 72443.6
12:03:30	55.1	63.4 UNDER	58.1	45.1 323593.7
12:04:00	62.3	67.8 UNDER	65.1	58.1 1698244
12:04:30	58.3	59.4 UNDER	59.1	57.1 676083
12:05:00	55	59 UNDER	58.1	49.1 316227.8
12:05:30	54	58 UNDER	56.1	50.1 251188.6
12:06:00	55.8	59.1 UNDER	58.1	51.1 380189.4
12:06:30	56.7	60.6 UNDER	58.1	54.1 467735.1
12:07:00	53.6	58.2 UNDER	56.1	50.1 229086.8
12:07:30	53.0 57	61 UNDER	60.1	48.1 501187.2
12:07:30	59.2	62.2 UNDER	61.1	57.1 831763.8
12:08:30	58.8	62.2 UNDER	61.1	55.1 758577.6
12:09:00	53.1	57.4 UNDER	55.1	48.1 204173.8
12:09:30	53.5	57.8 UNDER	55.1	50.1 223872.1
12.03.30	J3.J	J7.0 UNDER	JJ.1	JU.1 2230/2.1

12:10:00	57.8	59.4 UNDER	59.1	53.1	602559.6
12:10:30	59.6	65 UNDER	62.1	57.1	912010.8
12:11:00	58.7	60.2 UNDER	59.1	56.1	741310.2
12:11:30	57.2	60.2 UNDER	59.1	54.1	524807.5
12:12:00	58	65 UNDER	59.1	55.1	630957.3

******** Filename Test Locat Employee N Employee N Department	******** ion ame umber 9320 Leesb	***********MON10VA 7ERZ, EJAENV urg Pike	*****	*****	*****
Calibrator Calibrator ******	Type Cal. Date *******	  *******	*****	*****	*****
METROSONIC REPORT PRI	S db-3080 NTED ON 03	V1.12 SERIAL /21/19 at 15:36	# 3895 :27		
User ID: _					
LOGGING ST TOTAL LOGG LOGGING ST TOTAL INTE INTERVAL L	ARTED ING TIME OPPED RVALS ENGTH	.03/20/19 at 12 .0 DAYS 00:49:4 .03/20/19 at 13 0.1	:28:30 8 :18:18		
AUTO STOP. CLOCK SYNC RESPONSE R FILTER	 H ATE	.NO .YES .SLOW .A WT.			
PRE-TEST C PRE-TEST C POST-TEST CUTOFF USE	ALIBRATION ALIBRATION CALIBRATIO D FOR TIME	TIME03/20/ RANGE40.1 T N NOT DONE HISTORY Lav	19 AT 09:2 O 140.1 dB NONE	4:41	
<<< SUMMAR	Y REPORT F	OR TEST NUMBER	1 OF 1 >>>		

EXCHANGE R ATE...... ....3dB

CUTOFFS... ....... ... 80dB 90dB CEILING... ...... ....115dB

DOSE CRITE DOSE CRITE	RION LEVEL RION LENGT	90dB H 8 HOURS							
Lav Lav ( 80). Lav ( 90). SEL	65. 54. 40. 99.	3dB 4dB 1dB 9dB							
TWA TWA ( 80). TWA ( 90).	55. 44. 40.	5dB 6dB 1dB							
Lmax Lpk TIME OVER	85. UNDER 115dB00	0dB 03/20/19 RANGE :00:00.00	а	t 12:54:28					
DOSE ( 80) PROJ. DOSE DOSE ( 90) PROJ. DOSE	 ( 80)  ( 90)	0	0.00% 0.00% 0.00% 0.00%						
<<< TIME H	ISTORY REP	ORT FOR TEST	NU	MBER 1 OF	1>>>				
TIME	Lav dBA	Lmax dBA		Lpk dBC	L(10.0) dBA		L(99.9) dBA		
3/20/2019	1								
12:28:30	64.1		67.4	UNDER		67.1		56.1	2570396
12:29:00	65.9	)	71.8	UNDER		70.1		58.1	3890451
12:29:30	57.7	•	64.7	UNDER		61.1		50.1	588843.7
12:30:00	65.3	<b>;</b>	68.6	UNDER		67.1		55.1	3388442
12:30:30	63.1		69	UNDER		67.1		57.1	2041738
12:31:00			67.4	UNDER		66.1		61.1	2884032
12:31:30				UNDER		67.1		62.1	3801894
12:32:00				UNDER		69.1		63.1	4786301
12:32:30				UNDER		70.1		60.1	5248075
12:33:00				UNDER		63.1		57.1	1412538
12:33:30 12:34:00				UNDER UNDER		66.1 65.1		57.1 57.1	2344229 2570396
12:34:30				UNDER		63.1		57.1	1621810
12:35:00				UNDER		66.1		59.1	2818383
12:35:30				UNDER		67.1		61.1	3630781
								<del>_</del>	

69.8 UNDER

67.8 UNDER

**67.8 UNDER** 

69.5 UNDER

70.6 UNDER

68.1

66.1

65.1

68.1

67.1

53.1

56.1

60.1

61.1

61.1

2187762

2041738

1949845 3548134

3981072

12:36:00

12:36:30

12:37:00

12:37:30

12:38:00

63.4

63.1

62.9

65.5

66

12:38:30	66.2	71 UNDER	70.1	54.1	4168694
12:39:00	67.1	71.4 UNDER	68.1	58.1	5128614
12:39:30	61.9	66.2 UNDER	63.1	58.1	1548817
12:40:00	65.9	67.8 UNDER	67.1	61.1	3890451
12:40:30	67.1	74.6 UNDER	72.1	51.1	5128614
12:41:00	64.6	67.2 UNDER	66.1	60.1	2884032
12:41:30	67.7	71.8 UNDER	71.1	60.1	5888437
12:42:00	64.3	68.2 UNDER	67.1	56.1	2691535
12:42:30	62.5	66.2 UNDER	65.1	54.1	1778279
12:43:00	62.6	64.7 UNDER	64.1	56.1	1819701
12:43:30	63.9	67.1 UNDER	66.1	57.1	2454709
12:44:00	65.3	68.4 UNDER	67.1	60.1	3388442
12:44:30	65.7	69 UNDER	67.1	60.1	3715352
12:45:00	64.2	67.4 UNDER	66.1	61.1	2630268
12:45:30	64.6	67.9 UNDER	67.1	59.1	2884032
12:46:00	66.4	69 UNDER	68.1	63.1	4365158
12:46:30	65.2	69.4 UNDER	69.1	61.1	3311311
12:47:00	66.6	68.6 UNDER	68.1	62.1	4570882
12:47:30	64	68.2 UNDER	66.1	56.1	2511886
12:48:00	64.6	66.7 UNDER	66.1		2884032
12:48:30	61.9	66.2 UNDER	64.1		1548817
12:49:00	63.7	68.2 UNDER	67.1	56.1	2344229
12:49:30	64.1	68.2 UNDER	67.1		2570396
12:50:00	63.8	67.8 UNDER	66.1	52.1	2398833
12:50:30	66.2	70.3 UNDER	68.1		4168694
12:51:00	68.7	76.2 UNDER	73.1		7413102
12:51:30	66.1	68.4 UNDER	67.1	60.1	4073803
12:52:00	65.4	68.6 UNDER	67.1	60.1	3467369
12:52:30	66.4	69.8 UNDER	69.1		4365158
12:53:00	65.7	68.6 UNDER	67.1		3715352
12:53:30	67	75 UNDER	71.1	60.1	5011872
12:54:00	73.8	85 UNDER	75.1	64.1 2	3988329
12:54:30	72	84.2 UNDER	75.1		5848932
12:55:00	60.2	65.6 UNDER	62.1		1047129
12:55:30	63.5	67 UNDER	66.1		2238721
12:56:00	64.8	67.4 UNDER	66.1		3019952
12:56:30	63.8	66.6 UNDER	66.1		2398833
12:57:00	65.6	68.7 UNDER	67.1		3630781
12:57:30	68.5	73.1 UNDER	71.1		7079458
12:58:00	64.8	66.6 UNDER	66.1		3019952
12:58:30	62.7	67 UNDER	65.1		1862087
12:59:00	66.1	70.3 UNDER	68.1		4073803
12:59:30	63.1	67.4 UNDER	66.1		2041738
13:00:00	64.8	67.4 UNDER	66.1		3019952
13:00:30	65.8	69.4 UNDER	68.1		3801894
13:01:00	64.7	68.8 UNDER	67.1		2951209

13:01:30	59.3	65.8 UNDER	63.1	51.1	851138
13:02:00	66.3	69.4 UNDER	68.1	58.1	4265795
13:02:30	65	69.8 UNDER	68.1	59.1	3162278
13:03:00	64	67 UNDER	66.1	58.1	2511886
13:03:30	65.9	71.4 UNDER	70.1	58.1	3890451
13:04:00	63.6	67.4 UNDER	66.1	59.1	2290868
13:04:30	64.7	69.4 UNDER	67.1	57.1	2951209
13:05:00	62.2	65 UNDER	64.1	59.1	1659587
13:05:30	65.6	67.8 UNDER	67.1	60.1	3630781
13:06:00	63	65.8 UNDER	64.1	58.1	1995262
13:06:30	60.9	65.4 UNDER	64.1	51.1	1230269
13:07:00	62.7	68.7 UNDER	67.1	46.1	1862087
13:07:30	63.7	67.4 UNDER	66.1	53.1	2344229
13:08:00	64.6	70.1 UNDER	65.1	61.1	2884032
13:08:30	66.5	71 UNDER	69.1	59.1	4466836
13:09:00	63.1	66.7 UNDER	65.1	60.1	2041738
13:09:30	67	70.2 UNDER	69.1	63.1	5011872
13:10:00	65.6	67 UNDER	66.1	61.1	3630781
13:10:30	64.1	66.6 UNDER	66.1	60.1	2570396
13:11:00	63.9	68.6 UNDER	67.1	57.1	2454709
13:11:30	64.8	66.7 UNDER	66.1	63.1	3019952
13:12:00	62.9	66.2 UNDER	65.1	52.1	1949845
13:12:30	64.2	68.2 UNDER	67.1	59.1	2630268
13:13:00	63.9	69.4 UNDER	66.1	59.1	2454709
13:13:30	64.2	67.8 UNDER	66.1	58.1	2630268
13:14:00	65.3	69.6 UNDER	67.1	61.1	3388442
13:14:30	62.9	66.6 UNDER	66.1	52.1	1949845
13:15:00	63.4	65.5 UNDER	65.1	61.1	2187762

13:15:30	65.7	68.2 UNDER	67.1	61.1 3715352
13:16:00	64.6	66.8 UNDER	65.1	62.1 2884032
13:16:30	62.5	65.4 UNDER	64.1	57.1 1778279
13:17:00	65	68 UNDER	67.1	61.1 3162278
13:17:30	64.7	67.8 UNDER	66.1	57.1 2951209
13:18:00	61.8	63.8 UNDER	63.1	58.1 1513561

******** Filename Test Locat Employee N Employee N Department	********* ion ame umber 1424 Woodh	***********MON11VA 7ERZ, EJAENV urst BLVD	******	*****	*****
Calibrator Calibrator *******	Type Cal. Date ******	  *******	*****	*****	*****
METROSONIC REPORT PRI	S db-3080 NTED ON 03	V1.12 SERIAL /21/19 at 15:36	# 3895 :42		
User ID: _					
LOGGING ST TOTAL LOGG LOGGING ST TOTAL INTE INTERVAL L	ARTED ING TIME OPPED RVALS ENGTH	.03/20/19 at 13 .0 DAYS 00:33:2 .03/20/19 at 14 0.67	:36:30 5 :09:55	;	
AUTO STOP. CLOCK SYNC RESPONSE R FILTER	 H ATE	.NO .YES .SLOW .A WT.			
PRE-TEST C PRE-TEST C POST-TEST CUTOFF USE	ALIBRATION ALIBRATION CALIBRATIO D FOR TIME	TIME03/20/ RANGE40.1 T N NOT DONE HISTORY Lav	19 AT 09:2 O 140.1 dB NONE	4:41	
<<< SUMMAR	Y REPORT F	OR TEST NUMBER	1 OF 1 >>>		
EXCHANGE R	ATE	3dB			

CUTOFFS... .....

CEILING...

... 80dB 90dB

...115dB

DOSE CRITE	RION LEVEL	90dB					
DOSE CRITE	RION LENGT	H 8 HOURS					
Lav	52.	6dB					
Lav ( 80).	40.	1dB					
Lav ( 90).	40.	1dB					
SEL	85.	5dB					
JLL	65.	345					
TWA	41.	OdB					
TWA ( 80).	40.	1dB					
TWA ( 90).	40.	1dB					
	60	0.10.00./00./40					
Lmax	63.	8dB 03/20/19 a	t 14:09:54				
Lpk	UNDER	RANGE					
TIME OVER	115dB00	:00:00.00					
DOSE ( 80)		0.00%	•				
PROJ. DOSE	( 80)	0.00%					
DOSE ( 90)		0.00%					
PROJ. DOSE	( 90)	0.00%					
r NOJ. DOJE	( 50)	0.0070	•				
<<< TIME H	ISTORY REP	ORT FOR TEST NU	MBER 1 OF	1>>>			
					. (22.2)		
TIME	Lav	Lmax	Lpk	L(10.0)	L(99.9)		
	dBA	dBA	dBC	dBA	dBA		
3/20/2019							
13:36:30			UNDER		54.1	50.1	
13:37:00			UNDER		50.1	48.1	100000
13:37:30	50.8	55.4	UNDER		52.1		120226.4
13:38:00	53.2	2 56.6	UNDER		55.1	50.1	208929.6
13:38:30	50.6	52.5	UNDER		51.1	47.1	114815.4
13:39:00	) 48.5	50.6	UNDER		49.1	46.1	70794.58
13:39:30	) 46.4	48.6	UNDER		47.1	45.1	43651.58
13:40:00	47.3	3 49.4	UNDER		49.1	45.1	53703.18
13:40:30	53.2	2 56.2	UNDER		55.1	49.1	208929.6
13:41:00	55.6	57.2	UNDER		56.1	53.1	363078.1
13:41:30	52.8	56.2	UNDER		55.1	49.1	190546.1
13:42:00	53.3	55.5	UNDER		55.1	50.1	213796.2
13:42:30	50.2	52.1	UNDER		51.1	49.1	104712.9
13:43:00			UNDER		51.1	49.1	104712.9
13:43:30			UNDER		50.1		67608.3
13:44:00			UNDER		56.1		181970.1
13:44:30			UNDER		52.1		144544
13:45:00			UNDER		53.1		120226.4
10.15.00	30.0	55.5			50.4		52005 72

51.4 UNDER

13:45:30

48

50.1

45.1 63095.73

13:46:00	48.2	51 UNDER	49.1	46.1	66069.34
13:46:30	49.7	53.6 UNDER	52.1	47.1	93325.43
13:47:00	53.5	54.8 UNDER	54.1	52.1	223872.1
13:47:30	55.5	60.6 UNDER	57.1	52.1	354813.4
13:48:00	56.4	62.4 UNDER	59.1	49.1	436515.8
13:48:30	52.1	59.4 UNDER	53.1	49.1	162181
13:49:00	55.7	62.2 UNDER	60.1	50.1	371535.2
13:49:30	50.5	57.2 UNDER	53.1	45.1	112201.8
13:50:00	55.5	59 UNDER	57.1	51.1	354813.4
13:50:30	56.7	63.4 UNDER	59.1	53.1	467735.1
13:51:00	56.6	61.8 UNDER	59.1	51.1	457088.2
13:51:30	49.4	53.8 UNDER	51.1	46.1	87096.36
13:52:00	49.8	52.5 UNDER	51.1	47.1	95499.26
13:52:30	51.4	56.6 UNDER	55.1	47.1	138038.4
13:53:00	53.7	56.6 UNDER	55.1	51.1	234422.9
13:53:30	50.3	51.1 UNDER	50.1	49.1	107151.9
13:54:00	48.4	50.6 UNDER	50.1	45.1	69183.1
13:54:30	48.1	49.8 UNDER	49.1	45.1	64565.42
13:55:00	48	50.1 UNDER	49.1	46.1	63095.73
13:55:30	47.4	50.4 UNDER	48.1	45.1	54954.09
13:56:00	53.1	54.9 UNDER	54.1	49.1	204173.8
13:56:30	52.2	53.9 UNDER	53.1	51.1	165958.7
13:57:00	50.3	53.4 UNDER	51.1	48.1	107151.9
13:57:30	50	53 UNDER	51.1	47.1	100000
13:58:00	48.6	50.6 UNDER	49.1	46.1	72443.6
13:58:30	50	54.8 UNDER	51.1	47.1	100000
13:59:00	55.1	60.5 UNDER	58.1	51.1	323593.7
13:59:30	52.9	57 UNDER	55.1	50.1	194984.5
14:00:00	50	52.4 UNDER	50.1	48.1	100000
14:00:30	49.6	51 UNDER	50.1	47.1	91201.08
14:01:00	49.3	50.6 UNDER	50.1	47.1	85113.8
14:01:30	56.8	63 UNDER	60.1	47.1	478630.1
14:02:00	54.3	59.8 UNDER	57.1	50.1	269153.5
14:02:30	51.2	53.5 UNDER	52.1	49.1	131825.7
14:03:00	50.6	52.1 UNDER	51.1	48.1	114815.4
14:03:30	50.8	54.6 UNDER	53.1	47.1	120226.4
14:04:00	56.5	61.4 UNDER	59.1	49.1	446683.6
14:04:30	52	53.4 UNDER	53.1	50.1	158489.3
14:05:00	51.8	53.5 UNDER	53.1	50.1	151356.1
14:05:30	54	57.4 UNDER	56.1	50.1	251188.6
14:06:00	49.8	50.8 UNDER	50.1	49.1	95499.26
14:06:30	51.8	56.1 UNDER	54.1	48.1	151356.1
14:07:00	49.7	51.8 UNDER	51.1	47.1	93325.43
14:07:30	49.8	54 UNDER	52.1	45.1	95499.26
14:08:00	57	62.2 UNDER	61.1	51.1	501187.2
14:08:30	52.8	57.8 UNDER	54.1	51.1	190546.1

14:09:00	51.7	55 UNDER	53.1	48.1 147910.8
14:09:30	57.4	63.8 UNDER	60.1	48.1 549540.9

******* Filename Test Locat Employee N Employee N Department	********* ion ame umber 9105 Lucky	***********MON12VA 7ERZ, EJAENV Estates Dr	*****	*****	*****
Calibrator Calibrator ******	Type Cal. Date ******	  ******	*****	*****	*****
METROSONIC REPORT PRI	S db-3080 NTED ON 03	V1.12 SERIAL /21/19 at 15:36	# 3897 :56		
User ID: _					
LOGGING ST TOTAL LOGG LOGGING ST TOTAL INTE INTERVAL L	ARTED ING TIME OPPED RVALS ENGTH	.03/20/19 at 12 .0 DAYS 00:37:2 .03/20/19 at 13 0.75	:23:57	7	

TOTAL IN	<b>ITE</b>	RVALS	0.7	5	
INTERVA	LL	ENGTH	.00:00:30		
AUTO ST	OP.		.NO		
CLOCK S	YNC	H	.YES		
RESPONS	SE R	ATE	.SLOW		
FILTER			.A WT.		
PRE-TES	ГС	ALIBRATION	TIME03/20/	19 AT 09:2	1:29
PRE-TES	ГС	ALIBRATION	RANGE39.9 T	O 139.9 dB	
POST-TE	ST	CALIBRATIO	N TIME03/20/	19 AT 13:4	4:08
POST-TE	ST	CALIBRATIO	N RANGE39.9	TO 139.9	
CUTOFF	USE	D FOR TIME	HISTORY Lav	NONE	
<<< SUN	1MAR	Y REPORT F	OR TEST NUMBER	1 OF 1 >>>	
EXCHAN	GE R	ATE	3dB		
CUTOFFS	S		80dB 90dB		

CEILING DOSE CRITE DOSE CRITE		90dB
Lav	57.	2dB
Lav ( 80).	39.	9dB
Lav ( 90).	39.	9dB
SEL	90.	7dB
TWA		2dB
TWA ( 80).	39.	9dB
TWA ( 90).	39.	9dB
		8dB 03/20/19 a t 13:23:56
Lpk		
TIME OVER	115dB00	:00:00.00
( · )		2.224
DOSE ( 80)		0.00%
PROJ. DOSE	,	0.00%
DOSE ( 90)		0.00%
PROJ. DOSE	( 90)	0.00%

<<< TIME H ISTORY REP ORT FOR TEST NU MBER 1 OF 1 >>>

TIME		Lav	Lmax	Lpk	L(10.0)		L(99.9)		
		dBA	dBA	dBC	dBA		dBA		
3	3/20/2019								
	12:46:30	57.	3 65	.2 UNDER	1	59.9		53.9	537031.8
	12:47:00	57.	6 60	.8 UNDER		59.9		54.9	575439.9
	12:47:30	58.	4	61 UNDER		59.9		56.9	691831
	12:48:00	57.	6 61	2 UNDER	1	60.9		55.9	575439.9
	12:48:30	55.	2 59	.3 UNDER		58.9		49.9	331131.1
	12:49:00	56.	9 61	6 UNDER		59.9		51.9	489778.8
	12:49:30	59.	1 60	.8 UNDER		60.9		55.9	812830.5
	12:50:00	54.	9 56	.8 UNDER	1	56.9		52.9	309029.5
	12:50:30	5	6	60 UNDER	1	58.9		52.9	398107.2
	12:51:00	56.	7 58	.4 UNDER	1	57.9		54.9	467735.1
	12:51:30	58.	5 61	.2 UNDER	1	59.9		56.9	707945.8
	12:52:00	5	8 60	.8 UNDER	1	59.9		54.9	630957.3
	12:52:30	57.	5 60	.4 UNDER	1	59.9		52.9	562341.3
	12:53:00	55.	8 58	.9 UNDER	1	57.9		51.9	380189.4
	12:53:30	63.	1 66	.6 UNDER	1	65.9		58.9	2041738
	12:54:00	59.	4 65	.6 UNDER	1	61.9		56.9	870963.6
	12:54:30	53.	6 56	.8 UNDER		55.9		49.9	229086.8
	12:55:00	58.	3 61	.5 UNDER	1	60.9		54.9	676083

12:55:30	58	61.9 UNDER	59.9	53.9 630957.3	
12:56:00	57.7	60.4 UNDER	59.9	54.9 588843.7	
12:56:30	55.5	57.2 UNDER	56.9	54.9 354813.4	
12:57:00	56.7	59.5 UNDER	58.9	51.9 467735.1	
12:57:30	58.2	60.4 UNDER	59.9	55.9 660693.4	
12:58:00	58.5	61.3 UNDER	60.9	53.9 707945.8	
12:58:30	49.4	53.6 UNDER	52.9	45.9 87096.36	
12:59:00	56.1	59.4 UNDER	58.9	50.9 407380.3	
12:59:30	56.7	59.5 UNDER	58.9	54.9 467735.1	
13:00:00	57.4	60 UNDER	59.9	53.9 549540.9	
13:00:30	51.1	55.6 UNDER	54.9	45.9 128825	
13:01:00	57.2	61 UNDER	60.9	52.9 524807.5	
13:01:30	60.5	63.2 UNDER	62.9	58.9 1122018	
13:02:00	57.4	60.8 UNDER	59.9	52.9 549540.9	
13:02:30	51.7	54.8 UNDER	54.9	46.9 147910.8	
13:03:00	59.2	64 UNDER	63.9	51.9 831763.8	
13:03:30	59.4	63.6 UNDER	62.9	56.9 870963.6	
13:04:00	57.5	59.6 UNDER	59.9	55.9 562341.3	
13:04:30	58.1	63.4 UNDER	61.9	52.9 645654.2	
13:05:00	55.7	58.3 UNDER	56.9	53.9 371535.2	
13:05:30	56.3	58 UNDER	57.9	53.9 426579.5	
13:06:00	57.2	59.2 UNDER	58.9	54.9 524807.5	
13:06:30	54.5	58.7 UNDER	58.9	47.9 281838.3	
13:07:00	55.6	59.2 UNDER	57.9	47.9 363078.1	
13:07:30	57.3	59.2 UNDER	58.9	55.9 537031.8	
13:08:00	53.9	58.3 UNDER	57.9	48.9 245470.9	
13:08:30	50.6	57.1 UNDER	54.9	44.9 114815.4	
13:09:00	60.7	66.7 UNDER	65.9	56.9 1174898	
13:09:30	59.3	64.4 UNDER	61.9	55.9 851138	
13:10:00	58	60.6 UNDER	60.9	54.9 630957.3	
13:10:30	57.2	63.1 UNDER	60.9	52.9 524807.5	
13:11:00	54.7	58 UNDER	57.9	51.9 295120.9	
13:11:30	57.6	59.6 UNDER	58.9	55.9 575439.9	
13:12:00	58.4	62.4 UNDER	61.9	54.9 691831	
13:12:30	53.7	55.6 UNDER	54.9	50.9 234422.9	
13:13:00	57.9	60.4 UNDER	60.9	52.9 616595	
13:13:30	58.2	60.5 UNDER	60.9	56.9 660693.4	
13:14:00	57.9	60.8 UNDER	59.9	55.9 616595	
13:14:30	54	57.6 UNDER	56.9	52.9 251188.6	
13:15:00	55.6	57.2 UNDER	56.9	53.9 363078.1	
13:15:30	56.6	60 UNDER	58.9	54.9 457088.2	
13:16:00	55.9	58.4 UNDER	57.9	53.9 389045.1	
13:16:30	53.4	57.2 UNDER	55.9	51.9 218776.2	
13:17:00	57.1	60.4 UNDER	58.9	52.9 512861.4	
13:17:30	58	60.4 UNDER	59.9	54.9 630957.3	
13:17:50	56.5	58.4 UNDER	57.9	53.9 446683.6	
13.10.00	50.5	JO. I GINDLIN	37.3	33.3 440003.0	

13:18:30	55.6	58.6 UNDER	57.9	51.9	363078.1
13:19:00	58.8	61.4 UNDER	60.9	57.9	758577.6
13:19:30	55.9	58.4 UNDER	57.9	53.9	389045.1
13:20:00	55.7	57.2 UNDER	56.9	52.9	371535.2
13:20:30	53.7	56.8 UNDER	56.9	47.9	234422.9
13:21:00	51.5	56.8 UNDER	55.9	44.9	141253.8
13:21:30	59.4	61.6 UNDER	61.9	55.9	870963.6
13:22:00	56.4	59.1 UNDER	57.9	53.9	436515.8
13:22:30	56.3	61.2 UNDER	59.9	50.9	426579.5
13:23:00	56.8	60.7 UNDER	58.9	55.9	478630.1
13:23:30	58.7	72.8 UNDER	60.9	55.9	741310.2

******** Filename Test Locat Employee N Employee N Department	******** ion ame umber 1308 Trap	**************************************	****	****	*****
Calibrator Calibrator ******	Type Cal. Date ******	  *******	*****	*****	*****
METROSONIC REPORT PRI	S db-3080 NTED ON 03	V1.20 SERIAL /21/19 at 15:37	# 5093 :12		
User ID: _					
LOGGING ST TOTAL LOGG LOGGING ST TOTAL INTE INTERVAL L	ARTED ING TIME OPPED RVALS ENGTH	.03/20/19 at 12 .0 DAYS 00:39:0 .03/20/19 at 13 0.78	:35:30 0 :14:30	)	
AUTO STOP. CLOCK SYNC RESPONSE R FILTER	 H ATE	.NO .YES .SLOW .A WT.			
PRE-TEST C PRE-TEST C POST-TEST POST-TEST CUTOFF USE	ALIBRATION ALIBRATION CALIBRATIO CALIBRATIO D FOR TIME	TIME03/20/ RANGE41.0 T N TIME03/20/ N RANGE41.0 HISTORY Lav	19 AT 09:3 O 141.0 dB 19 AT 13:4 TO 141.0 NONE	9:10 4:34	
<<< SUMMAR	Y REPORT F	OR TEST NUMBER	1 OF 1 >>>		

EXCHANGE R ATE...... ...3dB

CUTOFFS... ....... ... 80dB 90dB

CEILING		115dB	
DOSE CRITE	RION LEVEL	90dB	
DOSE CRITE	RION LENGT	H 8 HOURS	
Lav	57.	0dB	
Lav ( 80).	41.	0dB	
Lav ( 90).	41.	0dB	
SEL	90.	6dB	
TWA	46.	2dB	
TWA (80).	41.	0dB	
TWA ( 90).	41.	0dB	
Lmax	73.	4dB 03/20/19 a	t 12:42:28
Lpk	UNDER	RANGE	
TIME OVER	115dB00	:00:00.00	
DOSE (80)		0.00%	6
PROJ. DOSE	( 80)	0.00%	6
DOSE ( 90)		0.00%	6
PROJ. DOSE	( 90)	0.00%	6

<<< TIME H ISTORY REP ORT FOR TEST NU MBER 1 OF 1 >>>

	_						
TIME	Lav	Lmax	Lpk	L(10.0)	L(99.9)		
	dBA	dBA	dBC	dBA	dBA		
3/20/20	019						
12:35	:30	58.4	63.3 UNDER	(	50	54	691831
12:36	:00	57.4	62.4 UNDER	į	59	52	549540.9
12:36	:30	49.2	52.5 UNDER	ţ	51	47	83176.38
12:37	:00	51	54 UNDER	ţ	52	49	125892.5
12:37	:30	55.3	58 UNDER	į	56	53	338844.2
12:38	:00	57.1	60.9 UNDER	ţ	59	51	512861.4
12:38	:30	51.4	55.8 UNDER	ţ	53	49	138038.4
12:39	:00	55.4	62.2 UNDER	ţ	58	49	346736.9
12:39	:30	58	59.9 UNDER	ţ	59	54	630957.3
12:40	:00	59.4	64.8 UNDER	(	52	53	870963.6
12:40	:30	52.8	55.5 UNDER	ţ	54	50	190546.1
12:41	:00	54.4	58.9 UNDER	ţ	56	50	275422.9
12:41	:30	54.9	58.5 UNDER	ţ	56	52	309029.5
12:42	:00	63.9	73.4 UNDER	(	69	52	2454709
12:42	:30	62.1	71.9 UNDER	(	63	52	1621810
12:43	:00	62.3	67.7 UNDER	(	64	56	1698244
12:43	:30	56	60.4 UNDER	į	57	53	398107.2
12:44	:00	56.7	60 UNDER	Ţ	58	53	467735.1
12:44	:30	51.5	55.8 UNDER	1	54	47	141253.8

12:45:00	55.6	60.9 UNDER	59	48 363078.1
12:45:30	57.2	62.3 UNDER	59	53 524807.5
12:46:00	55.4	57.2 UNDER	56	51 346736.9
12:46:30	52.7	56.8 UNDER	55	50 186208.7
12:47:00	56	57.2 UNDER	56	54 398107.2
12:47:30	56.3	57.5 UNDER	57	54 426579.5
12:48:00	56.2	60.6 UNDER	58	52 416869.4
12:48:30	53.6	60.8 UNDER	57	49 229086.8
12:49:00	56.6	62.9 UNDER	60	51 457088.2
12:49:30	55.2	57 UNDER	56	53 331131.1
12:50:00	55.5	56.6 UNDER	56	54 354813.4
12:50:30	53.1	58 UNDER	55	48 204173.8
12:51:00	56.4	60.9 UNDER	58	52 436515.8
12:51:30	57.8	58.9 UNDER	58	56 602559.6
12:52:00	56.8	60.4 UNDER	58	53 478630.1
12:52:30	61.3	69.6 UNDER	65	52 1348963
12:53:00	58.3	64.9 UNDER	62	53 676083
12:53:30	61.6	65.7 UNDER	64	56 1445440
12:54:00	61.7	66.4 UNDER	64	54 1479108
12:54:30	58.4	62.9 UNDER	61	52 691831
12:55:00	57.6	61.9 UNDER	60	51 575439.9
12:55:30	56.7	60.9 UNDER	59	54 467735.1
12:56:00	54.4	56.8 UNDER	55	53 275422.9
12:56:30	60.2	64.6 UNDER	62	54 1047129
12:57:00	61.6	71.2 UNDER	65	54 1445440
12:57:30	59.3	64.4 UNDER	62	54 851138
12:58:00	61.4	68.8 UNDER	66	53 1380384
12:58:30	61.7	68.3 UNDER	66	51 1479108
12:59:00	52.2	56.8 UNDER	53	49 165958.7
12:59:30	55.1	58.4 UNDER	56	51 323593.7
13:00:00	52.9	55.5 UNDER	54	47 194984.5
13:00:30	50	53.4 UNDER	51	47 100000
13:01:00	54.4	57.7 UNDER	56	50 275422.9
13:01:30	55.1	56.9 UNDER	56	52 323593.7
13:02:00	53.8	54.9 UNDER	54	51 239883.3
13:02:30	51.4	55.3 UNDER	53	49 138038.4
13:03:00	56.7	63.3 UNDER	60	50 467735.1
13:03:30	54.6	56.4 UNDER	55	52 288403.2
13:04:00	55.7	59.1 UNDER	57	50 371535.2
13:04:30	49.6	51.8 UNDER	50	48 91201.08
13:05:00	54	57.7 UNDER	56	50 251188.6
13:05:30	55.5	57.2 UNDER	56	54 354813.4
13:06:00	54.3	56.4 UNDER	55	50 269153.5
13:06:30	50.9	54.8 UNDER	52	48 123026.9
13:07:00	51.3	52.7 UNDER	52	49 134896.3
13:07:30	52.7	54.1 UNDER	54	48 186208.7
10.07.50	32.7	J.I. JIIDLII	<b>J</b> .	10 100200.7

13:08:00	54.3	55.6 UNDER	55	51	269153.5
13:08:30	56.4	65.9 UNDER	61	48	436515.8
13:09:00	57.3	60.4 UNDER	59	53	537031.8
13:09:30	56.1	58.5 UNDER	57	54	407380.3
13:10:00	55.1	58.3 UNDER	57	50	323593.7
13:10:30	52.3	57.2 UNDER	54	50	169824.4
13:11:00	53.2	54.8 UNDER	54	51	208929.6
13:11:30	55.6	59.6 UNDER	58	53	363078.1
13:12:00	54.6	58.1 UNDER	55	51	288403.2
13:12:30	52.3	55.2 UNDER	53	50	169824.4
13:13:00	54.9	57.6 UNDER	55	53	309029.5
13:13:30	56	57.6 UNDER	57	53	398107.2
13:14:00	56.1	57.3 UNDER	57	54	407380.3

# **Certificate of Calibration**

for

#### ACOUSTICAL CALIBRATOR

Manufactured by: METROSONICS

Model No: CL304
Serial No: 3616
Calibration Recall No: 28756

#### Submitted By:

Customer: EVAN R. ZEIDERS

Company: SKELLY & LOY, INC.

Address: 449 EISENHOWER BLVD., STE. 300 HARRISBURG PA 17111

The subject instrument was calibrated to the indicated specification using standards traceable to the National Institute of Standards and Technology or to accepted values of natural physical constants. This document certifies that the instrument met the following specification upon its return to the submitter.

West Caldwell Calibration Laboratories Procedure No. CL304 METR

Upon receipt for Calibration, the instrument was found to be:

Within (X)

tolerance of the indicated specification. See attached Report of Calibration.

The information supplied relates to the calibrated item listed above.

West Caldwell Calibration Laboratories' calibration control system meets the requirements, ISO 10012-1 MIL-STD-45662A, ANSI/NCSL Z540-1, IEC Guide 25, ISO 9001:2008 and ISO 17025.

Note: With this Certificate, Report of Calibration is included.

Approved by:

Fe

Calibration Date:

26-Apr-18

Felix Christopher (QA Mgr.)

Certificate No:

28756 - 5

QA Doc. #1051 Rev. 2.0 10/1/01

Certificate Page 1 of 1

ISO/IEC 17025:2005

West Caldwell
Calibration
Laboratories, Inc.

1575 State Route 96, Victor, NY 14564, U.S.A.

ACCREDITED

Calibration Lab. Cert. # 1533.01

ISO/IEC 17025: 2005





1575 State Route 96, Victor NY 14564

### REPORT OF CALIBRATION

Metrosonics Acoustical Calibrator

Model No.: CL304

Serial No.: 3616

I. D. No.: XXXX

Company: Skelly & Loy, Inc.

Calibration results: After data: ..... Before data: ... X ...

Before & after data same: .......

Sound Pressure Level at 999.99 Hz and pressure of 1013 hPa (mbar)

was 102.29 dB re 20 µPa

Sound Pressure Level:

Frequency: **Pass** 

Distortion: **Pass** 

Stability:

All tested parameters:

**Pass** 

**Pass Pass**  Laboratory Environment:

Ambient Temperature:

20.2

°C

Ambient Humidity:

32.6

% RH kPa

Ambient Pressure:

98.624

Calibration Date: 26-Apr-2018

Calibration Due: 26-Apr-2019

Report Number:

28756 -5

Control Number:

28756

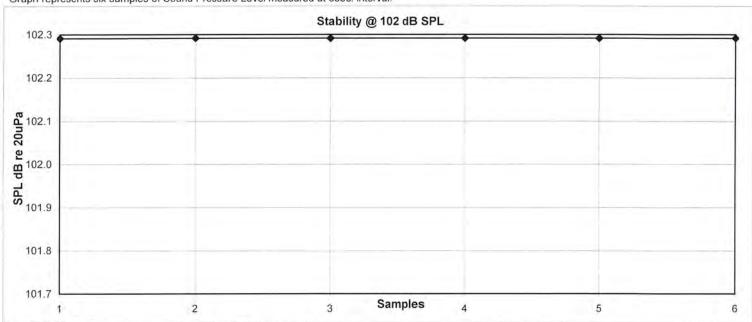
The above listed instrument meets or exceeds the tested manufacturer's specifications.

This Calibration is traceable through NIST test numbers:

822/275722-14

The expanded uncertainty of calibration: 0.11 dB at 95% confidence level with a coverage factor of k=2.

Graph represents six samples of Sound Pressure Level measured at 5sec. interval.



The above listed instrument was checked using calibration procedure documented in West Caldwell

Calibration Laboratories Inc. procedure:

Rev. 7.0 Jan. 24, 2014 Doc. # 1038 CL304METR

Calibration was performed by West Caldwell Calibration Laboratories Inc. under Operating Procedures

intended to implement the requirements of ISO10012-1, IEC Guide 25, ANSI/NCSL Z540-1, (MIL-STD-45662A) and ISO 9001:2008, ISO 17025

Cal. Date: 26-Apr-2018

Measurements performed by: ...

Calibrated on WCCL system type 9700

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James Zhu Rev. 7.0 Jan. 24, 2014 Doc. # 1038CL304METR

1575 State Route 96, Victor NY 14564 Tel. (585) 586-3900 FAX (585) 586-4327

### Calibration Data Record

for

Metrosonics Acoustical Calibrator Company: Skelly & Loy, Inc. Model No.: CL304

Serial No.: 3616

All tested parameters: Pass

Measured Sound Pressure Level (Six samples measured at 5 sec. interval)

Sample	1	102.29 dB re 20 μPa	
	2	102.29	
	3	102.29	
	4	102.29	
	5	102.29	
	6	102.29	
	Average	102.29	Spec. 102 dB ± 0.3 dB

Frequency measured (Three samples at 30 sec. Interval)

Sample	1	999.96 Hz	
	2	1000.00	
	3	1000.00	
	Average	999.99	Spec. 1000 Hz ± 2.0%

Distortion measured -40.1 dB Spec. ≤-34 dB

struments used for ca	alibration:		Date of Cal.	Traceability No.	Re-cal. Due Date
Brüel & Kjær	4231	S/N 2308998	1-Aug-2017	822/275722-14	1-Aug-2018
Brüel & Kjær	4134	S/N 854464	1-Aug-2017	822/275722-14	1-Aug-2018
Brüel & Kjær	2669	S/N 2148476	1-Aug-2017	683/281764-14	1-Aug-2018
HP	34401A	S/N US360980	1-Aug-2017	,205342	1-Aug-2018
Brüel & Kjær	2636	S/N 1323964	1-Aug-2017	822/275722-14	1-Aug-2018

Cal. Date: 26-Apr-2018

Tested by: James Zhu

Calibrated on WCCL system type 9700

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Rev. 7.0 Jan. 24, 2014 Doc. # 1038CL304METR

ISO/IEC 17025: 2005



1575 State Route 96, Victor NY 14564



### REPORT OF CALIBRATION

Metrosonics Acoustical Calibrator

Model No.: CL304

Serial No.: 3616

I. D. No.: XXXX

Company: Skelly & Loy, Inc.

Calibration results:

Before data: ...... After data: ... X...

Before & after data same: .......

Sound Pressure Level at 999.99 Hz and pressure of 1013 hPa (mbar)

was 102.05 dB re 20 µPa

Sound Pressure Level:

**Pass** 

Frequency:

Pass Pass

Distortion: Stability:

**Pass** 

All tested parameters:

**Pass** 

Laboratory Environment:

Ambient Temperature:

20.2

°C

Ambient Humidity:

32.6

% RH kPa

Ambient Pressure:

98.624

Calibration Date: 26-Apr-2018

Calibration Due: 26-Apr-2019

Report Number: Control Number: 28756 -5 28756

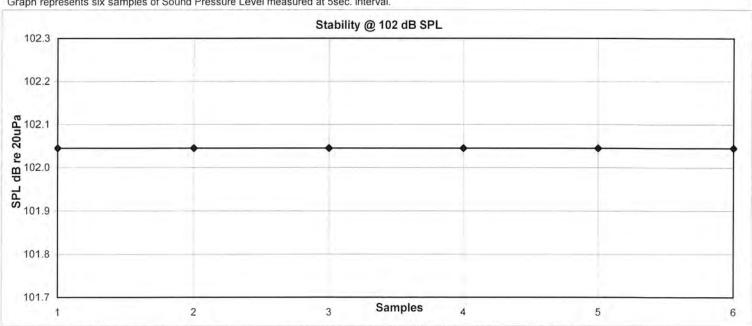
The above listed instrument meets or exceeds the tested manufacturer's specifications.

This Calibration is traceable through NIST test numbers:

822/275722-14

The expanded uncertainty of calibration: 0.11 dB at 95% confidence level with a coverage factor of k=2.

Graph represents six samples of Sound Pressure Level measured at 5sec. interval.



The above listed instrument was checked using calibration procedure documented in West Caldwell

Calibration Laboratories Inc. procedure:

Rev. 7.0 Jan. 24, 2014 Doc. # 1038 CL304METR

Calibration was performed by West Caldwell Calibration Laboratories Inc. under Operating Procedures

intended to implement the requirements of ISO10012-1, IEC Guide 25, ANSI/NCSL Z540-1, (MIL-STD-45662A) and ISO 9001:2008, ISO 17025

Cal. Date: 26-Apr-2018

Measurements performed by: ......

Calibrated on WCCL system type 9700

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James Zhu Rev. 7.0 Jan. 24, 2014 Doc. # 1038CL304METR

1575 State Route 96, Victor NY 14564 Tel. (585) 586-3900 FAX (585) 586-4327

### Calibration Data Record

for

Metrosonics Acoustical Calibrator Company: Skelly & Loy, Inc.

stical Calibrator Model No.: CL304

Serial No.: 3616

All tested parameters: Pass

Measured Sound Pressure Level (Six samples measured at 5 sec. interval)

102.05 dB re 20 µPa Sample 1 2 102.05 3 102.05 4 102.05 5 102.05 6 102.05 Average 102.05 Spec. 102 dB ± 0.3 dB

Frequency measured (Three samples at 30 sec. Interval)

Sample 1 999.96 Hz
2 1000.00
3 1000.00
Average 999.99 Spec. 1000 Hz ± 2.0%

Distortion measured -42.7 dB Spec. ≤-34 dB

nstruments used for ca	alibration:		Date of Cal.	Traceability No.	Re-cal. Due Date
Brüel & Kjær	4231	S/N 2308998	1-Aug-2017	822/275722-14	1-Aug-2018
Brüel & Kjær	4134	S/N 854464	1-Aug-2017	822/275722-14	1-Aug-2018
Brüel & Kjær	2669	S/N 2148476	1-Aug-2017	683/281764-14	1-Aug-2018
HP	34401A	S/N US360980	1-Aug-2017	,205342	1-Aug-2018
Brüel & Kjær	2636	S/N 1323964	1-Aug-2017	822/275722-14	1-Aug-2018

Cal. Date: 26-Apr-2018

Tested by: James Zhu

Calibrated on WCCL system type 9700

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Rev. 7.0 Jan. 24, 2014 Doc. # 1038CL304METR

# **Certificate of Calibration**

for

PERMISSIBLE SOUND LEVEL METER

Manufactured by: METROSONICS

Model No: db3080 Serial No: 5093 Calibration Recall No: 28756

Submitted By:

Customer: EVAN R. ZEIDERS

Company: SKELLY & LOY, INC.

Address: 449 EISENHOWER BLVD., STE. 300 HARRISBURG PA 17111

The subject instrument was calibrated to the indicated specification using standards traceable to the National Institute of Standards and Technology or to accepted values of natural physical constants. This document certifies that the instrument met the following specification upon its return to the

West Caldwell Calibration Laboratories Procedure No. db3080 METR

Upon receipt for Calibration, the instrument was found to be:

Within (X)

tolerance of the indicated specification. See attached Report of Calibration.
The information supplied relates to the calibrated item listed above.
West Caldwell Calibration Laboratories' calibration control system meets the requirements, ISO 10012-1 MIL-STD-45662A, ANSI/NCSL Z540-1, IEC Guide 25, ISO 9001:2008 and ISO 17025.

Note: With this Certificate, Report of Calibration is included.

Approved by:

FC

Calibration Date: 26

26-Apr-18

Felix Christopher (QA Mgr.)

Certificate No:

submitter.

28756 - 4

QA Doc. #1051 Rev. 2.0 10/1/01

Certificate Page 1 of 1

ISO/IEC 17025:2005

West Caldwell
Calibration
Laboratories, Inc.

1575 State Route 96, Victor, NY 14564, U.S.A.

ACCREDITED
Calibration Lab. Cert. # 1533.01

1575 State Route 96, Victor NY 14564 Tel. (585) 586-3900 FAX (585) 586-4327

## Calibration Data Record

Manufacturer: Metrosonics

Model No.: db-3080

Submitted by,

Permissible Sound Level Meter

S/N: 5093

Company: Skelly & Loy, Inc.

Test	Function	Tole	rance		Measured values			
	1.41.6.11.2	Min	Max		Before	Out	After	Out
0.	SPL Reading with 102.0dB SPL	101.4	102.6		102.0		102.0	
1.	Level Accuracy	93.4	94.6	94dB	94.0	li li	94.0	
,	Level Modulady	103.4	104.6	104dB	104.0		104.0	
		113.4	114.6	114dB	113.9		113.9	
,2.	Frequency Response	88.0	97.8	8kHz	93.2		93.2	
,~.	A Weighting	92.1	97.9	4kHz	97.5		97.5	
	/ Trongitting	93.3	97.1	2kHz	94.8	1 1	94.8	
		92.6	95.4	1kHz	93.9		93.9	
		89.4	92.2	500Hz	90.9	-	90.9	
		84.0	86.8	250Hz	85.5		85.5	
		76.5	79.3	125Hz	78.3		78.3	
		65.9	69.7	63Hz	69.2		69.2	***
		51.8	57.5	31.5Hz	57.2		57.2	
	C Weighting	86.1	95.9	8kHz	88.8		88.8	
		90.3	96.1	4kHz	95.8		95.8	
		91.9	95.7	2kHz	93.7		93.7	
		92.6	95.4	1kHz	94.0		94.0	
		92.6	95.4	500Hz	94.3		94.3	
		92.6	95.4	250Hz	94.4		94.4	
		92.4	95.2	125Hz	94.4		94.4	
		91.3	95.1	63Hz	93.9		93.9	
		88.2	93.9	31.5Hz	91.3		91.3	
3		412.1			Sea S			
	SLM	113.4	114.6		114.0		114.0	
	L avg. / Leq	113.4	114.6		114.0		114.0	
	L max.	113.4	114.6		114.0		114.0	
	L pk	116.1	117.9		117.7		117.7	-
	Dose %	2.432.			2.22		4.22.	
	0.18% @ 94 dB 1kHz	0.14%	0.22%		0.19%		0.19%	
	0.73% @ 104 dB 1kHz	0.58%	0.88%		0.76%		0.76%	***
	2.90% @ 114 dB 1kHz	2.32%	3.48%		3.02%		3.02%	
1	Inherent noise level				60.4		60.4	

### DB3080METR\_5093\_Apr-26-2018

in the control of the	evel with a coverage factor of k=		
	Test Instrumentation	DUT	Total DUT
Parameter	Uncertainty	Uncertainty	Uncertainty
Reading with mic. @ 1 kHz:	0.11	0.1	0.15
Meter linearity:	0.17	0.1	0.20
Attenuator accuracy:	0.17	0.1	0.20
Freq. Response: 63 Hz to 8 kHz	0.10	0.1	0.14
Inherent noise level:	0.024	0.1	0.10
Functions:	0.11	0.1	0.15
Sensitivity:	0.11	0.1	0.15
Dose:	0.30	0.1	0.32

Calibration Date: 26-Apr-2018

Measurements performed by:

James Zhu



1575 State Route 96, Victor NY 14564

ISO/IEC 17025: 2005



### REPORT OF CALIBRATION

Metrosonics Permissible Sound Level Meter

Model No.: db3080

Serial No.: 51

Company: Skelly & Loy, Inc.

I. D. No.: XXXX

Calibration results:

Before data: ...... After data: ......

Laboratory Environment:

20.2 °C

All tested parameters: Pass

Before & after data same: ... X...

Ambient Temperature: Ambient Humidity:

% RH

Ambient Pressure:

32.6 kPa

98.624

Calibration Date: 26-Apr-2018

Calibration Due: 26-Apr-2019 Report Number:

28756 -4

Control Number:

28756

The above listed instrument meets or exceeds the tested manufacturer's specifications.

For details see "Calibration Data Record"

This Calibration is traceable through NIST test numbers listed below.

The absolute uncertainty of calibration: See last page. Unless otherwise noted, the reported values are both "as found" and "as left" data.

The above listed instrument was checked using calibration procedure documented in West Caldwell Rev. 7.0 Jan. 24, 2014 Doc. # 1038 DB3080METR Calibration Laboratories Inc. procedure:

Calibration was performed by West Caldwell Calibration Laboratories Inc. under Operating Procedures intended to implement the requirements of ISO10012-1, IEC Guide 25, ANSI/NCSL Z540-1, (MIL-STD-45662A) and ISO 9001:2008, ISO 17025

NIST Traceable Ins	struments:		Date of Cal.	Traceability No.	Re-cal. Due Date
Brüel & Kjær	4226	S/N 2272364	1-Aug-2017	822/275722-15	1-Aug-2018

Cal. Date: 26-Apr-2018

Measurements performed by: ......

Calibrated on WCCL system type 9700

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James Zhu Rev. 7.0 Jan. 24, 2014 Doc. # 1038 DB3080METR

# **Certificate of Calibration**

for

PERMISSIBLE SOUND LEVEL METER

Manufactured by: ME

METROSONICS

Model No:

db3080

Serial No: Calibration Recall No: 4618 28756

Submitted By:

Customer:

**EVAN R. ZEIDERS** 

Company:

SKELLY & LOY, INC.

Address:

449 EISENHOWER BLVD., STE. 300

HARRISBURG

PA 17111

The subject instrument was calibrated to the indicated specification using standards traceable to the National Institute of Standards and Technology or to accepted values of natural physical constants. This document certifies that the instrument met the following specification upon its return to the submitter.

West Caldwell Calibration Laboratories Procedure No.

db3080

METR

Upon receipt for Calibration, the instrument was found to be:

Within (X)

tolerance of the indicated specification. See attached Report of Calibration.

The information supplied relates to the calibrated item listed above.

West Caldwell Calibration Laboratories' calibration control system meets the requirements, ISO 10012-1 MIL-STD-45662A, ANSI/NCSL Z540-1, IEC Guide 25, ISO 9001:2008 and ISO 17025.

Note: With this Certificate, Report of Calibration is included.

Approved by:



Calibration Date:

26-Apr-18

Felix Christopher (QA Mgr.)

Certificate No:

28756 -3

QA Doc. #1051 Rev. 2.0 10/1/01

Certificate Page 1 of 1

ISO/IEC 17025:2005

West Caldwell Calibration

uncompromised calibration Laboratories, Inc.

1575 State Route 96, Victor, NY 14564, U.S.A

ACCREDITED

Calibration Lab. Cert. # 1533.01

1575 State Route 96, Victor NY 14564 Tel. (585) 586-3900 FAX (585) 586-4327

## Calibration Data Record

for

Manufacturer: Metrosonics

Model No.: db-3080

Permissible Sound Level Meter Submitted by,

Company: Skelly & Loy, Inc.

S/N: 4618

Test	Function	Tole	rance		Measured values				
1000		Min	Max		Before	Out	After	Out	
,0.	SPL Reading with 102.0dB SPL	101.4	102.6		102.1		102.1		
,1.	Level Accuracy	93.4	94.6	94dB	94.1		94.1		
,	20101710001100	103.4	104.6	104dB	104.3		104.3		
		113.4	114.6	114dB	114.1		114.1		
,2.	Frequency Response	88.0	97.8	8kHz	92.5		92.5		
	A Weighting	92.1	97.9	4kHz	96.8	1	96.8		
	7, Trongittung	93.3	97.1	2kHz	94.5		94.5		
		92.6	95.4	1kHz	94.1		94.1		
		89.4	92.2	500Hz	91.4		91.4		
		84.0	86.8	250Hz	86.2	1 -	86.2		
		76.5	79.3	125Hz	78.9		78.9		
		65.9	69.7	63Hz	69.1		69.1		
		51.8	57.5	31.5Hz	56.1		56.1		
	C Weighting	86.1	95.9	8kHz	90.6		90.6		
	3 3	90.3	96.1	4kHz	95.0	1 1	95.0		
		91.9	95.7	2kHz	93.1		93.1		
		92.6	95.4	1kHz	94.1		94.1		
		92.6	95.4	500Hz	94.7		94.7		
		92.6	95.4	250Hz	94.7		94.7		
		92.4	95.2	125Hz	94.7		94.7		
		91.3	95.1	63Hz	93.9		93.9		
		88.2	93.9	31.5Hz	91.5		91.5		
3		1.00							
	SLM	113.4	114.6		113.9		113.9		
	L avg. / Leq	113.4	114.6		113.9		113.9		
	L max.	113.4	114.6	history	114.1		114.1		
	L pk	116.1	117.9	J. Constant	117.8		117.8		
	Dose %								
	0.18% @ 94 dB 1kHz	0.14%	0.22%		0.18%		0.18%		
	0.73% @ 104 dB 1kHz	0.58%	0.88%		0.78%		0.78%		
	2.90% @ 114 dB 1kHz	2.32%	3.48%		2.95%		2.95%		
4	Inherent noise level				60.1		60.1		

### DB3080METR\_4618\_Apr-26-2018

expanded uncertainty of calibration at 95% confidence I			
	Test Instrumentation	DUT	Total DUT
Parameter	Uncertainty	Uncertainty	Uncertainty
Reading with mic. @ 1 kHz:	0.11	0.1	0.15
Meter linearity:	0.17	0.1	0.20
Attenuator accuracy:	0.17	0.1	0.20
Freq. Response: 63 Hz to 8 kHz	0.10	0.1	0.14
Inherent noise level:	0.024	0.1	0.10
Functions:	0.11	0.1	0.15
Sensitivity:	0.11	0.1	0.15
Dose:	0.30	0.1	0.32

Calibration Date: 26-Apr-2018

Measurements performed by:

James Zhu



1575 State Route 96, Victor NY 14564

ISO/IEC 17025: 2005



### REPORT OF CALIBRATION

for

Metrosonics Permissible Sound Level Meter

Model No.: db3080 Company: Skelly & Loy, Inc. Serial No.: 4618

I. D. No.: XXXX

Calibration results:

Before data: ...... After data: .......

Before & after data same: ...X... Laboratory Environment;

Ambient Temperature: 20.2 °C

All tested parameters: Pass

Ambient Humidity: 32.6 % RH
Ambient Pressure: 98.624 kPa

For details see "Calibration Data Record"

Calibration Date: 26-Apr-2018

Calibration Due: 26-Apr-2019
Report Number: 28756 -3
Control Number: 28756

The above listed instrument meets or exceeds the tested manufacturer's specifications.

This Calibration is traceable through NIST test numbers listed below.

The absolute uncertainty of calibration: See last page, Unless otherwise noted, the reported values are both "as found" and "as left" data.

The above listed instrument was checked using calibration procedure documented in West Caldwell

Calibration Laboratories Inc. procedure:

Rev. 7.0 Jan. 24, 2014 Doc. # 1038 DB3080METR

Calibration was performed by West Caldwell Calibration Laboratories Inc. under Operating Procedures

intended to implement the requirements of ISO10012-1, IEC Guide 25, ANSI/NCSL Z540-1, (MIL-STD-45662A) and ISO 9001:2008, ISO 17025

 NIST Traceable Instruments:
 Date of Cal.
 Traceability No.
 Re-cal. Due Date

 Brüel & Kjær
 4226
 S/N 2272364
 1-Aug-2017
 822/275722-15
 1-Aug-2018

Cal. Date: 26-Apr-2018

Measurements performed by: .....

Calibrated on WCCL system type 9700

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James Zhu

Rev. 7.0 Jan. 24, 2014 Doc. # 1038 DB3080METR

# **Certificate of Calibration**

for

PERMISSIBLE SOUND LEVEL METER

Manufactured by:

Calibration Recall No:

METROSONICS

Model No:

db3080

Serial No:

3897 28756

Submitted By:

Customer:

EVAN R. ZEIDERS

Company:

SKELLY & LOY, INC.

Address:

449 EISENHOWER BLVD., STE. 300

HARRISBURG

PA 17111

The subject instrument was calibrated to the indicated specification using standards traceable to the National Institute of Standards and Technology or to accepted values of natural physical constants. This document certifies that the instrument met the following specification upon its return to the submitter.

West Caldwell Calibration Laboratories Procedure No.

db3080

METR

Upon receipt for Calibration, the instrument was found to be:

Within (X)

tolerance of the indicated specification. See attached Report of Calibration.

The information supplied relates to the calibrated item listed above.

West Caldwell Calibration Laboratories' calibration control system meets the requirements, ISO 10012-1 MIL-STD-45662A, ANSI/NCSL Z540-1, IEC Guide 25, ISO 9001:2008 and ISO 17025.

Note: With this Certificate, Report of Calibration is included.

Approved by:



Calibration Date:

26-Apr-18

Felix Christopher (QA Mgr.)

Certificate No:

28756 - 2

QA Doc. #1051 Rev. 2.0 10/1/01

Certificate Page 1 of 1

ISO/IEC 17025:2005

West Caldwell Calibration Laboratories, Inc.

uncompromised calibration Laboratol 1575 State Route 96. Victor, NY 14564, U.S.A.

Calibration Lab. Cert. # 1533.01

1575 State Route 96, Victor NY 14564 Tel. (585) 586-3900 FAX (585) 586-4327

# Calibration Data Record

for

Manufacturer: Metrosonics

Model No.: db-3080

Company: Skelly & Loy, Inc.

S/N: 3897

Permissible Sound Level Meter Submitted by,

Test	Function	Tole	rance		Measured values			
		Min	Max		Before	Out	After	Out
0	CDI Dooding with 102 0dB CDI	101.4	102.6		102.0		102.0	
0.	SPL Reading with 102.0dB SPL	101.4	102.0	-	102.0	-	102.0	
1.	Level Accuracy	93.4	94.6	94dB	94.1	1 1	94.1	
		103.4	104.6	104dB	104.0		104.0	
		113.4	114.6	114dB	114.1		114.1	
			- 12.2					
2.	Frequency Response	88.0	97.8	8kHz	94.0		94.0	
, 2.	A Weighting	92.1	97.9	4kHz	97.8	-	97.8	
	A Weighting	93.3	97.1	2kHz	95.6	-	95.6	
		92.6	95.4	1kHz	94.2		94.2	
		89.4	92.2	500Hz	91.2	-	91.2	
		84.0	86.8	250Hz	85.6		85.6	
		76.5	79.3	125Hz	77.7		77.7	
		65.9	69.7	63Hz	68.0		68.0	-
				***************************************				-
		51.8	57.5	31.5Hz	55.5	-	55.5	
	C Weighting	86.1	95.9	8kHz	92.0		92.0	
		90.3	96.1	4kHz	92.8		92.8	
		91.9	95.7	2kHz	94.0		94.0	
		92.6	95.4	1kHz	94.0		94.0	
		92.6	95.4	500Hz	94.1		94.1	
		92.6	95.4	250Hz	94.3		94.3	
		92.4	95.2	125Hz	94.0		94.0	
		91.3	95.1	63Hz	93.2		93.2	
		88.2	93.9	31.5Hz	90.4		90.4	
3								-
•	SLM	113.4	114.6		114.0		114.0	
	L avg. / Leq	113.4	114.6		114.0	1	114.0	
	L max.	113.4	114.6		114.0		114.0	
	L pk	116.1	117.9		116.6		116.6	
	Dose %							
		0.14%	0.22%		0.19%		0.19%	
	0.18% @ 94 dB 1kHz	0.14%	0.22%		0.19%	-	0.19%	-
	0.73% @ 104 dB 1kHz 2.90% @ 114 dB 1kHz	2.32%	3.48%		3.14%	-		-
	2.90% @ 114 dB 1KHZ	2.32%	3.40%		3.14%	-	3.14%	-
1	Inherent noise level				59.4		59.4	

#### DB3080METR\_3897\_Apr-26-2018

expanded uncertainty of calibration at 95% confidence I	ever with a coverage factor of K-	2.	
Parameter	Test Instrumentation Uncertainty	DUT Uncertainty	Total DUT Uncertainty
Reading with mic. @ 1 kHz:	0.11	0.1	0.15
Meter linearity:	0.17	0.1	0.20
Attenuator accuracy:	0.17	0.1	0.20
Freq. Response: 63 Hz to 8 kHz	0.10	0.1	0.14
Inherent noise level:	0.024	0.1	0.10
Functions:	0.11	0.1	0.15
Sensitivity:	0.11	0.1	0.15
Dose:	0.30	0.1	0.32

Calibration Date: 26-Apr-2018

Measurements performed by:

James Zhu



1575 State Route 96, Victor NY 14564

ISO/IEC 17025: 2005



°C

### REPORT OF CALIBRATION

for

Metrosonics Permissible Sound Level Meter

Model No.: db3080 Company: Skelly & Loy, Inc. Serial No.: 3897

I. D. No.: XXXX

Calibration results:

Before data: ...... After data: .......

Before & after data same: ...X... Laboratory Environment:

Ambient Temperature: 20.2

All tested parameters: Pass

Ambient Humidity: 32.6 % RH

Ambient Pressure: 98.624 kPa

For details see "Calibration Data Record"

Ambient Pressure: 98.624 kPa

Calibration Date: 26-Apr-2018

Calibration Due: 26-Apr-2019
Report Number: 28756 -2

Control Number: 28756

The above listed instrument meets or exceeds the tested manufacturer's specifications.

This Calibration is traceable through NIST test numbers listed below.

The absolute uncertainty of calibration: See last page. Unless otherwise noted, the reported values are both "as found" and "as left" data.

The above listed instrument was checked using calibration procedure documented in West Caldwell

Calibration Laboratories Inc. procedure:

Rev. 7.0 Jan. 24, 2014 Doc. # 1038 DB3080METR

Calibration was performed by West Caldwell Calibration Laboratories Inc. under Operating Procedures intended to implement the requirements of ISO10012-1, IEC Guide 25, ANSI/NCSL Z540-1, (MIL-STD-45662A) and ISO 9001:2008, ISO 17025

NIST Traceable Ins	struments:		Date of Cal.	Traceability No.	Re-cal. Due Date
Brüel & Kjær	4226	S/N 2272364	1-Aug-2017	822/275722-15	1-Aug-2018

Cal. Date: 26-Apr-2018

Measurements performed by: .....

Calibrated on WCCL system type 9700

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James Zhu
Rév. 7.0 Jan. 24/2014 Doc. # 1038 DB3080METR

# Certificate of Calibration

PERMISSIBLE SOUND LEVEL METER

Manufactured by:

METROSONICS

Model No:

db3080

Serial No:

3895

Calibration Recall No:

28756

Submitted By:

Customer:

EVAN R. ZEIDERS

Company:

SKELLY & LOY, INC.

Address:

449 EISENHOWER BLVD., STE. 300

HARRISBURG

PA 17111

The subject instrument was calibrated to the indicated specification using standards traceable to the National Institute of Standards and Technology or to accepted values of natural physical constants. This document certifies that the instrument met the following specification upon its return to the submitter.

West Caldwell Calibration Laboratories Procedure No.

db3080

METR

Upon receipt for Calibration, the instrument was found to be:

(X) Within

tolerance of the indicated specification. See attached Report of Calibration. The information supplied relates to the calibrated item listed above. West Caldwell Calibration Laboratories' calibration control system meets the requirements, ISO 10012-1 MIL-STD-45662A, ANSI/NCSL Z540-1, IEC Guide 25, ISO 9001:2008 and ISO 17025.

Note: With this Certificate, Report of Calibration is included.

Approved by:



Calibration Date:

26-Apr-18

Felix Christopher (QA Mgr.)

Certificate No:

28756 - 1

West Caldwell Calibration

QA Doc. #1051 Rev. 2.0 10/1/01

Certificate Page 1 of 1

ISO/IEC 17025:2005



uncompromised calibration Laboratories, Inc. 1575 State Route 96, Victor, NY 14564, U.S.A.

Calibration Lab. Cert. # 1533.01

1575 State Route 96, Victor NY 14564 Tel. (585) 586-3900 FAX (585) 586-4327

# Calibration Data Record

for

Manufacturer: Metrosonics

Permissible Sound Level Meter Model No.: db-3080

S/N: 3895

Submitted by,

Company: Skelly & Loy, Inc.

Test	Function	Tole	rance			asured va	lues	× =
		Min	Max		Before	Out	After	Out
,0.	SPL Reading with 102.0dB SPL	101.4	102.6		102.0		102.0	
,1.	Level Accuracy	93.4	94.6	94dB	94.0		94.0	
		103.4	104.6	104dB	104.0		104.0	
		113.4	114.6	114dB	114.0		114.0	
,2.	Frequency Response	88.0	97.8	8kHz	93.6		93.6	
,	A Weighting	92.1	97.9	4kHz	94.9		94.9	-
	3,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1	93.3	97.1	2kHz	95.6		95.6	
		92.6	95.4	1kHz	94.0		94.0	
		89.4	92.2	500Hz	91.4		91.4	
		84.0	86.8	250Hz	85.3		85.3	
		76.5	79.3	125Hz	77.6		77.6	
		65.9	69.7	63Hz	67.6		67.6	
		51.8	57.5	31.5Hz	54.0		54.0	
	C Weighting	86.1	95.9	8kHz	92.0	1 1	92.0	
		90.3	96.1	4kHz	93.2		93.2	-
		91.9	95.7	2kHz	94.4		94.4	
		92.6	95.4	1kHz	94.0	1	94.0	
		92.6	95.4	500Hz	94.0		94.0	
		92.6	95.4	250Hz	94.0		94.0	
		92.4	95.2	125Hz	94.0		94.0	
		91.3	95.1	63Hz	93.1		93.1	
		88.2	93.9	31.5Hz	89.6	-	89.6	
,3	7.3	1.3a.0	84.0		W. S			
	SLM	113.4	114.6		114.0		114.0	
	L avg. / Leq	113.4	114.6		114.0		114.0	
	L max.	113.4	114.6		114.2		114.2	
	L pk	116.1	117.9	-	116.8	-	116.8	
	Dose %	1,7521	2.3121		12.02.0		12.5	
	0.18% @ 94 dB 1kHz	0.14%	0.22%		0.17%		0.17%	
	0.73% @ 104 dB 1kHz	0.58%	0.88%		0.78%		0.78%	
	2.90% @ 114 dB 1kHz	2.32%	3.48%		2.93%	-	2.93%	
4	Inherent noise level				62.4		62.4	

#### DB3080METR\_3895\_Apr-26-2018

	Test Instrumentation	DUT	Total DUT
Parameter	Uncertainty	Uncertainty	Uncertainty
Reading with mic. @ 1 kHz:	0.11	0.1	0.15
Meter linearity:	0.17	0.1	0.20
Attenuator accuracy:	0.17	0.1	0.20
Freq. Response: 63 Hz to 8 kHz	0.10	0.1	0.14
Inherent noise level:	0.024	0.1	0.10
Functions:	0.11	0.1	0.15
Sensitivity:	0.11	0.1	0.15
Dose:	0.30	0.1	0.32

Calibration Date: 26-Apr-2018

Measurements performed by:

James Zhu

Page 2 of 2



1575 State Route 96, Victor NY 14564

ISO/IEC 17025: 2005



#### REPORT OF CALIBRATION

for

Metrosonics Permissible Sound Level Meter

Model No.: db3080

Company: Skelly & Loy, Inc.

Serial No.: 3895

I. D. No.: XXXX

Calibration results:

Before data: ...... After data: .......

Before & after data same: ...X...

All tested parameters: Pass

Laboratory Environment:

Ambient Temperature:

Ambient Pressure:

20.2 °C

Ambient Humidity:

32.6 98.624 % RH kPa

For details see "Calibration Data Record"

Calibration Date: 26-Apr-2018

Calibration Due: 26-Apr-2019
Report Number: 28756 -1

Control Number: 28756

The above listed instrument meets or exceeds the tested manufacturer's specifications.

This Calibration is traceable through NIST test numbers listed below.

The absolute uncertainty of calibration: See last page. Unless otherwise noted, the reported values are both "as found" and "as left" data.

The above listed instrument was checked using calibration procedure documented in West Caldwell

Calibration Laboratories Inc. procedure:

Rev. 7.0 Jan. 24, 2014 Doc. # 1038 DB3080METR

Calibration was performed by West Caldwell Calibration Laboratories Inc. under Operating Procedures

intended to implement the requirements of ISO10012-1, IEC Guide 25, ANSI/NCSL Z540-1, (MIL-STD-45662A) and ISO 9001:2008, ISO 17025

 NIST Traceable Instruments:
 Date of Cal.
 Traceability No.
 Re-cal. Due Date

 Brüel & Kjær
 4226
 S/N 2272364
 1-Aug-2017
 822/275722-15
 1-Aug-2018

Cal. Date: 26-Apr-2018

Measurements performed by: ......

Calibrated on WCCL system type 9700

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James Zhu

Rev. 7.0 Jan. 24, 2014 Doc. # 1038 DB3080METR



## **Supplied Accessories**

< 1 / 1 >

Model

NC-74

**Product Name** 

Sound Calibrator

Ensure all the items below are in the package. If there is a missing part, please contact your supplier.

Type	Description	Quantity	Note
NC-74	Main unit	1	#35836431
	Soft case	1	
	Batteries IEC LR6 (size AA)	2	
NC-74-002	1/2-inch microphone adapter	1	mounted on main unit
······································	Instruction manual	1	
···	Inspection certificate	1	This sheet
	Document for China RoHS	1	only to China
	ANAIRO TT TT		
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· ····· · · · · · · · · · · · · · · ·			
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## **Inspection Certificate**

**INSPECTOR** 

M. pidapa

We hereby certify that this product has been tested and calibrated at our factory according to RION specifications and that the product satisfies all relevant requirements.

RION CO., LTD. 3-20-41 Higashimotomachi, Kokubunji, Tokyo 185-8533, Japan

Sound and Vibration Measuring Instrument Section Product Information and software downloads can be found on our web-site:

http://svmeas.rion.co.jp/.

Please check it out.

NºC02040201



ISO 17025: 2005, ANSI/NCSL Z540:1994 Part 1 ACCREDITED by NVLAP (an ILAC MRA signatory)



NVLAP Lab Code: 200625-0

## Calibration Certificate No.34210

instrument:

Sound Level Meter

Model: Manufacturer: **NL42** Rion

Serial number: Tested with:

01122580

Microphone UC52 s/n 144597

Preamplifier NH24 s/n 22621

Type (class):

Customer:

McCormick Taylor, Inc.

Tel/Fax:

215-592-4200 ext.1313 /

Date Calibrated:7/7/2015 Cal Due:

Status: Received Sent In tolerance: Х

Out of tolerance: See comments:

Contains non-accredited tests: Yes X No

Calibration service: \_\_\_ Basic X Standard

Address:

5511 Capital Center Drive, Suite

560 Raleigh, NC 27606

#### Tested in accordance with the following procedures and standards:

Calibration of Sound Level Meters, Scantek Inc., Rev. 6/22/2012 SLM & Dosimeters - Acoustical Tests, Scantek Inc., Rev. 7/6/2011

#### Instrumentation used for calibration: Nor-1504 Norsonic Test System:

Instrument - Manufacturer	Description	5/N	Cal. Date	Traceability evidence Cal. Lab / Accreditation	Cal. Due
483B-Norsonic	SME Cal Unit	31052	Oct 7, 2014	Scantek, Inc./ NVLAP	Oct 7, 2015
DS-360-SRS	Function Generator	33584	Sep 30, 2013	ACR Env./ A2LA	Sep 30, 2015
34401A-Agilent Technologies	Digital Voltmeter	US36120731	Oct 1, 2014	ACR Env. / A2LA	Oct 1, 2015
HM30-Thommen	Meteo Station	1040170/39633	Oct 3, 2014	ACR Env./ A2LA	Oct 3, 2015
PC Program 1019 Norsonic	Calibration software	v.6.1T	Validated Nov 2014	Scantek, Inc.	-
1251-Norsonic	Calibrator	30878	Nov 10, 2014	Scantek, Inc./ NVLAP	Nov 10, 2015
4225-Brüel&Kjær	Multifunction calibrator	2305103	Jul 28, 2014	Scantek, Inc./ NVLAP	Jul 28, 2015

Instrumentation and test results are traceable to SI (International System of Units) through standards maintained by NIST (USA) and NPL (UK).

#### Environmental conditions:

Temperature (°C)	Barometric pressure (kPa)	Relative Humidity (%)
24.2	100.25	49.1

Calibrated by:	♪ Lydon Dawkins ٨	Authorized signatory:	Valentin Buzduga
Signature	Kerton ) aucheur	Signature	12
Date	7/7/2015	. Date	7/07/2015

Calibration Certificates or Test Reports shall not be reproduced, except in full, without written approval of the laboratory. This Calibration Certificate or Test Reports shall not be used to claim product certification, approval or endorsement by NVŁAP, NIST, or any agency of the federal government.

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Page 1 of 2



ISO 17025: 2005, ANSI/NCSL Z540:1994 Part 1 ACCREDITED by NVLAP (an ILAC MRA signatory)



NVLAP Lab Code: 200625-0

### Calibration Certificate No.34205

Instrument:

Sound Level Meter

Model:

NL42

Manufacturer:

Rion

Serial number: Tested with:

01222875\_017997

Microphone UC52 s/n 144499

Preamplifier NH24 s/n 22922

Type (class):

Customer:

**Mccormick Taylor** 

Tel/Fax:

717-540-6040 /

Date Calibrated:7/2/2015

Status:

Received X

Cal Due:

In tolerance: Out of tolerance:

See comments:

Contains non-accredited tests: Yes X No

Sent

Address:

Calibration service: \_\_ Basic X Standard 5 Capital Drive, Suite 400

Harrisburg, PA 17110

Tested in accordance with the following procedures and standards: Calibration of Sound Level Meters, Scantek Inc., Rev. 6/22/2012 SLM & Dosimeters - Acoustical Tests, Scantek Inc., Rev. 7/6/2011

Instrumentation used for calibration: Nor-1504 Norsonic Test System:

		n fai	Cal Data	Traceability evidence	Cal. Due	
Instrument - Manufacturer	Description	S/N	Cal. Date	Cal. Lab / Accreditation	cal, Due	
483B-Norsonic	SME Cal Unit	31052	Oct 7, 2014	Scantek, Inc./ NVLAP	Oct 7, 2015	
DS-360-SRS	Function Generator	33584	Sep 30, 2013	ACR Env./ A2LA	Sep 30, 2015	
34401A-Agilent Technologies	Digital Voltmeter	US36120731	Oct 1, 2014	ACR Env. / A2LA	Oct 1, 2015	
HM30-Thommen	Meteo Station	1040170/39633	Oct 3, 2014	ACR Env./ A2LA	Oct 3, 2015	
PC Program 1019 Norsonic	Calibration software	v.6.1T	Validated Nov 2014	Scantek, Inc.		
1251-Norsonic	Calibrator	30878	Nov 10, 2014	Scantek, Inc./ NVLAP	Nov 10, 2015	
4226-Brüel&Kjær	Multifunction calibrator	2305103	Jul 28, 2014	Scantek, Inc./ NVLAP	Jul 28, 2015	

Instrumentation and test results are traceable to SI (International System of Units) through standards maintained by NIST (USA) and NPL (UK).

#### **Environmental conditions:**

Temperature (°C)	Barometric pressure (kPa)	Relative Humidity (%)
23.1	99.78	69.1

Calibrated by:	Lydon Dawkins	Authorized signatory:	Valentin Buzatiga
Signature	Lendon Dambers	Signature	49
Date	7/2/2015	Date	7/02/2015

Calibration Certificates or Test Reports shall not be reproduced, except in full, without written approval of the laboratory. This Calibration Certificate or Test Reports shall not be used to claim product certification, approval or endorsement by NVLAP, NIST, or any agency of the federal government.

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Page 1 of 2



ISO 17025: 2005, ANSI/NCSL Z540:1994 Part 1 ACCREDITED by NVLAP (an ILAC MRA signatory)



NVLAP Lab Code: 200625-0

### Calibration Certificate No.34211

Instrument:

**Sound Level Meter** 

Model:

**NL42** 

Manufacturer:

Rion

Serial number:

01222874\_017995

Tested with:

Microphone UC52 s/n 144498

Preamplifier NH24 s/n 22921

Type (class):

Customer:

McCormick Taylor, Inc.

Tel/Fax:

215-592-4200 ext.1313 /

Date Calibrated:7/7/2015 Cal Due:

Status: Received

Х In tolerance:

Out of tolerance:

Address:

See comments: Contains non-accredited tests: Yes X No

Sent

X.

Calibration service: \_\_\_ Basic X Standard

5511 Capital Center Drive, Suite

560 Raleigh, NC 27606

Tested in accordance with the following procedures and standards:

Calibration of Sound Level Meters, Scantek Inc., Rev. 6/22/2012 SLM & Dosimeters - Acoustical Tests, Scantek Inc., Rev. 7/6/2011

#### Instrumentation used for calibration: Nor-1504 Norsonic Test System:

Instrument - Manufacturer	Description	S/N	Cal. Date	Traceability evidence Cal. Lab / Accreditation	Cal. Due
483B-Norsonic	SME Cal Unit	31052	Oct 7, 2014	Scantek, Inc./ NVLAP	Oct 7, 2015
DS-360-SRS	Function Generator	33584	Sep 30, 2013	ACR Env./ A2LA	Sep 30, 2015
34401A-Agilent Technologies	Digital Voltmeter	US36120731	Oct 1, 2014	ACR Env. / A2LA	Oct 1, 2015
HM30-Thommen	Meteo Station	1040170/39633	Oct 3, 2014	ACR Env./ A2LA	Oct 3, 2015
PC Program 1019 Norsonic	Calibration software	v.6.1T	Validated Nov 2014	Scantek, Inc.	
1251-Norsonic	Calibrator	30878	Nov 10, 2014	Scantek, Inc./ NVLAP	Nov 10, 2015
4226-Brüel&Kjær	Multifunction calibrator	2305103	Jul 28, 2014	Scantek, Inc./ NVLAP	Jul 28, 2015

Instrumentation and test results are traceable to SI (International System of Units) through standards maintained by NIST (USA) and NPL (UK).

#### **Environmental conditions:**

Temperature (°C)	Barometric pressure (kPa)	Relative Humidity (%)
25.0	100.26	44.5

Calibrated by:	Lydon Dawkins	Authorized signatory:	Valenti <del>n Buzdug</del> a
Signature	Ludon Davellero	Signature	12
Date	7/7/2015	Date	7/07/2015

Calibration Certificates or Test Reports shall not be reproduced, except in full, without written approval of the laboratory. This Calibration Certificate or Test Reports shall not be used to claim product certification, approval or endorsement by NVLAP, NIST, or any agency of the federal government.

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Page 1 of 2



## **Supplied Accessories**

< 1 / 1 >

Model

NL-42

**Product Name** 

Sound Level Meter, Class 2

Ensure all the items below are in the package.

If there is a missing part, please contact your supplier.

Type	Description	Quantity	Note
NL-42	Main unit	1	06345938
NL-42-025	Storage case	1	WC-52-150627
WS-10	Windscreen	1	
NL-42-033	Windscreen fall prevention rubber	1	attached to the main unit
VM-63-017	Hand strap	1	
LR6	Size AA alkaline batteries	4	
	CD-ROM (Instruction manual, Serial Interface manual, Technical notes, Program option manual)	1	
	Description for IEC 61672-1	1	
	SD memory card (512 MByte)	1	only when NX-42EX is pre-installed
	Inspection certificate	1	This sheet
	Document for China RoHS	1	only to China

## **Inspection Certificate**

INSPECTOR

M. pidapa

We hereby certify that this product has been tested and calibrated at our factory according to RION specifications and that the product satisfies all relevant requirements.

RION CO., LTD. 3-20-41 Higashimotomachi, Kokubunji, Tokyo 185-8533, Japan

Sound and Vibration Measuring Instrument Section Product information and software downloads can be found on our web-site:

http://svmeas.rion.co.jp/ Please check it out.

NºC11030302

				Rout	te 7 Wideni	ng Project
Site #	R1	Description :	11304 Water F	Pointe Circle, Res	ston, Virginia 2019	4
Done By: Meter:	JJW/KTT	2				
Monitoring I	Data: Date Start Time End Time Duration Leq.	11/17/15 9:35 AM 9:50 AM 15 MIN			Atmospheric Data Wind Speed (mph) 8 Temp. (F)	
Traffic Data  Weather Co  Site Data:	Roadway Direction Traffic Total: Cars MT HT Buses Motorcycles	Route 7  EB WB 260 228 252 202 7 18 1 8	0 0 elding Factor:	0 0	52  Humidity (%) 63  ent Type :	
	the photo abov	e are from noise		st structure and	A from noise	Notes:
meter to edge  McCormick Ta		the closeset trav	el lane measure	ed in feet.		
INICOULTILICK I	aviol. IIIC					

Done By: JJW/KTT					Rout	te 7 Wideni	ng Projec	:t		
Monitoring Data: Date 11/17/15 Date Start Time 9:36 AM End Time 9:36 AM End Time Duration 15 MiN Leq. 63.2	Site #	R2	Description :	11119 Loran R	oad, Great Falls,	, Virginia 22066				
Start Time 9.35 AM Wordspeed (mph) Duration 15 kM 8  Leq. 63.2 Traffic Data Roadway Route 7 Direction EB WB Traffic Total: 220 220	Done By: Meter:	JJW/KTT	1							
Poincetion  E8 WB  Direction  E8 WB  Traffic Total: 260 228 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Monitoring	Date Start Time End Time Duration	9:35 AM 9:50 AM 15 MIN			Data Wind Speed (mph) 8				
*Distances in the photo above are from noise meter to nearest structure and from noise meter to edge of pavement of the closeset travel lane measured in feet.	Weather Co	Roadway Direction Traffic Total: Cars MT HT Buses Motorcycles nditions	EB WB 260 228 252 202 7 18 1 8			Humidity (%) 63				
			ve are from noise 1			A from noise	Notes: T	ime:? Car enters		
			or the closeset trav	er iane measure	eu in ieet.					

				Rout	e 7 Wideni	ng Project				
Site #	R3	Description :	1155 Markell Co	ourt, Reston, Vir	ginia 20194					
Done By: Meter:	JJW/KTT →	9							think	
Monitoring	Data: Date Start Time End Time Duration Leq.	11/17/15 9:35 AM 9:50 AM 15 MIN			Atmospheric Data Wind Speed (mph) 8 Temp. (F)					
Traffic Data  Weather Co	Roadway Direction Traffic Total: Cars MT HT Buses Motorcycles	Route 7  EB WB 260 228 252 202 7 18 1 8	0 0	0 0 0	52  Humidity (%) 63  ent Type :					
		49 19			Leesbirg Pike	Notes:	Monitor	ing Notes		
	e of pavement o	ve are from noise in the closeset trav			I from noise					

			Rout	te 7 Wideni	ng Project
Site #	R4	Description: 10805 Pir	ney Pond Drive, Great	t Falls, Virginia 220	66
Done By: Meter:	JJW/KTT	3			
Monitoring	Data: Date Start Time End Time Duration Leq.	11/17/15 9:35 AM 9:50 AM 15 MIN		Atmospheric Data Wind Speed (mph) 8 Temp. (F)	
Traffic Dat	Roadway Direction Traffic Total: Cars MT HT Buses Motorcycles	Route 7  EB WB 260 228 0 0 252 202 7 18 1 8	0 0	52 Humidity (%) 63	
Site Data:	Site Surface (alp	oha): Shielding Fact	or:Paveme	ent Type :	
		ve are from noise meter to n		d from noise	Notes: 9:42 AM- Lawn mower engine made a loud popping noise. 9:46 AM- Landscaping company across the street mowing and weed wacking.
meter to eda	ge of pavement o	f the closeset travel lane me	asured in feet.		
McCormick <sup>1</sup>	Taylor, Inc				

				Rout	te 7 Wideni	ng Proje	ect			
Site #	R5	Description :	10411 Van Patt	tern Lane, Great	t Falls, Virginia 220	066				
Done By: Meter:	JJW/KTT	1					THE ACTION AND ADDRESS OF THE ACTION AND ADD			
Monitoring	Data: Date Start Time End Time Duration Leq.	11/17/15 10:40 AM 10:55 AM 15 MIN			Atmospheric Data Wind Speed (mph) 10 Temp. (F)					
Traffic Data  Weather Co	Roadway Direction Traffic Total: Cars MT HT Buses Motorcycles	Route 7  EB WB 357 257 329 239 14 14 14 4  ha): Shie	elding Factor :	0 0	56  Humidity (%) 59  ent Type :					
		Control of the Control	O BEET N	11200 138		i ———		Monito	ring Notes	
Leesbu Lee	1	RES			N	Notes:	Privacy Fence (	8ft)		
Leesburg P	ike,									
		ve are from noise i			d from noise					
meter to edg	ge of pavement o	f the closeset trav	el lane measure	ed in feet.						
McCormick 7	Taylor, Inc									

				Rout	e 7 Wideni	ng Proje	ect				
Site #	R6	Description :	9629 Locust Hil	Il Drive, Great Fa	alls, Virginia 22066						
Done By: Meter:	JJW/KTT	3								X	
Monitoring	Data: Date Start Time End Time Duration Leq.	11/17/15 10:40 AM 10:55 AM 15 MIN			Atmospheric Data Wind Speed (mph) 10 Temp. (F)						1 111
Traffic Data  Weather Co	Roadway Direction Traffic Total: Cars MT HT Buses Motorcycles	Route 7  EB   WB  357   257  329   239  14   14  14   4	0 0	0 0	56  Humidity (%) 59  ent Type :						
			0		71			Monitor	ing Notes		
		ve are from noise nof the closeset trav	neter to neares		I from noise	Notes:	Privacy Fence (8	oft)			
McCormick 7	Taylor, Inc										

				Rout	te 7 Wideni	ng Project
Site #	R7	Description :	1253 Dunn Mea	ndow Court, Vier	nna, Virginia 22182	2
Done By: Meter:	JJW/KTT →	2				
Monitoring	Data: Date Start Time End Time Duration Leq.	11/17/15 10:40 AM 10:55 AM 15 MIN			Atmospheric Data Wind Speed (mph) 10 Temp. (F)	
Traffic Data  Weather Co  Site Data:	Roadway Direction Traffic Total: Cars MT HT Buses Motorcycles	Route 7  EB WB  357 257  329 239  14 14  14 4	0 0 elding Factor:	0 0 Paveme	56  Humidity (%) 59  ent Type :	
				1		Monitoring Notes
					Î N	Notes:
		ve are from noise i If the closeset trav			l from noise	
	1					
McCormick T	avlor. Inc					

				Rout	te 7 Wideni	ng Project		
Site #	R8	Description :	1293 Colvin Fo	rest Drive, Vienr	na, Virginia 22182			
Done By: Meter:	JJW/KTT	9						1
Monitoring	Data: Date Start Time End Time Duration Leq.	11/17/15 10:40 AM 10:55 AM 15 MIN			Atmospheric Data Wind Speed (mph) 10 Temp. (F)			
Traffic Data	Roadway Direction Traffic Total: Cars MT HT Buses Motorcycles	Route 7  EB WB  357 257  329 239  14 14  14 4	0 0	0 0	56  Humidity (%) 59			
	Site Surface (alp	oha): Shie	elding Factor :	Paveme	ent Type :			
Coming ordered					Î N	Notes:	Monitoring Notes	
		ve are from noise r of the closeset trav			l from noise			
McCormick T	aylor, Inc							

				Rout	te 7 Wideni	ng Project		
Site #	R9	Description :	9393 Farmingd	ale Court, Great	Falls, Virginia 220	66		
Done By: Meter:	JJW/KTT	1						
Monitoring	Data: Date Start Time End Time Duration Leq.	11/17/15 11:40 AM 11:55 AM 15 MIN			Atmospheric Data Wind Speed (mph) 10 Temp. (F)			
Weather Co	Roadway Direction Traffic Total: Cars MT HT Buses Motorcycles	Route 7  EB WB 392 308 375 292 15 13 2 3	0 0	0 0	58  Humidity (%) 60  ent Type :			
7			8		ÎN	Notes:	Monitoring Note	es
		\$ <b>₹</b> €	Fami	node 6				
meter to edg	ge of pavement o	ve are from noise of the closeset trav			1 from noise			
McCormick 7	aylor, Inc							

				Rout	te 7 Widenii	ng Project			
Site #	R10	Description :	9356 Mildred C	ourt, Vienna, Vir	ginia 22182				
Done By: Meter:	JJW/KTT	9				S. S			
Monitoring	Data: Date Start Time End Time Duration Leq.	11/17/15 11:40 AM 11:55 AM 15 MIN			Atmospheric Data Wind Speed (mph) 10				
Traffic Data	Roadway Direction Traffic Total: Cars MT HT Buses Motorcycles	Route 7  EB WB 392 308 375 292 15 13 2 3	0 0	0 0	58  Humidity (%)  60				
Weather Co	onditions Site Surface (alp		elding Factor :		ent Type :				
	SE SE		•		N Less Harro Pite	Notes:	Monitorin	g Notes	
	RIO &				Oko .				
		ve are from noise in the closeset trav			d from noise				
McCormick T	aylor, Inc								

				Rout	te 7 Wideni	ning Project
Site #	R11	Description :	9026 Leesburg	Pike, Vienna, Vi	irginia 22182	
Done By: Meter:	JJW/KTT	3				
Monitoring I	Data: Date Start Time End Time Duration Leq.	11/17/15 11:40 AM 11:55 AM 15 MIN			Atmospheric Data Wind Speed (mph) 10 Temp. (F)	
Traffic Data	Roadway Direction Traffic Total: Cars MT HT Buses Motorcycles nditions	Route 7  EB WB  392 308  375 292  15 13  2 3	0 0	0 0	58  Humidity (%)  60	
Site Data:	Site Surface (alp	ha): Shi	elding Factor :	Paveme	ent Type :	
		ve are from noise of the closeset trav			I from noise	Notes:
meter to edge	e of pavement of	i the closeset trav	ei iane measure	eu in ieet.		
McCormick Ta	avlor. Inc					

				Rout	te 7 Wideni	ng Project			
Site #	R12	Description :	8850 Glenridg	e Court, Vienna,	Virginia 22182				
Done By: Meter:	JJW/KTT →	2						N PT	
Monitoring	Data: Date Start Time End Time Duration Leq.	11/17/15 11:40 AM 11:55 AM 15 MIN			Atmospheric Data Wind Speed (mph) 10 Temp. (F)				
Traffic Data  Weather Co  Site Data:	Roadway Direction Traffic Total: Cars MT HT Buses Motorcycles	Route 7  EB WB 392 308 375 292 15 13 2 3	0 0	0 0 Paveme	58  Humidity (%) 60  ent Type :				
*Distances in		R12  ve are from noise and the closeset trav	meter to neares		d from noise	Notes: Min	imal traffic on Leesburg	Pike.	
McCormick T									

Address	Start	Measur	emen	nt Time	Leg	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overa
R1	Time								-,									Leq 57.2
189	11/17/2015	9:35:06	004	00:10.0	54	64	58.1	51.3		57.2	55.6	52.3	51.5	51.5			251188.6	31.2
190	11/17/2015	9:35:16	_	00:10.0	57.9	67.9	61.7	53.6	Ĥ	61.5	61	57.7	54.1	53.9			616595.0	ł
190	11/17/2015		00d	00:10.0	53.1	63.1	54.9	52.2	-,-	54.5	53.9	52.5	52.3	52.3			204173.8	
192	11/17/2015	9:35:36	00d	00:10.0	56.4	66.4	58.5	53.9	-,-	57.7	57.5	56.2	54.2	54			436515.8	
193	11/17/2015	9:35:46	00d	00:10.0	57	67	60.1	54.6		59.8	59.7	56.5	54.7	54.7			501187.2	1
194	11/17/2015	9:35:56	00d	00:10.0	53.6	63.6	54.8	52.9		54.8	54.7	53.5	53	52.9			229086.8	1
195	11/17/2015	9:36:06	00d	00:10.0	54.4	64.4	54.9	53.1	-,-	54.9	54.8	54.5	53.2	53.2			275422.9	]
196	11/17/2015	9:36:16	00d	00:10.0	56	66	56.9	54.5		56.9	56.8	56.1	54.6	54.6			398107.2	
197	11/17/2015	9:36:26	00d	00:10.0	53.9	63.9	55.9	52.2		55.6	55.4	54.2	52.8	52.5			245470.9	
198	11/17/2015	9:36:36	00d	00:10.0	54	64	55.6	52.2		55.5	55.3	53.3	52.3	52.3			251188.6	
199	11/17/2015	9:36:46		00:10.0	64.1	74.1	68.1	55.5		67.8	67.5	58.6	55.8	55.6			2570395.8	
200	11/17/2015	9:36:56	00d	00:10.0	60.3	70.3	63.4	59.9		62.3	61.9	60.4	60	59.9			1071519.3	
201	11/17/2015	9:37:06	_	00:10.0	60.1	70.1	60.5	59.8		60.4	60.2	60	59.9	59.9			1023293.0	ŀ
202 203	11/17/2015 11/17/2015	9:37:16 9:37:26		00:10.0 00:10.0	59.6 59.1	69.6 69.1	60.8 59.7	58.2 58.3	-,-	60.8 59.6	60.7 59.6	59.9 59.2	58.3 58.4	58.3 58.4			912010.8 812830.5	
203	11/17/2015	9:37:36		00:10.0	56.9	66.9		56.4		58.2	57.7	56.9	56.6	56.5			489778.8	ł
205	11/17/2015	9:37:46		00:10.0		66.9		55	-,-	59.2	58.7	56.2	55.1	55.1			489778.8	1
206	11/17/2015	9:37:56		00:10.0		69.2		56.9	-,-	60.6	60.4	59.5	57.1	57			831763.8	
207	11/17/2015	9:38:06		00:10.0	55	65	56.9	53.9		56.7	56.4	55	54	54			316227.8	1
208	11/17/2015	9:38:16	00d	00:10.0	52.2	62.2	55.5	50.1		55.1	54.9	52.1	50.3	50.2			165958.7	1
209	11/17/2015	9:38:26	00d	00:10.0	50.6	60.6	51.4	50.1		51.2	50.9	50.4	50.2	50.2			114815.4	]
210	11/17/2015	9:38:36	00d	00:10.0	52.2	62.2	53.4	50.6	-,-	53.2	53.2	52.2	51	50.9			165958.7	
211	11/17/2015	9:38:46	00d	00:10.0	60.2	70.2	62.3	50.9	-,-	62.1	61.9	59.7	52.6	51.3			1047128.5	l
212	11/17/2015	9:38:56	_	00:10.0	60	70		57.2	-,-	62.1	62	60.6	57.7	57.6			1000000.0	
213	11/17/2015	9:39:06		00:10.0	57.5	67.5	59.1	56.2	-:-	59	58.7	57.4	56.3	56.3			562341.3	l
214	11/17/2015		00d	00:10.0		68		56.4	-,-	59.4	59.3	57.5	56.4	56.4			630957.3	
215	11/17/2015		_	00:10.0	60.6	70.6		59.2	-,-	62	61.9	60.2	59.5	59.5			1148153.6	
216 217	11/17/2015 11/17/2015	9:39:36 9:39:46	00d 00d	00:10.0 00:10.0	58.8 61.1	68.8 71.1	59.7 62.1	58.1 58.9	-,-	59.5 62.1	59.4 62	58.7 61.1	58.3 59.2	58.2 59.1			758577.6 1288249.6	
218	11/17/2015	9:39:56	00d	00:10.0	57.1	67.1	60.2	54.9		59.9	59.7	57.7	55.4	55.3			512861.4	
219	11/17/2015	9:40:06	_	00:10.0	55	65	56.1	53.8	-,-	56	55.9	54.8	54.1	54			316227.8	i
220	11/17/2015	9:40:16	_	00:10.0	54	64		53.7	-,-	54.4	54.3	53.9	53.7	53.7			251188.6	1
221	11/17/2015	9:40:26	00d	00:10.0	56.4	66.4	57.9	53.8		57.6	57.2	56.6	54.5	54			436515.8	1
222	11/17/2015	9:40:36	00d	00:10.0	56.2	66.2	57.4	55.1		57.3	57.2	56.6	55.2	55.2			416869.4	1
223	11/17/2015	9:40:46	00d	00:10.0	58.1	68.1	59.5	55.2		59.1	58.6	57.9	55.8	55.5			645654.2	
224	11/17/2015	9:40:56	00d	00:10.0	58.2	68.2	59.7	57.5		59.6	59.4	58	57.7	57.5			660693.4	
225	11/17/2015	9:41:06	00d	00:10.0	58.6	68.6	60.8	56.9		60.6	60.5	57.4	57	57			724436.0	
226	11/17/2015	9:41:16	00d	00:10.0	62.4	72.4	64.3	60.2		64.1	64	61.9	61.3	60.9			1737800.8	
227	11/17/2015	9:41:26		00:10.0	60.2	70.2	61.5	59.3		61.4	61.4	60	59.6	59.4			1047128.5	
228	11/17/2015	9:41:36		00:10.0	58.6	68.6		56.8		59.6	59.6	59.2	57.3	57.2			724436.0	
229 230	11/17/2015	9:41:46 9:41:56		00:10.0 00:10.0	55.6	65.6 64.1	56.8 55.5	55.1 52.8	-,-	56.4 55.4	56.3	55.5	55.3 53	55.2 52.9			363078.1 257039.6	ł
231	11/17/2015 11/17/2015	9:42:06		00:10.0		62.8		51.8		53.6	55.2 53.5	54.3 53	52	51.9			190546.1	ł
232	11/17/2015	9:42:16		00:10.0	52.1	62.1	53.1	51.0	-,-	53.0	52.9	52	51.2	51.2			162181.0	l
233	11/17/2015			00:10.0	54.6	64.6		52.1	-,-	55.4	55.3	54.3	54	53.3			288403.2	i
234	11/17/2015	9:42:36	00d	00:10.0	55.3	65.3	56.3	53.8	-,-	56.1	56	55.2	54	53.9			338844.2	1
235	11/17/2015	9:42:46	00d	00:10.0	57.3	67.3	57.7	56.3		57.6	57.6	57.3	56.9	56.9			537031.8	1
236	11/17/2015	9:42:56	00d	00:10.0	57.3	67.3	58.2	56.3		58	57.7	57.3	56.5	56.5			537031.8	1
237	11/17/2015	9:43:06	00d	00:10.0	58.3	68.3	59.5	57.3		59.5	59.3	58.3	57.6	57.4			676083.0	
238	11/17/2015	9:43:16		00:10.0		67.6	59	56.4		58.9	58.7	57.3	56.6	56.5			575439.9	
239	11/17/2015	9:43:26	_	00:10.0		65.7	57.9			57.7	57.2	56	54.7	54.6			371535.2	Į.
240	11/17/2015	9:43:36		00:10.0		63.7	54.9			54.9	54.8	53.5	52.8	52.7			234422.9	l
241	11/17/2015	9:43:46		00:10.0	50.9	60.9	52.5	50.4		52.3	52.1	50.8	50.5	50.4			123026.9	ł
242	11/17/2015 11/17/2015	9:43:56	_	00:10.0	52.8	62.8 64.1	53.6		7-	53.4	53.4	52.9	50.8	50.7			190546.1 257039.6	ł
243 244	11/17/2015	9:44:06 9:44:16		00:10.0 00:10.0	54.1 54.8	64.8	54.4 55.6	53.3 54.2	$\mathbb{H}$	54.4 55.5	54.4 55.4	54.2 54.6	53.5 54.3	53.4 54.2		<u> </u>	301995.2	ł
244	11/17/2015	9:44:16	_	00:10.0		67.4				57.7	55.4	54.6	56.4	54.2			549540.9	ł
245	11/17/2015	9:44:36	_	00:10.0		68.8			H	60.1	60	57.4	57.6	57.5			758577.6	l
247	11/17/2015	9:44:46		00:10.0		70				61.6	61.4	60.1	58.8	58.4			1000000.0	1
248	11/17/2015	9:44:56		00:10.0		66.8			-,-	57.8	57.7	57.1	56.1	55.8			478630.1	1
249	11/17/2015	9:45:06		00:10.0		65.2	55.5		-,-	55.5	55.5	55.2	55	55			331131.1	]
250	11/17/2015	9:45:16	00d	00:10.0	56.5	66.5	58	55	-,-	57.9	57.8	55.7	55.2	55.1			446683.6	1
251	11/17/2015	9:45:26	00d	00:10.0	55.6	65.6	56.9	55.1		56.4	56.2	55.7	55.3	55.2			363078.1	
252	11/17/2015	9:45:36	00d	00:10.0	54	64	55.2	52.9		55.1	55	53.9	53	52.9			251188.6	
253	11/17/2015	9:45:46	00d	00:10.0	53	63	54.7	50.9		54.6	54.6	53.1	51.1	51			199526.2	
254	11/17/2015	9:45:56		00:10.0		61.4		49.6		52.8	52.7	51.3	50.5	50			138038.4	Į.
255	11/17/2015	9:46:06		00:10.0		59.5		48.4		51.3	50.2	48.9	48.5	48.5		<u> </u>	89125.1	
256	11/17/2015	9:46:16		00:10.0		64.3		51		55	54.9	54.6	51.6	51.1			269153.5	l
257	11/17/2015	9:46:26		00:10.0		64.5				55.9	55.7	54.2	53.5	53.3			281838.3	l
258	11/17/2015	9:46:36		00:10.0		63.2	54.6			54.5	54.4	53.3	52.8	52.5			208929.6	ł
259	11/17/2015	9:46:46		00:10.0	54.9	64.9		51.4	-,-	56	56	55 54	51.6	51.5			309029.5	ł
260	11/17/2015	9:46:56		00:10.0	54 54.8	64.8		53.5 54	-,-	55.5 55.4	55.3 55.3	54 54.6	53.6 54.2	53.5 54.1			251188.6 301995.2	ł
261	11/17/2015	9:47:06		00:10.0														

A al al ma a a	Start	Manaum		4 Time a	Lon	15	LDAAV	LNAIN		1.014	LNID	LNI2	1.014	LAIF	0	Hadau	Investor Lon	Overall
Address	Time	Measur	emen	it Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Leg
R1																		57.2
263	11/17/2015	9:47:26	00d	00:10.0	52.9	62.9	53.4	52.4	-,-	53.4	53.4	52.8	52.5	52.4			194984.5	
264	11/17/2015	9:47:36	00d	00:10.0	54.4	64.4	55.9	53.1	-,-	55.8	55.4	54.2	53.2	53.2			275422.9	
265	11/17/2015	9:47:46	00d	00:10.0	56.3	66.3	57	55.3	-,-	56.9	56.9	56.4	55.5	55.4			426579.5	
266	11/17/2015	9:47:56	00d	00:10.0	59.1	69.1	60.5	55.5	-,-	60.5	60.3	59	55.6	55.6			812830.5	
267	11/17/2015	9:48:06	00d	00:10.0	58.2	68.2	60.2	57.1	-,-	60.2	60.1	58.2	57.3	57.2			660693.4	
268	11/17/2015	9:48:16	00d	00:10.0	58.6	68.6	60	57.5	-,-	59.9	59.6	58.1	57.7	57.6			724436.0	
269	11/17/2015	9:48:26	00d	00:10.0	60.4	70.4	61.4	58.7	-,-	61.2	61.2	60.8	58.9	58.8			1096478.2	
270	11/17/2015	9:48:36	00d	00:10.0	62.2	72.2	64	58.4	-,-	63.9	63.8	61.8	59.3	58.6			1659586.9	
271	11/17/2015	9:48:46	00d	00:10.0	54.7	64.7	60.4	52.3	-,-	59.8	59	54.3	52.6	52.5			295120.9	
272	11/17/2015	9:48:56	00d	00:10.0	54.5	64.5	55.6	52	-,-	55.6	55.5	54	52.3	52.2			281838.3	
273	11/17/2015	9:49:06	00d	00:10.0	54.9	64.9	55.4	54.5	-,-	55.3	55.2	54.9	54.6	54.6			309029.5	
274	11/17/2015	9:49:16	00d	00:10.0	57	67	58.4	54.8	-,-	58.4	58.3	56.5	54.8	54.8			501187.2	
275	11/17/2015	9:49:26	00d	00:10.0	55.8	65.8	57.6	54.6	-,-	57.4	57.3	55.9	54.8	54.7			380189.4	
276	11/17/2015	9:49:36	00d	00:10.0	53.2	63.2	55.1	51.4	-,-	55	54.9	53.5	51.6	51.5			208929.6	
277	11/17/2015	9:49:46	00d	00:10.0	55.7	65.7	58.4	51.5	-,-	58.2	57.7	54.9	51.8	51.5			371535.2	
278	11/17/2015	9:49:56	00d	00:10.0	57.6	67.6	59	56.1	-,-	58.8	58.6	57.6	56.4	56.3			575439.9	

Address	Start	Measur	omo-	t Timo	Leg	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overall
	Time	ivieasui	emei	it iiiie	Leq	LE	LIVIAA	LIVIIIN	Ly	LINT	LINZ	LINS	LIN4	LINO	Over	Onder	iliverse Log	Leg
R2									_								042040.0	63.2
191	11/17/2015	9:35:09	_	00:10.0		69.6			7,7	61.8	61.6	59.8	58.4	58.4			912010.8	
192 193	11/17/2015 11/17/2015	9:35:19 9:35:29	_	00:10.0 00:10.0	58.7 56.4	68.7 66.4	62.2 58	55.3 55.2	747	62.1 57.6	61.9 57.2	57.7 55.9	55.6 55.3	55.4 55.2			741310.2 436515.8	
194	11/17/2015	9:35:39		00:10.0	59.7	69.7	61.6	57.8	_	61.1	60.3	59.1	58	57.9			933254.3	
195	11/17/2015	9:35:49		00:10.0	57.6	67.6	62.1	54.4	_	61.9	61.7	56.5	54.6	54.5			575439.9	
196	11/17/2015	9:35:59	00d	00:10.0	55.7	65.7	58.1	53.6	-,-	58	58	55.1	53.7	53.6			371535.2	
197	11/17/2015	9:36:09		00:10.0		66.5	58		_	58	57.9	56.6	53.5	53.5			446683.6	
198	11/17/2015	9:36:19	_	00:10.0	63.3	73.3	65	57.9		64.8	64.4	62.8	59.2	58.6			2137962.1	
199 200	11/17/2015 11/17/2015	9:36:29 9:36:39	00d 00d	00:10.0 00:10.0	64.2 65.4	74.2 75.4	65 66.8	63.6 64.2		65 66.7	64.9 66.3	64.2 65	63.8 64.4	63.7 64.3			2630268.0 3467368.5	
200	11/17/2015	9:36:49	00d	00:10.0	66.9	76.9	69.1	65.1		69	68.8	66.3	65.3	65.3			4897788.2	
202	11/17/2015	9:36:59	00d	00:10.0	63.6	73.6	68.9	60.7	-,-	68.4	67.7	63.1	62	61.4			2290867.7	
203	11/17/2015	9:37:09	00d	00:10.0	62.2	72.2	63.9	58.6	-,-	63.9	63.8	61.3	58.8	58.7			1659586.9	
204	11/17/2015	9:37:19	00d	00:10.0	68.4	78.4	71.4	63.4	-,-	71.2	71.1	67.5	63.5	63.4			6918309.7	
205	11/17/2015	9:37:29		00:10.0		71.8	68.3	59.2		67.9	67.2	60.3	59.2	59.2			1513561.2	
206 207	11/17/2015	9:37:39 9:37:49		00:10.0 00:10.0		70.4 69.5	60.8	59.5		61 60.5	61 60.3	60.4 59	59.6 58.6	59.5 58.6			1096478.2 891250.9	
207	11/17/2015 11/17/2015	9:37:49	00d	00:10.0	61.4	71.4	62.5	58.6 60.3		62.4	62.3	61.2	60.5	60.4			1380384.3	
209	11/17/2015			00:10.0	60.3	70.3	61.8	57.8		61.7	61.7	60.9	58.1	58			1071519.3	
210	11/17/2015	9:38:19	00d	00:10.0	60.7	70.7	62.1	57.4	-,-	62.1	62	60.7	57.8	57.6			1174897.6	
211	11/17/2015	9:38:29		00:10.0	65.7	75.7	69.3	60.3		69.2	68.6	62.6	60.5	60.4	<u> </u>		3715352.3	
212	11/17/2015	9:38:39		00:10.0	63.8	73.8	69.2	60.3		68.8	68.6	63.8	60.7	60.5			2398832.9	
213	11/17/2015	9:38:49		00:10.0	61.9	71.9	63.1	60.2		63	62.9	61.4	60.3	60.2			1548816.6	
214 215	11/17/2015 11/17/2015	9:38:59 9:39:09	_	00:10.0 00:10.0	64.7 63.9	74.7 73.9	65.6 65.1	62.3 62.3	_	65.5 65	65.5 64.4	65 63.7	63.1 62.9	62.7 62.5			2951209.2 2454708.9	
216	11/17/2015	9:39:19	_	00:10.0	68.5	78.5	72.4	61.3		72.3	72.1	67	62.2	61.9			7079457.8	
217	11/17/2015	9:39:29	00d	00:10.0	56.9	66.9	61.3	55.5	-,-	60.5	59.6	57.3	55.7	55.6			489778.8	
218	11/17/2015	9:39:39	00d	00:10.0	57.1	67.1	60	54.9	-,-	59.7	59	56.9	55.2	55			512861.4	
219	11/17/2015	9:39:49	00d	00:10.0	58.1	68.1	59.2	56.5	_	59.1	59	57.7	56.6	56.6			645654.2	
220	11/17/2015		_	00:10.0		69.2	60.9	56.9		60.8	60.8	58.5	57.1	57			831763.8	
221 222	11/17/2015 11/17/2015	9:40:09 9:40:19	00d	00:10.0 00:10.0		74.1 77.8	65.8 69.9	60.8 65.5	_	65.7 69.1	65.6 68.8	62.9 67.2	61.4 65.7	61.1 65.6			2570395.8 6025595.9	
223	11/17/2015	9:40:29	00d	00:10.0	69.4	79.4	71.1	66.9	_	71.1	71	69.8	67.4	67.2			8709635.9	
224	11/17/2015	9:40:39	00d	00:10.0	66	76	67.3	64.9		67	66.6	65.9	65.4	65.1			3981071.7	
225	11/17/2015	9:40:49	00d	00:10.0	69.3	79.3	73	66.5	-,-	72	70.4	68.1	66.9	66.7			8511380.4	
226	11/17/2015	9:40:59	00d	00:10.0	68.2	78.2	73.7	59.4		73.7	73.5	66.5	59.6	59.5			6606934.5	
227	11/17/2015	9:41:09		00:10.0	61.7	71.7	63.2	59.5		63.1	63.1	61.3	60.3	60.2			1479108.4	
228 229	11/17/2015 11/17/2015	9:41:19 9:41:29		00:10.0 00:10.0	61 60.8	71 70.8	62.3 62.4	59.1 59.3		62.2 62.3	62.2	60.5 60.7	59.3 59.6	59.1 59.5			1258925.4 1202264.4	
230	11/17/2015	9:41:39		00:10.0	60.8	70.8	62.3	59.4		62.1	62	60.4	59.7	59.5			1202264.4	
231	11/17/2015	9:41:49		00:10.0	60.3	70.3	62.3	57.9		62.2	61.8	60.6	58.7	58.3			1071519.3	
232	11/17/2015	9:41:59	00d	00:10.0	59.3	69.3	61.3	57.3		60.9	60.7	58.2	57.5	57.4			851138.0	
233	11/17/2015	9:42:09	00d	00:10.0	64.8	74.8	66.6	61.2	-,-	66.3	66.2	64.5	62.3	61.6			3019951.7	
234	11/17/2015	9:42:19		00:10.0	62.1	72.1	64.8	61.1		64.3	63.6	62.4	61.3	61.2			1621810.1	
235 236	11/17/2015 11/17/2015	9:42:29 9:42:39		00:10.0 00:10.0	63 64	73 74	65.1 65.1	61.2 63.3	7,7	65.1 64.9	64.9 64.6	61.6 63.9	61.3 63.5	61.3 63.4			1995262.3 2511886.4	
237	11/17/2015	9:42:49		00:10.0		75.7	66.6	63.9	-,-	66.5	66.4	65.8	65.2	64.8			3715352.3	
238	11/17/2015	9:42:59		00:10.0		71.9				63.1	62.7	62.2	61.7	61.4			1548816.6	
239	11/17/2015	9:43:09	00d	00:10.0	53.5	63.5	60.4	50.3	-,-	59.4	58.5	53.5	50.7	50.4			223872.1	
240	11/17/2015	9:43:19	_	00:10.0	50.1	60.1	50.4	49.6		50.3	50.3	50.2	49.7	49.6			102329.3	
241	11/17/2015	9:43:29	_	00:10.0		61.6	54	50.2	_	53.3	52.5	50.8	50.4	50.3			144544.0	
242 243	11/17/2015 11/17/2015	9:43:39 9:43:49	_	00:10.0 00:10.0	56.8 63.4	66.8 73.4	57.3 65.2	54 56.8	_	57.2 65	57.2 64.9	56.8 63	55.4 58	55 57.5			478630.1 2187761.6	
243	11/17/2015	9:43:49		00:10.0	67.3	77.3	68.7	65.2	_	68.6	68.5	66.8	65.4	65.4	Ė	<u> </u>	5370318.0	
245	11/17/2015	9:44:09		00:10.0		75.4	68.2	63.8	_	68	67.5	65.4	64.6	64.1			3467368.5	
246	11/17/2015	9:44:19	00d	00:10.0	62	72	63.8	60.4		63.5	63.4	62.2	61.2	61			1584893.2	
247	11/17/2015	9:44:29		00:10.0		70.3	60.9	59.3	_	60.7	60.7	60.4	59.6	59.5			1071519.3	
248	11/17/2015	9:44:39	_	00:10.0		70.5	61		-,-	60.9	60.8	60.4	60.2	60.1			1122018.5	l
249 250	11/17/2015 11/17/2015	9:44:49 9:44:59		00:10.0 00:10.0		72.1 69.8	63.1 61	60.9 59.4		63 60.8	62.9 60.5	62.1 59.7	61.3 59.5	61.2 59.4			1621810.1 954992.6	
250 251	11/17/2015	9:44:59		00:10.0		73.7	65.6	60.9	_	65.5	65.3	63.2	62.3	61.8	<u> </u>		2344228.8	
252	11/17/2015	9:45:19		00:10.0		70.2	62.5	57.4		62.2	61.9	60.9	57.9	57.7			1047128.5	
253	11/17/2015	9:45:29		00:10.0		67.7	58.9	56.3		58.8	58.7	57.2	56.6	56.4			588843.7	
254	11/17/2015	9:45:39		00:10.0		68.6	59.6	58		59.5	59.4	58.4	58.1	58			724436.0	
255	11/17/2015	9:45:49		00:10.0		71.9		59.1		63.4	63.3	61	60	59.6			1548816.6	
256	11/17/2015	9:45:59 9:46:09		00:10.0 00:10.0		74.7	67.3	61.6		67.2	67 61.7	64.2	61.9	61.8			2951209.2 1000000.0	
257 258	11/17/2015 11/17/2015			00:10.0	60 61.7	70 71.7	61.9 62.9	58.5 59.4		61.8 62.9	61.7 62.7	59.5 61.9	58.7 60	58.6 59.8			1479108.4	
259	11/17/2015	9:46:29		00:10.0		69.8	63.3	55.9		63.2	63.1	57.7	56.1	56			954992.6	l
260	11/17/2015	9:46:39		00:10.0	60.2	70.2	62.9	58.6		62.5	61.8	60.5	58.9	58.7			1047128.5	
261	11/17/2015	9:46:49		00:10.0		69.2	61.6	56.9		61.5	61.4	59	57.2	57			831763.8	
262	11/17/2015	9:46:59		00:10.0		65.9	57	54.9		56.9	56.7	55.8	55	55			389045.1	
263 264	11/17/2015	9:47:09		00:10.0		71.5	65 71.5	57 63.3		64.4	63.8	59.7	57.2	57			1412537.5	
	11/17/2015	9:47:19	uud	00:10.0	68	78	71.5	62.3	177	71.3	70.9	67.6	63.6	62.9			6309573.4	

	Start																	Overall
Address	Time	Measur	emen	t Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Lea
R2	Tillle																	63.2
11/2			_						_									03.2
265	11/17/2015	9:47:29	00d	00:10.0	61.2	71.2	62.6	59.7	-,-	62.4	62.3	60.8	59.9	59.8			1318256.7	
266	11/17/2015	9:47:39	00d	00:10.0	64.5	74.5	65.9	61.7		65.8	65.8	64.4	62.7	62.2			2818382.9	
267	11/17/2015	9:47:49	00d	00:10.0	64.6	74.6	68.2	61.5	-,-	67.8	67.4	62.5	61.6	61.6			2884031.5	
268	11/17/2015	9:47:59	00d	00:10.0	68.3	78.3	71.2	66.1	-,-	70.9	70.7	68	66.3	66.3			6760829.8	
269	11/17/2015	9:48:09	00d	00:10.0	63.6	73.6	66.2	61.8	-,-	66	65.8	63.9	62	61.9			2290867.7	
270	11/17/2015	9:48:19	00d	00:10.0	64.2	74.2	65.4	62.5		65.1	65.1	63.9	63	62.7			2630268.0	
271	11/17/2015	9:48:29	00d	00:10.0	60.7	70.7	63.7	59.7	-,-	63.3	62.7	60.6	59.8	59.8			1174897.6	
272	11/17/2015	9:48:39	00d	00:10.0	60.8	70.8	61.3	60.4		61.2	61.1	60.8	60.6	60.5			1202264.4	
273	11/17/2015	9:48:49	00d	00:10.0	59.7	69.7	60.4	59.2	-,-	60.4	60.3	59.7	59.5	59.3			933254.3	
274	11/17/2015	9:48:59	00d	00:10.0	59.7	69.7	61	58.6	-,-	60.9	60.8	59.1	58.7	58.6			933254.3	
275	11/17/2015	9:49:09	00d	00:10.0	57.7	67.7	60.3	55.2		59.9	59.4	58.6	55.6	55.3			588843.7	
276	11/17/2015	9:49:19	00d	00:10.0	58.7	68.7	60.7	54.5		60.6	60.4	58.2	54.8	54.7			741310.2	
277	11/17/2015	9:49:29	00d	00:10.0	63.3	73.3	67.5	59.3	-,-	67.3	66.9	60.1	59.5	59.4			2137962.1	
278	11/17/2015	9:49:39	00d	00:10.0	63.4	73.4	67	62.5	-,-	66	64.8	63.8	62.6	62.6			2187761.6	
279	11/17/2015	9:49:49	00d	00:10.0	59.6	69.6	62.6	58.7	-,-	62.2	61.4	59.7	58.8	58.8			912010.8	
280	11/17/2015	9:49:59	00d	00:10.0	60.1	70.1	60.4	59.7	-,-	60.3	60.3	60.2	59.9	59.8			1023293.0	

Address	Start	Measur	emer	nt Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overa
R3	Time																_	Leq 58.1
189	11/17/2015	9:35:09	ood	00:10.0	52.3	62.3	58.3	50.6		57.4	56.6	52.2	50.8	50.7			169824.4	30.1
190	11/17/2015	9:35:19		00:10.0	52.3	62.2	53.4	51.6	Н	53	52.6	52.2	51.7	51.7			165958.7	
190	11/17/2015	9:35:29		00:10.0	54.9	64.9	55.8	53.4	-	55.7	55.6	54.5	53.7	53.6			309029.5	
192	11/17/2015	9:35:39		00:10.0	55.7	65.7	56.4	54.9	-	56.3	56.1	55.7	55.7	55			371535.2	
193	11/17/2015	9:35:49		00:10.0	56.9	66.9	_	55.6		57.5	57.5	57	56.4	56.2			489778.8	
193	11/17/2015	9:35:59		00:10.0	56.7	66.7	60.9	53.0		60.7	60.3	54.2	53.3	53.2			467735.1	
195	11/17/2015	9:36:09		00:10.0	58.3	68.3	_	55.9		61.1	60.8	57.7	56.2	56			676083.0	
196	11/17/2015	9:36:19		00:10.0	54.7	64.7	57	53.5	-	56.7	56.6	54.5	53.8	53.7			295120.9	l
197	11/17/2015	9:36:29		00:10.0	57.2	67.2		54.5		58.5	58.4	57.4	54.7	54.6			524807.5	
198	11/17/2015	9:36:39		00:10.0	55.9	65.9				57.7	57.3	55.3	54.4	54.2			389045.1	
199	11/17/2015	9:36:49		00:10.0	60.7	70.7	62.1	57.7		62	61.8	60.1	59	58.4			1174897.6	
200	11/17/2015	9:36:59		00:10.0	59.9	69.9		58.9		61.5	61.4	60.1	59.2	59			977237.2	
201	11/17/2015	9:37:09		00:10.0	61.3	71.3	62.9	59.5		62.8	62.7	60.9	59.7	59.5			1348962.9	
202	11/17/2015	9:37:19		00:10.0	59.4	69.4		56.2		61.9	61.8	59.1	56.6	56.3			870963.6	
203	11/17/2015	9:37:29		00:10.0	59.6	69.6		58.6		60.7	60.4	59.7	59.1	58.9			912010.8	
204	11/17/2015	9:37:39		00:10.0	58	68		54.9		60.2	60	58.5	55.4	55.1			630957.3	
205	11/17/2015	9:37:49		00:10.0	60.2	70.2		56.6		61.5	61.5	60	57.1	56.6			1047128.5	
206	11/17/2015	9:37:59		00:10.0	58.1	68.1	61.9			61.7	61.4	57.8	55.3	54.9			645654.2	
207	11/17/2015	9:38:09		00:10.0	58	68		54.5		59.6	59.5	57.8	55.1	55			630957.3	
208	11/17/2015	9:38:19		00:10.0	58.8	68.8		56		60.6	60.5	59	56.2	56.2			758577.6	
209	11/17/2015	9:38:29		00:10.0	59.8	69.8		56.5		62.7	62.5	58.2	56.9	56.8			954992.6	1
210	11/17/2015	9:38:39		00:10.0	60.1	70.1	62.8	58.4		62.6	62.6	60	59	58.7			1023293.0	1
211	11/17/2015	9:38:49	_	00:10.0	58.3	68.3		56.4		59.8	59.7	57.7	56.7	56.6			676083.0	1
211	11/17/2015	9:38:59		00:10.0	62.4	72.4	64.3	59.2	-	64.2	64.1	62.4	59.4	59.2			1737800.8	1
213	11/17/2015	9:39:09		00:10.0	58.9	68.9	_	58.2	-	61.3	60.7	59	58.4	58.3			776247.1	1
213	11/17/2015	9:39:19		00:10.0	56.8	66.8		55.7		58.1	58	56.9	56	55.8			478630.1	1
214	11/17/2015	9:39:29		00:10.0	56.5	66.5	57.6	54.8	-	57.5	57.4	56.4	55	55.8			446683.6	1
216	11/17/2015	9:39:39		00:10.0	58.1	68.1	59	57.1	-	58.9	58.6	57.8	57.2	57.1			645654.2	
217	11/17/2015	9:39:49		00:10.0	58.8	68.8	60.8	55.4	-	60.6	60.4	59.3	56.4	55.8			758577.6	
218	11/17/2015	9:39:59		00:10.0	55	65	_	53.6	-	56.4	56.2	54.2	53.8	53.7			316227.8	
219	11/17/2015	9:40:09		00:10.0	56.1	66.1	57.6	53.6		57.5	57.3	56.1	53.9	53.7			407380.3	
220	11/17/2015	9:40:19		00:10.0	59.4	69.4	_	54.8		62.1	62	57.6	54.9	54.9			870963.6	
221	11/17/2015	9:40:29		00:10.0	61.6	71.6	_	60.9	-	62.1	62.1	61.6	61	61			1445439.8	
222	11/17/2015	9:40:39		00:10.0	58.9	68.9				61.7	61.4	60.2	54.9	54.8			776247.1	
223	11/17/2015	9:40:49		00:10.0	58.1	68.1	60.1	54.8		60.1	60.1	57.4	55.3	55.1			645654.2	
224	11/17/2015	9:40:59		00:10.0	55.9	65.9	59.8	53.8		59.3	58.9	55.8	54.1	53.9			389045.1	
225	11/17/2015	9:41:09		00:10.0	56.7	66.7	57.7	54.8		57.6	57.6	56.8	55.1	54.9			467735.1	
226	11/17/2015	9:41:19		00:10.0	53.4	63.4	57	51.8		56.6	55.8	52.8	52.1	52			218776.2	
227	11/17/2015	9:41:29		00:10.0	59.2	69.2	61	55.4		60.9	60.8	59.3	56.9	56.7			831763.8	
228	11/17/2015	9:41:39		00:10.0	59.2	69.2		56.9		60.3	60.2	59.2	57.5	57.1			831763.8	
229	11/17/2015	9:41:49		00:10.0	57.7	67.7	59.6	56		59.4	59.2	57.3	56.5	56.3			588843.7	
230	11/17/2015	9:41:59		00:10.0	58.1	68.1	60.2	53.6		60.1	60	56.6	53.8	53.7			645654.2	
231	11/17/2015	9:42:09		00:10.0	54.1	64.1	59.9			59.3	58.5	53.2	51.6	51.5			257039.6	
232	11/17/2015	9:42:19		00:10.0	59.5	69.5	60	55.8		59.9	59.8	59.4	57.6	57.4			891250.9	
233	11/17/2015	9:42:29		00:10.0	58.9	68.9		56.8		61	60.8	58.3	57.0	56.9			776247.1	
234	11/17/2015	9:42:39		00:10.0	59.1	69.1	61.1	57.6		61	60.8	58.9	57.8	57.7			812830.5	
235	11/17/2015	9:42:49		00:10.0	58.8	68.8		57.2		60.2	59.9	58.6	57.5	57.4			758577.6	
236	11/17/2015	9:42:59	_	00:10.0	58.3	68.3				59.4	59.2	58.3	57.5	57.4			676083.0	1
237	11/17/2015	9:43:09	_	00:10.0	58.5	68.5				59.1	59	58.6	57.7	57.7			707945.8	1
238	11/17/2015	9:43:19	_	00:10.0	57.3	67.3	58.6	56.5	-	58.4	58.3	57.3	56.7	56.6			537031.8	1
239	11/17/2015	9:43:29	_	00:10.0	54.7	64.7			-	57.2	57	54.4	53.9	53.9			295120.9	1
240	11/17/2015	9:43:39	_	00:10.0	53.2	63.2				54.1	54.1	53.3	52.7	52.6			208929.6	1
241	11/17/2015	9:43:49		00:10.0	53.6	63.6	_	50.9	-	55.8	55.2	52.4	51.1	51			229086.8	1
242	11/17/2015	9:43:59		00:10.0	53.2	63.2	56.2	50.8	-	56	55.9	54	50.9	50.8			208929.6	1
243	11/17/2015	9:44:09	_	00:10.0	54.2	64.2		50	-	55.8	55.8	53.8	50.5	50.3			263026.8	1
244	11/17/2015	9:44:19	_	00:10.0	62.8	72.8		55.1	-	65.7	65.3	62.4	55.7	55.3			1905460.7	1
245	11/17/2015	9:44:29	_	00:10.0	58	68		56.3		59.3	59.3	57.6	56.6	56.4			630957.3	1
246	11/17/2015	9:44:39	_	00:10.0	59.3	69.3	60		-	59.9	59.9	59.3	58.4	58.3			851138.0	1
247	11/17/2015	9:44:49		00:10.0	59.3	69.3		57.5		61.1	60.8	59.6	57.9	57.8			851138.0	1
248	11/17/2015	9:44:59		00:10.0	60.3	70.3		57.3		62.4	61.9	59.7	58.2	57.7			1071519.3	1
249	11/17/2015	9:45:09	_	00:10.0	56.6	66.6				60.1	59.6	56.8	54.9	54.8			457088.2	1
250	11/17/2015	9:45:19		00:10.0	57.1	67.1	58.1	54.3		58.1	58	57.2	54.8	54.4			512861.4	1
251	11/17/2015	9:45:29		00:10.0	59.5	69.5	60.9	57.8		60.8	60.6	59.5	58.1	58			891250.9	1
252	11/17/2015	9:45:39		00:10.0	55.5	65.5		54.2		57.2	56.9	55.9	54.4	54.3			354813.4	1
253	11/17/2015	9:45:49	_	00:10.0	56.8	66.8				58.9	58.9	56.5	53	52.8			478630.1	1
254	11/17/2015	9:45:59		00:10.0	57.5	67.5		54.1		60.2	60	56.3	54.3	54.1			562341.3	1
255	11/17/2015	9:46:09		00:10.0	59.6	69.6		58.6		60.4	60.2	59.5	58.8	58.8			912010.8	1
256	11/17/2015	9:46:19	_	00:10.0	57.2	67.2		54.6		60.4	60.3	57.1	54.8	54.7			524807.5	1
257	11/17/2015	9:46:29	_	00:10.0	58.2	68.2		55.3		59.1	59.1	58.2	55.8	55.5			660693.4	1
258	11/17/2015	9:46:39		00:10.0	58.9	68.9		55.4		60.7	60.5	59.1	56.2	55.7			776247.1	1
259	11/17/2015	9:46:49		00:10.0	53.2	63.2		50.9		55.1	55	53.5	51.2	55.7			208929.6	ı
260	11/17/2015	9:46:59		00:10.0	55.2	65.2	56.5	50.9		56.4	56.2	55.6	52.3	51.8			331131.1	1
261	11/17/2015	9:47:09	_	00:10.0	57.1	67.1	58			57.9	57.9	57.4	55.3	55.1			512861.4	1
	,,2013	٥. ٢٠ .٥٥		55.10.0	55.8	57.1	57.5			57.2	57.5	55.9	54.1	53.9	<b>-</b>		380189.4	ı

Address	Start	Measure	ment	t Time	Leg	LE	LMAX	LMIN	Ιv	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overall
Audiess	Time	Wiedsure	incin	· mile	Leq		LIVIAA	LIVIIIA	Ly	LIVI	LIVE	LIVS	LIVT	LING	Ovei	Onder	mverse Log	Leq
R3																		58.1
263	11/17/2015	9:47:29	00d	00:10.0	56.8	66.8	58.1	55.6	-,-	57.9	57.7	56.7	55.8	55.8			478630.1	
264	11/17/2015	9:47:39	00d	00:10.0	58.3	68.3	60.1	55.2	-,-	60	59.8	58.4	56.4	55.7			676083.0	
265	11/17/2015	9:47:49	00d	00:10.0	53.5	63.5	55.2	52.9	-,-	54.8	54.7	53.4	53	53			223872.1	
266	11/17/2015	9:47:59	00d	00:10.0	57	67	58.3	54	-,-	58.2	58	56.7	55.2	55			501187.2	
267	11/17/2015	9:48:09	00d	00:10.0	58.1	68.1	60	56	-,-	59.9	59.8	57.9	56.2	56.2			645654.2	1
268	11/17/2015	9:48:19	00d	00:10.0	58.3	68.3	59.7	56.7	-,-	59.6	59.5	57.9	57	56.9			676083.0	
269	11/17/2015	9:48:29	00d	00:10.0	58.5	68.5	59.5	57.4		59.4	59.2	58.6	57.7	57.4			707945.8	
270	11/17/2015	9:48:39	00d	00:10.0	59.4	69.4	61.7	57.4	-,-	61.6	61.3	59.2	57.7	57.5			870963.6	1
271	11/17/2015	9:48:49	00d	00:10.0	59.9	69.9	61.1	57.7	-,-	61	60.9	60.1	57.8	57.8			977237.2	1
272	11/17/2015	9:48:59	00d	00:10.0	58.8	68.8	61.3	55.8	-,-	61.2	60.9	58.1	56.1	56			758577.6	
273	11/17/2015	9:49:09	00d	00:10.0	58.6	68.6	60.7	57.3	-,-	60.6	60.6	58.4	57.6	57.5			724436.0	1
274	11/17/2015	9:49:19	00d	00:10.0	60	70	62.1	58.2	-,-	61.9	61.4	59.8	58.5	58.4			1000000.0	1
275	11/17/2015	9:49:29	00d	00:10.0	55.2	65.2	58.3	53.1	-,-	58.1	57.7	54.5	53.2	53.1			331131.1	1
276	11/17/2015	9:49:39	00d	00:10.0	58.5	68.5	60.2	54	-,-	60.1	59.8	58.6	54.2	54.1			707945.8	1
277	11/17/2015	9:49:49	00d	00:10.0	57.3	67.3	59.6	56.3		59.3	58.9	57.2	56.4	56.4			537031.8	
278	11/17/2015	9:49:59	00d	00:10.0	56.7	66.7	58.4	54.5	-,-	58.3	58.1	57.1	54.7	54.6			467735.1	1

Address	Start Time	Measur	emer	nt Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log
R4	Time																
189	11/17/2015	9:35:00	00d	00:10.0	61.9	71.9	62.6	61.4		62.7	62.7	62	61.3	61.2			1548816.6
190	11/17/2015	9:35:10	00d	00:10.0	61	71	62.2	58.7		62.2	62.2	61.3	59	58.1			1258925.4
191	11/17/2015	9:35:20	00d	00:10.0	57.7	67.7	59.7	55.8	-,-	59.6	59.6	57.6	55.6	55.5			588843.7
192	11/17/2015	9:35:30		00:10.0	59.3	69.3	60.5	56.6		60.6	60.6	59.4	58.3	57.5			851138.0
193	11/17/2015	9:35:40		00:10.0	58.5	68.5	60.5	57.5	-:-	59.9	59.9	58.3	57.6	57.3			707945.8
194 195	11/17/2015	9:35:50		00:10.0	61.2	71.2	63.3	57.6		63.7	63.7	61.3	58.3	57.4			1318256.7 602559.6
195	11/17/2015 11/17/2015	9:36:00 9:36:10		00:10.0 00:10.0	57.8 55.7	67.8 65.7	60.2 56.5	55.2 54.7		60.2 56.8	60.2 56.8	57.7 55.7	55.3 54.8	54.7 54.6			371535.2
197	11/17/2015	9:36:20		00:10.0	63	73	66.4	56.2		67.3	67.3	61.8	57.5	57.2			1995262.3
198	11/17/2015	9:36:30		00:10.0	61.5	71.5	62.7	59.2		63	63	61.9	60.8	57.8			1412537.5
199	11/17/2015	9:36:40	00d	00:10.0	55.6	65.6	59.2	54.8	-,-	56.5	56.5	55.8	54.9	54.8			363078.1
200	11/17/2015	9:36:50	00d	00:10.0	56.1	66.1	56.6	55.6		56.8	56.8	56	55.5	55.5			407380.3
201	11/17/2015	9:37:00	00d	00:10.0	61.9	71.9	65.8	55.3		66.4	66.4	61.1	55	52.7			1548816.6
202	11/17/2015	9:37:10	00d	00:10.0	54.7	64.7	56.6	51.9		57.3	57.3	55	51.7	51.6			295120.9
203	11/17/2015	9:37:20	00d	00:10.0	59.4	69.4	61	56.6		61.3	61.3	59.4	57.5	57.4			870963.6
204	11/17/2015	9:37:30		00:10.0	58.5	68.5	60.3	56.5	-,-	59.8	59.8	58.4	56.5	56.2			707945.8
205	11/17/2015	9:37:40		00:10.0	60.3	70.3	62	56.3		62.3	62.3	60.6	57.9	56.2			1071519.3
206	11/17/2015	9:37:50		00:10.0	65.4	75.4	67.4	62	-:-	67.6	67.6	64.6	63.8	63.8			3467368.5
207	11/17/2015	9:38:00		00:10.0	59.6	69.6	64.8	58.7		61.5	61.5	59.1	58.7	58.4			912010.8
208 209	11/17/2015 11/17/2015	9:38:10 9:38:20		00:10.0 00:10.0	61.2	71.2 75.1	61.9 68.9	58.8 60		62.1 69.5	62.1 69.5	61.4	60.3	59.5 59.9			1318256.7 3235936.6
210	11/17/2015	9:38:30		00:10.0	63.5	73.5	69.4	59		69.3	69.3	61.2	59.2	58.5			2238721.1
210	11/17/2015	9:38:40		00:10.0	59.6	69.6		58.5		60.8	60.8	59.6	58.6	58.5			912010.8
212	11/17/2015	9:38:50		00:10.0	64	74	66.8	60.5	-:-	67	67	63.5	61.6	61.5			2511886.4
213	11/17/2015	9:39:00		00:10.0	59.5	69.5	62.8	58.5	-,-	60.7	60.7	59.6	58.4	58.4			891250.9
214	11/17/2015	9:39:10		00:10.0	63.1	73.1	64.1	59.6		64.1	64.1	63.1	62.1	60.7			2041737.9
215	11/17/2015	9:39:20	00d	00:10.0	59.3	69.3	63.8	58.1		61.9	61.9	58.8	58.3	58			851138.0
216	11/17/2015	9:39:30	00d	00:10.0	59.3	69.3	61	57.7		61.5	61.5	58.9	57.6	57.5			851138.0
217	11/17/2015	9:39:40	00d	00:10.0	60.1	70.1	61.6	58.8		61.9	61.9	59.6	58.7	58.6			1023293.0
218	11/17/2015	9:39:50	00d	00:10.0	66.9	76.9	71.1	58.9		71.6	71.6	65.6	62.9	60.1			4897788.2
219	11/17/2015	9:40:00	00d	00:10.0	55.7	65.7	64.6	53.3		60	60	54.4	53.4	52.8			371535.2
220	11/17/2015	9:40:10	00d	00:10.0	53.9	63.9	56.2	52.2		56.8	56.8	53.2	52.4	51.8			245470.9
221	11/17/2015	9:40:20		00:10.0	50.1	60.1	53.5	49.1		52.6	52.6	49.8	49.3	49			102329.3
222	11/17/2015	9:40:30		00:10.0	57.4	67.4	59.9	49.3		60.1	60.1	58.4	50.1	49.7			549540.9
223	11/17/2015	9:40:40		00:10.0	55.4	65.4	59.7	53	-:-	58.5	58.5	55	53.1	52.5			346736.9
224	11/17/2015	9:40:50		00:10.0	55.2	65.2	57.8	52.6	-:-	58.1	58.1	54.3	52.9	52.2			331131.1 851138.0
225 226	11/17/2015 11/17/2015	9:41:00 9:41:10		00:10.0 00:10.0	59.3 59.8	69.3 69.8	60.6 62.3	54.2 56.8		60.7 62.5	60.7 62.5	59.9 59.3	56.7 57.3	54.1 56.1			954992.6
227	11/17/2015	9:41:20		00:10.0	59.3	69.3	60.8	56.3		61.5	61.5	59.4	57	55.9			851138.0
228	11/17/2015	9:41:30		00:10.0	60.2	70.2	61.7	58.2	-:-	62	62	60.5	58.5	58.1			1047128.5
229	11/17/2015	9:41:40		00:10.0	60.4	70.4	61.7	58.9		62.1	62.1	60.7	59.2	58.7			1096478.2
230	11/17/2015	9:41:50	00d	00:10.0	61.9	71.9	62.9	60.8		63	63	61.9	60.8	60.8			1548816.6
231	11/17/2015	9:42:00	00d	00:10.0	61.8	71.8	62.6	61.3		62.7	62.7	61.7	61.2	61			1513561.2
232	11/17/2015	9:42:10	00d	00:10.0	63	73	63.6	61.2		63.7	63.7	63.4	61.6	61.3			1995262.3
233	11/17/2015	9:42:20	00d	00:10.0	62.2	72.2	63.4	60.5		63.2	63.2	62.6	60.8	60.1			1659586.9
234	11/17/2015	9:42:30	00d	00:10.0	60	70	62.1	58		62.3	62.3	59.7	57.9	57.7			1000000.0
235	11/17/2015	9:42:40		00:10.0	62.7	72.7	65	61.3		65.5	65.5	62	61.6	61			1862087.1
236	11/17/2015	9:42:50		00:10.0	64.3	74.3	66	62.6		66.1	66.1	64.6	62.6	62.2			2691534.8
237	11/17/2015	9:43:00		00:10.0	62.9	72.9	63.6	61.9		63.7	63.7	63.2	62.3	61.4			1949844.6
238	11/17/2015 11/17/2015	9:43:10		00:10.0	61.2	71.2	62.3	59.3	-,-	62.6		61.5	59.3	58.9			1318256.7
239 240	11/17/2015	9:43:20 9:43:30		00:10.0 00:10.0	56.4 57.2	66.4 67.2	59.6 58	54.4 55.6		58.6 57.9		55.5 57.5	54.5 55.6	54.2 55.2			436515.8 524807.5
240	11/17/2015	9:43:40	+	00:10.0	57.6	67.6		56.8		58.7	58.7	57.8	57	56.8			575439.9
242	11/17/2015	9:43:50		00:10.0	57.3	67.3	58.4	55.7	-:-	58.3	58.3	57.6	55.9	55.4			537031.8
243	11/17/2015	9:44:00		00:10.0	53.3	63.3	57.4	52	-,-	55.2	55.2	53	52.1	51.8			213796.2
244	11/17/2015	9:44:10		00:10.0	58.9	68.9	61.7	54		62.5	62.5	57.3	56.1	54.6			776247.1
245	11/17/2015	9:44:20	00d	00:10.0	52.3	62.3	56.4	49.7	-,-	55.5	55.5	51.1	50.3	49.5			169824.4
246	11/17/2015	9:44:30	00d	00:10.0	54	64	56.7	52.4	-,-	57.4	57.4	53.2	52.4	52.3			251188.6
247	11/17/2015	9:44:40	00d	00:10.0	53.1	63.1	55.5	51.1	-,-	55.9	55.9	52.3	51.1	50.9			204173.8
248	11/17/2015	9:44:50	00d	00:10.0	61.3	71.3	65.2	55.4		65.9	65.9	60.7	55.9	55.7			1348962.9
249	11/17/2015	9:45:00	00d	00:10.0	61.8	71.8	65.3	60.1		64.5	64.5	61.9	60	59.9			1513561.2
250	11/17/2015	9:45:10		00:10.0	59.3	69.3	61.8	57.9		61.3	61.3	58.7	58.1	57.8			851138.0
251	11/17/2015	9:45:20		00:10.0	61.1	71.1	62.3	59.6	-,-	62.6		61	59.5	59.4			1288249.6
252	11/17/2015	9:45:30		00:10.0	59.5	69.5	60.3	58.2	-,-	60.5	60.5	59.7	58.4	57.8			891250.9
253	11/17/2015	9:45:40		00:10.0	60.2	70.2	61	59.2	-,-	61.3	61.3	60.3	59.1	58.9			1047128.5
254	11/17/2015	9:45:50		00:10.0	62.3	72.3	64.2	59.8		64.4	64.4	62.7	60.3	59.8			1698243.7
255 256	11/17/2015 11/17/2015	9:46:00 9:46:10		00:10.0 00:10.0	65.5	75.5 72.4	67.7 63.9	63.8		68.5 63.8	68.5 63.8	65.2 62.5	63.8	63.2 60.1			3548133.9 1737800.8
256	11/17/2015	9:46:10		00:10.0	56.7	66.7	62.2	54.8		60		56.4	54.9	54.9			467735.1
257	11/17/2015	9:46:30		00:10.0	59.6	69.6		56.8		62.2	62.2	58.9	58.2	57.5			912010.8
259	11/17/2015	9:46:40		00:10.0	61.8	71.8		60.7	-i-	63.3	63.3	61.7	61.2	60.5			1513561.2
260	11/17/2015	9:46:50		00:10.0	61.7	71.7	62.9	60.6		63.1	63.1	61.6	60.7	60.5			1479108.4
261	11/17/2015	9:47:00		00:10.0	63.6	73.6		60.9		65.5	65.5	63.3	61.8	61.2			2290867.7
262	11/17/2015	9:47:10		00:10.0	60.2	70.2	62.1	58.2	-,-	62.5	62.5	59.8	58.2	57.9			1047128.5
263	11/17/2015	9:47:20	00d	00:10.0	57.1	67.1	60.9	55.7	-,-	59.5	59.5	56.6	55.8	55.4			512861.4
264	11/17/2015	9:47:30	00d	00:10.0	55.1	65.1	58.1	51.9	-,-	58.1	58.1	54.3	51.7	51.3	l		323593.7

Overall Lea 60.7

Address	Start	Measur	emen	t Time	Leq	LE	LMAX	LMIN	Lv	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overa
	Time				- 4													Lea
R4																		60.7
265	11/17/2015	9:47:40	00d	00:10.0	55.4	65.4	56.5	53.3	-,-	56.7	56.7	55.6	54.4	54.2			346736.9	
266	11/17/2015	9:47:50	00d	00:10.0	57.5	67.5	59.6	54.4	-,-	60.3	60.3	57.5	55.7	54.3			562341.3	
267	11/17/2015	9:48:00	00d	00:10.0	55.6	65.6	57.3	54.5		57.4	57.4	55.1	54.5	54.5			363078.1	
268	11/17/2015	9:48:10	00d	00:10.0	53.8	63.8	55.1	52.9	-,-	55.1	55.1	53.8	53.1	52.6			239883.3	1
269	11/17/2015	9:48:20	00d	00:10.0	53.2	63.2	54.3	52.3		54.8	54.8	53.2	52.5	52.3			208929.6	]
270	11/17/2015	9:48:30	00d	00:10.0	58.6	68.6	59.2	54.3	-,-	59.2	59.2	58.7	58.3	57			724436.0	
271	11/17/2015	9:48:40	00d	00:10.0	61.6	71.6	64.9	58.4		65.2	65.2	60.6	58.5	58.5			1445439.8	]
272	11/17/2015	9:48:50	00d	00:10.0	63.7	73.7	64.8	62.6	-,-	64.3	64.3	63.8	62.6	62.4			2344228.8	
273	11/17/2015	9:49:00	00d	00:10.0	63.8	73.8	67.3	59.9	-,-	67.9	67.9	63.2	59.8	59.8			2398832.9	
274	11/17/2015	9:49:10	00d	00:10.0	59.5	69.5	61.7	57.4		62	62	59.1	57.5	57.4			891250.9	
275	11/17/2015	9:49:20	00d	00:10.0	63.3	73.3	64.7	61.7		64.8	64.8	63.1	61.9	61.5			2137962.1	
276	11/17/2015	9:49:30	00d	00:10.0	62.2	72.2	63.7	60.2	-,-	63.8	63.8	62.7	60.3	59.5			1659586.9	]
277	11/17/2015	9:49:40	00d	00:10.0	61.3	71.3	62.8	59		63	63	61.3	59.4	58.5			1348962.9	]
278	11/17/2015	9:49:50	00d	00:10.0	57.5	67.5	59.1	56.3		59	59	57.5	56.1	55.9			562341.3	]

Address	Start	Measur	omor	nt Timo	Leg	LE	LMAX	I MINI	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overal
	Time	ivieasur	emer	it iime	Leq	LE	LIVIAX	LIVIIN	Ly	LINI	LNZ	LN3	LN4	LN5	Over	Under	Inverse Log	Leq
R5																		59.5
131	11/17/2015	10:40:06		00:10.0	59.9	69.9	61.4	57.7		61.3	61.3	60.7	57.9	57.9			977237.2	-
132	11/17/2015	10:40:16		00:10.0	55.5	65.5	59.5	53.5	-,-	59.1	58.8	55.4	53.7	53.6			354813.4	-
133 134	11/17/2015 11/17/2015	10:40:26 10:40:36	_	00:10.0 00:10.0	53.1 55.5	63.1 65.5	55.8 56.6	50.9 54.4	-,-	55.3 56.5	54.4 56.5	52.7 55.5	51 54.5	51 54.4			204173.8 354813.4	ł
135	11/17/2015	10:40:46	_	00:10.0	54.7	64.7	56.6	52.4	-	56.5	56.4	54.4	52.5	52.5			295120.9	1
136	11/17/2015	10:40:56	_	00:10.0	53.3	63.3	55.7	51.9	-	55.2	54.8	53.6	52.1	52			213796.2	1
137	11/17/2015	10:41:06	00d	00:10.0	58.4	68.4	61	52	-,-	60.9	60.8	56.2	52.5	52.3			691831.0	1
138	11/17/2015	10:41:16	00d	00:10.0	62.5	72.5	64.5	60	-,-	64.1	63.8	61.7	60.1	60.1			1778279.4	
139	11/17/2015	10:41:26	00d	00:10.0	62	72	65.6	60.2		65.5	65.3	61.2	60.3	60.3			1584893.2	
140	11/17/2015	10:41:36		00:10.0	62.4	72.4	64.9	60	-,-	64.8	64.5	61.4	60.1	60.1			1737800.8	
141	11/17/2015	10:41:46		00:10.0	60.5	70.5	62.1	58.9	-,-	61.6	61.2	60.6	59.1	59			1122018.5	-
142 143	11/17/2015 11/17/2015	10:41:56		00:10.0 00:10.0	60.3 61.4	70.3 71.4	62.5	58.3 58.8		62.5 63.4	62.4 62.6	59.9 60.7	58.5 58.9	58.4 58.9			1071519.3 1380384.3	-
143	11/17/2015	10:42:06 10:42:16		00:10.0	59.4	69.4	63.8 63.7	52.5		63.1	62.4	60.7	55.9	53.7			870963.6	1
145	11/17/2015	10:42:26		00:10.0	49.8	59.8	52.5	47.5		51.7	51.6	49.6	47.6	47.6			95499.3	1
146	11/17/2015	10:42:36		00:10.0	54.3	64.3	56.4	51.7	-,-	56.3	56.1	53.7	52.1	51.9			269153.5	1
147	11/17/2015	10:42:46	00d	00:10.0	54.6	64.6	56.6	51.8		56.6	56.4	54.5	52.9	52.4			288403.2	
148	11/17/2015	10:42:56	00d	00:10.0	47.9	57.9	51.8	46.8		51.2	50.6	47.7	46.8	46.8			61659.5	
149	11/17/2015	10:43:06		00:10.0	55.2	65.2	58.4	47.1	-,-	58.3	58.2	51.2	47.4	47.2			331131.1	
150	11/17/2015	10:43:16		00:10.0	60.2	70.2	61.6	58.3		61.5	61.3	59.5	58.8	58.6			1047128.5	1
151 152	11/17/2015	10:43:26		00:10.0 00:10.0	61.4 59.2	71.4 69.2	63.5 61.9	59.7		63.4 60.8	63.2 59.6	61.3 58.7	60.1 57.5	57.3			1380384.3 831763.8	1
152	11/17/2015 11/17/2015	10:43:36 10:43:46		00:10.0	60.1	70.1	63.3	57.3 57.1		63.3	63.1	59.5	57.5	57.3			1023293.0	1
154	11/17/2015	10:43:56	_	00:10.0	59.1	69.1	61.2	55.4		61.1	61	59.5	56	55.6			812830.5	1
155	11/17/2015	10:44:06	_	00:10.0	56.1	66.1	56.8	55.2	-,-	56.5	56.5	56	55.3	55.3			407380.3	1
156	11/17/2015	10:44:16	00d	00:10.0	57.1	67.1	59.3	55.9	-,-	59.2	58.9	56.6	56	56			512861.4	1
157	11/17/2015	10:44:26	00d	00:10.0	51.4	61.4	55.9	49.6	-,-	55.5	54.9	51.1	49.7	49.6			138038.4	
158	11/17/2015	10:44:36	_	00:10.0	50.8	60.8	53.1	48.4	-,-	52.4	51.7	50.4	48.5	48.5			120226.4	1
159	11/17/2015	10:44:46		00:10.0	54.2	64.2	56.1	51.3	-,-	56	55.9	54.5	51.5	51.4			263026.8	
160	11/17/2015	10:44:56	_	00:10.0 00:10.0	60.1 59.4	70.1	66.8 67.5	51.6	-	63.8	60.5	55.3	53.7 54	52.5			1023293.0 870963.6	ł
161 162	11/17/2015 11/17/2015	10:45:06 10:45:16		00:10.0	61.2	69.4 71.2	62.1	53.7 59.3		67.2 62.1	66.4 62	56.9 61.3	59.6	53.8 59.5			1318256.7	
163	11/17/2015	10:45:26		00:10.0	61.4	71.4	62.4	60	-	62.3	62.2	61.5	60.7	60.4			1380384.3	
164	11/17/2015	10:45:36		00:10.0	55.8	65.8	60	54.5		59.5	59	55.4	54.6	54.6			380189.4	
165	11/17/2015	10:45:46	00d	00:10.0	56	66	56.7	55		56.7	56.5	55.9	55.1	55.1			398107.2	1
166	11/17/2015	10:45:56	00d	00:10.0	62.2	72.2	64.7	56.7		64.7	64.5	61.2	57	56.8			1659586.9	
167	11/17/2015	10:46:06	00d	00:10.0	61.3	71.3	62.9	59.7	-,-	62.3	62.1	61.6	60.9	60.4			1348962.9	
168	11/17/2015	10:46:16		00:10.0	57.8	67.8	59.7	55.5	-,-	59.5	59.4	57.9	55.8	55.6			602559.6	-
169	11/17/2015	10:46:26		00:10.0	56.3	66.3	58.9	54.7	-,-	58.8	58.4	56.4	54.9	54.8			426579.5	-
170 171	11/17/2015 11/17/2015	10:46:36		00:10.0 00:10.0	53.5 54.2	63.5 64.2	55.7 55.4	53 52.9		55.3 55.3	54.9 55.1	53.4 54.2	53 53.1	53 53.1			223872.1 263026.8	
171	11/17/2015	10:46:46 10:46:56		00:10.0	53.8	63.8	57.6	50.9		56.8	55.8	52.4	50.9	50.9			239883.3	
173	11/17/2015	10:47:06		00:10.0	64.6	74.6	68.7	57.6		67.7	66.8	61.3	58.5	58.5			2884031.5	1
174	11/17/2015	10:47:16	00d	00:10.0	64.4	74.4	70.4	60.7	-,-	69.8	69.5	63.3	60.7	60.7			2754228.7	
175	11/17/2015	10:47:26	00d	00:10.0	61.4	71.4	62.4	60	-,-	62.3	62.2	61.5	60.7	60.6			1380384.3	
176	11/17/2015	10:47:36	00d	00:10.0	59.6	69.6	60.9	58.3	-,-	60.7	60.6	59.3	58.4	58.4			912010.8	
177	11/17/2015	10:47:46		00:10.0	62.8	72.8	65.1	60.6		65	64.8	62.3	60.8	60.7			1905460.7	-
178	11/17/2015	10:47:56		00:10.0	60.9	70.9	61.6	_	-	61.5	61.4	60.9	60.4	60.2			1230268.8	ł
179 180	11/17/2015 11/17/2015	10:48:06 10:48:16	_	00:10.0 00:10.0	62.7 60.6	72.7 70.6	65.3 61.5	60.5 59.7	Ë	65.1 61.4	64.4	62.2 60.7	61.4 59.8	61 59.8			1862087.1 1148153.6	1
181	11/17/2015	10:48:26	_	00:10.0	54.1	64.1	60.2	51.4	-,-	59.5	58.5	54.5	51.5	51.4			257039.6	1
182	11/17/2015	10:48:36	_	00:10.0	53.5	63.5	57	49.8	-	56.9	56.6	52.4	50.4	50.2			223872.1	1
183	11/17/2015	10:48:46	_	00:10.0	47.5	57.5	49.8	46.5	-,-	49.4	49	47.4	46.7	46.6			56234.1	]
184	11/17/2015	10:48:56	00d	00:10.0	52.1	62.1	54.7	48.6		54.3	53.4	51.2	49.9	49.8			162181.0	1
185	11/17/2015	10:49:06	_	00:10.0	54.5	64.5	56.9	52	-	56.8	56.5	54	52.3	52.2			281838.3	4
186	11/17/2015	10:49:16	_	00:10.0	65.6	75.6	69.9	56.6		69.8	69.4	61.1	56.7	56.6			3630780.5	-
187	11/17/2015	10:49:26		00:10.0	63.6	73.6	69.4	61.5		68.5	67.7	63.9	62.1	62			2290867.7	1
188 189	11/17/2015 11/17/2015	10:49:36 10:49:46		00:10.0 00:10.0	58.3 60.4	68.3 70.4	61.5	56.5 59.1		60.9 61.2	60.4	58 60.6	56.9 59.3	56.7 59.2			676083.0 1096478.2	1
189	11/17/2015	10:49:46	_	00:10.0	60.4	70.4	61.3 62.7	59.1		62.5	62.2	60.3	59.3	59.2			1174897.6	1
191	11/17/2015	10:50:06		00:10.0	62.1	72.1	65.5	59		65.2	64.7	61.2	59.3	59.1			1621810.1	1
192	11/17/2015	10:50:16		00:10.0	60.5	70.5	63.5	57.6		63.3	62.9	59.8	58.8	58.6			1122018.5	]
193	11/17/2015	10:50:26	00d	00:10.0	50.8	60.8	57.6	48.4	-,-	56.8	56	50.1	48.6	48.5			120226.4	1
194	11/17/2015	10:50:36		00:10.0	53.1	63.1	55.2	49.2		55	54.5	52.2	50.5	49.9			204173.8	4
195	11/17/2015	10:50:46		00:10.0	57.9	67.9	59.4	54.9		59.2	59.1	57.6	55.6	54.9			616595.0	-
196	11/17/2015	10:50:56		00:10.0	62	72	65.2	58		65	64.9	59.5	58.2	58.1			1584893.2	-
197	11/17/2015 11/17/2015	10:51:06 10:51:16		00:10.0	61.3	71.3	63.1	59 61.0		62.9	62.9	61.2	59.3	59.2			1348962.9 2511886.4	ł
198 199	11/17/2015 11/17/2015	10:51:16		00:10.0 00:10.0	60.8	74 70.8	66.7 63	61.9 58.5		66.6 62.4	66.3 62.3	63.3 60.8	62.1 58.8	62 58.7			1202264.4	1
200	11/17/2015	10:51:26		00:10.0	62.5	70.8	64.6	60.7	-	64.5	64.3	61.7	60.9	60.8			1778279.4	1
201	11/17/2015	10:51:46		00:10.0	57.2	67.2	63.6	54.6	-,-	63	62.3	56.6	55	54.9			524807.5	1
202	11/17/2015	10:51:56		00:10.0	54.1	64.1	56	52.4		55.1	54.7	54.4	53.4	52.7			257039.6	1
203	11/17/2015	10:52:06		00:10.0	56.9	66.9	61.4	51.9		60.9	59.9	53.4	52.1	52			489778.8	
204	11/17/2015	10:52:16	00d	00:10.0	56.8	66.8	61.5	52.8		61.3	60.7	55.4	53.4	52.9			478630.1	l .

	Start																	Overall
Address	Time	Measur	emen	nt Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Leg
R5																		59.5
205	11/17/2015	10:52:26	00d	00:10.0	57.3	67.3	59.9	54.4		59.6	59.3	56.8	54.6	54.5			537031.8	
206	11/17/2015	10:52:36	00d	00:10.0	56.5	66.5	58.8	53.6	-,-	58.4	58.2	56.4	54.3	54.1			446683.6	
207	11/17/2015	10:52:46	00d	00:10.0	56.4	66.4	58.9	53.9	-,-	58.7	58.3	55.8	54.4	54.3			436515.8	
208	11/17/2015	10:52:56	00d	00:10.0	59	69	61.4	56.1	-,-	61.3	60.9	58.3	57.2	56.3			794328.2	
209	11/17/2015	10:53:06	00d	00:10.0	64.9	74.9	70	57.3	-,-	69.6	69.2	58.1	57.4	57.4			3090295.4	
210	11/17/2015	10:53:16	00d	00:10.0	58.1	68.1	67.8	55.8	-,-	66.6	65.1	57.8	56	55.9			645654.2	1
211	11/17/2015	10:53:26	00d	00:10.0	56.2	66.2	56.9	55.6	-,-	56.9	56.9	56.4	55.6	55.6			416869.4	1
212	11/17/2015	10:53:36	00d	00:10.0	57.3	67.3	59.1	55.6	-,-	58.4	57.8	56.9	55.7	55.6			537031.8	1
213	11/17/2015	10:53:46	00d	00:10.0	60.2	70.2	61.2	58.3	-,-	61.1	61.1	60.3	58.9	58.5			1047128.5	1
214	11/17/2015	10:53:56	00d	00:10.0	57.1	67.1	58.3	56.1	-,-	58.1	58.1	57.2	56.2	56.2			512861.4	1
215	11/17/2015	10:54:06	00d	00:10.0	59.9	69.9	60.8	56.6	-,-	60.7	60.7	59.9	57.6	57.1			977237.2	1
216	11/17/2015	10:54:16	00d	00:10.0	60.1	70.1	60.7	59.1	-,-	60.6	60.5	60	59.3	59.2			1023293.0	1
217	11/17/2015	10:54:26	00d	00:10.0	57.1	67.1	60.3	56		59.9	59.4	57	56.2	56.2			512861.4	]
218	11/17/2015	10:54:36	00d	00:10.0	56.3	66.3	57.8	54.2		57.8	57.7	56.1	55.1	54.5			426579.5	]
219	11/17/2015	10:54:46	00d	00:10.0	53	63	54.5	51.4		54.3	54.2	53	51.5	51.5			199526.2	]
220	11/17/2015	10:54:56	00d	00:10.0	54	64	56.5	50.6	-,-	56.4	56.4	51.9	50.7	50.7			251188.6	]

Address R6	Time		emen	it Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overa
							-100 01		-,						O C C	oesi	reise zeg	Leg
49	11/17/2015	10:40:01	nnd	00:10.0	63.6	73.6	68.1	56.2		68.9	68.9	61.6	58	57.8			2290867.7	60.1
50		10:40:01		00:10.0	60.2	70.2			-	63.1	63.1	59.8	57	55.8			1047128.5	ł
51	11/17/2015 11/17/2015	10:40:11		00:10.0	61.2	70.2	62.8		_	62.9	62.9	59.8	59.4	55.8			1318256.7	
52	11/17/2015	10:40:31		00:10.0	63	73			_	65.5	65.5	62.9	60.7	60.5			1995262.3	1
53	11/17/2015	10:40:41		00:10.0	63	73	65.1	60.4	<del></del>	64.8	64.8	63.3	60.4	60.2			1995262.3	
54	11/17/2015	10:40:51		00:10.0	58.6	68.6	60.4	57.6		60.1	60.1	58.5	57.7	57.7			724436.0	1
55	11/17/2015	10:41:01	00d	00:10.0	58.3	68.3	58.9	57.7		58.9	58.9	58.3	57.8	57.7			676083.0	1
56	11/17/2015	10:41:11	00d	00:10.0	61	71	63.1	58.5		63.4	63.4	61	58.6	58.4			1258925.4	1
57	11/17/2015	10:41:21	00d	00:10.0	60.3	70.3	62.8	57.4		62.3	62.3	60.3	57.5	57.1			1071519.3	]
58	11/17/2015	10:41:31	00d	00:10.0	55.5	65.5	57.5	54.2	-,-	57.5	57.5	55.3	54.1	54			354813.4	]
59	11/17/2015	10:41:41	00d	00:10.0	61	71	62.7	57		63.1	63.1	61.3	59.4	59.2			1258925.4	
60	11/17/2015	10:41:51	00d	00:10.0	56.5	66.5	62.6	53.6		59.9	59.9	56	53.8	53.3			446683.6	
61	11/17/2015	10:42:01		00:10.0	56.4	66.4	58.6		<del></del>	59.4	59.4	56.2	53.6	53.3			436515.8	
62	11/17/2015	10:42:11		00:10.0	58.4	68.4	60.9		_	61.3	61.3	59.1	55.5	55.4			691831.0	
63	11/17/2015	10:42:21		00:10.0	56.7	66.7	59.2	54.4	_	59.5	59.5	56.3	54.2	54.2			467735.1	
64	11/17/2015	10:42:31		00:10.0	57.8	67.8	60.2		_	60.3	60.3	57.1	56.2	56			602559.6	ł
65 66	11/17/2015 11/17/2015	10:42:41		00:10.0 00:10.0	60.1 58.9	70.1 68.9	60.9 61.4		_	61 61.6	61 61.6	60.1 59	59.1 56.1	59 55.6			1023293.0 776247.1	ł
67	11/17/2015	10:42:51	_	00:10.0	58.5	68.5	59.4	56.2	<del></del>	59.6	59.6	58.9	56.9	56.8			707945.8	ł
68	11/17/2015	10:43:01	00d	00:10.0	56.7	66.7	57.3	56.2	_	57.3	57.3	56.8	56.5	55.9			467735.1	1
69	11/17/2015	10:43:21		00:10.0	57.3	67.3	57.9		_	57.9	57.9	57.6	56.5	56.2			537031.8	1
70	11/17/2015	10:43:31	00d	00:10.0	60	70	60.9		_	61.3	61.3	59.9	59.3	58.5			1000000.0	1
71	11/17/2015	10:43:41	00d	00:10.0	61.1	71.1	62.1	60.3	_	62.2	62.2	61.1	60.2	60			1288249.6	1
72	11/17/2015	10:43:51	_	00:10.0	58.8	68.8	60.9	55.8	_	60.9	60.9	58.3	56.5	55.3			758577.6	1
73	11/17/2015	10:44:01	00d	00:10.0	52.4	62.4	55.8	50.3		54.8	54.8	51.5	50.1	50.1			173780.1	1
74	11/17/2015	10:44:11	00d	00:10.0	57.8	67.8	61.8	50.3		62.4	62.4	56.9	52.2	51			602559.6	]
75	11/17/2015	10:44:21	00d	00:10.0	62.2	72.2	64.2	60.3		64.4	64.4	61.9	60.8	59.8			1659586.9	
76	11/17/2015	10:44:31		00:10.0	60.6	70.6	61.6	59.3		61.8	61.8	60.6	59.6	58.9			1148153.6	
77	11/17/2015	10:44:41	00d	00:10.0	58.9	68.9	59.6	56.8		59.7	59.7	59.3	57	56.1			776247.1	l
78	11/17/2015	10:44:51		00:10.0	57.8	67.8	59.2	56.3	_	59.5	59.5	58	56.5	56.1			602559.6	l
79	11/17/2015	10:45:01		00:10.0	58.8	68.8	59.6		_	59.6	59.6	59.2	58	57.6			758577.6	
80	11/17/2015	10:45:11		00:10.0	57.3	67.3	58.2	56.5	_	58.6	58.6	57.2	56.9	56.4			537031.8	
81 82	11/17/2015 11/17/2015	10:45:21		00:10.0	59.8	69.8 70.8	61.9		_	62.3	62.3	60.2 60.8	57	57			954992.6 1202264.4	
83	11/17/2015	10:45:31		00:10.0 00:10.0	60.8 59.5	69.5	62.8 61.4	59 56.9	_	63.1 61.9	63.1 61.9	59.3	58.8 56.5	58.7 56	_		891250.9	
84	11/17/2015	10:45:51	_	00:10.0	56	66		51.6	-	60.6	60.6	54.3	51.6	51.2			398107.2	
85	11/17/2015	10:46:01		00:10.0	61.2	71.2	63.1	54.8	_	62.9	62.9	61.3	59.7	57.9			1318256.7	
86	11/17/2015	10:46:11	_	00:10.0	61.1	71.1	63.8		-	64.4	64.4	60.6	59.3	58.6			1288249.6	1
87	11/17/2015	10:46:21	00d	00:10.0	60.7	70.7	64.8	58.5		65.8	65.8	59	58.4	58			1174897.6	1
88	11/17/2015	10:46:31	00d	00:10.0	62.5	72.5	63.9	58.5		64	64	62.8	60.4	59.2			1778279.4	1
89	11/17/2015	10:46:41	00d	00:10.0	60.2	70.2	62.7	59.3		62.1	62.1	60	59.4	59.1			1047128.5	]
90	11/17/2015	10:46:51	00d	00:10.0	59.8	69.8	62	58.2		62.7	62.7	59	58	58			954992.6	]
91	11/17/2015	10:47:01	00d	00:10.0	56	66	60.4	53.8		58.7	58.7	55.3	53.7	53.6			398107.2	
92	11/17/2015	10:47:11	00d	00:10.0	56.1	66.1	57.1	53.8		57.3	57.3	55.9	55.7	54.7			407380.3	l
93	11/17/2015	10:47:21		00:10.0	54.8	64.8	57.1	53	_	56.7	56.7	54.4	53.1	52.8			301995.2	
94	11/17/2015	10:47:31	00d	00:10.0	59.9	69.9	62.5	56.2	_	63.1	63.1	59.4	58.7	57.9			977237.2	l
95	11/17/2015	10:47:41		00:10.0	64.8	74.8	69		_	69.9	69.9	61.9	60.2	59.4			3019951.7	ł
96	11/17/2015	10:47:51		00:10.0	62.1				_	66 58	66	-	57.6	56.8			1621810.1	
97 98	11/17/2015 11/17/2015	10:48:01	_	00:10.0 00:10.0	55.2 57.8	65.2 67.8	57.8 59		-	59.3	58 59.3	55.6 57.8	51.9 56.5	50.8 56.3			331131.1 602559.6	
98	11/17/2015	10:48:11		00:10.0	57.8	68.3			_	59.3	59.3	58.6	56.6	56.4			676083.0	1
100	11/17/2015	10:48:31	_	00:10.0	59.9	69.9			_	62.4	62.4	60.7	57.4	55.7			977237.2	1
101	11/17/2015	10:48:41		00:10.0	60.8	70.8			_	61.8	61.8	60.9	60.1	58.8			1202264.4	1
102	11/17/2015	10:48:51		00:10.0	59.2	69.2			_	61.1	61.1	59.1	58.2	58			831763.8	1
103	11/17/2015	10:49:01	00d	00:10.0	57.7	67.7	59.2			59.1	59.1	57.7	56.9	56.9			588843.7	]
104	11/17/2015	10:49:11	00d	00:10.0	57.8	67.8			_	58.9	58.9	57.5	56.7	56.7			602559.6	
105	11/17/2015	10:49:21	00d	00:10.0	57.8	67.8	60	54.3		60.3	60.3	57.6	54.3	53.6			602559.6	]
106	11/17/2015	10:49:31	00d	00:10.0	61.2	71.2	65.4	53.4		66.2	66.2	60.6	53.3	53.2			1318256.7	
107	11/17/2015	10:49:41		00:10.0	60.6	70.6			_	61.4	61.4	60.5	59.8	59.8			1148153.6	
108	11/17/2015	10:49:51		00:10.0	61.2	71.2			-	62.8	62.8	61.3	60.1	60			1318256.7	
109	11/17/2015	10:50:01		00:10.0	57.6	67.6			_	59.7	59.7	57.8	55.7	55.7	<u> </u>		575439.9	
110	11/17/2015	10:50:11		00:10.0	58.9	68.9		54.7	_	61.9	61.9	58.8	54.8	54.4			776247.1	
111	11/17/2015	10:50:21		00:10.0	51.5	61.5			_	54	54	50.9	49.7	49.2			141253.8	
112	11/17/2015	10:50:31		00:10.0	56.2	66.2			_	59.3	59.3	56.1	53.3	52.9			416869.4	
113	11/17/2015	10:50:41		00:10.0	62.6	72.6			_	67.1	67.1	61.3	59.2	58.9			1819700.9	
114	11/17/2015	10:50:51		00:10.0	63.1	73.1			_	67.7	67.7	60.7	58.1	57.9			2041737.9	
115	11/17/2015	10:51:01		00:10.0	61.3	71.3	65 56.6		-,-	65.5	65.5	60.6	56.1	55.1			1348962.9 275422.9	1
116	11/17/2015	10:51:11	_	00:10.0	54.4	64.4	56.6		-	56.8	56.8	53.6	52 56.9	51.9				ł
117 118	11/17/2015 11/17/2015	10:51:21 10:51:31		00:10.0 00:10.0	61 67.5	71 77.5	64.3 72.3		_	64.9 72.3	64.9 72.3	61.1 64.2	56.8 63.4	56.4 62.3	_		1258925.4 5623413.3	
	11/17/2015	10:51:31		00:10.0	61.9	71.9			_	63.8	63.8	62.4	58.1	57.6			1548816.6	
110		10.31.41	oou	55.10.0					_									ł
119 120	11/17/2015	10:51:51	004	00:10.0	56.3	66.3	58.9	53.6		59.2	59.2	56.3	53.9	51.9			426579.5	

Address	Start	Measur	emer	nt Time	Leq	LE	LMAX	LMIN	Lv	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overall
R6	Time																	60.1
NO							_		_									00.1
122	11/17/2015	10:52:11	00d	00:10.0	55.3	65.3	58.3	50.9		58.5	58.5	55.1	52.2	52			338844.2	
123	11/17/2015	10:52:21	00d	00:10.0	59.5	69.5	61.8	52.8		62.1	62.1	59.7	55.7	53.9			891250.9	
124	11/17/2015	10:52:31	00d	00:10.0	59	69	61.6	55.5		61.8	61.8	58.4	55.4	54.9			794328.2	
125	11/17/2015	10:52:41	00d	00:10.0	61.1	71.1	61.8	60.4		62	62	61.2	60.6	60.4			1288249.6	
126	11/17/2015	10:52:51	00d	00:10.0	62	72	63.7	58.8		64.1	64.1	62.2	59.1	57.6			1584893.2	
127	11/17/2015	10:53:01	00d	00:10.0	56.6	66.6	58.8	56.1	-,-	57.5	57.5	56.5	56.1	55.8			457088.2	1
128	11/17/2015	10:53:11	00d	00:10.0	58	68	59.3	56.1		59.9	59.9	57.9	56.7	55.1			630957.3	
129	11/17/2015	10:53:21	00d	00:10.0	64.2	74.2	69.6	55.4	-,-	70.1	70.1	61	56.2	55			2630268.0	
130	11/17/2015	10:53:31	00d	00:10.0	60.5	70.5	65	59.5		62.1	62.1	60.2	59.8	59.2			1122018.5	]
131	11/17/2015	10:53:41	00d	00:10.0	58.1	68.1	59.6	57.8		58.6	58.6	58.1	57.7	57.6			645654.2	
132	11/17/2015	10:53:51	00d	00:10.0	58.9	68.9	61.8	55.7		62.4	62.4	58.9	55.6	55.5			776247.1	
133	11/17/2015	10:54:01	00d	00:10.0	61.1	71.1	63.5	59		64	64	60.7	59.4	58.3			1288249.6	
134	11/17/2015	10:54:11	00d	00:10.0	62	72	64.9	57.8		65.2	65.2	62.2	57.9	57.4			1584893.2	
135	11/17/2015	10:54:21	00d	00:10.0	62.5	72.5	65	60.6		65.4	65.4	62	60.5	60.5			1778279.4	]
136	11/17/2015	10:54:31	00d	00:10.0	60.9	70.9	64.5	60		61.7	61.7	61.1	59.9	59.4			1230268.8	
137	11/17/2015	10:54:41	00d	00:10.0	60.8	70.8	61.7	59.6		61.8	61.8	61.2	59.9	59.3			1202264.4	1
138	11/17/2015	10:54:51	00d	00:10.0	57.4	67.4	59.6	56.3		59.2	59.2	57.5	56.5	55.9			549540.9	1

Address	Start	Measur	emer	nt Time	Leg	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overa
R7	Time	ivieasui	emei	it iiiie	Leq	LE	LIVIAA	LIVIIIN	Ly	LINI	LINZ	LINS	LIV4	LIND	Over	Olldei	iliverse Log	Leg 64.4
133	11/17/2015	10:40:01	00d	00:10.0	66.7	76.7	69.5	62.2	-,-	69.4	69.3	66.8	62.5	62.3			4677351.4	04.4
134	11/17/2015	10:40:11	00d	00:10.0	67	77	68.4	63	-,-	68.3	68.2	66.4	65.7	65.1			5011872.3	1
135	11/17/2015	10:40:21	00d	00:10.0	67.1	77.1	68.8	65.7	-,-	67.8	67.6	66.8	65.9	65.8			5128613.8	
136	11/17/2015	10:40:31	00d	00:10.0	66.8	76.8	70.7	61.1	-,-	70.6	70.4	65.9	61.7	61.4			4786300.9	
137	11/17/2015	10:40:41		00:10.0	58.2	68.2	61.9	55.6	-,-	61.8	61.6	57.6	55.8	55.7			660693.4	
138	11/17/2015	10:40:51		00:10.0	62.6	72.6	66	57.9	-,-	65.7	65.3	60.6	58	58			1819700.9	
139 140	11/17/2015 11/17/2015	10:41:01		00:10.0 00:10.0	64 64.3	74 74.3	66.6 65.1	59.7 60.6		66.5 64.9	66.4 64.8	65.1 64.3	60.1 62.1	59.9 61			2511886.4 2691534.8	
140	11/17/2015	10:41:11		00:10.0	63.6	73.6	66	61.3	-,-	65.9	65.8	63.7	61.9	61.5			2290867.7	1
142	11/17/2015	10:41:31		00:10.0	64.9	74.9	66.3	61.4	-,-	66.2	66.2	64.5	62.6	61.5			3090295.4	1
143	11/17/2015	10:41:41	00d	00:10.0	67.6	77.6	69.5	63.7	-,-	69.4	69.3	66.6	63.9	63.8			5754399.4	
144	11/17/2015	10:41:51	00d	00:10.0	64.3	74.3	69.7	59.5	-,-	69.5	69.3	62.9	60.3	60.2			2691534.8	
145	11/17/2015	10:42:01		00:10.0	64.3	74.3	65.8	58.1	-,-	65.7	65.6	64.8	58.3	58.1			2691534.8	
146	11/17/2015	10:42:11		00:10.0	64.9	74.9	66.2	62.9	-,-	66	65.9	65.1	63.8	63.2			3090295.4	
147 148	11/17/2015 11/17/2015	10:42:21		00:10.0 00:10.0	66.8 63	76.8 73	69.6 66.5	62.5 59.8		69.4	69.3 65.2	66 64	62.6 60.2	62.6 60			4786300.9 1995262.3	
140	11/17/2015	10:42:41		00:10.0	58.2	68.2	60.8	55.2	-,-	66 60.7	60.7	58	55.4	55.3			660693.4	
150	11/17/2015	10:42:51		00:10.0	57.2	67.2	57.9	56.5	-,-	57.7	57.5	57.1	56.6	56.6			524807.5	1
151	11/17/2015	10:43:01	00d	00:10.0	62.7	72.7	63.8	57.9	-,-	63.7	63.7	62.5	60.6	59			1862087.1	1
152	11/17/2015	10:43:11	00d	00:10.0	59.8	69.8	61.6	57		61.5	61.4	60.2	57.5	57.2			954992.6	
153	11/17/2015	10:43:21		00:10.0	56.6	66.6	59.9	55.1	-,-	59.4	58.8	56.9	55.6	55.3			457088.2	
154	11/17/2015	10:43:31		00:10.0	56.9	66.9	60	52.7	-,-	59.8	59.7	55.8	52.9	52.8			489778.8	
155	11/17/2015	10:43:41		00:10.0	59.3	69.3	61.7	56.1		61.6	61.5	57.8	57.1	56.6			851138.0	-
156 157	11/17/2015 11/17/2015	10:43:51 10:44:01		00:10.0 00:10.0	66 65.8	76 75.8	68.3 66.8	61.5 65.1	7/2 	68.2 66.8	68.1 66.7	65.4 65.7	61.7 65.2	61.6 65.2			3981071.7 3801894.0	1
157	11/17/2015	10:44:01		00:10.0	63.4	75.8	66.1	59.8	747 745	66	65.9	63.3	60.4	65.2			2187761.6	1
159	11/17/2015	10:44:21		00:10.0	67.2	77.2	69.1	64.4	-,-	69	68.8	67	64.9	64.7			5248074.6	
160	11/17/2015	10:44:31	_	00:10.0	66.5	76.5	67.9	64.4	-,-	67.8	67.7	66.5	65.2	64.7			4466835.9	1
161	11/17/2015	10:44:41	00d	00:10.0	60.6	70.6	64.4	57.9	-,-	64	63.7	60.9	58	57.9			1148153.6	]
162	11/17/2015	10:44:51	00d	00:10.0	56.9	66.9	60.8	51.1	-,-	60.6	60.4	56.8	51.3	51.2			489778.8	
163	11/17/2015	10:45:01		00:10.0	61.3	71.3	63.3	51.4	-,-	62.8	62.4	61.6	52.5	51.8			1348962.9	
164	11/17/2015	10:45:11		00:10.0	63.6	73.6	65.4	61.6	-,-	64.7	64.6	63.3	61.8	61.7			2290867.7	
165	11/17/2015	10:45:21		00:10.0	64.4	74.4	67	62.1	-,-	66.8	66.6	64.1	62.4	62.2			2754228.7	
166 167	11/17/2015 11/17/2015	10:45:31 10:45:41		00:10.0 00:10.0	61.3 61.6	71.3 71.6	63.4	59.6 59.5		63.3	62.9 63.2	61.1 61.3	59.7 59.5	59.7 59.5			1348962.9 1445439.8	ł
168	11/17/2015	10:45:51	_	00:10.0	67	77	69.2	63	-,-	67.6	67.5	66.5	64.6	63.2			5011872.3	1
169	11/17/2015	10:46:01		00:10.0	67.8	77.8	71.6	63.5	-,-	71.4	71.4	66.6	64.5	63.9			6025595.9	
170	11/17/2015	10:46:11	00d	00:10.0	63.9	73.9	65	62.5	-,-	64.8	64.7	63.7	62.9	62.8			2454708.9	
171	11/17/2015	10:46:21	00d	00:10.0	62.7	72.7	64	61.2	-,-	63.8	63.7	62.8	61.4	61.4			1862087.1	
172	11/17/2015	10:46:31	00d	00:10.0	65.9	75.9	66.9	62.8	-,-	66.8	66.6	66	63.6	63.1			3890451.4	
173	11/17/2015	10:46:41		00:10.0	64	74	65.9	60.7	-,-	65.6	65.4	64.5	61.9	61.3			2511886.4	
174 175	11/17/2015 11/17/2015	10:46:51 10:47:01		00:10.0 00:10.0	60 62.5	70 72.5	61.3 66.4	58.3 58.6		61.2 65.7	61.1 65.1	60.1	58.5 58.8	58.4 58.8			1000000.0 1778279.4	
176	11/17/2015	10:47:01		00:10.0	65.3	75.3	67.2	63.5		67.1	67.1	65.1	63.8	63.8			3388441.6	
177	11/17/2015	10:47:21		00:10.0	60.7	70.7	63.5	59	-,-	63.1	62.5	60.8	59.2	59			1174897.6	
178	11/17/2015	10:47:31	00d	00:10.0	64.3	74.3	65.7	61.6	-,-	65.7	65.6	63.8	62.9	62.2			2691534.8	1
179	11/17/2015	10:47:41	00d	00:10.0	65	75	66.1	62.9	-,-	66	66	64.9	63.7	63			3162277.7	
180	11/17/2015	10:47:51	00d	00:10.0	66.2	76.2	67.9	63.3	-,-	67.8	67.7	66.4	63.6	63.5			4168693.8	
181	11/17/2015	10:48:01	_	00:10.0	63.1	73.1	64.5	61.1	-,-	64.5	64.5	63	61.6	61.2			2041737.9	
182	11/17/2015 11/17/2015	10:48:11		00:10.0	65 59.7	75 69 7	66			65.9	65.9	65.4	63.5	62.8			3162277.7	-
183 184	11/17/2015	10:48:21	_	00:10.0 00:10.0	58.7 64.3	68.7 74.3	62.9 67.7	54 53.6		62.7 67.6	62.5 67.4	57.8 60.9	54.7 53.8	54.2 53.6			741310.2 2691534.8	1
184	11/17/2015	10:48:31		00:10.0	67.9	77.9	69.3	65.1	Ė	69.2	69.1	68.4	65.3	65.2			6165950.0	1
186	11/17/2015	10:48:51		00:10.0	64.4	74.4	68.3	59.6	-,-	67.7	67.2	65.1	61.2	60.3			2754228.7	1
187	11/17/2015	10:49:01	_	00:10.0	54.4	64.4	59.6	52.5	÷	58.8	58.1	54.6	52.9	52.8			275422.9	
188	11/17/2015	10:49:11	00d	00:10.0	58.3	68.3	60.8	52.4	-,-	60.6	60.2	58	53	52.6			676083.0	
189	11/17/2015	10:49:21	_	00:10.0	58.3	68.3	61.1	56		60.3	59.9	57.9	56.1	56			676083.0	
190	11/17/2015	10:49:31		00:10.0	63	73	64.5	60.6		64.2	64.1	63.2	61.4	61.1			1995262.3	1
191 192	11/17/2015 11/17/2015	10:49:41 10:49:51	_	00:10.0 00:10.0	63.8 64.3	73.8 74.3	66 65.8	59.7 62.2	747 	65.8 65.6	65.7 65.5	63.8 64.3	60 62.9	59.9 62.5			2398832.9 2691534.8	ł
192	11/17/2015	10:49:51	_	00:10.0	69.3	79.3	71.4	63.6		71.3	71.3	69.3	63.8	63.8	<u> </u>		8511380.4	1
193	11/17/2015	10:50:11		00:10.0	61.6	79.5	68.6	59		67.2	65.9	62.6	59.5	59.2			1445439.8	1
195	11/17/2015	10:50:21		00:10.0	67.9	77.9	69.9	59.3	-,-	69.8	69.7	67.2	63.7	61.1			6165950.0	1
196	11/17/2015	10:50:31	00d	00:10.0	67.8	77.8	69.7	65.1	-,-	69.6	69.4	67.8	65.7	65.4			6025595.9	]
197	11/17/2015	10:50:41	00d	00:10.0	61	71	65.1	58.8	-,-	64.7	64.6	60.2	58.9	58.9			1258925.4	
198	11/17/2015	10:50:51		00:10.0	61.1	71.1	63.1	59.7	-,-	62.8	61.8	60.5	60	59.9			1288249.6	
199	11/17/2015	10:51:01		00:10.0	64.6	74.6	65.3	63.1		65.3	65.2	64.6	63.5	63.5			2884031.5	
200	11/17/2015	10:51:11		00:10.0	63.5	73.5	65.8	59.6	-	65.6	65.4	63.8	60	59.7			2238721.1	1
201 202	11/17/2015 11/17/2015	10:51:21		00:10.0 00:10.0	61.8	71.8 71	64.6 62.9	57.6 57.7	-	64.5 62.6	64.3 62.3	62.2 61.2	58.6 58.3	58 57.8			1513561.2 1258925.4	1
	11/17/2015	10:51:31	_	00:10.0	61 61.2	71.2	62.9	57.7	-v- -v-	62.6 62.7	62.6	61.2	58.3 58.8	57.8			1318256.7	1
203		10.01.41	Jou	50.10.0					H						<del>                                     </del>			1
203 204	11/17/2015	10:51:51	00d	00:10.0	65.4	75.4	68	60.6	-,-	67.8	67.6	65.1	60.9	60.8			3467368.5	

									_									
Address	Start Time	Measur	emen	nt Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overall Leg
R7																		64.4
206	11/17/2015	10:52:11	00d	00:10.0	63.1	73.1	65.1	60.5	-,-	65	64.9	63.2	61.1	60.7			2041737.9	
207	11/17/2015	10:52:21	00d	00:10.0	66.4	76.4	67.2	62.7	-,-	67.1	67	66.6	64.8	63.6			4365158.3	
208	11/17/2015	10:52:31	00d	00:10.0	66.2	76.2	67	65.3	-,-	66.9	66.7	66.1	65.7	65.5			4168693.8	
209	11/17/2015	10:52:41	00d	00:10.0	63.1	73.1	65.9	59.4	-,-	65.4	65	63.4	59.5	59.5			2041737.9	
210	11/17/2015	10:52:51	00d	00:10.0	61.2	71.2	65	58.2	-,-	64.5	64	61.8	58.9	58.4			1318256.7	
211	11/17/2015	10:53:01	00d	00:10.0	60.4	70.4	63.6	55.6	-,-	63.2	62.9	59	55.9	55.8			1096478.2	
212	11/17/2015	10:53:11	00d	00:10.0	57.2	67.2	63.6	51.9	-,-	63.2	62.7	55.6	52.1	52			524807.5	
213	11/17/2015	10:53:21	00d	00:10.0	62.6	72.6	65.5	57.8	-,-	65.3	65.1	61.2	59.4	59.2			1819700.9	
214	11/17/2015	10:53:31	00d	00:10.0	62.2	72.2	63.9	60.4	-,-	63.8	63.8	61.6	60.6	60.5			1659586.9	
215	11/17/2015	10:53:41	00d	00:10.0	62.6	72.6	64.4	61	-,-	64.2	64.1	62.2	61.2	61			1819700.9	1
216	11/17/2015	10:53:51	00d	00:10.0	63.1	73.1	64.5	61.7	-,-	64.4	64.2	62.9	61.9	61.8			2041737.9	1
217	11/17/2015	10:54:01	00d	00:10.0	66.4	76.4	67.5	64.5	-,-	67.5	67.4	66.2	65	64.9			4365158.3	
218	11/17/2015	10:54:11	00d	00:10.0	69.6	79.6	72.2	64.9	-,-	72.1	72.1	68	65.2	65.1			9120108.4	1
219	11/17/2015	10:54:21	00d	00:10.0	69.7	79.7	73.3	66.3	-,-	73.1	72.7	68.6	66.6	66.4			9332543.0	]
220	11/17/2015	10:54:31	00d	00:10.0	67.1	77.1	72.8	60.7	-,-	72.1	70.8	68.9	62.3	61.5			5128613.8	
221	11/17/2015	10:54:41	00d	00:10.0	59.5	69.5	63.8	54.6	-,-	63.4	63	57.3	54.9	54.7			891250.9	]
222	11/17/2015	10:54:51	00d	00:10.0	64.4	74.4	66.4	62.8	-,-	66.3	66.1	63.9	63.1	62.9			2754228.7	1

Address	Start	Measur	emer	nt Time	Leg	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overall
	Time	IVICUSUI	Cilici	it iiiic	LCY		LIVIPOX	LIVIIIV	-7	-141	-14-		-14-7		OVC.	Onaci	mverse Log	Leq
R8	44 /47 /2045	10.10.00	004	00.10.0	04	01	0.0	70.2	Т	05.7	04.0	70.0	72.4	71.4			125902541.2	63.3
70		10:40:06		00:10.0	81	91	86			85.7	84.9	78.9	72.4	71.4			125892541.2	
71 72	11/17/2015 11/17/2015	10:40:16 10:40:26		00:10.0 00:10.0	67.3 60.3	77.3 70.3	77.7 61.5	61.4 59.6		76.7 61.4	75.5 61.3	65.7 60.1	61.7 59.7	61.5 59.7			5370318.0 1071519.3	
72	11/17/2015	10:40:36		00:10.0	62.7	72.7	65.6	59.2		65.5	65.3	62.3	59.7	59.5			1862087.1	
74		10:40:46		00:10.0	60.1	70.1	61.4	59		61.3	61.3	59.5	59.2	59.2			1023293.0	
75		10:40:56		00:10.0	59.8	69.8	61.6		_	61.3	60.8	59.5	59	58.9			954992.6	
76	11/17/2015	10:41:06	00d	00:10.0	59.7	69.7	61.2	58.4	-,-	61	60.9	59.2	58.6	58.5			933254.3	
77	11/17/2015	10:41:16	00d	00:10.0	60.4	70.4	61.3	59.7	-,-	61.2	60.9	60.5	60.2	60			1096478.2	
78		10:41:26	_	00:10.0	60.1	70.1	60.7	59.1	_	60.6	60.6	60.2	59.4	59.4			1023293.0	
79		10:41:36		00:10.0	58.9	68.9	59.6		_	59.5	59.3	58.8	58.4	58.4			776247.1	
80 81	11/17/2015 11/17/2015	10:41:46 10:41:56		00:10.0 00:10.0	59.1 58.6	69.1 68.6	59.1	58.2 58.2	~-	60 59	59.9 59	59.1 58.7	58.3 58.3	58.3 58.3			812830.5 724436.0	
82	11/17/2015	10:41:36		00:10.0	59.9	69.9	60.7	58.3		60.6	60.4	59.9	58.6	58.6			977237.2	
83	11/17/2015	10:42:16		00:10.0	59.6	69.6	62.1	56.4	-,-	62	61.8	60	56.8	56.5			912010.8	
84	11/17/2015	10:42:26	00d	00:10.0	55.3	65.3	56.7	54	-,-	56.6	56.5	55.4	54.5	54.2			338844.2	
85	11/17/2015	10:42:36	00d	00:10.0	54.1	64.1	54.6	53.3	-,-	54.6	54.5	53.9	53.5	53.4			257039.6	
86	11/17/2015	10:42:46	00d	00:10.0	57.5	67.5	59.1	54.6	-,-	59	58.9	57.2	54.8	54.7			562341.3	
87	11/17/2015	10:42:56		00:10.0	57.9	67.9	58.9	56.6	-,-	58.9	58.8	57.5	56.7	56.6			616595.0	
88		10:43:06		00:10.0	60.2	70.2	62.3	58.2	_	62.2	62	60	58.3	58.3			1047128.5	
89	11/17/2015	10:43:16		00:10.0	57.1	67.1	60.2	55.6		59.5	59.1	57.5	55.8	55.8			512861.4	
90 91	11/17/2015 11/17/2015	10:43:26 10:43:36		00:10.0 00:10.0	55.4 55.9	65.4 65.9	56.9 56.9	54.6 54.7	20	56.5 56.9	56.2 56.7	55.3 55.6	54.7 55.1	54.7 55			346736.9 389045.1	
91	11/17/2015	10:43:46		00:10.0	56.6	66.6	57.5	55.7		57.4	57.3	56.3	55.1	55.8	_		457088.2	
93	11/17/2015	10:43:56	_	00:10.0	56.8	66.8	58.3	55.3		58.1	58	56.9	55.5	55.4	_		478630.1	
94	11/17/2015	10:44:06	00d	00:10.0	55.7	65.7	56.8	54.4	-,-	56.7	56.5	55.9	54.9	54.5			371535.2	
95	11/17/2015	10:44:16	00d	00:10.0	55.2	65.2	56.5	53.8	-,-	56.4	56.3	55.1	53.9	53.9			331131.1	
96		10:44:26		00:10.0	53.6	63.6		53.2	_	54.6	54.2	53.6	53.3	53.3			229086.8	
97	11/17/2015	10:44:36		00:10.0	62.8	72.8	65.7	53.6		65.1	65	62.1	54.3	53.8			1905460.7	
98	11/17/2015	10:44:46		00:10.0	63.6	73.6	67.2	61.1		67	66.7	62.8	61.3	61.2			2290867.7	
99 100	11/17/2015 11/17/2015	10:44:56 10:45:06		00:10.0 00:10.0	58.1 57.7	68.1 67.7	61.5 59	56.2 56.2	7.7	61.1 58.9	60.6 58.9	58.4 56.8	56.6 56.5	56.4 56.3			645654.2 588843.7	
101	11/17/2015	10:45:16		00:10.0	59.7	69.7	61.5	58.6	-,-	61.4	61.1	58.9	58.7	58.6			933254.3	
102	11/17/2015	10:45:26		00:10.0	60.6	70.6	63.2	58.1	-,-	63.1	63.1	60.4	58.2	58.2			1148153.6	
103	11/17/2015	10:45:36	00d	00:10.0	58	68	59.4	56.9	-,-	59.2	59	58.1	57.1	57			630957.3	
104	11/17/2015	10:45:46	00d	00:10.0	55.5	65.5	57.6	53.6	-,-	57.3	57.1	56.2	53.9	53.9			354813.4	
105	11/17/2015	10:45:56		00:10.0	54.3	64.3	55.4	53.5	_	55.3	55.3	53.9	53.6	53.6			269153.5	
106	11/17/2015	10:46:06		00:10.0	57.9	67.9	59.2	55	_	59.2	59	57.8	55.1	55.1			616595.0	
107 108	11/17/2015 11/17/2015	10:46:16 10:46:26		00:10.0 00:10.0	58.1 56.9	68.1 66.9	59.3 57.7	57.1 55.9	_	59.2 57.6	59.2 57.5	58.2 57.1	57.5 56.2	57.2 56			645654.2 489778.8	
108	11/17/2015	10:46:36		00:10.0	56.9	67	58.6	55.5	_	58.5	58.4	56.1	55.7	55.6			501187.2	
110	11/17/2015	10:46:46		00:10.0	58.3	68.3	59.2	57.6	_	59	59	58.2	57.7	57.7			676083.0	
111	11/17/2015	10:46:56	00d	00:10.0	57	67	58	56.4	-,-	57.9	57.6	57	56.5	56.5			501187.2	
112	11/17/2015	10:47:06	00d	00:10.0	58.3	68.3	58.8	57	-,-	58.6	58.6	58.4	57.2	57.1			676083.0	
113	11/17/2015	10:47:16	00d	00:10.0	60.3	70.3	62.2	58.2	-,-	62.2	62	59.9	58.6	58.5			1071519.3	
114	11/17/2015	10:47:26		00:10.0	56.9	66.9	58.2	56.6		57.8	57.4	56.9	56.7	56.7			489778.8	
115	11/17/2015	10:47:36		00:10.0	59.4	69.4	61.9	56.5	-,-	61.7	61.2	58.9	56.9	56.6			870963.6	
116 117	11/17/2015 11/17/2015	10:47:46 10:47:56		00:10.0 00:10.0	57.8 55.6	67.8 65.6	59.4 58.6	56.3 53.7	7.7	59.4 58.2	59.1 58	57.2 55.9	56.6 54.3	56.4 53.9			602559.6 363078.1	
118		10:48:06	_	00:10.0	53.2	63.2	55		_	54.7	54.7	53		51.8			208929.6	
119		10:48:16	_	00:10.0	52.5	62.5	53.4			53.3	53.1	52.4	51.9	51.9			177827.9	
120		10:48:26	00d	00:10.0	52.6	62.6	53.7			53.7	53.6	52.5	51.5	51.4			181970.1	
121		10:48:36	_	00:10.0	52.6	62.6			_	53.8	53.4	52.1	51.4	51.3			181970.1	
122	11/17/2015	10:48:46		00:10.0	59.1	69.1	61.7	54	_	61.6	61.4	58	54.9	54.5			812830.5	
123	11/17/2015	10:48:56		00:10.0	61.9	71.9		57.5		64 73.6	63.9	60.8	57.7	57.6			1548816.6	
124 125		10:49:06 10:49:16	_	00:10.0 00:10.0	66.9 57.8	76.9 67.8	74.1 59.5	59.5 56.9		73.6 59.3	72.2 59.2	61.8 57.6	60.2 57	60 57			4897788.2 602559.6	
125		10:49:16	_	00:10.0	57.8	68.6		55.7	_	59.3	59.2	57.6	56.1	56			724436.0	
127		10:49:36	_	00:10.0	60.1	70.1	64		_	63.7	62.8	59.5	57.6	57.3			1023293.0	
128		10:49:46	_	00:10.0	58.7	68.7	59.7	55.9	_	59.7	59.6	59	57.2	56.5			741310.2	
129	11/17/2015	10:49:56	00d	00:10.0	52.8	62.8	55.9	51	-,-	55.2	54.8	53.3	51.9	51.5			190546.1	
130		10:50:06	_	00:10.0	56.2	66.2	58.5	50.6	_	58.4	57.9	54.7	50.9	50.8			416869.4	
131	11/17/2015	10:50:16	_	00:10.0	55.5	65.5	58.5	53.9	_	58.1	57.8	55.4	54.2	54			354813.4	
132	11/17/2015	10:50:26	_	00:10.0	56.8	66.8		55.5	_	57.3	57.2	56.7	56.2	56			478630.1	
133 134		10:50:36 10:50:46	_	00:10.0 00:10.0	55.4 55.1	65.4 65.1	58.8 56.2	52.8 52.3	_	58.4 56.1	58.1 56.1	54.4 55.2	53.1 52.4	53 52.4			346736.9 323593.7	
134		10:50:46		00:10.0	57.9	67.9	60.5	55.4	_	60.1	59.2	56.2	55.6	55.5	Ė		616595.0	
136		10:51:06		00:10.0	62.7	72.7	65.2	60.4		64.6	64	62.3	61.5	61.4			1862087.1	
137		10:51:16	_	00:10.0	59.3	69.3	62			61.6	61.1	59.5	57.6	57.6			851138.0	
138		10:51:26	_	00:10.0	57.8	67.8		56.9	_	58.2	58.2	57.8	57.2	57			602559.6	
139	11/17/2015	10:51:36	00d	00:10.0	56.1	66.1	56.9	55.7	-,-	56.7	56.6	56	55.8	55.8			407380.3	
140	11/17/2015	10:51:46	_	00:10.0	56.2	66.2	57.6	55.6		57.5	57.4	56.1	55.8	55.7			416869.4	
141	11/17/2015	10:51:56	_	00:10.0	60.7	70.7	65.8			65.2	64.5	59	55.4	55.4			1174897.6	
142 143	11/17/2015	10:52:06	_	00:10.0	56.2	66.2	58.3	54.7		57.7	57.5	56.2	54.9	54.7			416869.4 323593.7	
	11/17/2015	10:52:16	oou	00:10.0	55.1	65.1	57.4	53.8	<u> </u>	57.3	57.2	55	54.6	54.1			J2JJJJ.1	

Address	Start Time	Measur	emen	nt Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overall Lea
R8																		63.3
144	11/17/2015	10:52:26	00d	00:10.0	54	64	55.6	53.2		55.4	55	53.8	53.4	53.4			251188.6	
145	11/17/2015	10:52:36	00d	00:10.0	52.8	62.8	54	51.8		53.9	53.6	52.9	52.2	51.9			190546.1	
146	11/17/2015	10:52:46	00d	00:10.0	55	65	56.5	51.7		56.5	56.4	54.3	52	51.8			316227.8	
147	11/17/2015	10:52:56	00d	00:10.0	56	66	56.6	55.3		56.6	56.5	56	55.4	55.4			398107.2	
148	11/17/2015	10:53:06	00d	00:10.0	60.3	70.3	62.9	55.4		62.8	62.4	58.3	56	55.7			1071519.3	
149	11/17/2015	10:53:16	00d	00:10.0	61.5	71.5	63.5	58.8		63.5	63.4	61.8	59.4	59.1			1412537.5	
150	11/17/2015	10:53:26	00d	00:10.0	57.6	67.6	58.9	57.3		58.7	58.3	57.6	57.4	57.3			575439.9	
151	11/17/2015	10:53:36	00d	00:10.0	57.5	67.5	58	56.9		57.9	57.8	57.4	57.1	57			562341.3	
152	11/17/2015	10:53:46	00d	00:10.0	60.2	70.2	62.6	57.2		62.5	61.9	59.1	57.8	57.5			1047128.5	
153	11/17/2015	10:53:56	00d	00:10.0	58.6	68.6	61.9	56.2		61.7	61.4	58	56.8	56.6			724436.0	
154	11/17/2015	10:54:06	00d	00:10.0	55.5	65.5	56.5	54.2		56.3	56.2	56	54.4	54.3			354813.4	
155	11/17/2015	10:54:16	00d	00:10.0	53.6	63.6	55.3	52.3		54.5	54.3	53.6	52.6	52.4			229086.8	
156	11/17/2015	10:54:26	00d	00:10.0	54.4	64.4	55.3	53.7		55.2	55.1	54.3	53.8	53.7			275422.9	
157	11/17/2015	10:54:36	00d	00:10.0	55	65	56	54		56	55.9	54.8	54.2	54			316227.8	
158	11/17/2015	10:54:46	00d	00:10.0	56.8	66.8	57.5	54.7		57.3	57.2	57	55	55			478630.1	
159	11/17/2015	10:54:56	00d	00:10.0	59	69	61.2	57.4		60.9	60.1	58.1	57.8	57.7			794328.2	

Address	Start	Measur	emer	nt Time	Leg	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Over
	Time	ivicasui	Cilici	it iiiie	Leq		LIVIAA	LIVIIIV	Ly	LIVI	LIVE	LING	LIVY	LING	Ovei	Onder	iliverse Log	Leo
R9	44 (47 (2045	44.40.04	00.1	00.40.0						E4.0	E2.6			F2.5	Ī	Ì	100526.2	58.
85	11/17/2015	11:40:04	_	00:10.0		63		52.4		54.3	53.6	53	52.7	52.6			199526.2 316227.8	ł
86 87	11/17/2015 11/17/2015	11:40:14 11:40:24	_	00:10.0 00:10.0	55 57	65 67	55.9 58.7	53.6 54.8	-	55.6 58.6	55.5 58.4	54.8 57.1	54 55.4	53.7 55.1			501187.2	ł
88	11/17/2015	11:40:34		00:10.0	55.5	65.5	56.5	54		56.4	56.3	55.2	54.3	54.2			354813.4	1
89	11/17/2015	11:40:44		00:10.0	53.9	63.9	56.7	50.2		56.6	56.3	54.1	51.1	50.7			245470.9	1
90	11/17/2015	11:40:54	_	00:10.0	52.1	62.1	53.3	49.9	-	53.1	52.8	52	50.1	50			162181.0	1
91	11/17/2015	11:41:04	00d	00:10.0	55.1	65.1	57.6	52	-,-	57.5	57.4	53.3	52.3	52.1			323593.7	1
92	11/17/2015	11:41:14	00d	00:10.0	59	69	59.8	57.6	-,-	59.6	59.5	58.8	58	58			794328.2	
93	11/17/2015	11:41:24	00d	00:10.0	62.4	72.4	65.2	58.9	-,-	65	64.8	60.9	59.1	59			1737800.8	
94	11/17/2015	11:41:34	00d	00:10.0	61	71	64.5	56.5	-,-	64.1	64	60.9	57.7	57			1258925.4	
95	11/17/2015	11:41:44	00d	00:10.0	56.2	66.2	56.7	55.1	-,-	56.7	56.6	56.2	55.3	55.2			416869.4	
96	11/17/2015	11:41:54		00:10.0	59.2	69.2	59.9	56.7	-,-	59.8	59.7	59.1	57.9	57.6			831763.8	ł
97	11/17/2015	11:42:04		00:10.0	60	70	61.7	58.7	-,-	61.6	61.4	59.6	58.9	58.8			1000000.0	ł
98 99	11/17/2015 11/17/2015	11:42:14 11:42:24		00:10.0 00:10.0	58.8 53.8	68.8 63.8	60.1 55.8	55.8 52.4		59.9 55.2	59.8 54.9	59.3 53.9	56.8 52.6	56.3 52.5			758577.6 239883.3	ł
100	11/17/2015	11:42:34		00:10.0	57.1	67.1	58.6	54.9		58.5	58.4	55.9	55.3	55.1			512861.4	ł
101	11/17/2015	11:42:44		00:10.0	52.6	62.6	54.9	49.3	-,-	54.7	54.3	53.4	50.3	49.8			181970.1	1
102	11/17/2015	11:42:54		00:10.0	47.9	57.9	49.3	47.3	-,-	48.9	48.7	48.1	47.5	47.4			61659.5	1
103	11/17/2015	11:43:04	00d	00:10.0	51.1	61.1	55.3	47.1	-,-	54.3	53.4	48.4	47.2	47.2			128825.0	1
104	11/17/2015	11:43:14	00d	00:10.0	59	69	60.4	55.3	-,-	60.3	60.3	58.8	57.5	56.9			794328.2	1
105	11/17/2015	11:43:24	00d	00:10.0	60.5	70.5	63.6	55.8	-,-	63.5	63.3	60	56	55.9			1122018.5	]
106	11/17/2015	11:43:34	00d	00:10.0	56.1	66.1	58.3	54	-,-	57.3	56.7	55.9	54.3	54.1			407380.3	
107	11/17/2015	11:43:44	00d	00:10.0	65.1	75.1	69.3	58.3	-,-	69.2	68.7	62.3	59.8	59.1			3235936.6	1
108	11/17/2015	11:43:54		00:10.0	61.1	71.1	65.8	60.4	-,-	64.7	63.7	61.3	60.7	60.6	<u> </u>		1288249.6	1
109	11/17/2015	11:44:04		00:10.0	59.2	69.2	61.8	57.4	-,-	61.3	60.6	58.6	57.6	57.5	<u> </u>		831763.8	1
110	11/17/2015	11:44:14	_	00:10.0	58.5	68.5	62.3	56	-,-	62.3	62.1	57.5	56.2	56.2	<del></del>	<del></del>	707945.8	1
111	11/17/2015	11:44:24	00d	00:10.0	55.1	65.1	56.8	53.1		56.7	56.7	55.5	53.3	53.2			323593.7	ł
112 113	11/17/2015 11/17/2015	11:44:34 11:44:44		00:10.0 00:10.0	55.7 51	65.7 61	57.4 56.7	52.4 47.3	-	57.3 56.4	57.2 56	54.9 50.5	52.6 47.6	52.5 47.4			371535.2 125892.5	ł
114	11/17/2015	11:44:54	_	00:10.0	53.2	63.2	56	47.3	-,-	56	55.8	52.1	47.3	47.4			208929.6	1
115	11/17/2015	11:45:04	_	00:10.0	51.5	61.5	54.9	50.6	-,-	53.8	52.7	52	50.7	50.7			141253.8	1
116	11/17/2015	11:45:14		00:10.0	54.4	64.4	55.9	50.5	-,-	55.7	55.2	54.6	51	50.6			275422.9	1
117	11/17/2015	11:45:24	00d	00:10.0	59.8	69.8	62.1	55.8	-,-	62	61.7	58.7	56	55.9			954992.6	1
118	11/17/2015	11:45:34	00d	00:10.0	60.8	70.8	63	59.2	-,-	62.9	62.7	60.6	59.4	59.3			1202264.4	1
119	11/17/2015	11:45:44	00d	00:10.0	58.6	68.6	60.2	56.9	-,-	60	59.7	58.6	57	56.9			724436.0	]
120	11/17/2015	11:45:54	00d	00:10.0	56.9	66.9	60.3	55.5	-,-	60.2	60.2	56.3	55.7	55.6			489778.8	
121	11/17/2015	11:46:04		00:10.0	57.2	67.2	58.2	56		58.1	58	56.9	56.2	56.2			524807.5	
122	11/17/2015	11:46:14		00:10.0	55.7	65.7	57.6	54		57.6	57.4	55.9	54.1	54			371535.2	l
123	11/17/2015	11:46:24		00:10.0	54	64	54.5	53.2		54.4	54.4	54.1	53.4	53.3			251188.6	ł
124 125	11/17/2015 11/17/2015	11:46:34 11:46:44		00:10.0 00:10.0	54.6 59.2	64.6 69.2	57.1 60	52.9 57.1	-,-	56.8 59.8	56.3 59.7	53.5 59.2	53 57.7	53 57.4			288403.2 831763.8	ł
125	11/17/2015	11:46:54		00:10.0	57.5	67.5	59.8	54.9		59.6	59.5	57.5	55.1	55			562341.3	1
127	11/17/2015	11:47:04		00:10.0	57.2	67.2	58.3	55	-,-	58.1	58	57.3	55.5	55.2			524807.5	1
128	11/17/2015	11:47:14		00:10.0	59.3	69.3	62	55.1	-,-	61.8	61.7	57.6	55.5	55.5			851138.0	1
129	11/17/2015	11:47:24	00d	00:10.0	60.4	70.4	61.6	58.8	-,-	61.5	61.4	60.8	58.9	58.9			1096478.2	1
130	11/17/2015	11:47:34	00d	00:10.0	58.9	68.9	59.7	58.1	-,-	59.6	59.5	59	58.3	58.2			776247.1	]
131	11/17/2015	11:47:44	00d	00:10.0	60.1	70.1	61.2	58.9	-,-	61.1	61	59.7	59	58.9			1023293.0	
132		11:47:54		00:10.0	58.7	68.7	60.9	57	-	60.8	60.8	58.4	57.1	57.1			741310.2	
133	11/17/2015	11:48:04		00:10.0	57.8	67.8		56.1		59.1	59	58.1	56.6	56.2	<u> </u>		602559.6	l
134		11:48:14		00:10.0	55.8	65.8	56.6	55.1		56.5	56.4	55.9	55.2	55.2	<del></del>		380189.4	ł
135	11/17/2015 11/17/2015	11:48:24	_	00:10.0 00:10.0	54 52.6	64	55.2	52.8	-	54.9	54.8	54.5	53.1	53.1	<del></del>		251188.6 181970.1	ł
136 137	11/17/2015 11/17/2015	11:48:34 11:48:44		00:10.0	52.6 55.4	62.6 65.4	55.1 56.2	50 54.6		54.6 56.1	53.9 56.1	52.2 55.3	50.1 54.7	50 54.7			181970.1 346736.9	ł
138	11/17/2015	11:48:54	_	00:10.0	53.4	63.9	55.2	51.7	-,-	55.1	55.1	54.7	52.2	54.7			245470.9	1
139	11/17/2015	11:49:04		00:10.0	56.1	66.1	58.3	51.6	-,-	58.2	58.1	54.9	51.8	51.7			407380.3	1
140	11/17/2015	11:49:14	_	00:10.0	56.8	66.8	58.6	54.8	-	58.3	58.1	56.6	54.9	54.9			478630.1	1
141	11/17/2015	11:49:24		00:10.0	58.9	68.9	59.3	58.4		59.2	59.2	59	58.6	58.6			776247.1	]
142	11/17/2015	11:49:34	00d	00:10.0	59.5	69.5	61.1	57.2	-,-	61	60.9	59.8	57.5	57.3			891250.9	
143	11/17/2015	11:49:44	00d	00:10.0	60.3	70.3	61.5	59.5	-,-	61.3	61.1	60.2	59.6	59.5			1071519.3	
144	11/17/2015	11:49:54	00d	00:10.0	59.4	69.4	61	58.3	-,-	60.5	60.1	59.3	58.4	58.4			870963.6	
145	11/17/2015	11:50:04		00:10.0	58	68	61.3	54.1	-,-	61.1	61	58	54.2	54.2	<u> </u>	<u> </u>	630957.3	l
146	11/17/2015	11:50:14		00:10.0	56.1	66.1	57.1	54.1	-,-	57	56.9	56.4	54.6	54.2			407380.3	ł
147	11/17/2015	11:50:24		00:10.0	54.5	64.5	56.6	52.8		56.2	55.8	54	53	52.9	<del> </del>	<u> </u>	281838.3	ł
148		11:50:34		00:10.0	59.8	69.8	62.1	55.6		62	62	59.3	57.1	56.6			954992.6 676092.0	ł
149		11:50:44		00:10.0		68.3	59.4	54.5		59.9 59.3	59.6	58.3	54.7 57.5	54.6			676083.0 676083.0	ł
150 151	11/17/2015 11/17/2015	11:50:54 11:51:04		00:10.0 00:10.0	58.3 54.4	68.3 64.4	59.4 59	57.2 51		59.3 58.7	59.3 58	58.2 54.3	57.5 51.4	57.3 51.2			275422.9	ł
151	11/17/2015	11:51:04		00:10.0	54.4 56.9	66.9	58.3	52.7		58.7	58 58.2	54.3	51.4 54.3	51.2 53.4			489778.8	1
153	11/17/2015	11:51:14		00:10.0	59.4	69.4	61.1	56.1	-,-	61	60.9	55.6	56.3	56.2			870963.6	1
154	11/17/2015	11:51:34		00:10.0	62.9	72.9	66.8	59.7	-,-	66.4	66.3	60.9	59.8	59.8			1949844.6	1
155	11/17/2015	11:51:44		00:10.0	62	72		60.9	-,-	64.1	64	62.1	61.1	61			1584893.2	1
156		11:51:54		00:10.0	56	66	61	54.4	-,-	60.3	59.7	55.5	54.6	54.5			398107.2	]
157	11/17/2015	11:52:04	00d	00:10.0	58.8	68.8	61.3	55.9	-,-	61.1	61.1	57.6	56.1	56			758577.6	]
	11/17/2015	11:52:14	004	00:10.0	57.7	67.7	58.9	56.6	I	58.5	58.3	57.9	56.8	56.7			588843.7	

	Start																	Overall
Address	Time	Measur	emen	nt Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Lea
R9																		58.1
159	11/17/2015	11:52:24	00d	00:10.0	54.3	64.3	57.6	51.5	-,-	57.2	57.1	53.8	51.7	51.6			269153.5	
160	11/17/2015	11:52:34	00d	00:10.0	52.8	62.8	53.8	51.6	-,-	53.6	53.5	52.9	51.9	51.7			190546.1	
161	11/17/2015	11:52:44	00d	00:10.0	54.3	64.3	54.8	53.3		54.7	54.7	54.4	53.8	53.7			269153.5	
162	11/17/2015	11:52:54	00d	00:10.0	56.4	66.4	60	53		59.4	59	54.6	53.2	53.1			436515.8	
163	11/17/2015	11:53:04	00d	00:10.0	60.5	70.5	63.8	54.5		63.7	63.5	60.4	55.4	54.8			1122018.5	
164	11/17/2015	11:53:14	00d	00:10.0	56.6	66.6	57.5	54.5	-,-	57.5	57.4	56.8	54.9	54.8			457088.2	
165	11/17/2015	11:53:24	00d	00:10.0	63	73	66.2	55.9	-,-	66	65.7	60.9	56.4	56.1			1995262.3	
166	11/17/2015	11:53:34	00d	00:10.0	60.8	70.8	65	59.4	-,-	64.7	64.6	59.9	59.5	59.4			1202264.4	
167	11/17/2015	11:53:44	00d	00:10.0	59	69	60	57.9	-,-	59.8	59.7	59	58.1	58			794328.2	
168	11/17/2015	11:53:54	00d	00:10.0	60.6	70.6	61	59.2	-,-	60.9	60.9	60.6	60	59.7			1148153.6	
169	11/17/2015	11:54:04	00d	00:10.0	56	66	59.4	55.3	-,-	58.9	58.3	56	55.4	55.4			398107.2	
170	11/17/2015	11:54:14	00d	00:10.0	55.7	65.7	57.2	53.9	-,-	57.1	57	55.9	54.2	54.1			371535.2	
171	11/17/2015	11:54:24	00d	00:10.0	54.4	64.4	55.4	53.6		55.3	55.2	54	53.6	53.6			275422.9	
172	11/17/2015	11:54:34	00d	00:10.0	52.4	62.4	55.3	50.9	-,-	55.1	54.8	52	51.2	51.1			173780.1	
173	11/17/2015	11:54:44	00d	00:10.0	52.4	62.4	55.2	49.5	-,-	55.1	55	50.8	49.8	49.7			173780.1	
174	11/17/2015	11:54:54	00d	00:10.0	52.2	62.2	54.7	51.5	-,-	53.7	53	52.4	51.6	51.5			165958.7	

Address	Start	Measur	emen	nt Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overa
R10	Time				•												0	Leq 62.9
107	11/17/2015	11:40:09	00d	00:10.0	65.6	75.6	67.3	63.2		67.2	67.1	65.7	63.8	63.5			3630780.5	02.9
108	11/17/2015	11:40:19		00:10.0	59.3	69.3	63.2	57.5		62.7	62.3	59.5	58.4	57.8			851138.0	
109	11/17/2015	11:40:29		00:10.0	59.8	69.8	61.4	56.4		61.3	61.2	59.4	57	56.6			954992.6	
110	11/17/2015	11:40:39		00:10.0	63.6	73.6	66.5	57.1		66.4	66.3	60.8	57.3	57.2			2290867.7	
111	11/17/2015	11:40:49	00d	00:10.0	64.7	74.7	66.4	64	-,-	66.1	65.8	64.6	64.2	64.1			2951209.2	
112	11/17/2015	11:40:59	00d	00:10.0	66	76	67.5	64.3	-,-	67.4	67.3	65.9	64.6	64.5			3981071.7	
113	11/17/2015	11:41:09	00d	00:10.0	63.2	73.2	64.6	61.3		64.3	64.3	64	61.5	61.4			2089296.1	
114	11/17/2015	11:41:19		00:10.0	60.1	70.1	61.8	58.8		61.7	61.5	60.2	59	58.9			1023293.0	
115	11/17/2015	11:41:29		00:10.0	62.1	72.1	63.1	58.8		63	62.9	62.4	59	58.9			1621810.1	
116	11/17/2015	11:41:39		00:10.0	62.2	72.2	63.3	59.8	-	63.2	63.2	62.5	60.2	60			1659586.9	
117 118	11/17/2015 11/17/2015	11:41:49 11:41:59		00:10.0 00:10.0	61.8 63.6	71.8 73.6	63 65.2	59.7 60.3		62.9 65.1	62.9 64.9	62.1 63.5	60.7	59.9 60.5			1513561.2 2290867.7	
119	11/17/2015	11:42:09	_	00:10.0	63.8	73.8	64.9	62.3		64.8	64.8	63.7	62.5	62.4	_		2398832.9	
120	11/17/2015	11:42:19		00:10.0	62	73.0	63.8	58.8		63.6	63.4	62.8	59.2	59			1584893.2	
121	11/17/2015	11:42:29		00:10.0	64.4	74.4	65.1	60.9		65	64.9	64.5	63.2	62.3			2754228.7	
122	11/17/2015	11:42:39	00d	00:10.0	64	74	66.9	61.2		66.8	66.7	62.5	61.7	61.5			2511886.4	
123	11/17/2015	11:42:49	00d	00:10.0	63.5	73.5	66.8	62	-,-	66.5	66.1	63.2	62.2	62.1			2238721.1	
124	11/17/2015	11:42:59	00d	00:10.0	60.6	70.6	62.9	58.5		62.8	62.8	59.9	58.9	58.8			1148153.6	
125	11/17/2015	11:43:09	00d	00:10.0	59.3	69.3	60.6	57.5		60.5	60.5	59.2	57.7	57.6			851138.0	
126	11/17/2015	11:43:19		00:10.0	64.4	74.4	66	60.5		65.9	65.8	64.6	61.8	61.4			2754228.7	
127	11/17/2015	11:43:29		00:10.0	60.7	70.7	62.2	59.3		62.1	62	60.6	59.6	59.4			1174897.6	
128 129	11/17/2015	11:43:39 11:43:49		00:10.0	61.6 60.8	71.6 70.8	63.8 61.8	59.9	Ë	63.7	63.2	61 60.6	60.1 60.3	60.3			1445439.8 1202264.4	
129	11/17/2015 11/17/2015	11:43:49	_	00:10.0 00:10.0	60.8	70.8	63.2	60.2 56.2		61.7 63	61.7 63	59.5	56.4	56.4			1023293.0	
131	11/17/2015	11:44:09	_	00:10.0	62.2	70.1	65	59.4	Ė	64.2	63.5	60.9	59.7	59.6			1659586.9	
132	11/17/2015	11:44:19		00:10.0	65.4	75.4	66.2	63.4	<u>.</u>	66.1	66	65.7	64.5	64			3467368.5	
133	11/17/2015	11:44:29		00:10.0	63.9	73.9	65.5	61.7	-,-	65.4	65.3	63.9	62.2	61.9			2454708.9	
134	11/17/2015	11:44:39	00d	00:10.0	63.1	73.1	66	60.5	-,-	65.8	65.3	61.8	60.8	60.6			2041737.9	
135	11/17/2015	11:44:49	00d	00:10.0	63.1	73.1	66.1	60.7	-,-	65.9	65.7	63.4	61.6	61.1			2041737.9	
136	11/17/2015	11:44:59	00d	00:10.0	60.9	70.9	62.1	59.8	-,-	62	61.9	60.6	60.3	60			1230268.8	
137	11/17/2015	11:45:09	00d	00:10.0	58.7	68.7	61.2	57.2		60.8	60.2	58.7	57.4	57.3			741310.2	
138	11/17/2015	11:45:19	00d	00:10.0	56.8	66.8	59.7	54.4		59.6	59.4	56.7	55.4	54.8			478630.1	
139	11/17/2015	11:45:29		00:10.0	53.6	63.6	55.5	52.2		55.2	54.8	53.2	52.5	52.3			229086.8	
140	11/17/2015	11:45:39		00:10.0	58.5	68.5	61.5	54.6	-,-	61.3	61.2	56.8	54.7	54.7			707945.8	
141	11/17/2015	11:45:49	_	00:10.0	63.5	73.5	64.9	60.9		64.8	64.6	63.4	61.1	61			2238721.1	
142 143	11/17/2015 11/17/2015	11:45:59 11:46:09		00:10.0 00:10.0	64.7 63.6	74.7 73.6	66.9 65.6	62.7 61		66.7 65.5	66.5 65.5	64.3 62.7	63.2 61.2	62.9 61.1			2951209.2 2290867.7	
143	11/17/2015	11:46:19	_	00:10.0	65.8	75.8	67.2	64.3		67.1	66.9	65.6	64.5	64.4			3801894.0	
145	11/17/2015	11:46:29		00:10.0	66.5	76.5	67.2	65.3	-,-	67.1	67	66.5	66	65.9			4466835.9	
146	11/17/2015	11:46:39		00:10.0	63.5	73.5		59.8		66.5	66.3	63	61.1	60.6			2238721.1	
147	11/17/2015	11:46:49	00d	00:10.0	60.5	70.5	62.4	56.5	-,-	62.3	62.2	60.4	56.8	56.7			1122018.5	
148	11/17/2015	11:46:59	00d	00:10.0	62.4	72.4	63.7	61.3		63.5	63	62.3	61.5	61.4			1737800.8	
149	11/17/2015	11:47:09	00d	00:10.0	65.5	75.5	68.8	61.2		68.3	67.7	64.1	61.6	61.4			3548133.9	
150	11/17/2015	11:47:19	00d	00:10.0	66.7	76.7	70.1	64.2		70	69.9	65.6	64.4	64.2			4677351.4	
151	11/17/2015	11:47:29		00:10.0	60.7	70.7	64.7	58.4	-,-	64.7	64.5	60.2	58.8	58.6			1174897.6	
152	11/17/2015	11:47:39		00:10.0	62.4	72.4	64.6	58.4		64.5	64.2	62	59.5	58.6			1737800.8	
153	11/17/2015	11:47:49		00:10.0	65.2	75.2	67.8	60.8		67.7	67.5	63.1	61.9	61.2			3311311.2	
154 155	11/17/2015 11/17/2015	11:47:59 11:48:09		00:10.0 00:10.0	63 64	_	66.3 64.9	60 60	-	66 64.8	65.7 64.8	63.5 64.1	60.7 60.7	60.4			1995262.3 2511886.4	
156	11/17/2015	11:48:19	_	00:10.0	62.3	72.3	64.2	60.1	-	64	63.9	62.6	60.3	60.3			1698243.7	
157	11/17/2015			00:10.0	64.6	74.6	65.6	62		65.5	65.4	65	62.3	62.2			2884031.5	
158	11/17/2015			00:10.0	62.7	72.7	64.4	59.1		64.3	64.2	62.9	59.4	59.2			1862087.1	
159	11/17/2015	11:48:49		00:10.0	63		64.9	61.7		64.8	64.8	62.6	62.2	62			1995262.3	
160	11/17/2015	11:48:59		00:10.0	60.2	70.2	61.7	58.8		61.3	61.2	60.2	59	58.9			1047128.5	
161	11/17/2015	11:49:09	00d	00:10.0	60.6	70.6	61.9	59.9	-,-	61.8	61.7	60.3	60.1	60			1148153.6	
162	11/17/2015	11:49:19		00:10.0	68.5	78.5	71.9	60.1	-,-	71.8	71.6	64.8	60.6	60.3			7079457.8	
163	11/17/2015	11:49:29	_	00:10.0	63.4	73.4	71.3	60.9		70.7	69.4	62.5	61.4	61.3			2187761.6	
164	11/17/2015	11:49:39		00:10.0	58.6	68.6	60.9	54.5	-,-	60.7	60.4	59.3	56.1	55.3	<del> </del>		724436.0	
165	11/17/2015 11/17/2015	11:49:49 11:49:59		00:10.0	61.4 64.4	71.4 74.4	63.9	54.1 62.4	Ë	63.7 64.9	63.6	60.6 64.4	54.2 62.7	54.1 63.5			1380384.3 2754228.7	
166 167	11/17/2015	11:49:59 11:50:09		00:10.0 00:10.0	64.4	74.4	65 64.3	63.4 62.7		64.9	64.8 64.2	64.4	63.7 62.9	63.5			2754228.7	
167	11/17/2015	11:50:09		00:10.0	64.5	74.5	65.3	63.7	2.5	65.2	65.2	64.5	63.9	63.8			2818382.9	
169	11/17/2015	11:50:19		00:10.0	61.6		64.2	60.5	Ė	63.6	63.5	61.6	60.8	60.7			1445439.8	
170	11/17/2015			00:10.0	63.1	73.1	64.8	61.5	-	64.7	64.4	63	61.8	61.7			2041737.9	
171	11/17/2015	11:50:49		00:10.0	61.4	71.4	62.6	59.7		62.5	62.3	61.7	60.1	59.9			1380384.3	
172	11/17/2015	11:50:59		00:10.0	64.1	74.1	66	61.3		65.8	65.6	63.6	62.6	62.4			2570395.8	
173	11/17/2015	11:51:09	00d	00:10.0	63.1	73.1	64.4	61.7	-,-	64.4	64.2	63.1	61.9	61.8			2041737.9	
174	11/17/2015	11:51:19	00d	00:10.0	63.3	73.3	65.4	60.5	Ŀ	64.9	64.1	63.2	61	60.8			2137962.1	
175	11/17/2015	11:51:29		00:10.0	58.4	68.4	64.4	53.9	Ŀ	63.3	62.5	58.1	54.4	54.1			691831.0	
176	11/17/2015	11:51:39		00:10.0	58.7	68.7	61.8	53.3	Ŀ	61.7	61.6	57.5	53.6	53.4			741310.2	
177	11/17/2015	11:51:49		00:10.0	63.6	73.6	64.7	61.5	~	64.6	64.6	63.1	62.2	61.8			2290867.7	
178	11/17/2015	11:51:59		00:10.0	61.8	71.8	64.1	58.4	-,-	64	63.9	62	59.4	58.8	<del></del>		1513561.2	
179	11/17/2015	11:52:09	00d	00:10.0	60.1	70.1	63.8	54.7	-,-	63.2	62.8	58.5	55.1	54.8			1023293.0	i .

	6																	
Address	Start Time	Measure	emen	t Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overall Lea
R10	Tillic																	62.9
180	11/17/2015	11:52:19	00d	00:10.0	61.5	71.5	64.5	59.4	-,-	64.4	64.3	60.8	59.7	59.6			1412537.5	
181	11/17/2015	11:52:29	00d	00:10.0	64.5	74.5	67.1	60.4	-,-	66.6	65.9	62.9	60.7	60.5			2818382.9	1
182	11/17/2015	11:52:39	00d	00:10.0	65.7	75.7	68.5	59.4	-,-	68.4	68.3	66.6	60.8	60.2			3715352.3	1
183	11/17/2015	11:52:49	00d	00:10.0	58.3	68.3	60.1	57.1	-,-	60	59.8	58.2	57.4	57.3			676083.0	
184	11/17/2015	11:52:59	00d	00:10.0	59	69	59.9	57.6	-,-	59.8	59.7	59	58	57.9			794328.2	
185	11/17/2015	11:53:09	00d	00:10.0	57	67	58	55.4	-,-	57.7	57.5	57.2	55.8	55.6			501187.2	1
186	11/17/2015	11:53:19	00d	00:10.0	59	69	59.3	57.4	-,-	59.3	59.2	58.9	58.1	57.9			794328.2	
187	11/17/2015	11:53:29	00d	00:10.0	61.2	71.2	62.7	59.2	-,-	62.6	62.4	60.9	60	59.4			1318256.7	
188	11/17/2015	11:53:39	00d	00:10.0	59.4	69.4	62.2	54.9	-,-	62.2	61.8	58.9	55.2	55			870963.6	1
189	11/17/2015	11:53:49	00d	00:10.0	64.4	74.4	66.3	61.1	-,-	66.2	66.2	64.4	61.4	61.3			2754228.7	1
190	11/17/2015	11:53:59	00d	00:10.0	63.5	73.5	64.8	58.9	-,-	64.7	64.7	64.3	59.3	59.1			2238721.1	1
191	11/17/2015	11:54:09	00d	00:10.0	64.1	74.1	65.9	62.1	-,-	65.8	65.7	64.2	62.3	62.2			2570395.8	1
192	11/17/2015	11:54:19	00d	00:10.0	62.5	72.5	64.6	60.4	-,-	63.9	63.7	63	61	60.6			1778279.4	1
193	11/17/2015	11:54:29	00d	00:10.0	63.2	73.2	64	62.3	-,-	64	63.8	63.2	62.4	62.3			2089296.1	1
194	11/17/2015	11:54:39	00d	00:10.0	61.7	71.7	63.5	60.8	-,-	63.3	63.1	61.6	61.1	60.9			1479108.4	1
195	11/17/2015	11:54:49	00d	00:10.0	62	72	63.2	61		63.1	63	61.9	61.1	61.1			1584893.2	1
196	11/17/2015	11:54:59	00d	00:10.0	60.5	70.5	61.6	59.7	-,-	61.4	61.3	60.4	59.8	59.8			1122018.5	1

Address	Start	Measur	emei	nt Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log
R11	Time				-												
12	11/17/2015	11:40:05	00d	00:10.0	66.5	76.5	69.5	61.9		69.4	69.4	65.9	62.3	61.5			4466835.9
13	11/17/2015	11:40:15		00:10.0	64.3	74.3	66.2	62.2	Н	66.3	66.3	64.4	62	61.9			2691534.8
14	11/17/2015	11:40:25		00:10.0	62.6	72.6	63.1	62		63.1	63.1	62.6	62.1	61.9			1819700.9
15	11/17/2015	11:40:35		00:10.0	62	72	64.2	60		64.5	64.5	61.6	60	60			1584893.2
16	11/17/2015	11:40:45		00:10.0	62.8	72.8	63.9	60.9		64.2	64.2	63.2	60.9	60.5			1905460.7
17	11/17/2015	11:40:55	00d	00:10.0	61.5	71.5	64.2	60	-,-	64	64	60.8	60.2	59.1			1412537.5
18	11/17/2015	11:41:05	00d	00:10.0	62.7	72.7	66	57.3	-,-	66.3	66.3	61.6	57.4	56.7			1862087.1
19	11/17/2015	11:41:15	00d	00:10.0	62.6	72.6	66.1	58.8		66.1	66.1	62.7	60	57			1819700.9
20	11/17/2015	11:41:25	00d	00:10.0	57.9	67.9	60.9	55.1	-,-	61.9	61.9	57.7	55	54.7			616595.0
21	11/17/2015	11:41:35	00d	00:10.0	59.3	69.3	60.5	58.4	-,-	60.7	60.7	59.4	58.4	58			851138.0
22	11/17/2015	11:41:45	00d	00:10.0	60.2	70.2	62.6	58.4	-,-	63	63	59.2	58.7	58.5			1047128.5
23	11/17/2015	11:41:55		00:10.0	65.8	75.8	66.7	62.6		67	67	65.8	64.8	63.6			3801894.0
24	11/17/2015	11:42:05		00:10.0	64.9	74.9	67.4	63		67.6	67.6	64.5	62.9	62.1			3090295.4
25	11/17/2015	11:42:15		00:10.0	64.6	74.6	66.1	61.8	7.7	66.3	66.3	65.3	61.8	61.8			2884031.5
26	11/17/2015 11/17/2015	11:42:25		00:10.0	69.9	79.9 74.8	73.8	64.5 63.5	-,-	74.5	74.5	68.4 64.5	64.7	64.1 63.5			9772372.2 3019951.7
27 28	11/17/2015	11:42:35 11:42:45		00:10.0 00:10.0	64.8 62.6	72.6	66.1 65.4	61.7	-,-	66.6 63.8	66.6 63.8	62.6	64 61.6	61.2			1819700.9
29	11/17/2015	11:42:55		00:10.0	62.8	72.8	64.3	59.8		64.4	64.4	63.3	60	59.1			1905460.7
30	11/17/2015	11:43:05		00:10.0	60.9	70.9	62.8	57.9	-,-	63	63	61.4	57.9	57.8			1230268.8
31	11/17/2015	11:43:15		00:10.0	61	71	63.1	57.7		63.5	63.5	60.9	57.5	57.3			1258925.4
32	11/17/2015	11:43:25		00:10.0	58.9	68.9	61.3	55.9		61.9	61.9	58.4	55.9	55.8			776247.1
33	11/17/2015	11:43:35	00d	00:10.0	60.9	70.9	63.4	59.1	-,-	64	64	60.3	58.8	57.5			1230268.8
34	11/17/2015	11:43:45	00d	00:10.0	61.4	71.4	63.3	58.1		63.8	63.8	60.8	58.7	57.8			1380384.3
35	11/17/2015	11:43:55	00d	00:10.0	63.5	73.5	65.1	61.7	-,-	65.4	65.4	63.3	61.7	61			2238721.1
36	11/17/2015	11:44:05	00d	00:10.0	64.8	74.8	68.3	60.3		68.6	68.6	63.6	60.3	59.6			3019951.7
37	11/17/2015	11:44:15	00d	00:10.0	60.7	70.7	68.7	52.5	-,-	66.9	66.9	59.4	52.2	52			1174897.6
38	11/17/2015	11:44:25	00d	00:10.0	64.2	74.2	66.4	52.1	-,-	66.5	66.5	65.4	54.8	53.1			2630268.0
39	11/17/2015	11:44:35	00d	00:10.0	64.6	74.6	66.1	63.1		66.2	66.2	64.9	63	62.7			2884031.5
40	11/17/2015	11:44:45		00:10.0	63.7	73.7	66.5	61.2	-,-	66.5	66.5	63.6	61.3	60.2			2344228.8
41	11/17/2015	11:44:55		00:10.0	61.4	71.4	65.6	52.8	-,-	65.4	65.4	59.1	52.5	52.2			1380384.3
42	11/17/2015	11:45:05		00:10.0	60.7	70.7	63.2	52.4	-,-	63.3	63.3	62.1	54.2	52.4			1174897.6
43	11/17/2015	11:45:15		00:10.0	62.8	72.8	64.1	61.5		64.4	64.4	62.6	61.7	61.2			1905460.7 2187761.6
44 45	11/17/2015 11/17/2015	11:45:25 11:45:35		00:10.0 00:10.0	63.4 63.2	73.4 73.2	65.9 65.2	60.5 61.1		65.7 65.1	65.7 65.1	63.4 63.5	60.4 61	60.1 60.7			2089296.1
46	11/17/2015	11:45:45		00:10.0	61.8	71.8	63.2	60.1		63.6	63.6	61.9	60	59.8			1513561.2
47	11/17/2015	11:45:55		00:10.0	65.1	75.1	66.5	62.9	-,-	66.9	66.9	65	63.7	63.2			3235936.6
48	11/17/2015	11:46:05		00:10.0	64.6	74.6	65.3	63.6		65.6	65.6	64.6	64.1	62.5			2884031.5
49	11/17/2015	11:46:15		00:10.0	64.7	74.7	66.1	62.9		66.4	66.4	64.5	63.4	62.6			2951209.2
50	11/17/2015	11:46:25	00d	00:10.0	65.7	75.7	66.4	64.5	-,-	66.6	66.6	66	64.4	64.2			3715352.3
51	11/17/2015	11:46:35	00d	00:10.0	66.8	76.8	68.6	64.8	-,-	68.8	68.8	66.9	64.9	64.1			4786300.9
52	11/17/2015	11:46:45	00d	00:10.0	59	69	64.8	57.4		61.6	61.6	58.5	57.7	56.5			794328.2
53	11/17/2015	11:46:55	00d	00:10.0	58.5	68.5	60.7	56.6		61.1	61.1	57.7	56.7	56.4			707945.8
54	11/17/2015	11:47:05	00d	00:10.0	59.2	69.2	60.9	56.5	-,-	61.3	61.3	59.4	56.9	56.7			831763.8
55	11/17/2015	11:47:15		00:10.0	56.9	66.9	60.8	55.5	-,-	59	59	57.1	55	55			489778.8
56	11/17/2015	11:47:25	_	00:10.0	61.5	71.5	63.6	58.4	-,-	64.1	64.1	61.2	58.9	58.9			1412537.5
57	11/17/2015	11:47:35		00:10.0	62.2	72.2	63.6	60.5		63.8	63.8	63	60.5	60.4			1659586.9
58	11/17/2015	11:47:45	_	00:10.0	59.9	69.9	61.6	58.2		61.5	61.5	59.9	58	57.9			977237.2 3548133.9
59 60	11/17/2015 11/17/2015	11:47:55 11:48:05	_	00:10.0 00:10.0	65.5 65.6	75.5 75.6	66.4 67	63.6		66.6 67.4	66.6 67.4	65.5 65.9	64.6 63.8	63.7 63.3			3630780.5
61	11/17/2015	11:48:15	_	00:10.0	65.5	75.5	67.3	63.9		67.3	67.3	65.3	64.3	64			3548133.9
62	11/17/2015	11:48:25	_	00:10.0	66.6	76.6		64.1	-,-	68	68	66.9	65.6	64.3			4570881.9
63	11/17/2015	11:48:35	_	00:10.0	67.5	77.5		66.4	-,-	68.9	68.9	67.4	66.5	66.1			5623413.3
64	11/17/2015	11:48:45	_	00:10.0	64	74		61.5		67.1	67.1	63.2	61.8	61.3			2511886.4
65	11/17/2015	11:48:55	_	00:10.0	61.3	71.3		58.1	-,-	63.9	63.9	61.1	57.7	57.6			1348962.9
66	11/17/2015	11:49:05	00d	00:10.0	62	72	62.9	59.5	-,-	63	63	62.3	60.3	59.1			1584893.2
67	11/17/2015	11:49:15	00d	00:10.0	61.6	71.6	63.8	57.8		64.1	64.1	61.1	57.7	57.3			1445439.8
68	11/17/2015	11:49:25	00d	00:10.0	59.1	69.1	60.6	57.8		61	61	58.7	58	58			812830.5
69	11/17/2015	11:49:35	_	00:10.0	57.3	67.3	58.3	56.6		58.7	58.7	57.2	56.9	56.4			537031.8
70	11/17/2015	11:49:45	_	00:10.0	56.4	66.4		54.5		59.1	59.1	56.1	54.7	54.4			436515.8
71	11/17/2015	11:49:55	_	00:10.0	62.7	72.7	65.1	55		65.3	65.3	63.3	56.6	55.7			1862087.1
72	11/17/2015	11:50:05	_	00:10.0	64.6	74.6		61.6		66.7	66.7	64.6	62.5	60.8			2884031.5
73	11/17/2015	11:50:15	_	00:10.0	64.2	74.2		62.2	-	66	66	64.1	62.6	61.9			2630268.0
74 75	11/17/2015	11:50:25	_	00:10.0	66.8	76.8		60.8		69.3	69.3	68.3	61.2	60.6			4786300.9 2137962.1
75 76	11/17/2015 11/17/2015	11:50:35 11:50:45	_	00:10.0 00:10.0	63.3 60.6	73.3 70.6	68.8 62.7	60.6		67.2	67.2	61.8 60	60.5	60.3			2137962.1 1148153.6
76	11/17/2015	11:50:45	_	00:10.0	60.6	70.6		58.6 59.3		63.3 63.3	63.3 63.3	60.4	58.6 59.4	58.3 59.1			1148153.6
78	11/17/2015	11:51:05	_	00:10.0	65.9	75.9		59.5	-,-	71	71	62.8	60.1	59.5			3890451.4
78	11/17/2015	11:51:05	_	00:10.0	64.7	74.7	70.2	59.5	-,-	70.2	70.2	62.7	59.4	58.7			2951209.2
80	11/17/2015	11:51:15	_	00:10.0	59.5	69.5	60.2	58.8	-,-	60.3	60.3	59.4	59.2	58.4			891250.9
81	11/17/2015	11:51:35		00:10.0	59.3	69.3	62	57.8	-,-	62.6	62.6	58.6	57.8	57.7			851138.0
82	11/17/2015	11:51:45	_	00:10.0	57.8	67.8	59.7	56.1	-,-	60.3	60.3	57.7	56.3	56			602559.6

Overall Leq 63.4

	Start															1		Overall
Address	Time	Measur	emen	nt Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Leg
R11																		63.4
83	11/17/2015	11:51:55	00d	00:10.0	60.5	70.5	63.5	58		64.1	64.1	59.8	57.8	57.5			1122018.5	
84	11/17/2015	11:52:05	00d	00:10.0	64.8	74.8	65.7	63.5		66.1	66.1	64.4	64	64			3019951.7	1
85	11/17/2015	11:52:15	00d	00:10.0	60.1	70.1	64.6	59.3		61.5	61.5	60.1	59.1	59.1			1023293.0	1
86	11/17/2015	11:52:25	00d	00:10.0	63.2	73.2	65.3	60.6	-,-	65.4	65.4	62.3	61.5	60.4			2089296.1	
87	11/17/2015	11:52:35	00d	00:10.0	65.7	75.7	67.4	63		67.5	67.5	65.2	63.1	62.8			3715352.3	
88	11/17/2015	11:52:45	00d	00:10.0	63.5	73.5	67.5	56.3		67.2	67.2	62.4	56.3	55.6			2238721.1	
89	11/17/2015	11:52:55	00d	00:10.0	62.6	72.6	66.7	55.6		66.8	66.8	59.5	56.5	55.2			1819700.9	
90	11/17/2015	11:53:05	00d	00:10.0	63.5	73.5	67.8	58.8		68.2	68.2	62.4	59.1	58.8			2238721.1	
91	11/17/2015	11:53:15	00d	00:10.0	56.3	66.3	60.3	52.3		60.5	60.5	54.6	52.2	52.1			426579.5	
92	11/17/2015	11:53:25	00d	00:10.0	55.4	65.4	58.1	53.2		57.8	57.8	54.8	53.3	53.3			346736.9	
93	11/17/2015	11:53:35	00d	00:10.0	62.8	72.8	64.4	57.3		64.6	64.6	62.7	62	58.3			1905460.7	
94	11/17/2015	11:53:45	00d	00:10.0	60.9	70.9	63	59.2		63.1	63.1	60.8	59.5	59.1			1230268.8	
95	11/17/2015	11:53:55	00d	00:10.0	65.2	75.2	66.5	60.6		67	67	65.1	64	63.1			3311311.2	
96	11/17/2015	11:54:05	00d	00:10.0	69.1	79.1	71.7	65.6		72.2	72.2	69.3	65.7	65.4			8128305.2	
97	11/17/2015	11:54:15	00d	00:10.0	63.5	73.5	71.1	61.6	-,-	66.2	66.2	63.4	62	61.4			2238721.1	
98	11/17/2015	11:54:25	00d	00:10.0	62.9	72.9	64.6	61.3		64.6	64.6	62.9	61.2	60.6			1949844.6	
99	11/17/2015	11:54:35	00d	00:10.0	61.3	71.3	63.1	59.8		63.9	63.9	61.1	59.9	59.1			1348962.9	
100	11/17/2015	11:54:45	00d	00:10.0	60.9	70.9	62.2	59.2		62.3	62.3	61.3	59.6	58.2			1230268.8	
101	11/17/2015	11:54:55	00d	00:10.0	59.8	69.8	61.7	56.7		61.9	61.9	60.1	57	56			954992.6	

Address	Start	Measur	emen	ıt Time	Lea	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overall
R12	Time	Wicasai	Cilici	· · · · · · ·	Leq		LIVIPOL		-7	2112		LIVO	214-7	2113	Over	Onuci	miverse 20g	Leq 65.2
56	11/17/2015	11:40:03	00d	00:10.0	66.7	76.7	68.4	65.5		68.3	68.1	66.5	65.8	65.7			4677351.4	03.2
57	11/17/2015	11:40:13		00:10.0	65.1	75.1	67.1	63.3	-	67	66.8	65.2	64	63.9			3235936.6	1
58	11/17/2015	11:40:23		00:10.0	63	73	64.3	61.4	_	64.1	64.1	62.9	61.8	61.5			1995262.3	1
59	11/17/2015	11:40:33		00:10.0	61.8	71.8	63.7	60.3		63.1	62.9	62.2	60.7	60.5			1513561.2	1
60	11/17/2015	11:40:43	00d	00:10.0	60.7	70.7	62.1	58.7		61.9	61.9	60.9	59.1	58.9			1174897.6	]
61	11/17/2015	11:40:53	00d	00:10.0	60.9	70.9	62.3	60		62.1	61.8	61	60.2	60.1			1230268.8	
62	11/17/2015	11:41:03	00d	00:10.0	60.2	70.2	63.1	56.7		62.9	62.4	59.7	57.1	56.9			1047128.5	
63	11/17/2015	11:41:13		00:10.0	62.8	72.8	64.7	60.4		64.6	64.4	61.7	61.3	61			1905460.7	
64	11/17/2015	11:41:23		00:10.0	65.3	75.3	66.5	63.5		66.4	66.3	65.4	64.2	64.1			3388441.6	
65 66	11/17/2015	11:41:33		00:10.0	65.8	75.8	68.7 70.9	60.8		68.5	68.4 70.6	63.8 69.5	60.9	60.9			3801894.0 9120108.4	ł
67	11/17/2015 11/17/2015	11:41:43 11:41:53		00:10.0 00:10.0	69.6 66	79.6 76	68.5	68.4 63.2		70.8 68.4	68.3	66.2	68.5 63.4	68.5 63.3			3981071.7	-
68	11/17/2015	11:42:03	_	00:10.0	62.7	72.7	65.7	56.9	-	65.4	65.3	63.5	57.3	57.1			1862087.1	1
69	11/17/2015	11:42:13	00d	00:10.0	64.4	74.4	66.6	58.7	_	66.4	66.2	64.1	60.4	60.2			2754228.7	1
70	11/17/2015	11:42:23	00d	00:10.0	63.8	73.8	64.5	63.2		64.5	64.4	63.8	63.5	63.4			2398832.9	1
71	11/17/2015	11:42:33	00d	00:10.0	64.2	74.2	66	61		65.9	65.9	63.5	61.4	61.2			2630268.0	
72	11/17/2015	11:42:43	00d	00:10.0	65.4	75.4	67.2	61.4		67.2	67.1	65.9	63.2	62.3			3467368.5	
73	11/17/2015	11:42:53	00d	00:10.0	58.9	68.9	61.4	56	-	60.8	60.6	59.1	56.4	56.1			776247.1	
74	11/17/2015	11:43:03		00:10.0	62.6	72.6	65.2	57.8	_	64.9	64.7	62.5	59.4	59			1819700.9	
75	11/17/2015	11:43:13		00:10.0	57.2	67.2	59.2	55.2		59.1	58.8	56.2	55.3	55.2			524807.5	1
76 77	11/17/2015 11/17/2015	11:43:23 11:43:33	_	00:10.0	61.1 65.7	71.1 75.7	62.9	59.2	-	62.7	62.4 68.6	60.8 63.2	59.5	59.5 59.4			1288249.6 3715352.3	1
77	11/17/2015	11:43:33		00:10.0 00:10.0	65.7 68.7	75.7 78.7	68.9 69.9	59.3 67.7		68.7 69.8	68.6 69.6	63.2	59.6 67.8	59.4 67.8			7413102.4	1
79	11/17/2015	11:43:53	_	00:10.0	67.6	77.6	68.4	66.9	_	68.1	68	67.7	67.4	67.8			5754399.4	1
80	11/17/2015	11:44:03	_	00:10.0	65.2	75.2	66.9	63.8	-	66.6	66.5	65.6	64	63.9			3311311.2	1
81	11/17/2015	11:44:13		00:10.0	64.1	74.1	65.6	62.8	_	65.1	64.9	64.4	63.7	63.2			2570395.8	1
82	11/17/2015	11:44:23	00d	00:10.0	63.7	73.7	64.7	62.1		64.6	64.5	63.6	62.3	62.2			2344228.8	]
83	11/17/2015	11:44:33	00d	00:10.0	64.8	74.8	68.3	63.3		66.8	65.4	63.9	63.4	63.4			3019951.7	
84	11/17/2015	11:44:43	00d	00:10.0	65.1	75.1	68.4	62.7		68	67.7	65	63	62.8			3235936.6	
85	11/17/2015	11:44:53		00:10.0	62.7	72.7	65.8	57.5		65.6	65.4	62.9	58.2	57.8			1862087.1	
86	11/17/2015	11:45:03		00:10.0	56.2	66.2	58	55.1	_	57.9	57.8	56.2	55.3	55.2			416869.4	
87	11/17/2015	11:45:13		00:10.0	57.1	67.1	59.7	53.6	-	59.3	59.1	54.9	53.7	53.7			512861.4	
88 89	11/17/2015 11/17/2015	11:45:23 11:45:33		00:10.0 00:10.0	58.9 66.1	68.9 76.1	61.7 67.5	55.9 58.4		61.5 67.4	61.1 67.3	58.4 65.9	56.2 62.2	56.1 60.5			776247.1 4073802.8	-
90	11/17/2015	11:45:43		00:10.0	65.5	75.5	67.1	64.2		66.9	66.4	65.1	64.3	64.3			3548133.9	1
91	11/17/2015	11:45:53	_	00:10.0	65.6	75.6	67.1	63.9	-	67.1	67	66.3	64.1	64			3630780.5	1
92	11/17/2015	11:46:03		00:10.0	66.3	76.3	68.2	63.2	_	68.1	67.9	66.1	63.8	63.3			4265795.2	1
93	11/17/2015	11:46:13	00d	00:10.0	64.8	74.8	66.1	62.3		66	66	64.9	62.6	62.4			3019951.7	1
94	11/17/2015	11:46:23	00d	00:10.0	65.7	75.7	67	62.7		67	66.9	66.3	63	62.8			3715352.3	
95	11/17/2015	11:46:33	00d	00:10.0	63.4	73.4	66.3	59.7		66.2	66	64.2	60.3	59.9			2187761.6	
96	11/17/2015	11:46:43		00:10.0	66	76	68	59.7		67.9	67.7	65.7	61.6	60.1			3981071.7	
97	11/17/2015	11:46:53		00:10.0	65.5	75.5	66.9	63.4	_	66.8	66.7	65.2	63.8	63.6			3548133.9	
98	11/17/2015	11:47:03	_	00:10.0	64.4	74.4	66.5	62.9	-	66.3	66	64.1	63.1	63			2754228.7	
99 100	11/17/2015 11/17/2015	11:47:13 11:47:23		00:10.0 00:10.0	64.1 62.7	74.1 72.7	66.1 65.6	62.2 61	_	66 64.8	65.7 64.2	63.8 61.4	62.4 61.1	62.3 61			2570395.8 1862087.1	-
100	11/17/2015	11:47:33		00:10.0	66.9	76.9	67.6	65.6		67.5	67.5	66.8	66.4	66.2			4897788.2	1
102	11/17/2015	11:47:43		00:10.0	66.1	76.1	68	64.1	-,-	67.8	67.6	66.4	64.5	64.2			4073802.8	1
103	11/17/2015	11:47:53	00d	00:10.0	67.7	77.7	70		-,-	69.9	69.8	67.7	64.6				5888436.6	1
104	11/17/2015	11:48:03	00d	00:10.0	68.3	78.3	69.5	64.4		69.4	69.4	68.2	66.3	65.4			6760829.8	
105	11/17/2015	11:48:13	00d	00:10.0	67.5	77.5	68.4	66.1		68.2	68.1	67.6	66.3	66.3			5623413.3	l
106	11/17/2015	11:48:23		00:10.0	66.6	76.6	68.3	65	_	68.2	68.2	66.7	65.1	65.1			4570881.9	l
107	11/17/2015	11:48:33		00:10.0	64	74	66.6			66.5	66.5	63.9	62.1	61.3			2511886.4	-
108	11/17/2015	11:48:43		00:10.0	60.8	70.8	63.3	56.7		62.8	62.4	60.5	57.4				1202264.4	-
109 110	11/17/2015 11/17/2015	11:48:53 11:49:03		00:10.0 00:10.0	58.9 59.1	68.9 69.1	63.4 62.4	55.7 54.3	_	63.2 62.3	63 62.2	57.7 59.4	55.9	55.8 54.4			776247.1 812830.5	ł
110	11/17/2015	11:49:03		00:10.0	59.1 61.7	71.7	66.4	54.3 54.6	_	62.3	65.4	56.2	54.5 54.8	54.4			1479108.4	1
111	11/17/2015	11:49:23		00:10.0	65.9	75.9	67.9	63.2	_	67.8	67.7	66.4	63.4	63.3			3890451.4	1
113	11/17/2015	11:49:33	_	00:10.0	66.7	76.7	67.7	64.5	_	67.5	67.5	66.2	65.7	64.9			4677351.4	1
114	11/17/2015	11:49:43	00d	00:10.0	71.4	81.4	74.3	67.7		74.2	74	70.8	68.3	68.1			13803842.6	]
115	11/17/2015	11:49:53	00d	00:10.0	68.5	78.5	69.5	67.4		69.2	69.1	68.2	67.7	67.6			7079457.8	l
116	11/17/2015	11:50:03		00:10.0	69.1	79.1	70.8	66.9		70.7	70.6	68.4	67.2	67.1	<u></u>	<u> </u>	8128305.2	
117	11/17/2015	11:50:13		00:10.0	67.8	77.8	70.7	66.5	-	70.3	69.9	67.9	66.9	66.7			6025595.9	l
118	11/17/2015	11:50:23		00:10.0	66	76	67.6	64.1	_	67.5	67.3	66.3	64.5	64.2			3981071.7	ł
119	11/17/2015	11:50:33		00:10.0	61.2	71.2	64.7	57.9	_	64.5	64	60.9	58.1	58			1318256.7	1
120	11/17/2015	11:50:43		00:10.0	64.4	74.4	65.1	62.4	_	65.1	64.9	64.4	63.5	63.4			2754228.7	ł
121 122	11/17/2015 11/17/2015	11:50:53 11:51:03		00:10.0 00:10.0	63.4 62.1	73.4 72.1	65.2 63.4	61.3 60.9	_	65.1 63.3	65.1 63.1	63.2 62	61.8 61.4	61.5 61.2			2187761.6 1621810.1	1
122	11/17/2015	11:51:03		00:10.0	58.7	68.7	61.8	55.1	_	61.7	61.4	58	55.3	55.1			741310.2	1
124	11/17/2015	11:51:13	_	00:10.0	57.4	67.4	61.3	54.2	-	61.2	61.1	56.8	54.3	54.3			549540.9	1
125	11/17/2015	11:51:33		00:10.0	65.3	75.3	66.5	55.4	_	66.4	66.3	65.5	59.5	57.1			3388441.6	1
126	11/17/2015	11:51:43		00:10.0	66.2	76.2	67	65.4		66.6	66.4	66.2	65.5	65.5			4168693.8	]
	11/17/2015	11:51:53	00d	00:10.0	67.2	77.2	68.1	65.9		68	67.9	66.8	66.3	66.1			5248074.6	
127	11/1//2015																	

	Chamb																Overell
Address	Start Time	Measuremen	t Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overall Leg
R12																	65.2
129	11/17/2015	11:52:13 00d	00:10.0	67.5	77.5	68.5	65.6		68.3	68.3	67.7	66.1	65.8			5623413.3	
130	11/17/2015	11:52:23 00d	00:10.0	66	76	68.4	64.4		68	67.8	65.5	64.6	64.5			3981071.7	1
131	11/17/2015	11:52:33 00d	00:10.0	67.4	77.4	69.4	61.9		69.3	69.2	68	63.7	62.9			5495408.7	
132	11/17/2015	11:52:43 00d	00:10.0	63.2	73.2	66.3	55.6		66.2	65.8	63.3	57.5	56.4			2089296.1	
133	11/17/2015	11:52:53 00d	00:10.0	58.4	68.4	59.3	55.2		59.2	59	58.7	55.8	55.3			691831.0	
134	11/17/2015	11:53:03 00d	00:10.0	59	69	61.2	56.3		61.2	61	58.9	57	56.7			794328.2	
135	11/17/2015	11:53:13 00d	00:10.0	55.3	65.3	56.3	54.1		56.1	56	55.5	54.2	54.2			338844.2	
136	11/17/2015	11:53:23 00d	00:10.0	58.8	68.8	60.2	55.4		60	59.5	58.8	55.6	55.5			758577.6	
137	11/17/2015	11:53:33 00d	00:10.0	61.7	71.7	63.8	58.1		63.7	63.5	62	58.3	58.2			1479108.4	
138	11/17/2015	11:53:43 00d	00:10.0	64.3	74.3	66.3	61.4		65.7	65.3	63.6	61.7	61.5			2691534.8	
139	11/17/2015	11:53:53 00d	00:10.0	67.4	77.4	69.9	64.5		69.8	69.7	67.2	64.8	64.6			5495408.7	
140	11/17/2015	11:54:03 00d	00:10.0	67.3	77.3	68.5	65		68.4	68.3	67.1	65.3	65.1			5370318.0	
141	11/17/2015	11:54:13 00d	00:10.0	67.7	77.7	69.8	66.2		69.7	69.4	67.5	66.4	66.3			5888436.6	
142	11/17/2015	11:54:23 00d	00:10.0	67.3	77.3	68.1	65.7		68	67.9	67.5	66.3	65.8			5370318.0	]
143	11/17/2015	11:54:33 00d	00:10.0	64.2	74.2	65.9	62.6		65.8	65.3	64.4	62.9	62.7			2630268.0	]
144	11/17/2015	11:54:43 00d	00:10.0	62.8	72.8	64.4	62.1		64.2	63.9	62.8	62.2	62.2			1905460.7	]
145	11/17/2015	11:54:53 00d	00:10.0	65.5	75.5	66.9	62.6		66.8	66.7	65.2	63.4	63.4			3548133.9	]

**APPENDIX B - TRAFFIC DATA** 

E	NTRADA© - Environmental	Traffic Data Input Sheet (V 2018-09)	
1. Purpose of Analysis:	2-Scenario: Existing & Design (Noise)	1a. Period: 24-hour 1b. Segmen	t Length (mi.): 2.10
2. Is the Analysis Segment Signalized:	Yes	2a. Does it Remain Signalized After Project	et Completion: Yes
3. Analysis Facility Name & Number:	Leesburg Pike (Route 7)	3	a. Area Type: Urban <u>Defination</u>
4. Project Title/Proj. Number/UPC Number:	Route 7 Corridor Improvements Design-B	Build / 0007-029-225, 0007-029-942 / 106917, 99478	_
4a. Analysis Segment Begining:	Route 7917 (Reston Ave)	4b. Fac.	ility Direction: East-West
4c. Analysis Segment Ending:	Route 606 (Baron Cameron Ave)	4d. Revo	erse Direction: No
5. VDOT District:	9. Northern Virginia 5a. Juri	isdiction: Fairfax Co	5b. Terrain: Rolling PCE= 2.50
6. Name/Year 1:	Existing 2018	Name/Year 2:	Design 2040
7. Volume-Delay Function (Travel-Time Model):	BPR		
Selected BPR Parameters & Formulation:	<u>а</u> <b>В</b> 0.15 4.00	BPR Model: t= t0 * (1.0 + 0.15 * (v/c)^4.00)	Link to additional Parameters for most Volume-Delay Models
Analysis Facility Type (FT):     Capacity:     10. Facility Cross Section:	NEW - Facility type selections are now Existing Year 2018  Major Arterial with PS>50 mph 960 pcphpl Divided	available for Design year  Design Year 2040  Major Arterial with PS>50 mph  960 pcphpl  Divided	Starting point Starting point
11. Posted Speed (PS, mph):	55	55	Ending point /
12. Free-Flow Speed (F-FS) Calculation Method: 12a. Free-Flow Speed, mph: Smb= Mid-block F-F Speed (Signalized Facility)	Smb= 0.79 * PS + 12 55	Smb= 0.79 * PS + 12 55	Analysis Segment Length
13. Number of Lane:	Eastbound Westbound 2 2	Eastbound Westbound 3 3	
14. Lane Width (ft.):	11	11	
15. Shoulder Width (ft.):	Inside Outside	Inside Outside	Note:
16. Access Density (# of access/mi.):	4	4	your note here
17. Analysis Segment No. of Signals:	4	4	
18. Average Cycle Length (sec.):	225	212	
19. Average Green Time per Cycle (sec.):	150	135	
20. Signal Coordination:  Delay caused by signal, mph:	Excellent Coord.	Excellent Coord.	
21. Truck Input Type: Hourly	Analysis Segment Truck I Existing Year 2018	nput Type and Daily Traffic Volume  Design Year 2040	
22. Two-way ADT or AADT:	51,600	74,000	ADT: Average Daily Traffic, AADT: Annual ADT
22a. Is No-build Condition ADT or AADT Available:	No		
Existing & F	uture Traffic Inputs (The default	time periods for the Noise Study are 6:00 AM to	9:00 PM)
23. Design - Build & No-Build Traff	ic Assignment: Constrained - Noise Study	y 23a. Is Current Hourly Speed Available:	Yes 23b. Initial: GM
24. Apply Existing K-factor & D-factor to th	e Design Year: Yes	24b. Apply Existing Hourly % Truck:	Yes

H				E	NTRADA@	) - Environm	ental Traffi	c Data Inpu
Use "Paste-a	s-value" opti	ion.						
Starting		Exis	sting Hourly:	: % K-factor,	% D-factor, %	6 Truck and Colle	cted Speed	
Time	Tow-way	Eastbound	Eastboun	d % Truck	Westbou	ınd % Truck	Eastbound	Westbound
11110	K-factor	D-factor	2X-6T	3X & up	2X-6T	3X & up	Existing Avg	. Speed, mph
0:00	0.8%	35%	0.9%	5.7%	1.3%	1.0%	52	53
1:00	0.5%	45%	3.0%	1.0%	1.8%	3.1%	54	52
2:00	0.3%	44%	2.6%	2.7%	4.3%	2.9%	53	51
3:00	0.4%	65%	2.3%	4.6%	4.7%	3.9%	54	52
4:00	1.6%	75%	1.6%	1.7%	3.2%	3.0%	57	52
5:00	3.9%	75%	2.1%	1.6%	4.5%	2.8%	56	53
6:00	6.1%	78%	2.3%	3.3%	4.8%	2.2%	46	51
7:00	5.1%	62%	4.6%	4.4%	4.0%	2.6%	24	50
8:00	5.6%	62%	3.0%	2.3%	5.0%	2.8%	39	49
9:00	5.3%	65%	2.9%	3.0%	4.2%	2.9%	45	48
10:00	4.7%	59%	3.7%	2.9%	4.6%	3.3%	52	47
11:00	4.6%	57%	4.0%	2.2%	4.9%	4.4%	52	46
12:00	4.6%	53%	5.1%	3.1%	3.0%	3.7%	52	47
13:00	5.0%	49%	3.9%	3.2%	2.0%	3.2%	51	44
14:00	5.4%	47%	2.5%	1.9%	3.8%	3.2%	53	45
15:00	6.7%	39%	2.8%	2.1%	2.8%	3.0%	52	48
16:00	7.4%	38%	2.7%	1.8%	2.2%	2.2%	51	47
17:00	7.3%	39%	3.0%	1.3%	1.4%	1.8%	51	48
18:00	7.0%	37%	1.7%	1.0%	0.9%	2.1%	53	46
19:00	5.6%	35%	2.0%	1.3%	0.8%	1.4%	53	48
20:00	4.4%	40%	0.9%	1.3%	1.4%	1.2%	51	49
21:00	3.6%	38%	1.3%	0.5%	1.0%	0.9%	52	50
22:00	2.5%	34%	0.9%	0.6%	0.4%	0.3%	54	52
23:00	1.6%	31%	0.8%	0.8%	1.1%	1.1%	54	52
	100%					Avg. Speed:	50	49
EN	TRADA prog	gram is develope	ed by <b>Ed Azim</b> i	i @VDOT-NOV	A/TP	5 1		For

E	NTRADA© - Environmental	Traffic Data Input Sheet (V 2018-09)	
1. Purpose of Analysis:	2-Scenario: Existing & Design (Noise)	la. Period: 24-hour lb. Segmen	nt Length (mi.): 4.25
2. Is the Analysis Segment Signalized:	Yes	2a. Does it Remain Signalized After Proje	ect Completion: Yes
3. Analysis Facility Name & Number:	Leesburg Pike (Route 7)		3a. Area Type: Urban <u>Defination</u>
4. Project Title/Proj. Number/UPC Number:	Route 7 Corridor Improvements Design-B	Build / 0007-029-225, 0007-029-942 / 106917, 99478	
4a. Analysis Segment Begining:	Route 606 (Baron Cameron Ave)	4b. Fac	cility Direction: East-West
4c. Analysis Segment Ending:	Route 694 (Lewinsville Rd)	4d. Rev	verse Direction: No
5. VDOT District:	9. Northern Virginia 5a. Juri	isdiction: Fairfax Co	5b. Terrain: Rolling PCE= 2.50
6. Name/Year 1:	Existing 2018	Name/Year 2:	Design 2040
7. Volume-Delay Function (Travel-Time Model):	BPR		
8. Selected BPR Parameters & Formulation:	<u>α</u> <u>β</u> 0.15 4.00	BPR Model: t= t0 * (1.0 + 0.15 * (v/c)^4.00)	Link to additional Parameters for most Volume-Delay Models
	NEW - Facility type selections are now		
9. Analysis Facility Type (FT):		Design Year 2040 Major Arterial with PS>50 mph	Starting point
Capacity: 10. Facility Cross Section:	960 pcphpl Divided	960 pcphpl Divided	Ending point
11. Posted Speed (PS, mph):	55	55	
12. Free-Flow Speed (F-FS) Calculation Method:	Smb= 0.79 * PS + 12	Smb= 0.79 * PS + 12	<del>                                    </del>
12a. Free-Flow Speed, mph:   Smb= Mid-block F-F Speed (Signalized Facility)	55	55	Analysis Segment Length
13. Number of Lane:	Eastbound Westbound 2 2	Eastbound Westbound 3 3	
14. Lane Width (ft.):	11	11	
15. Shoulder Width (ft.):	Inside Outside	Inside Outside	Note:
16. Access Density (# of access/mi.):	4	4	your note here
17. Analysis Segment No. of Signals:	5	5	
18. Average Cycle Length (sec.):	231	230	
19. Average Green Time per Cycle (sec.):	164	168	
20. Signal Coordination: Delay caused by signal, mph:	Excellent Coord.	Excellent Coord.	
	Analysis Segment Truck I Existing Year 2018	Input Type and Daily Traffic Volume Design Year 2040	
21. Truck Input Type: Hourly	Entiting Four 2010	263.5.1.1.22.10	
22. Two-way ADT or AADT:	61,600	103,000	ADT: Average Daily Traffic, AADT: Annual ADT
22a. Is No-build Condition ADT or AADT Available:	No		
Existing & F	uture Traffic Inputs (The default	time periods for the Noise Study are 6:00 AM to	9:00 PM)
23. Design - Build & No-Build Traff	ic Assignment: Constrained - Noise Study	23a. Is Current Hourly Speed Available:	Yes 23b. Initial: GM
24. Apply Existing K-factor & D-factor to th	e Design Year: Yes	24b. Apply Existing Hourly % Truck:	Yes

H				E	NTRADA@	) - Environm	ental Traffi	e Data Inpu
Use "Paste-a	s-value" opti	ion.						
Starting		Exis	sting Hourly:	: % K-factor,	% D-factor, %	6 Truck and Colle	cted Speed	
Time	Tow-way	Eastbound	Eastboun	d % Truck	Westbou	ınd % Truck	Eastbound	Westbound
111110	K-factor	D-factor	2X-6T	3X & up	2X-6T	3X & up	Existing Avg	. Speed, mph
0:00	0.8%	34%	1.3%	2.1%	1.1%	1.1%	51	51
1:00	0.5%	40%	3.7%	2.8%	2.6%	1.0%	51	50
2:00	0.4%	43%	1.4%	2.6%	2.5%	2.8%	52	51
3:00	0.5%	59%	2.7%	2.9%	4.3%	2.8%	53	50
4:00	1.6%	70%	2.3%	2.2%	3.9%	3.7%	56	50
5:00	3.9%	69%	2.6%	2.1%	4.0%	2.9%	52	49
6:00	5.8%	71%	2.7%	2.9%	3.9%	3.3%	41	45
7:00	5.8%	60%	3.3%	3.4%	3.2%	3.5%	31	43
8:00	5.8%	59%	3.5%	3.5%	4.4%	2.9%	29	42
9:00	5.4%	61%	3.0%	3.6%	3.3%	2.9%	33	44
10:00	4.8%	57%	3.2%	2.9%	4.3%	3.0%	42	44
11:00	4.6%	55%	3.9%	2.6%	4.3%	3.6%	41	43
12:00	4.9%	51%	4.2%	3.3%	3.2%	3.1%	41	42
13:00	5.0%	48%	4.3%	2.9%	3.2%	2.9%	42	41
14:00	5.7%	45%	3.1%	2.5%	2.8%	3.1%	42	43
15:00	6.7%	42%	2.5%	2.2%	3.0%	2.8%	45	40
16:00	6.6%	44%	2.4%	2.1%	2.5%	3.1%	44	31
17:00	6.1%	50%	2.2%	1.9%	3.0%	3.6%	44	23
18:00	6.2%	45%	1.9%	1.8%	2.5%	2,3%	43	27
19:00	5.7%	37%	1.8%	1.3%	1.0%	1.3%	45	41
20:00	4.8%	36%	0.9%	1.2%	1.0%	1.0%	48	44
21:00	3.9%	37%	1.3%	0.6%	0.8%	0.8%	49	48
22:00	2.8%	36%	0.9%	0.8%	1.1%	1.0%	50	48
23:00	1.7%	33%	1.2%	0.5%	1.5%	0.8%	41	50
	100%	-		0.0.1		Avg. Speed:	44	43
EN		eram is develope	d by <b>Ed Azim</b> i	i @VDOT-NOV	A/TP	11.g. speed.		For

	NTRADA© - Environme	ntal Tueffie Date Innu	4 Shoot (V 2019 00)		
	NTRADA© - Environme	ntai Traine Data inpu	it Sheet (V 2018-09)		
1. Purpose of Analysis:	2-Scenario: Existing & Design (Nois	se) la. Period:	24-hour 1b. Segmen	t Length (mi.): 0.48	
2. Is the Analysis Segment Signalized:	Yes	2a. Does	it Remain Signalized After Project	ct Completion: Yes	
3. Analysis Facility Name & Number:	Leesburg Pike (Route 7)		3	Ba. Area Type: Urban	<u>Defination</u>
4. Project Title/Proj. Number/UPC Number:	Route 7 Corridor Improvements Des	sign-Build / 0007-029-225, 0007-	-029-942 / 106917, 99478		
4a. Analysis Segment Begining:	Route 694 (Lewinsville Rd)		4b. Fac	ility Direction: East-West	
4c. Analysis Segment Ending:	Route 8912 (Jarrett Valley Dr)		4d. Reve	erse Direction: No	
5. VDOT District:	9. Northern Virginia 5a	a. Jurisdiction: Fairfax Co		5b. Terrain: Rolling	PCE= 2.50
6. Name/Year 1:	Existing 2018		Name/Year 2:	Design 2040	
7. Volume-Delay Function (Travel-Time Model):	BPR				
8. Selected BPR Parameters & Formulation:	<u>α</u> <u>β</u> 0.15 4.00	BPR Model: t= t0 * (1.	.0 + 0.15 * (v/c)^4.00)	Link to additional Parameters f	or most Volume-Delay Models
	NEW - Facility type selections are Existing Year 2018	now available for Design year	Design Year 2040	Starting point	1 1
9. Analysis Facility Type (FT):	Minor Arterial with PS<50 mph		Minor Arterial with PS<50 mph		
Capacity: 10. Facility Cross Section:	700 pcphpl Divided		700 pcphpl Divided		Ending point
11. Posted Speed (PS, mph):	45		45	l i i i i i i i i i i i i i i i i i i i	·
12. Free-Flow Speed (F-FS) Calculation Method:  12a. Free-Flow Speed, mph:  Smb= Mid-block F-F Speed (Signalized Facility)	Smb= 0.79 * PS + 12 48		Smb= 0.79 * PS + 12 48		
	Eastbound Westbound		Eastbound Westbound	Analysis Seg	gment Length
13. Number of Lane:	2 2		3 3		
14. Lane Width (ft.):	1 l Inside Outside		11 Inside Outside		
15. Shoulder Width (ft.):				Note: your note here	
16. Access Density (# of access/mi.):	4		4		
17. Analysis Segment No. of Signals:	1		1		
18. Average Cycle Length (sec.):	210		230		
19. Average Green Time per Cycle (sec.):	139		173		
20. Signal Coordination: Delay caused by signal, mph:	Excellent Coord.		Excellent Coord.		
	Analysis Segment Tru Existing Year 2018	uck Input Type and Daily	Traffic Volume Design Year 2040		
21. Truck Input Type: Hourly	Existing Teat 2016		Design Teal 2040		
22. Two-way ADT or AADT:	51,800		82,000	ADT: Average Da	ily Traffic, AADT: Annual ADT
22a. Is No-build Condition ADT or AADT Available:	No				
Existing & F	uture Traffic Inputs (The def	ault time periods for the N	Noise Study are 6:00 AM to	9:00 PM)	
23. Design - Build & No-Build Traff	ic Assignment: Constrained - Noise	Study 23a. Is C	Current Hourly Speed Available:	Yes 23b. Initial:	GM
24. Apply Existing K-factor & D-factor to th	e Design Year: Yes	24b. A	Apply Existing Hourly % Truck:	Yes	

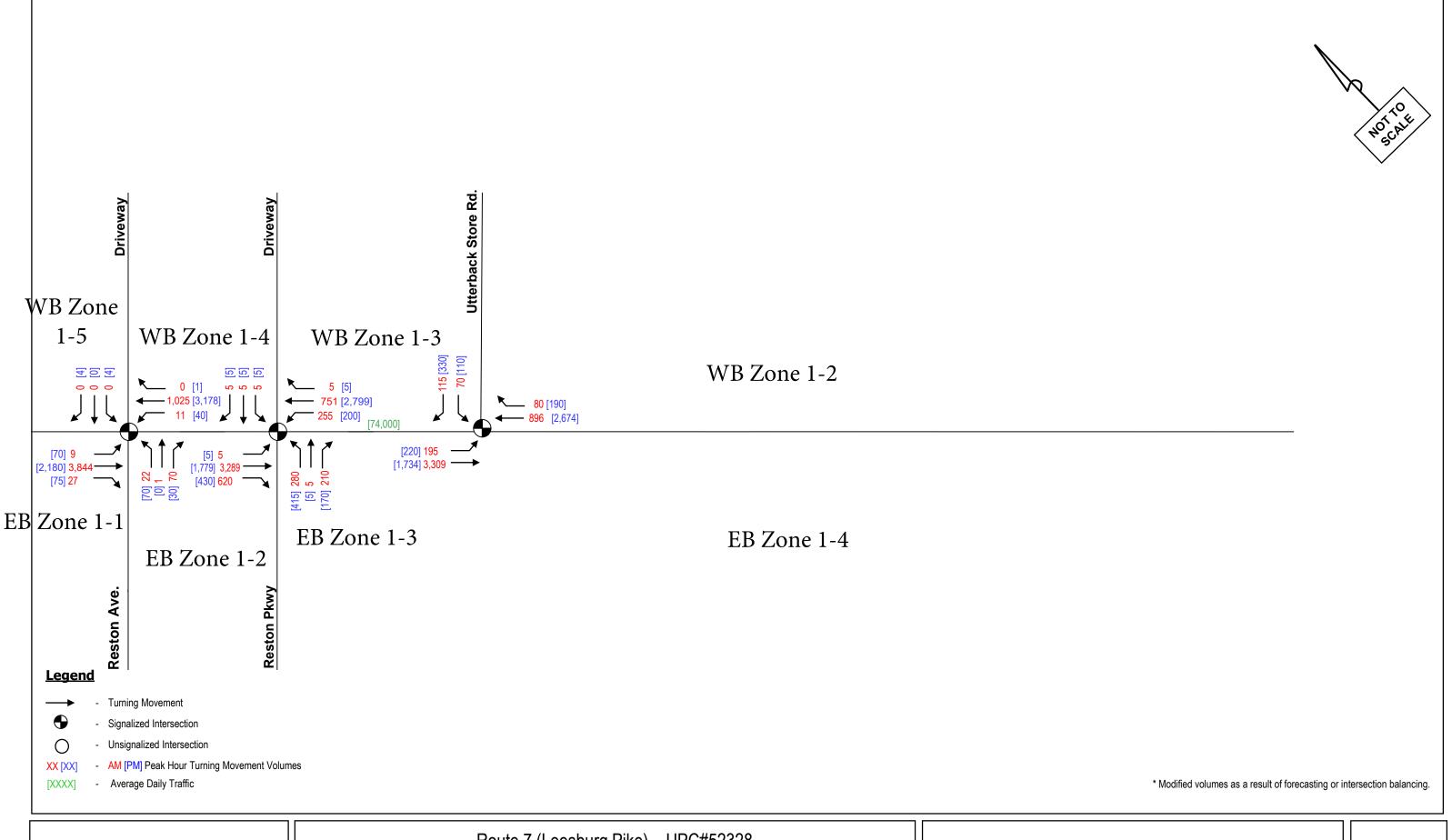
H				E	NTRADA@	) - Environm	ental Traffic	Data Inpu	t Sheet (V 20	18-09)			
Use "Paste-a	s-value" opti	on											
	is-value opti		sting Hourly:	: % K-factor.	% D-factor, %	6 Truck and Colle	ected Speed		_				
Starting	Tow-way	Eastbound		d % Truck		ınd % Truck	Eastbound	Westbound		1			
Time	K-factor	D-factor	2X-6T	3X & up	2X-6T	3X & up	Existing Avg.	Speed, mph					
0:00	1.0%	34%	2.6%	1.9%	0.6%	1.6%	49	53					
1:00	0.5%	37%	6.5%	3.9%	3.4%	1.4%	49	51					
2:00	0.4%	44%	2.9%	5.7%	3.2%	4.3%	49	53					
3:00	0.5%	58%	1.5%	3.8%	4.0%	2.0%	50	52					
4:00	1.8%	68%	2.5%	1.6%	3.8%	3.4%	52	55					
5:00	4.2%	64%	3.4%	1.9%	4.7%	3.4%	48	54					
6:00	6.1%	69%	2.9%	2.6%	4.6%	3.5%	46	49					
7:00	7.1%	65%	2.5%	1.9%	5.4%	3.9%	44	45					
8:00	6.6%	64%	1.4%	2.3%	5.5%	2.8%	39	46					
9:00	6.2%	66%	2.0%	2.5%	5.3%	2.9%	41	46					
10:00	4.8%	58%	3.0%	2.6%	5.2%	3.8%	41	46					
11:00	4.4%	62%	4.8%	3.1%	4.5%	3.8%	41	47					
12:00	4.3%	61%	4.1%	3.1%	4.0%	3.5%	40	47					
13:00	4.2%	60%	4.6%	4.1%	3.6%	3.4%	40	46					
14:00	4.8%	57%	5.1%	3.3%	2.9%	3.3%	37	39					
15:00	6.1%	51%	3.8%	2.1%	3.2%	2.8%	40	35					
16:00	6.0%	54%	2.6%	2.0%	3.4%	3.2%	42	23					
17:00	5.5%	57%	2.7%	0.6%	4.6%	3.9%	43	20					
18:00	5.3%	56%	2.3%	1.1%	3.1%	3.1%	43	25					
19:00	5.9%	38%	2.5%	0.6%	1.5%	1.0%	44	37					
20:00	4.9%	39%	1.7%	0.1%	3.9%	2.1%	45	27					
21:00	4.4%	43%	0.5%	0.5%	0.6%	1.0%	44	48					
22:00	3.1%	39%	1.0%	1.5%	1.3%	1.5%	48	48					
23:00	1.9%	37%	1.1%	0.0%	1.1%	0.2%	48	51					
	100%					Avg. Speed:	44	43					
EN	TRADA prog	gram is develope	ed by Ed Azimi	i @VDOT-NOV	A/TP			For	Question, Problem &	Comment:	Ed Azimi	V 2018-09	

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VERSION 2.2													
					Build -	50 ft Test F	Receiver				I.o.	udest Hour	(50 ft )
Compatible with ENTRADA v. 2	018-09		EB or NB			WB or SB		EB or NB	WB or SB	200 ft		uuest nour	(3011.)
Roadway	HOURS	Auto	Med Trk	Heavy Trk	Auto	Med Trk	Heavy Trk	Leq	Leq	Combine d	NB	SB	Combine
	0:00	56.2	43.7	57.2	59.0	47.9	52.2	59.8	60.1	63.0	6:00	16:00	16:00
Zone 1	1:00	55.3	48.0	48.6	56.1	46.6	54.4	56.8	58.6	60.8			
	2:00 3:00	53.0 55.8	45.0 47.4	50.6 55.8	53.9 53.1	48.2 47.9	51.9 52.5	55.4 59.1	56.7 56.5	59.1 61.0			
	4:00	62.6	52.5	58.1	57.8	50.8	56.0	64.2	60.5	65.8			
	5:00	66.5	57.6	61.8	61.5	56.0	59.4	68.2	64.3	69.6			
	6:00	68.5	60.0	67.0	63.0	57.8	59.9	71.2	65.5	72.2			
	7:00 8:00	58.5 65.3	57.5 58.7	63.9 63.1	64.6 64.9	58.6 59.9	62.1 62.8	65.7 67.9	67.2 67.8	69.5 70.8			
	9:00	67.1	59.6	65.2	64.4	58.6	62.4	69.7	67.1	71.6			
Leesburg Pike (Route 7)	10:00	66.1	59.8	64.2	64.4	59.1	63.1	68.8	67.5	71.2			
From	11:00	65.9	59.9	62.7	64.5	59.5	64.5	68.3	68.2	71.2			
Route 7917 (Reston Ave) To	12:00 13:00	65.5 65.6	60.6 59.5	63.8 64.0	65.1 65.4	57.8 56.4	64.1 63.9	68.5 68.5	68.1 68.0	71.3 71.3			
Route 606 (Baron Cameron Ave)	14:00	65.8	57.7	61.9	66.1	59.9	64.6	67.8	69.0	71.4			
	15:00	66.0	58.3	62.5	67.8	60.2	65.9	68.1	70.4	72.4			
	16:00	66.3	58.5	62.1	68.4	59.7	65.1	68.2	70.5	72.5			
	17:00 18:00	66.4 66.0	59.0 56.1	60.8 59.2	68.3 68.3	57.6 55.6	64.1 64.7	68.0 67.2	70.0 70.0	72.1 71.8			
	19:00	64.8	55.6	59.2	67.5	54.3	62.1	66.2	68.8	70.7			
	20:00	64.4	51.7	58.7	66.1	55.3	60.1	65.6	67.3	69.5			
	21:00	63.2	52.1	53.4	65.4	53.2	58.1	64.0	66.4	68.3			
	22:00 23:00	61.2 58.8	48.5 45.6	52.2 51.0	64.1 62.3	47.8 50.5	52.0 55.9	61.9 59.6	64.5 63.5	66.4 65.0			
	20.00	36.6	43.0	31.0	02.3	30.3	MAX	71.2	70.5	72.5			
	0:00	59.3	47.7	55.1	62.2	49.9	55.3	60.9	63.2	65.2	6:00	15:00	15:00
Zone 2	1:00	57.8	50.9	55.1	59.7	51.2	52.4	60.2	60.9	63.6			
	2:00 3:00	57.3 59.5	46.1 51.2	54.2 56.9	58.4 57.9	49.8 51.7	55.6 55.2	59.2 61.8	60.6	63.0 64.2			
	4:00	65.4	56.3	61.5	61.5	54.9	60.1	67.3	64.4	69.1			
	5:00	69.2	60.6	65.1	65.2	58.8	62.8	71.0	67.8	72.7			
	6:00	71.0	62.7	68.4	65.0	59.0	63.7	73.3	68.0	74.4			
	7:00 8:00	66.2 65.2	60.3 59.9	66.0 65.6	65.4 65.4	58.9 60.4	64.8 64.1	69.6 69.0	68.6 68.5	72.2 71.8			
	9:00	66.1	59.7	66.1	65.1	58.7	63.6	69.6	68.0	71.9			
Leesburg Pike (Route 7)	10:00	66.6	59.9	64.9	65.1	59.8	63.8	69.4	68.2	71.8			
From	11:00	65.5	60.0	63.7	64.7	59.6	64.4	68.4	68.2	71.3			
Route 606 (Baron Cameron Ave) To	12:00 13:00	65.4 65.3	60.3 60.2	64.7 64.1	65.3 65.7	58.9 59.3	64.3 64.4	68.8 68.5	68.4 68.7	71.6 71.6			
Route 694 (Lewinsville Rd)	14:00	66.0	59.3	63.9	68.4	60.7	66.5	68.6	71.0	73.0			
	15:00	67.7	59.5	64.4	70.8	62.9	68.0	69.8	73.1	74.7			
	16:00 17:00	67.8	59.5	64.4	67.0	59.6	66.1	69.9	70.0	72.9			
	18:00	68.2 67.0	59.4 57.8	64.2 63.1	60.5 64.1	57.1 57.9	64.4	70.1 68.8	66.4 67.3	71.6 71.1			
	19:00	65.4	56.2	60.2	69.5	57.1	63.6	66.9	70.7	72.2			
	20:00	66.1	53.3	60.0	68.3	56.0	61.4	67.3	69.3	71.4			
	21:00 22:00	65.9	54.5	56.5	67.4	54.1	59.5	66.7	68.2	70.5			
	23:00	64.9 59.9	51.7 48.8	56.6 50.5	66.4 65.4	54.4 54.5	59.4 57.1	65.7 60.6	67.5 66.3	69.7 67.4			
		33.3	1.0.0	30.3	00.7	55	MAX	73.3	73.1	74.7			
	0:00	56.7	49.0	53.1	59.8	45.6	55.3	58.8	61.2	63.2	6:00	7:00	7:00
Zone 3	1:00	53.8	50.4	53.6	56.4	49.9	51.5	57.6	58.3	61.0			
	2:00	53.7	46.7	55.1	54.8	48.1	54.9	57.8	58.3	61.1			

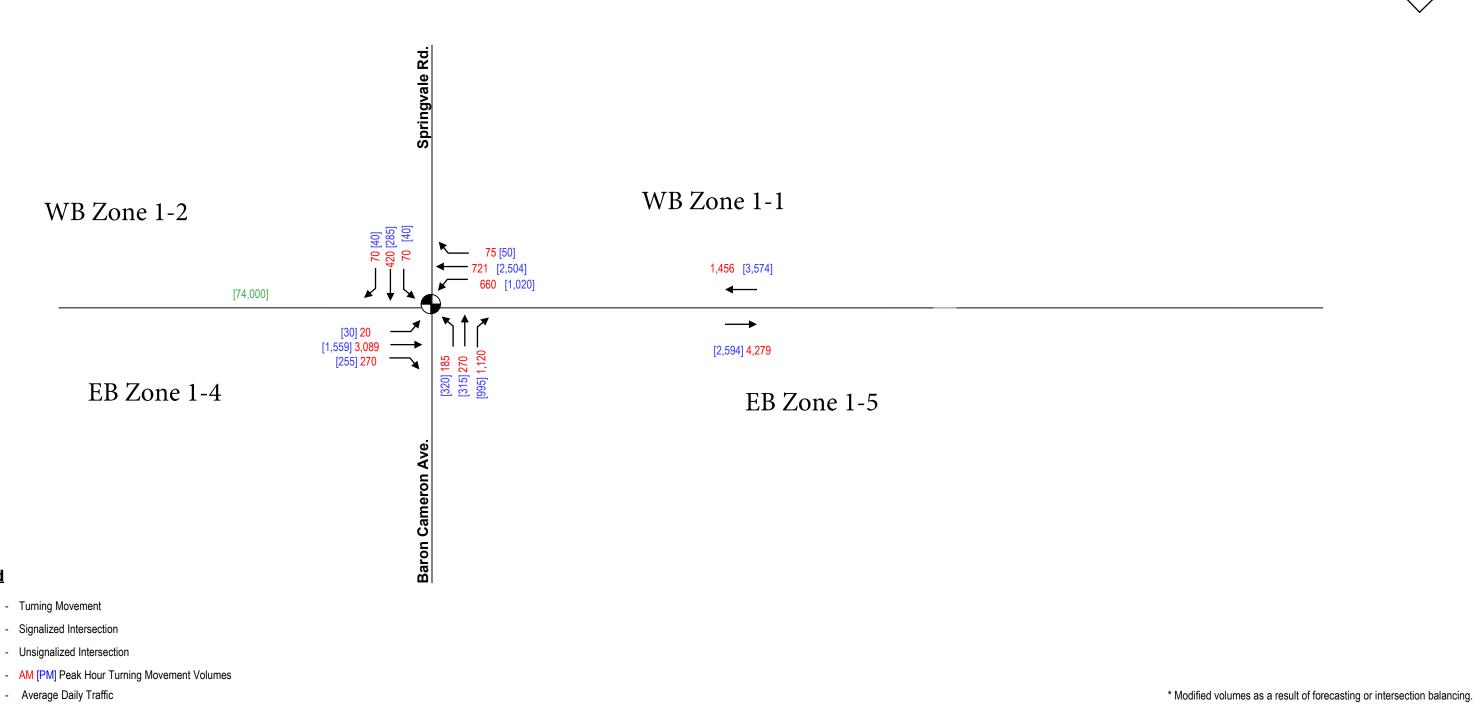
		I									
					Build -	50 ft Test I	Receiver				Loudest Hour (50 ft.)
Compatible with ENTRADA v. 2	018-09		EB or NB			WB or SB		EB or NB	WB or	200 ft	
	3:00	56.0	46.0	55.5	54.6	48.9	51.3	59.0	57.0	61.1	
	4:00	62.4	54.5	58.0	58.9	53.0	58.0	64.2	62.1	66.3	
	5:00	65.7	59.2	62.2	63.1	58.1	62.2	67.9	66.3	70.2	
	6:00	67.6	60.4	65.4	64.1	59.1	63.3	70.2	67.4	72.0	
	7:00	68.1	60.2	64.5	65.2	60.9	64.9	70.1	68.8	72.5	
	8:00	67.7	57.3	64.9	65.1	60.8	63.3	69.8	68.2	72.1	
	9:00	67.6	58.8	65.2	64.5	60.1	62.9	69.9	67.6	71.9	
Leesburg Pike (Route 7)	10:00	65.9	58.8	63.7	64.3	59.8	63.9	68.4	67.8	71.2	
From	11:00	65.7	60.8	64.4	63.5	58.3	63.1	68.8	66.9	71.0	
Route 694 (Lewinsville Rd)	12:00	65.5	59.9	64.2	63.5	57.8	62.7	68.6	66.8	70.8	
То	13:00	65.2	60.2	65.2	63.6	57.5	62.7	68.9	66.7	70.9	
Route 8912 (Jarrett Valley Dr)	14:00	65.5	61.0	64.6	63.7	56.9	63.0	68.9	66.8	71.0	
	15:00	66.3	60.3	63.2	66.0	59.3	64.2	68.7	68.8	71.7	
	16:00	66.5	58.8	63.2	60.2	56.5	62.5	68.7	65.2	70.3	
	17:00	66.5	58.9	57.8	56.6	56.5	62.7	67.6	64.4	69.3	
	18:00	66.2	57.9	60.2	58.9	55.2	61.6	67.7	64.1	69.2	
	19:00	65.1	57.1	56.4	67.2	57.0	60.7	66.2	68.4	70.4	
	20:00	64.4	54.7	47.9	62.9	58.4	61.6	64.9	66.1	68.5	
	21:00	64.4	49.3	54.8	65.6	51.4	59.1	64.9	66.6	68.9	
	22:00	62.4	50.4	57.7	64.3	53.5	59.6	63.9	65.8	68.0	
	23:00	60.1	48.5	43.5	62.4	50.8	48.9	60.4	62.9	64.8	

													TRAF	FFIC IN	IPUTS F	FOR W	VORST	CASE I	NOISE	HOUR	CALC	JATIC	N						
		Westbou	und CNEs				E	xisting	(2 Lan	ies)			Eac	h Lan	e Existi	ing		1	Fotal F	uture	Build (	3 Lan	es)		Each	Lane	Futur	e Builc	i
							EB			WB			EB			WB			EB			WB			EB			WB	
Zone	TNM Model	From	То	Speed	WCNH Time	Autos	Med	Heavy	Autos	Med	Heavy	Autos	Med	Heavy	Autos	Med	Heavy	Autos	Med	Heavy	Autos	Med	Heavy	Autos	Med	Heavy	Autos	Med	Heavy
1	1 WB	Reston Ave	Baron Cameron	55	15:00	1295	38	29	1974	59	63	648	19	15	987	30	32	1858	55	41	2830	84	90	619	18	14	943	28	30
2	2 WB	Baron Cameron	Lewinsville	55	15:00	1632	43	38	2274	72	68	816	22	19	1137	36	34	2729	72	63	3803	121	113	910 794	24	21	1268 774	40	38
3	3 WB	Lewinsville	Jarrett Valley	45	15:00	1505	61	34	1467	50	44	753	31	17	734	25	22	2382	96	53	2323	79	69	/94	32	18	//4	26	23
		Truck % Breakdow	n					Existin	ng														Build						
_					Total	EB Autos %	Med %	Heavy %			VB Med %	Heavy %								E				WB	Med %				
Zone	From	То	Speed	WCNH Time					Total										Total	Autos %		Heavy %	Total	Autos %		Heavy %			
			22	15:00									1					ľ				2.1		94.2		2.0			
2	Reston Ave	Baron Cameron	55 55	15:00 15:00	1362	95.1	2.8	2.1	2096	94.2	2.8	3.0							1954	95.1	2.8	2.1	3004	94.2	2.8	3.0			
2 3	Reston Ave Baron Cameror Lewinsville		55 55 45	15:00 15:00 15:00																		2.1		94.2 94.2 94.0		3.0 2.8 2.8			
_	Baron Cameror	n Lewinsville Jarrett Valley	55 45	15:00	1362 1713	95.1 95.3	2.8 2.5	2.1	2096 2414	94.2 94.2	2.8 3.0	3.0	TRAF	FFIC IN	IPUTS F	FOR W	VORST	CASE I	1954 2864 2531	95.1 95.3 94.1	2.8 2.5 3.8	2.2	3004 4037 2471	94.2	2.8 3.0	2.8			
_	Baron Cameror	n Lewinsville	55 45	15:00	1362 1713	95.1 95.3	2.8 2.5 3.8	2.1	2096 2414 1561	94.2 94.2 94.0	2.8 3.0	3.0			IPUTS F		VORST		1954 2864 2531 NOISE	95.1 95.3 94.1 HOUR	2.8 2.5 3.8	2.2 2.1 JATIC	3004 4037 2471	94.2	2.8 3.0 3.2	2.8	ane Bu	ıild	
_	Baron Cameror	n Lewinsville Jarrett Valley	55 45	15:00	1362 1713	95.1 95.3	2.8 2.5 3.8	2.1 2.2 2.1	2096 2414 1561	94.2 94.2 94.0	2.8 3.0	3.0					VORST		1954 2864 2531 NOISE	95.1 95.3 94.1 HOUR	2.8 2.5 3.8	2.2 2.1 JATIC	3004 4037 2471	94.2	2.8 3.0 3.2	2.8	ane Bu	ıild wb	
_	Baron Cameron Lewinsville	Lewinsville Jarrett Valley  Eastbou	nd CNEs	15:00 15:00	1362 1713 1600	95.1 95.3 94.1	2.8 2.5 3.8	2.1 2.2 2.1 xisting	2096 2414 1561 (2 Lan	94.2 94.2 94.0 94.0	2.8 3.0 3.2	3.0 2.8 2.8 Autos	Eac EB	ch Lan	e Exist	ing wb	Heavy	Autos	1954 2864 2531 NOISE Fotal F	95.1 95.3 94.1 HOUR	2.8 2.5 3.8 CCALCU	2.2 2.1 JATIO 3 Lan	3004 4037 2471 DN es)	94.2 94.0	2.8 3.0 3.2	2.8 2.8 2.8	Autos	WB	Heavy
Zone	Baron Cameron Lewinsville  TIM Model 1EB	Lewinsville Jarrett Valley  Eastbou	nd CNEs	15:00 15:00 Speed 55	1362 1713 1600 WCNH Time 6:00	95.1 95.3 94.1 Autos 2306	2.8 2.5 3.8 Eb Med 56	2.1 2.2 2.1 xisting	2096 2414 1561 (2 Lan	94.2 94.2 94.0 100 WB Med 34	2.8 3.0 3.2 Heavy	3.0 2.8 2.8 2.8 Autos 1153	EB Med 28	Ch Lan	e Existi	ing WB Med	Heavy 8	Autos 3307	1954 2864 2531 NOISE Fotal F	95.1 95.3 94.1 HOUR Luture	2.8 2.5 3.8 CCALCU Build (	2.2 2.1 JATIC 3 Lan WB	3004 4037 2471 DN es)	94.2 94.0 Autos 1102	2.8 3.0 3.2 EB Med 27	2.8 2.8 2.8 Ach La	Autos 313	WB Med	7
Zone 1 2	Baron Cameron Lewinsville  TNM Model 1EB 2:EB	Eastbou  From Reston Ave Baron Cameron	ss 45  nd CNEs  To Baron Cameron Lewinsville	15:00 15:00 5peed 55 55	1362 1713 1600 WCNH Time 6:00 6:00	95.1 95.3 94.1 Autos 2306 2398	2.8 2.5 3.8 EB Med 56 69	2.1 2.2 2.1 xisting	2096 2414 1561 (2 Lan Autos 656 958	94.2 94.2 94.0 94.0 WB Med 34 40	2.8 3.0 3.2 Heavy 16 34	3.0 2.8 2.8 2.8 Autos 1153 1199	EB Med 28 35	Heavy 41 37	Autos 328 479	wB Med 17 20	Heavy 8	Autos 3307 4010	1954 2864 2531 NOISE Fotal F EB Med 81	95.1 95.3 94.1 HOUR Luture	2.8 2.5 3.8 CALCU Build (	2.2 2.1 JATIC 3 Lan WB Med 49 67	3004 4037 2471 DN es)	94.2 94.0 Autos 1102 1337	EB Med 27 38	2.8 2.8 ach La	Autos 313 534	WB  Med  16  22	7 19
Zone	Baron Cameron Lewinsville  TIM Model 1EB	Lewinsville Jarrett Valley  Eastbou	nd CNEs	15:00 15:00 Speed 55	1362 1713 1600 WCNH Time 6:00	95.1 95.3 94.1 Autos 2306	2.8 2.5 3.8 Eb Med 56	2.1 2.2 2.1 xisting	2096 2414 1561 (2 Lan Autos 656 958 915	94.2 94.2 94.0 100 WB Med 34	2.8 3.0 3.2 Heavy	3.0 2.8 2.8 2.8 Autos 1153	EB Med 28	Ch Lan	e Existi	ing WB Med	Heavy 8	Autos 3307	1954 2864 2531 NOISE Fotal F	95.1 95.3 94.1 HOUR Luture	2.8 2.5 3.8 CCALCU Build (	2.2 2.1 JATIC  3 Lan  WB  Med  49  67  72	3004 4037 2471 DN es)	94.2 94.0 Autos 1102	2.8 3.0 3.2 EB Med 27	2.8 2.8 2.8 Ach La	Autos 313	WB Med	7
Zone 1 2	Baron Cameron Lewinsville  TNM Model T1EB 2EB 3EB	Eastbou  From Reston Ave Baron Cameron	55 45  To Baron Cameron Lewinsville Jarrett Valley	15:00 15:00 5peed 55 55	1362 1713 1600 WCNH Time 6:00 6:00	95.1 95.3 94.1 Autos 2306 2398 2045	2.8 2.5 3.8 EB Med 56 69	2.1 2.2 2.1 xisting	2096 2414 1561 (2 Lan Autos 656 958 915	94.2 94.2 94.0 94.0 WB Med 34 40 46	2.8 3.0 3.2 Heavy 16 34 35	3.0 2.8 2.8 2.8 Autos 1153 1199	EB Med 28 35	Heavy 41 37	Autos 328 479	wB Med 17 20	Heavy 8	Autos 3307 4010	1954 2864 2531 NOISE Fotal F EB Med 81	95.1 95.3 94.1 HOUR tuture	2.8 2.5 3.8 CCALCU Build ( Autos 940 1602 1448	2.2 2.1 JATIC  3 Lan  WB  Med  49  67  72	3004 4037 2471 DN es)	94.2 94.0 Autos 1102 1337 1079	2.8 3.0 3.2 EB Med 27 38 33	2.8 2.8 ach La	Autos 313 534	WB  Med  16  22	7 19
Zone 1 2 3 3	Baron Cameror Lewinsville  TNM Model 1EB 2EB 3EB	Eastbou  From Reston Ave Baron Cameron Lewinsville Truck % Breakdow	55 45  A5  To Baron Cameron Lewinsville Jarrett Valley	15:00 15:00 15:00	1362 1713 1600 WCNH Time 6:00 6:00	95.1 95.3 94.1 Autos 2306 2398 2045	EB Med 56 69 63	2.1 2.2 2.1  Xisting  Heavy 81 74 56 Existin	2096 2414 1561 (2 Lan Autos 656 958 915	94.2 94.2 94.0 10 10 10 10 10 10 10 10 10 10 10 10 10	2.8 3.0 3.2 Heavy 16 34 35	Autos 1153 1199 1023	EB Med 28 35	Heavy 41 37	Autos 328 479	wB Med 17 20	Heavy 8	Autos 3307 4010	1954 2864 2531 NOISE Fotal F EB Med 81 1115 99	95.1 95.3 94.1 HOUR Future Heavy 116 123 89	2.8 2.5 3.8 CALCU Build ( Autos 940 1602 1448	2.2 2.1 JATIO 3 Lan WB Med 49 67 72	3004 4037 2471 DN es)	94.2 94.0 Autos 1102 1337 1079	2.8 3.0 3.2 EB Med 27 38 33	2.8 2.8 2.8 41 30	Autos 313 534	WB  Med  16  22	7 19
Zone 1 2	Baron Cameron Lewinsville  TNM Model T1EB 2EB 3EB	Eastbou  From Reston Ave Baron Cameron Lewinsville	55 45  To Baron Cameron Lewinsville Jarrett Valley	15:00 15:00 5peed 55 55	1362 1713 1600 WCNH Time 6:00 6:00	95.1 95.3 94.1 Autos 2306 2398 2045	2.8 2.5 3.8 EB Med 56 69	2.1 2.2 2.1  Xisting  Heavy 81 74 56 Existin	2096 2414 1561 (2 Lan Autos 656 958 915	94.2 94.2 94.0 94.0 WB Med 34 40 46	2.8 3.0 3.2 Heavy 16 34 35	3.0 2.8 2.8 2.8 Autos 1153 1199	EB Med 28 35	Heavy 41 37	Autos 328 479	wB Med 17 20	Heavy 8	Autos 3307 4010	1954 2864 2531 NOISE Fotal F EB Med 81	95.1 95.3 94.1 HOUR tuture	2.8 2.5 3.8 CALCU Build ( Autos 940 1602 1448	2.2 2.1 JATIC  3 Lan  WB  Med  49  67  72	3004 4037 2471 DN es)	94.2 94.0 Autos 1102 1337 1079	2.8 3.0 3.2 EB Med 27 38 33	2.8 2.8 ach La	Autos 313 534	WB  Med  16  22	7 19
Zone 1 2 3 3	Baron Cameron Lewinsville  TNM Model 1EB 2EB 3EB	Eastbou  From Reston Ave Baron Cameron Lewinsville Truck % Breakdow	TO Baron Cameron Lewinsville Jarrett Valley  n Speed	15:00 15:00 15:00 5peed 55 55 45	1362 1713 1600 WCNH Time 6:00 6:00	95.1 95.3 94.1 Autos 2306 2398 2045	2.8 2.5 3.8 EB Med 56 69 63	2.1 2.2 2.1  xisting  Heavy 81 74 56 Existin	2096 2414 1561 (2 Lan Autos 656 958 915	94.2 94.2 94.0 10ES) WB Med 34 40 46	2.8 3.0 3.2  Heavy 16 34 35	Autos 1153 1199 1023	EB Med 28 35	Heavy 41 37	Autos 328 479	wB Med 17 20	Heavy 8	Autos 3307 4010	1954 2864 2531 NOISE Fotal F EB Med 81 115 99	95.1 95.3 94.1 HOUR Heavy 116 123 89	2.8 2.5 3.8 CCALCU Build ( Autos 940 1602 1448	2.2 2.1 JATIC 3 Lan WB Med 49 67 72	3004 4037 2471 DN es) Heavy 22 57 55 8uild	94.2 94.0 Autos 1102 1337 1079 WB Autos %	EB Med 27 38 33	2.8 2.8 2.8 Ach La Heavy 39 41 30	Autos 313 534	WB  Med  16  22	7 19



Year 2040 Balanced Traffic Volumes for Noise Analysis ZONE 1





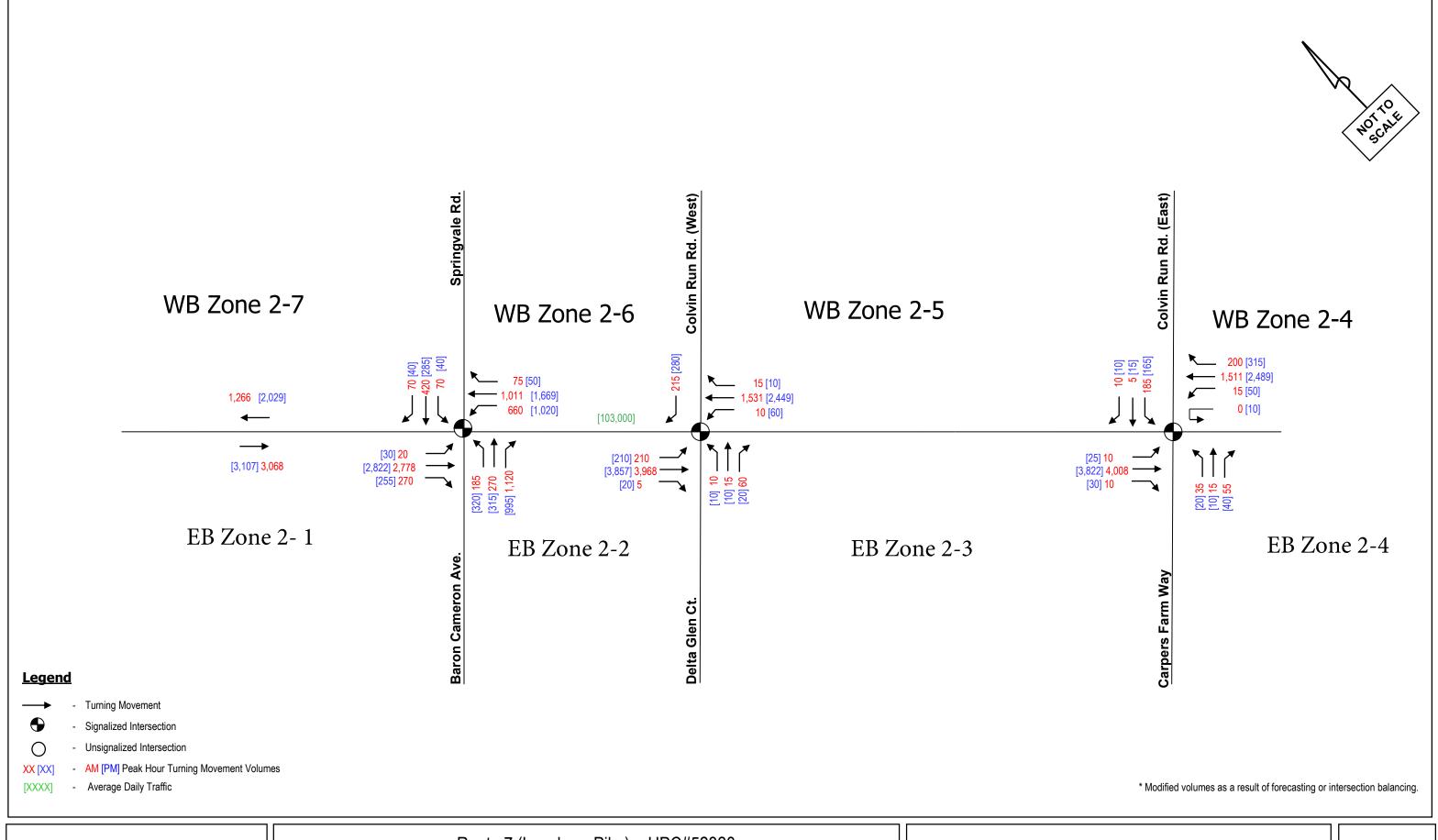
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Year 2040 Balanced Traffic Volumes for Noise Analysis ZONE 1

E.	ASTBOUND	TRAFFIC Z	one 1 (Rest	on > Baron (	Cameron) WCNI	15:00 PM		WE	STBOUND	TRAFFIC Zo	ne 1 (Resto	on > Baron (	Cameron) W	/CNH 15:00 PM	
		Route 3	7 EB Zone 1	1 Begin > R	eston Ave					Route 7 WB	Zone 1-1 (2	Zone 2 > Ba	ron Camero	n)	
						Total (3 Lanes)	1 Lane							Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	2211	737	Total Vehicles	Cars%	MT%	HT%		Cars	3367	1122
2325	0.951	0.028	0.021		MT	65	22	3574	0.942	0.028	0.03		MT	100	33
					HT	49	16						HT	107	36
						2325								3574	
		Route 7 EB	Zone 1-2 (F	Reston Ave >	Reston Pkwy)				Ro	oute 7 WB 2	one 1-2 (Ba	aron Camer	on >Utterba	ck)	_
				_		Total (3 Lanes)	1 Lane					_		Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	2106	702	Total Vehicles	Cars%	MT%	HT%		Cars	2698	899
2214	0.951	0.028	0.021		MT	62	21	2864	0.942	0.028	0.03		MT	80	27
					HT	46	15						HT	86	29
						2214								2864	
		Route 7 El	3 Zone 1-3 (	Resont Pkwy	y > Utterback)				F	Route 7 WB	Zone 1-3 (l	Jtterback >	Reston Pkw	,,	
		1	,	-		Total (3 Lanes)	1 Lane		1			-		Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	1858	619	Total Vehicles	Cars%	MT%	HT%		Cars	2830	943
1954	0.951	0.028	0.021		MT	55	18	3004	0.942	0.028	0.03		MT	84	28
					HT	41	14						HT	90	30
						1954								3004	
	R	Route 7 EB	Zone 1-4 (U	tterback > B	aron Cameron)				R	oute 7 WB	Zone 1-4 (R	eston Pkwy	> Reston A	•	
	1		ı	a i	•	Total (3 Lanes)	1 Lane			1	ı	<b>a</b>		Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	1754	585	Total Vehicles	Cars%	MT%	HT%		Cars	3032	1011
1844	0.951	0.028	0.021		MT	52	17	3219	0.942	0.028	0.03		MT	90	30
					HT	39	13						HT	97	32
						1844								3219	
		Route 7 E	B Zone 1-5 (	(Baron Came	eron > Zone 2					Route 7	WB Zone 1	-5 (Reston A	Ave > End)		
	T = -, 1			1 1		Total (3 Lanes)	1 Lane			T		1		Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%	4	Cars	2467	822	Total Vehicles	Cars%	MT%	HT%	4	Cars	3059	1020
2594	0.951	0.028	0.021	J	MT	73	24	3247	0.942	0.028	0.03	]	MT	91	30
					HT	54	18						HT	97	32
						2594	J							3247	<u> </u>

	EASTBOU	ND TRAFFIC	Zone 1 (Reston	> Baron Camero	on) WCNH	6:00 AM		W	ESTBOUND	TRAFFICZo	ne 1 (Resto	on > Baron (	Cameron) V	VCNH 6:00 AM	
		Route	e 7 EB Zone 1-1	Begin > Reston A	Ave				R	Route 7 WB	Zone 1-1 (2	Zone 2 > Ba	ron Camero	ın)	
						Total (3 Lanes)	1 Lane							Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	3663	1221	Total Vehicles	Cars%	MT%	HT%		Cars	1354	451
3880	0.944	0.023	0.033		MT	89	30	1456	0.93	0.048	0.022		MT	70	23
					HT	128	43						HT	32	11
						3880								1456	
		Route 7	B Zone 1-2 (Res	ton Ave > Restor	n Pkwy)				Ro	oute 7 WB 2	Zone 1-2 (Ba	aron Camer	on >Utterba	ack)	
						Total (3 Lanes)	1 Lane							Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	3695	1232	Total Vehicles	Cars%	MT%	HT%		Cars	908	303
3914	0.944	0.023	0.033	] [	MT	90	30	976	0.93	0.048	0.022		MT	47	16
					HT	129	43						HT	21	7
						3914								976	
		Route 7	EB Zone 1-3 (Res	sont Pkwy > Utte	erback)				R	loute 7 WB	Zone 1-3 (l	Jtterback >	Reston Pkw	/y)	
						Total (3 Lanes)	1 Lane							Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	3308	1103	Total Vehicles	Cars%	MT%	HT%		Cars	940	313
3504	0.944	0.023	0.033	]	MT	81	27	1011	0.93	0.048	0.022		MT	49	16
					HT	116	39						HT	22	7
						3504								1011	
		Route 7 E	B Zone 1-4 (Utte	erback > Baron Ca	ameron)				Ro	oute 7 WB	Zone 1-4 (R	eston Pkwy	> Reston A	ve)	
				_		Total (3 Lanes)	1 Lane					_		Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	3190	1063	Total Vehicles	Cars%	MT%	HT%		Cars	963	321
3379	0.944	0.023	0.033	]	MT	78	26	1036	0.93	0.048	0.022		MT	50	17
					HT	112	37						HT	23	8
						3379								1036	
		Route 7	EB Zone 1-5 (Ba	ron Cameron > Z	Zone 2						Route 7 V	VB Zone 1-5	j		
				-		Total (3 Lanes)	1 Lane					-		Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%	<u> </u>	Cars	4039	1346	Total Vehicles	Cars%	MT%	HT%		Cars	974	325
4279	0.944	0.023	0.033	J L	MT	98	33	1047	0.93	0.048	0.022	]	MT	50	17
					HT	141	47						HT	23	8
						4279								1047	
							·	 							

		2018 Pe	ak Total		AM			PM	
Roadway	Movement	AM	PM	Cars	MT	HT	Cars	MT	HT
Reston Ave	NB Thru	2	0	2	0	0	0	0	0
	NB Right	70	30	68	2	0	29	1	0
	NB Left	22	70	21	1	0	68	2	0
Rt 7 Turning Lanes	EB Right	27	75	26	1	0	73	2	0
	EB Left	9	70	9	0	0	68	2	0
	WB Left	11	40	11	0	0	39	1	0
	WB Right	0	1	0	0	0	1	0	0
Reston Pky	NB Thru	5	5	5	0	0	5	0	0
	NB Left	280	415	277	3	0	411	4	0
	NB Right	210	170	208	2	0	168	2	0
Rt 7 Turning Lanes	EB Right	620	430	614	6	0	426	4	0
	EB Left	5	5	5	0	0	5	0	0
	WB Left	255	200	252	3	0	198	2	0
	WB Right	5	5	5	0	0	5	0	0
Utterback Store Road	SB Right	115	330	112	3	0	320	10	0
	SB Left	70	110	68	2	0	107	3	0
Rt 7 Turning Lanes	WB Right	80	190	78	2	0	184	6	0
	EB Left	195	220	189	6	0	213	7	0
Baron Cameron Ave	NB Right	1120	995	1098	11	11	975	10	10
	NB Left	185	320	181	2	2	314	3	3
	NB Thru	270	315	265	3	3	309	3	3
Rt 7 Turning Lanes	WB Left	660	1020	647	7	7	1000	10	10
	EB Right	270	255	265	3	3	250	3	3
pringvale	SB Left	70	40	68	2	0	39	1	0
	SB Thru	420	285	407	13	0	276	9	0
	SB Right	70	40	68	2	0	39	1	0
Rt 7 Turning Lanes	EB Left	20	30	19	1	0	29	1	0
	WB Right	75	50	73	2	0	49	2	0



Year 2040 Balanced Traffic Volumes for Noise Analysis ZONE 2

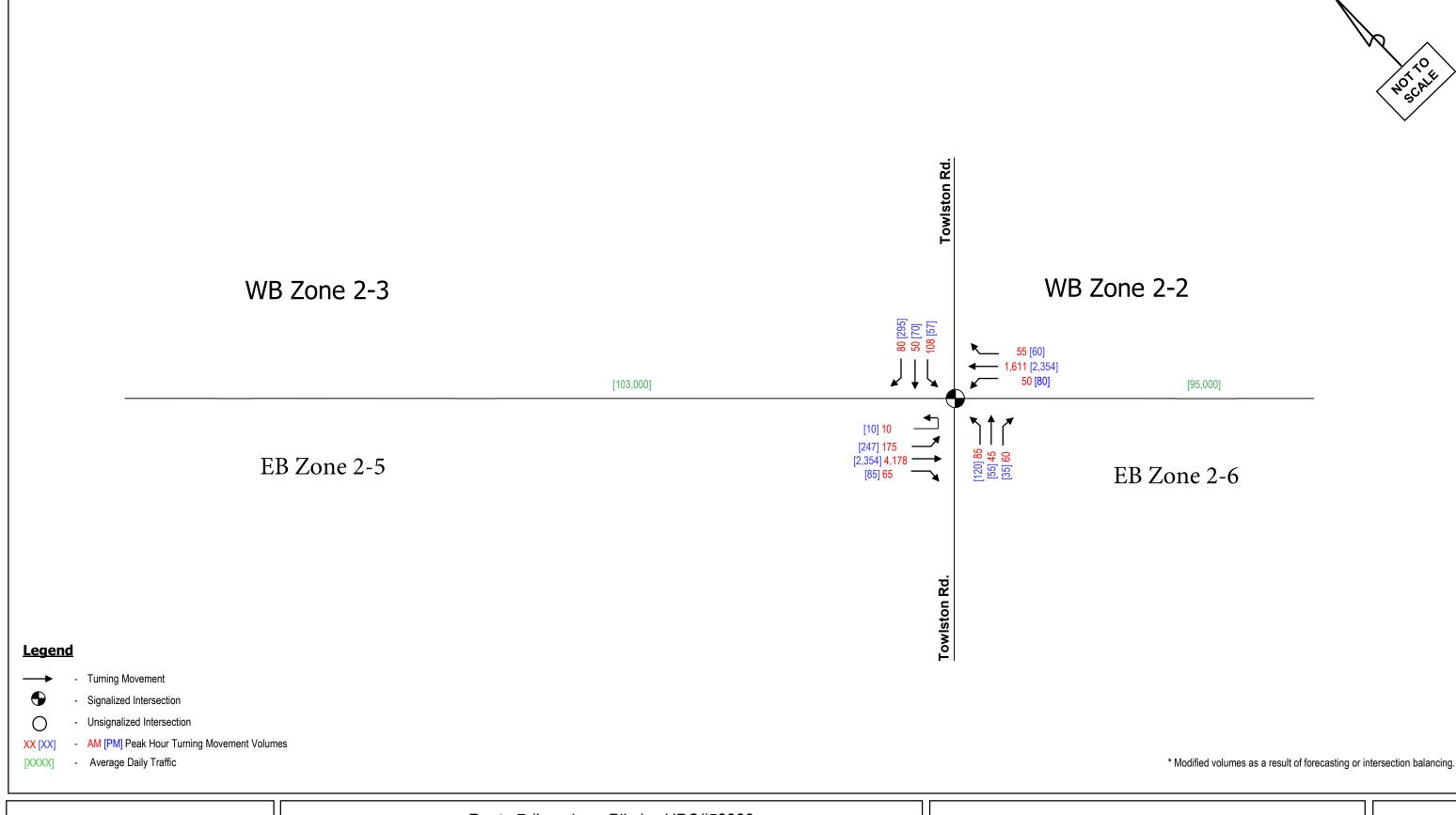


Fairfax, Virginia

Year 2040 Balanced Traffic Volumes for Noise Analysis ZONE 2

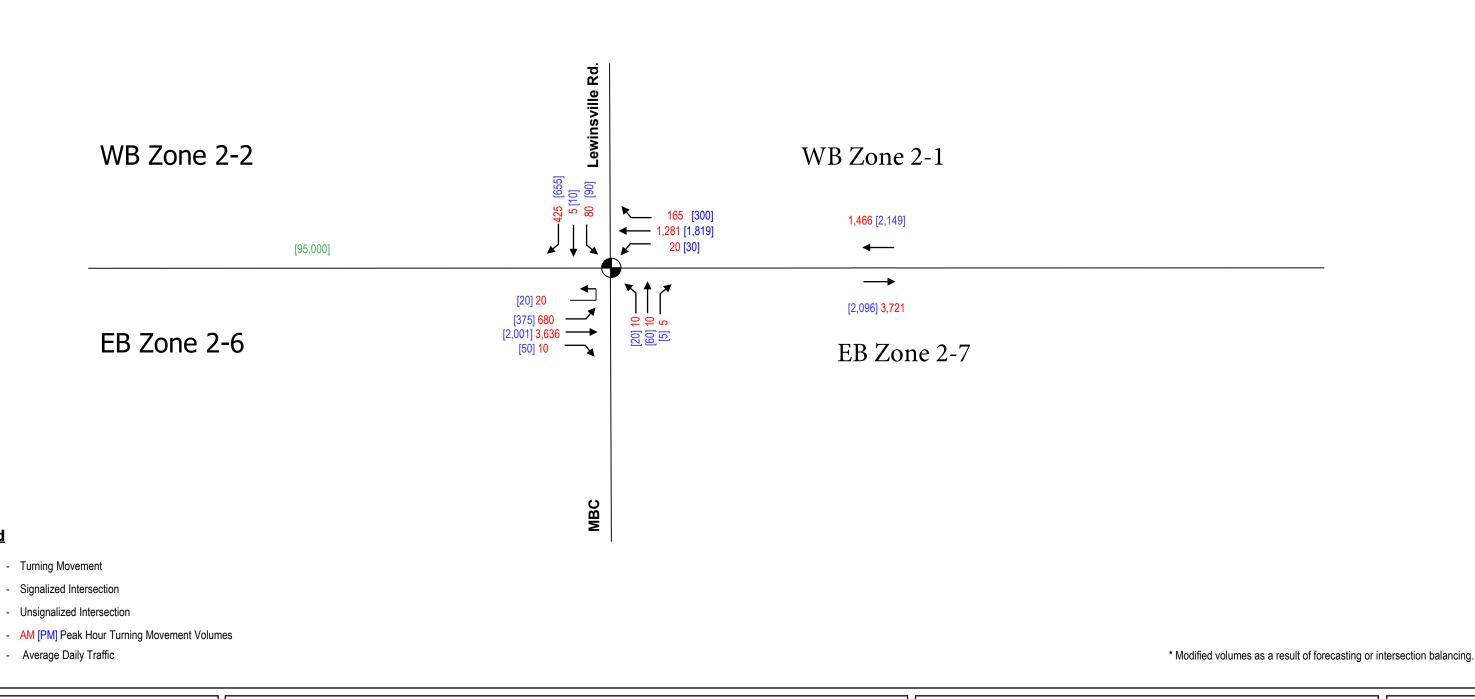
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Year 2040 Balanced Traffic Volumes for Noise Analysis ZONE 2





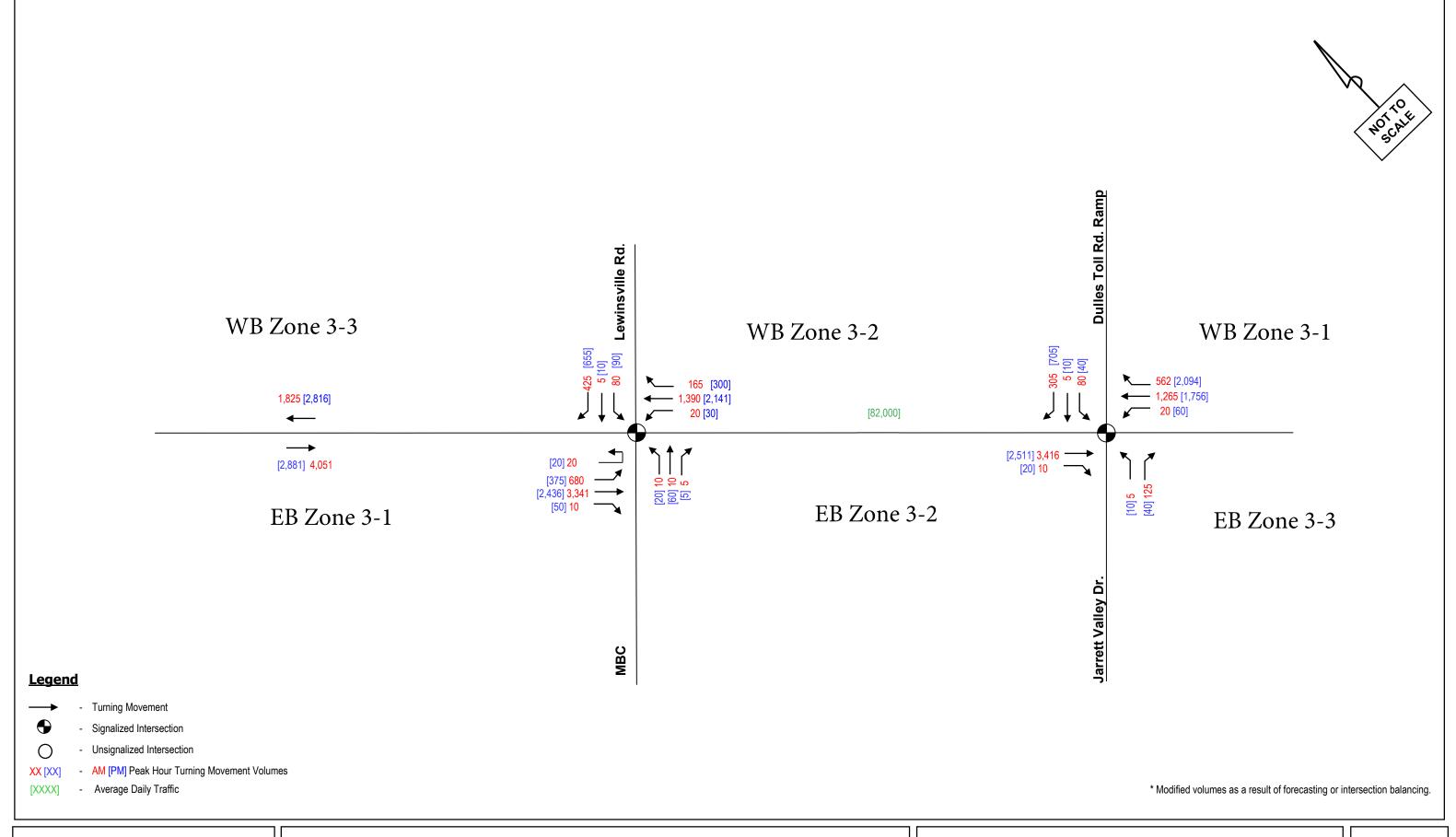
<u>Legend</u>

Year 2040 Balanced Traffic Volumes for Noise Analysis ZONE 2

E.	ASTBOUND	TRAFFIC Zo	ne 2 (Baror	Cameron :	> Lewinsville) W	/CNH 15:00 PM			WES	TBOUND T	RAFFIC Zon	e 2 (Baron	Cameron >	Lewinsville)	WCNH 15:00 PM	
		Route 7 I	R 70ne 2-1	(70ne 1 > R	aron Cameron)						Route 7 \	MR Zone 2.	1 (7one 3 >	Lewinsville)		
		Noute 7 i	LD ZOITC Z I	(ZONC 1 > D	aron cameron)	Total (3 Lanes)	1 Lane				Houte 7	V D ZOTIC Z .	I (ZONC 3 >	<u>LCWIII3VIIIC)</u>	Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%	ſ	Cars	2961	987	1	Total Vehicles	Cars%	MT%	HT%	1	Cars	2024	675
3107	0.953	0.025	0.022	-	MT	78	26		2149	0.942	0.03	0.028		MT	64	21
					HT	68	23	1					1	HT	60	20
				L		3107		1							2149	
		Route 7 EB	Zone 2-2 (E	Baron Came	ron > Delta Gate						Route 7 W	/B Zone 2-2	(Lewinsville	> Towlsont		
						Total (3 Lanes)	1 Lane								Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	3895	1298	1	Total Vehicles	Cars%	MT%	HT%	1	Cars	2349	783
4087	0.953	0.025	0.022	-	MT	102	34		2494	0.942	0.03	0.028		MT	75	25
					HT	90	30						_	HT	70	23
				-		4087									2494	
		Route	7 EB Zone 2	-3 (Delta Ga	te > Carpers)						Route 7	WB Zone 2-	3 (Towlstor	ı > Beulah)		
						Total (3 Lanes)	1 Lane								Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	3695	1232	1	Total Vehicles	Cars%	MT%	HT%	1	Cars	2618	873
3877	0.953	0.025	0.022		MT	97	32		2779	0.942	0.03	0.028		MT	83	28
					HT	85	28						='	HT	78	26
				-		3877									2779	
		Rout	e 7 EB Zone	2-4 (Carper	s > Beulah)						Route 7	WB Zone 2	-4 (Beulah :	> Carpers)		
				_		Total (3 Lanes)	1 Lane						_		Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	3847	1282		Total Vehicles	Cars%	MT%	HT%		Cars	2698	899
4037	0.953	0.025	0.022		MT	101	34		2864	0.942	0.03	0.028		MT	86	29
					HT	89	30							HT	80	27
						4037									2864	
		Route	7 EB Zone	2-5 (Beulah	> Towlston)						Route 7 \	WB Zone 2-	Carpers >	Delta Gate)		
				_		Total (3 Lanes)	1 Lane						_		Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	2569	856		Total Vehicles	Cars%	MT%	HT%		Cars	2373	791
2696	0.953	0.025	0.022		MT	67	22		2519	0.942	0.03	0.028		MT	76	25
					HT	59	20							HT	71	24
						2696									2519	
		Route 7	EB Zone 2-	6 (Towlston	> Lewinsville)					Ro	oute 7 WB Z	<mark>one 2-6 (De</mark>	elta Gate > E	Baron Came	<u> </u>	
						Total (3 Lanes)	1 Lane			,			•		Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	2331	777		Total Vehicles	Cars%	MT%	HT%		Cars	2580	860
2446	0.953	0.025	0.022		MT	61	20		2739	0.942	0.03	0.028		MT	82	27
					HT	54	18							HT	77	26
						2446									2739	
		Route	7 EB Zone 2	-7 (Lewinsv	ille > Zone 3)						Route 7 WE	3 Zone 2-7 (	Baron Came	ron > Zone	•	
	1			ı r		Total (3 Lanes)	1 Lane			ı	1		1		Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	1997	666		Total Vehicles	Cars%	MT%	HT%		Cars	1911	637
2096	0.953	0.025	0.022		MT	52	17		2029	0.942	0.03	0.028		MT	61	20
					HT	46	15	Į						HT	57	19
						2096									2029	

	EASTBOUND TRAFF	FIC Zone 2 (Baron Ca	meron > Lewinsville) WC	NH 6:00 AM			WES	TBOUND T	RAFFIC Zon	e 2 (Baron (	Cameron > L	ewinsville.	WCNH6:00 AM	
	Rout	te 7 EB Zone 2-1 (Zo	ne 1 > Baron Cameron)						Route 7 W	/B Zone 2-1	(Zone 3 > Le	ewinsville)		
				Total (3 Lanes)	1 Lane								Total (3 Lanes)	1 Lane
Total Vehicles	Cars% MT%	% HT%	Cars	2924	975		Total Vehicles	Cars%	MT%	HT%		Cars	1360	453
3068	0.953 0.02	5 0.022	MT	77	26		1466	0.928	0.039	0.033		MT	57	19
			HT	67	22							HT	48	16
				3068									1466	
	Route	7 EB Zone 2-2 (Baro	n Cameron > Delta Gate)						Route 7 W	3 Zone 2-2 (	Lewinsville >	> Towlsont		
				Total (3 Lanes)	1 Lane								Total (3 Lanes)	1 Lane
Total Vehicles	Cars% MT9		Cars	3949	1316		Total Vehicles	Cars%	MT%	HT%	_	Cars	1592	531
4183	0.944 0.02	7 0.029	MT	113	38		1716	0.928	0.039	0.033		MT	67	22
			HT	121	40							HT	57	19
				4183									1716	
	Ro	oute 7 EB Zone 2-3 (I	Delta Gate > Carpers)			ļ			Route 7 \	VB Zone 2-3	3 (Towlston:	> Beulah)		
	1	1	1	Total (3 Lanes)	1 Lane				1				Total (3 Lanes)	1 Lane
Total Vehicles	Cars% MT9		Cars	3802	1267	ŀ	Total Vehicles	Cars%	MT%	HT%	-	Cars	1657	552
4028	0.944 0.02	7 0.029	MT	109	36	ŀ	1786	0.928	0.039	0.033		MT	70	23
			HT	117	39							HT	59	20
		2 7.50.7	// 5   1   1	4028	<u> </u>	ŀ					1/5 11	٥ ١	1786	
		Route 7 EB Zone 2-4	(Carpers > Beulan)			ŀ			Route /	WB Zone 2-	4 (Beulah >	Carpers)	= : ! /ā :	
T-1-11/-1-1-1-	C0/ NATO	)/ LITO/	1	Total (3 Lanes)	1 Lane	-	T-4-13/-1-1-1	C0/	NATO/	LITO	Г	C	Total (3 Lanes)	1 Lane
Total Vehicles 4248	Cars% MT9 0.944 0.02		Cars MT	4010 115	1337 38	ŀ	Total Vehicles 1726	Cars% 0.928	MT% 0.039	HT% 0.033	-	Cars MT	1602 67	534 22
4246	0.944 0.02	0.029	J WIT	123	41	ŀ	1/20	0.928	0.039	0.055	-	HT	57	19
			пі	4248	41						L	пі	1726	19
	D	oute 7 EB Zone 2-5	(Roulah > Towlston)	4246					Poute 7 M	/R 70ng 2-5	(Carpers >D	elta Catel	1720	
	10	oute / LD Zone 2-3	(Deciral > Townston)	Total (3 Lanes)	1 Lane	ŀ			Noute / Vi	TO ZOITE Z-3	(Carpers >D	eita Gate)	Total (3 Lanes)	1 Lane
Total Vehicles	Cars% MT%	% HT%	Cars	4180	1393		Total Vehicles	Cars%	MT%	HT%	Г	Cars	1444	481
4428	0.944 0.02		MT	120	40	ŀ	1556	0.928	0.039	0.033		MT	61	20
1120	0.5 0.02	0.023	HT	128	43	ŀ	1550	0.020	0.003	0.000	·	HT	51	17
				4428	1						_		1556	
	Rou	ute 7 EB Zone 2-6 (To	owlston > Lewinsville)			ľ		Ro	ute 7 WB Zo	ne 2-6 (Del	ta Gate > Ba	ron Camer	on)	
			-	Total (3 Lanes)	1 Lane								Total (3 Lanes)	1 Lane
Total Vehicles	Cars% MT9	% HT%	Cars	4103	1368	ľ	Total Vehicles	Cars%	MT%	HT%	Γ	Cars	1620	540
4346	0.944 0.02	7 0.029	MT	117	39	j	1746	0.928	0.039	0.033	Ī	MT	68	23
	<u> </u>		HT	126	42							HT	58	19
				4346									1746	
	Ro	oute 7 EB Zone 2-7 (	Lewinsville > Zone 3)					F	Route 7 WB	Zone 2-7 (B	aron Camer	on > Zone	1)	
				Total (3 Lanes)	1 Lane								Total (3 Lanes)	1 Lane
Total Vehicles	Cars% MT9		Cars	3513	1171		Total Vehicles	Cars%	MT%	HT%		Cars	1175	392
3721	0.944 0.02	7 0.029	MT	100	33		1266	0.928	0.039	0.033	<u> </u>	MT	49	16
			HT	108	36							HT	42	14
				3721	1								1266	

Route 7 Wide	ning 2040 Peak Ho	ur Traffi	c for Side	e Roads Z	one 2 Ba	ron Cam	eron > Le	winsville	
Roadway	Movement		ak Total		AM			PM	
nodaway		AM	PM	Cars	MT	HT	Cars	MT	HT
Baron Cameron Ave	NB Right	1120	995	1098	11	11	975	10	10
	NB Left	185	320	181	2	2	314	3	3
	NB Thru	270	315	265	3	3	309	3	3
Rt 7 Turning Lanes	WB Left	660	1020	647	7	7	1000	10	10
	EB Right	270	255	265	3	3	250	3	3
Springvale	SB Left	70	40	68	2	0	39	1	0
	SB Thru	420	285	407	13	0	276	9	0
	SB Right	70	40	68	2	0	39	1	0
Rt 7 Turning Lanes	EB Left	20	30	19	1	0	29	1	0
	WB Right	75	50	73	2	0	49	2	0
Colvin Run Road -West	SB Right	215	280	211	2	2	274	3	3
Rt 7 Turning Lanes	WB Right	15	10	15	0	0	10	0	0
	EB Left	210	210	206	2	2	206	2	2
Delta Glen Ct	NB Right	60	20	59	1	0	20	0	0
	NB Thru	15	10	15	0	0	10	0	0
Dt 7 Turning Long-	NB Left	10	10	10	0	0	10	0	0
Rt 7 Turning Lanes	EB Right	5	20	5	0	0	20	0	0
Caldia Roma B. 1. 5	WB Left	10	60	10	0	0	59	1	0
Colvin Run Road -East	SB Right	10	10	10	0	0	10	0	0
	SB Thru	5	15	5	0	0	15	0	0
	SB Left	185	165	181	2	2	162	2	2
Rt 7 Turning Lanes	WB Right	200	315	196	2	2	309	3	3
C 5 W	EB Left	10	25	10	0	0	25	0	0
Carpers Farm Way	NB Left	35	20	35	0	0	20	0	0
	NB Thru	15	10	15	0	0	10	0	0
Dt 7 Toursia - Louis	NB Right	55	40	54	1	0	40	0	0
Rt 7 Turning Lanes	EB Right	10	30	10 15	0	0	30 50	0	0
Davidali.	WB Left	15	50					-	
Beulah	NB Left	150	305	147	2	2	299	3	3
	NB Thru	15	30	15 314	3	3	29 206	0 2	0 2
Dt 7 Turning Lance	NB Right	320	210						
Rt 7 Turning Lanes	EB Right	195	190	191	2	2	186	2	2
Forestville	WB Left SB Right	190 5	195 15	186 5	0	0	191 15	0	0
Forestville	SB Thru	50	10	49	1	1	10	0	0
	SB Left	75	40	74	1	1	39	0	0
Rt 7 Turning Lanes	EB Left	20	35	20	0	0	34	0	0
Rt / Turring Lanes	WB Right	25	40	25	0	0	39	0	0
Towlston Rd North				78	1	1	289	3	3
Towiston Rd North	SB Right SB Thru	80 50	295 70	49	1	1	69	1	1
	SB Left	108	57	106	1	1	56	1	1
Rt 7 Turning Lanes	EB Left	175	247	172	2	2	242	2	2
nc / Turring Laries	WB Right	55	60	54	1	1	59	1	1
Towlston RD South	NB Left	85	120	83	1	1	118	1	1
1011.3ton ND 30ath	NB Thru	45	55	44	0	0	54	1	1
	NB Till d NB Right	60	35	59	1	1	34	0	0
Rt 7 Turning Lanes	EB Right	65	85	64	1	1	83	1	1
,	WB Left	50	80	49	1	1	78	1	1
Lewinsville RD	SB Right	425	655	421	4	0	648	7	0
	SB Thru	5	10	5	0	0	10	0	0
	SB Left	80	90	79	1	0	89	1	0
Rt 7 Turning Lanes	WB Right	165	300	163	2	0	297	3	0
raining Lancs	EB Left	680	375	673	7	0	371	4	0
	EB Right	10	50	10	0	0	50	1	0
	WB Left	20	30	20	0	0	30	0	0
МВС	NB Left	10	20	10	0	0	20	0	0
	NB Thru	10	60	10	0	0	59	1	0
	NB Till d NB Right	5	5	5	0	0	5	0	0
	IND KIRIIL	J	ı J	3	U	U	3	0	J



Year 2040 Balanced Traffic Volumes for Noise Analysis ZONE 3

EAS	TBOUND T	RAFFIC Zon	e 3 (Lewins	ville > Jarre	tt Valley) WCN	H 15:00 PM		WESTB	<mark>OUND TRA</mark>	FFIC Zone 3	<mark>(Lewinsvil</mark>	le > Jarrett	Valley) WC	NH 15:00 P	M
		Route 7 E	B Zone 3-1	(Zone 2 > Le	ewinsville)					Route 7 Wi	B Zone 3-1 (	(End > DTR	Ramp)		
						Total (3 Lanes)	1 Lane						Т	otal (3 Lane	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	2711	904	Total Vehicles	Cars%	MT%	HT%		Cars	3675	1225
2881	0.941	0.038	0.021		MT	109	36	3910	0.94	0.032	0.028		MT	125	42
				='	HT	61	20					_	HT	109	36
						2881								3910	
	R	oute 7 EB Z	one 3-2 (Le	winsville > J	arrett Valley)				Rou	ite 7 WB Zo	ne 3-2 (DTF	R Ramp > Le	ewinsville)		
						Total (3 Lanes)	1 Lane						Т	otal (3 Lane	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	2382	794	Total Vehicles	Cars%	MT%	HT%		Cars	2323	774
2531	0.941	0.038	0.021		MT	96	32	2471	0.94	0.032	0.028		MT	79	26
				='	HT	53	18					_	HT	69	23
						2531								2471	
		Route 7 E	B Zone 3-3	(Jarrett Val	ley > End)				Ro	oute 7 WB	Zone 3-3 (Le	ewinsville >	Zone 2)		
						Total (3 Lanes)	1 Lane						Т	otal (3 Lane	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	2438	813	Total Vehicles	Cars%	MT%	HT%		Cars	2647	882
2591	0.941	0.038	0.021		MT	98	33	2816	0.94	0.032	0.028		MT	90	30
	•	·	· <u></u>	•	HT	54	18				• -	•	HT	79	26
						2591	_							2816	

	EASTBOUN	D TRAFFIC 2	Zone 3 (Lewinsv	ille > Jarrett Valley	y) WCNI	1 6:00 AM		WES	STBOUND 1	TRAFFIC Zoi	ne 3 (Lewin	sville > Jarı	ett Valley)	WCNH 6:00 AM	
		Route	7 EB Zone 3-1 (Z	one 2 > Lewinsville	e)					Route 7	WB Zone 3	-1 (End > D	TR Ramp)		
						Total (3 Lanes)	1 Lane							Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	3828	1276	Total Vehicles	Cars%	MT%	HT%		Cars	1697	566
4051	0.945	0.029	0.026		MT	117	39	1847	0.919	0.046	0.035		MT	85	28
					HT	105	35						HT	65	22
						4051								1847	
		Route 7 E	B Zone 3-2 (Lewi	insville > Jarrett Va	alley)				F	Route 7 WB	Zone 3-2 (I	OTR Ramp :	> Lewinsville	e)	
						Total (3 Lanes)	1 Lane							Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	3238	1079	Total Vehicles	Cars%	MT%	HT%		Cars	1447	482
3426	0.945	0.029	0.026		MT	99	33	1575	0.919	0.046	0.035		MT	72	24
					HT	89	30					='	HT	55	18
						3426								1575	
		Route	7 EB Zone 3-3 (J	larrett Valley > End	d)					Route 7 W	/B Zone 3-3	(Lewinsvill	e > Zone 2)		
						Total (3 Lanes)	1 Lane							Total (3 Lanes)	1 Lane
Total Vehicles	Cars%	MT%	HT%		Cars	3422	1141	Total Vehicles	Cars%	MT%	HT%		Cars	1677	559
3621	0.945	0.029	0.026		MT	105	35	1825	0.919	0.046	0.035		MT	84	28
			•		HT	94	31		•		•	=	HT	64	21
					•	3621								1825	

Roadway	Movement	2018 Pe	ak Total		AM			PM	
Roadway	Wovement	AM	PM	Cars	MT	HT	Cars	MT	HT
Lewinsville RD	SB Right	425	655	421	4	0	648	7	0
	SB Thru	5	10	5	0	0	10	0	0
	SB Left	80	90	79	1	0	89	1	0
Rt 7 Turning Lanes	WB Right	165	300	163	2	0	297	3	0
	EB Left	680	375	673	7	0	371	4	0
	EB Right	10	50	10	0	0	50	1	0
	WB Left	20	30	20	0	0	30	0	0
МВС	NB Left	10	20	10	0	0	20	0	0
	NB Thru	10	60	10	0	0	59	1	0
	NB Right	5	5	5	0	0	5	0	0
Jarrett Valley Road	NB Left	5	10	5	0	0	10	0	0
	NB Right	125	40	124	1	0	40	0	0
Rt 7 Turning Lanes	EB Right	10	20	10	0	0	20	0	0
	WB Left	20	60	20	0	0	59	1	0
DTR Off Ramp for	7 WB	305	705	281	12	122	649	28	28
DTR Off Ramp for	<sup>-</sup> 7 EB	80	40	78	1	1	39	0	0
DTR Off Ramp to Jarr	ett Valley	5	10	5	0	0	10	0	0
DTR On Ramp fron	n 7 WB	562	2094	551	6	6	2052	21	21
DTR On Ramp fror	n 7 EB	100	150	97	2	1	146	2	3

## APPENDIX C - ACOUSTICAL PROFILES

CNE A - W	all A2 Acoust	ical Profile (	Projection	NAD_1983_Stat	ePlane_Virginia_Nortl	h US Feet)
Station	X Coordinate	Y Coordinate		Wall Height	Top Elevation	Segment Length
			Wall A2	(Design Stationin	g 1175+00 to 1190+50)	
10+00.00	11,812,639	7,048,137	404.2	18.0	422.2	28
10+28.00	11,812,660	7,048,118	406.0	18.0	424.0	28
10+56.00	11,812,681	7,048,099	408.1	18.0	426.1	29
10+85.00	11,812,703	7,048,080	410.3	18.0	428.3	29
11+14.00	11,812,724	7,048,060	412.0	18.0	430.0	50
11+64.00	11,812,762	7,048,028	414.2	18.0	432.2	49
12+13.00	11,812,799	7,047,996	414.9	18.0	432.9	49
12+62.00	11,812,836	7,047,964	414.2	18.0	432.2	49
13+11.00	11,812,873	7,047,932	413.6	18.0	431.6	24
13+35.00	11,812,870	7,047,908	412.7	18.0	430.7	41
13+76.00	11,812,903	7,047,883	411.2	18.0	429.2	41
14+17.00	11,812,935	7,047,858	408.7	18.0	426.7	40
14+57.00	11,812,967	7,047,834	406.8	18.0	424.8	40
14+97.00	11,812,999	7,047,809	405.5	18.0	423.5	45
15+42.00	11,813,033	7,047,779	404.8	18.0	422.8	46
15+88.00	11,813,067	7,047,749	404.5	17.0	421.5	45
16+33.00	11,813,101	7,047,719	404.7	16.0	420.7	45
16+78.00	11,813,135	7,047,689	404.8	15.0	419.8	45
17+23.00	11,813,169	7,047,659	403.9	14.0	417.9	45
17+68.00	11,813,203	7,047,629	403.1	13.0	416.1	45
18+13.00	11,813,236	7,047,598	402.2	13.0	415.2	25
18+38.00	11,813,260	7,047,604	401.7	13.0	414.7	47
18+85.00	11,813,295	7,047,573	400.4	13.0	413.4	47
19+32.00	11,813,330	7,047,542	398.4	13.0	411.4	47
19+79.00	11,813,365	7,047,511	397.3	13.0	410.3	48
20+27.00	11,813,401	7,047,480	397.1	13.0	410.1	47
20+74.00	11,813,436	7,047,449	396.3	13.0	409.3	47
21+21.00	11,813,471	7,047,418	395.6	13.0	408.6	47
21+68.00	11,813,506	7,047,387	395.3	13.0	408.3	47
22+15.00	11,813,541	7,047,356	394.7	13.0	407.7	36
22+51.00	11,813,538	7,047,321	395.0	13.0	408.0	36
22+87.00	11,813,536	7,047,285	393.4	13.0	406.4	0

Station   XCoordinate   Y   Base   Wall Height   Top Elevation   Segment Length	CNEs B & D	- B1-B6 and D	01 Acoustica	l Profiles (F	Projection NAD_	1983_StatePlane_Virg	inia_North US Feet)
10+00.00	Station	X Coordinate	_		Wall Height	Top Elevation	Segment Length
10496.00				Wall B1	(Design Stationin	ng 166+50 to 168+00)	
1019-6.00   11,811,987   7,049,078   432.4   15.0   447.4   48   11+44.00   11,812,023   7,048,976   429.5   15.0   444.5   0   1.812,040   1.811,936   7,048,980   423.9   15.0   438.9   49   10+99.00   11,811,973   7,048,915   422.1   15.0   437.6   499   11+99.00   11,812,010   7,048,915   422.1   15.0   437.1   48   48   49   49   49   49   49   49	10+00.00	11,811,915	7,049,071	429.4	15.0	444.4	48
11+44.00	10+48.00	11,811,951	7,049,039	432.9	15.0	447.9	48
10+00.00	10+96.00	11,811,987	7,049,008	432.4	15.0	447.4	48
10+00.00	11+44.00	11,812,023	7,048,976				0
10+99.00   11,811,973   7,048,974   422.6   15.0   437.6   49   10+98.00   11,812,010   7,048,915   422.1   15.0   437.1   48   11+46.00   11,812,063   7,048,850   421.2   15.0   436.7   49   12+44.00   11,812,120   7,048,818   420.7   15.0   436.2   49   12+44.00   11,812,120   7,048,783   420.2   15.0   435.7   49   12+93.00   11,812,197   7,048,783   420.2   15.0   435.2   49   13+92.00   11,812,194   7,048,753   419.7   15.0   434.7   48   48   13+90.00   11,812,230   7,048,688   418.7   15.0   433.7   49   41+39.00   11,812,230   7,048,686   418.1   15.0   433.1   49   49   41+39.00   11,812,334   7,048,656   418.1   15.0   433.1   49   49   49   49   49   49   49   4				Wall B2	(Design Stationin	ng 167+25 to 176+75)	
10+98.00   11,812,010   7,048,915   422.1   15.0   437.1   48   48   11+46.00   11,812,046   7,048,883   421.7   15.0   436.7   49   11+95.00   11,812,048   7,048,858   421.7   15.0   436.7   49   12+44.00   11,812,120   7,048,818   420.7   15.0   435.7   49   12+44.00   11,812,157   7,048,818   420.7   15.0   435.7   49   12+30.00   11,812,157   7,048,785   420.2   15.0   435.2   49   13+42.00   11,812,230   7,048,721   419.2   15.0   434.2   49   49   41+99.00   11,812,267   7,048,688   418.7   15.0   433.7   49   41+88.00   11,812,341   7,048,654   418.1   15.0   433.1   49   41+88.00   11,812,341   7,048,654   417.6   15.0   432.6   49   49   41+98.00   11,812,341   7,048,654   417.6   15.0   432.0   48   48   48   48   48   48   48   4	10+00.00	11,811,936	7,048,980	423.9	15.0	438.9	49
11+46.00 11,812,046 7,048,883 421.7 15.0 436.7 49 11+95.00 11,812,020 7,048,885 421.2 15.0 436.2 49 12+49.00 11,812,125 7,048,785 420.2 15.0 435.7 49 12+93.00 11,812,137 7,048,785 420.2 15.0 435.2 49 13+42.00 11,812,139 4,7048,753 419.7 15.0 434.7 48 13+90.00 11,812,230 7,048,785 419.7 15.0 434.7 48 14+39.00 11,812,257 7,048,688 418.7 15.0 433.7 49 14+88.00 11,812,304 7,048,656 418.1 15.0 433.1 49 15+37.00 11,812,310 4,7048,656 418.1 15.0 433.1 49 15+37.00 11,812,317 7,048,891 417.0 15.0 432.6 49 15+86.00 11,812,317 7,048,591 417.0 15.0 432.0 48 16+34.00 11,812,414 7,048,529 416.7 15.0 431.7 24 16+58.00 11,812,421 7,048,511 415.8 15.0 431.2 39 16+97.00 11,812,422 7,048,511 415.8 15.0 430.8 40 17+37.00 11,812,482 7,048,485 415.1 15.0 429.9 39 18+15.00 11,812,540 7,048,485 415.1 15.0 429.6 24 18+39.00 11,812,540 7,048,433 414.6 15.0 429.9 39 18+15.00 11,812,540 7,048,334 414.6 15.0 429.6 48 18+39.00 11,812,634 7,048,334 414.6 15.0 429.6 48 18+39.00 11,812,637 7,048,485 415.1 15.0 429.6 48 18+39.00 11,812,637 7,048,334 414.6 15.0 429.6 48 18+39.00 11,812,637 7,048,334 414.1 15.0 429.1 48 19+35.00 11,812,637 7,048,334 414.1 15.0 429.1 48 19+35.00 11,812,637 7,048,342 413.3 15.0 428.6 24 10+60.00 11,812,637 7,048,366 414.1 15.0 429.1 48 11+93.00 11,812,637 7,048,330 414.1 15.0 429.1 24 10+60.00 11,812,637 7,048,330 414.1 15.0 429.1 35 10+36.00 11,812,637 7,048,300 414.1 15.0 429.1 35 11+43.00 11,812,737 7,048,300 414.1 15.0 429.1 35 11+43.00 11,812,782 7,048,334 413.6 15.0 428.6 24 11+98.00 11,812,785 7,048,300 414.1 15.0 429.1 35 11+43.00 11,812,782 7,048,334 413.6 15.0 428.6 36 11+1+38.00 11,812,885 7,048,300 414.1 15.0 429.1 35 11+43.00 11,812,895 7,048,300 414.1 15.0 429.1 35 11+43.00 11,812,895 7,048,313 410.6 15.0 428.6 36 11+1+38.00 11,812,895 7,048,313 410.9 15.0 428.6 36 11+1+38.00 11,812,999 7,048,000 410.2 15.0 426.6 41 11+458.00 11,812,999 7,048,000 410.2 15.0 424.4 24 11+458.00 11,812,999 7,048,000 410.2 15.0 424.1 48	10+49.00	11,811,973	7,048,947	422.6	15.0	437.6	49
11+95.00	10+98.00	11,812,010	7,048,915	422.1	15.0	437.1	48
12+44.00 11,812,120 7,048,818 420.7 15.0 435.7 49 12+93.00 11,812,157 7,048,785 420.2 15.0 435.2 49 13+42.00 11,812,157 7,048,785 420.2 15.0 435.2 49 13+42.00 11,812,230 7,048,721 419.2 15.0 434.7 48 13+90.00 11,812,267 7,048,688 418.7 15.0 433.7 49 14+88.00 11,812,340 7,048,656 418.1 15.0 433.7 49 15+37.00 11,812,341 7,048,656 418.1 15.0 432.6 49 15+37.00 11,812,347 7,048,656 418.1 15.0 432.6 49 15+37.00 11,812,347 7,048,559 416.7 15.0 432.0 48 16+34.00 11,812,414 7,048,559 416.7 15.0 431.2 39 16+98.00 11,812,424 7,048,559 416.7 15.0 431.2 39 16+97.00 11,812,425 7,048,511 415.8 15.0 430.8 40 17+37.00 11,812,427 7,048,485 415.1 15.0 430.8 40 17+37.00 11,812,427 7,048,431 414.6 15.0 429.9 39 18+15.00 11,812,563 7,048,437 414.6 15.0 429.6 48 18+39.00 11,812,563 7,048,427 414.6 15.0 429.6 48 18+39.00 11,812,563 7,048,427 414.6 15.0 429.6 48 19+35.00 11,812,663 7,048,394 414.1 15.0 429.6 48 19+35.00 11,812,663 7,048,344 414.1 15.0 429.1 48 19+35.00 11,812,665 7,048,324 413.7 15.0 428.7 0  **Wall B3 (Design Stationing 176+50 to 182+00)**  **Wall B3 (Design Stationing 176+50 to 182+00)**  10+00.00 11,812,665 7,048,324 413.6 15.0 428.6 24 10+84.00 11,812,686 7,048,324 413.6 15.0 429.1 35 11+43.00 11,812,799 7,048,283 413.6 15.0 428.6 36 11+79.00 11,812,767 7,048,400 415.2 15.0 428.6 24 10+84.00 11,812,686 7,048,324 413.6 15.0 428.6 24 10+84.00 11,812,686 7,048,324 413.6 15.0 428.6 24 10+84.00 11,812,686 7,048,324 413.6 15.0 428.6 36 11+79.00 11,812,779 7,048,283 413.6 15.0 428.6 36 11+79.00 11,812,779 7,048,283 413.6 15.0 428.6 36 11+79.00 11,812,787 7,048,193 412.5 15.0 426.6 41 12+97.00 11,812,875 7,048,193 410.9 15.0 426.6 41 12+97.00 11,812,875 7,048,193 410.9 15.0 426.6 41 12+97.00 11,812,875 7,048,193 410.9 15.0 426.6 41 13+38.00 11,812,875 7,048,193 410.9 15.0 426.6 41 13+38.00 11,812,987 7,048,193 410.9 15.0 426.6 41 13+38.00 11,812,999 7,048,044 409.1 15.0 424.4 424 14+15.00 11,812,999 7,048,044 409.1 15.0 424.4 424	11+46.00	11,812,046	7,048,883	421.7	15.0	436.7	49
12+93.00 11,812,157 7,048,785 420.2 15.0 435.2 49  13+42.00 11,812,194 7,048,753 419.7 15.0 434.7 48  13+90.00 11,812,230 7,048,71 419.2 15.0 433.7 49  14+39.00 11,812,230 7,048,686 418.7 15.0 433.7 49  14+88.00 11,812,304 7,048,656 418.1 15.0 433.1 49  15+37.00 11,812,341 7,048,624 417.6 15.0 432.0 48  15+37.00 11,812,341 7,048,624 417.6 15.0 432.0 48  16+34.00 11,812,414 7,048,559 416.7 15.0 432.0 38  16+34.00 11,812,424 7,048,559 416.7 15.0 431.7 24  16+58.00 11,812,423 7,048,537 416.2 15.0 431.7 24  16+58.00 11,812,423 7,048,435 416.2 15.0 431.2 39  17+37.00 11,812,423 7,048,458 415.1 15.0 430.8 40  17+37.00 11,812,482 7,048,459 414.9 15.0 429.9 39  17+76.00 11,812,511 7,048,459 414.9 15.0 429.9 39  17+76.00 11,812,563 7,048,459 414.6 15.0 429.6 24  18+39.00 11,812,563 7,048,427 414.6 15.0 429.6 48  18+37.00 11,812,563 7,048,394 414.1 15.0 429.1 48  19+35.00 11,812,563 7,048,400 415.2 15.0 429.1 36  10+00.00 11,812,634 7,048,394 414.1 15.0 429.1 36  10+36.00 11,812,637 7,048,394 413.7 15.0 429.1 24  10+60.00 11,812,652 7,048,400 415.2 15.0 429.1 24  10+60.00 11,812,653 7,048,400 415.2 15.0 428.6 24  11+08.00 11,812,666 7,048,304 413.6 15.0 428.6 24  11+08.00 11,812,763 7,048,394 413.6 15.0 428.6 24  11+08.00 11,812,652 7,048,400 415.2 15.0 429.1 24  10+60.00 11,812,653 7,048,404 413.6 15.0 428.6 24  11+08.00 11,812,763 7,048,307 414.1 15.0 429.1 24  10+60.00 11,812,664 7,048,307 414.1 15.0 428.6 36  11+79.00 11,812,765 7,048,304 413.6 15.0 428.6 36  11+79.00 11,812,785 7,048,394 413.6 15.0 428.6 36  11+79.00 11,812,785 7,048,394 413.6 15.0 428.6 36  11+79.00 11,812,844 7,048,859 413.6 15.0 428.6 36  11+79.00 11,812,844 7,048,859 413.6 15.0 428.6 36  11+79.00 11,812,878 7,048,394 413.6 15.0 428.6 36  11+79.00 11,812,878 7,048,394 413.6 15.0 428.6 36  11+79.00 11,812,898 7,048,414 415.5 15.0 428.6 36  11+79.00 11,812,898 7,048,414 415.5 15.0 426.6 41  12+97.00 11,812,898 7,048,414 41.1 15.0 426.6 41  12+97.00 11,812,998 7,048,414 40.9 15.0 424.4 44  13+88.00 11,812,998 7,048,414 409.9 15.0 424.4 44  14+10.00	11+95.00	11,812,083	7,048,850	421.2	15.0	436.2	49
13+42.00 11,812,194 7,048,753 419.7 15.0 434.7 48 13+90.00 11,812,230 7,048,721 419.2 15.0 434.2 49 14+39.00 11,812,304 7,048,656 418.1 15.0 433.1 49 14+38.00 11,812,304 7,048,656 418.1 15.0 433.1 49 15+37.00 11,812,341 7,048,654 417.6 15.0 432.6 49 15+37.00 11,812,341 7,048,691 417.0 15.0 432.0 48 16+34.00 11,812,414 7,048,591 417.0 15.0 432.0 48 16+34.00 11,812,423 7,048,591 417.0 15.0 431.7 24 16+58.00 11,812,423 7,048,591 416.2 15.0 431.7 24 16+58.00 11,812,423 7,048,537 416.2 15.0 431.2 39 16+97.00 11,812,452 7,048,511 415.8 15.0 430.8 40 17+37.00 11,812,452 7,048,511 415.8 15.0 430.8 40 17+37.00 11,812,551 7,048,459 414.9 15.0 429.9 39 18+15.00 11,812,563 7,048,333 414.6 15.0 429.6 24 18+39.00 11,812,563 7,048,334 414.6 15.0 429.6 48 18+39.00 11,812,563 7,048,362 413.7 15.0 429.1 48 19+35.00 11,812,634 7,048,362 413.7 15.0 429.1 48 19+35.00 11,812,634 7,048,366 414.1 15.0 429.1 48 19+35.00 11,812,634 7,048,364 414.1 15.0 429.1 48 19+35.00 11,812,637 7,048,364 414.1 15.0 429.1 36 10+00.00 11,812,637 7,048,344 413.6 15.0 429.1 35 11+43.00 11,812,793 7,048,324 413.3 15.0 428.6 24 10+84.00 11,812,673 7,048,324 413.3 15.0 428.6 24 11+98.00 11,812,793 7,048,324 413.3 15.0 429.1 35 11+43.00 11,812,793 7,048,324 413.3 15.0 429.1 35 11+43.00 11,812,793 7,048,324 413.3 15.0 428.6 36 11+79.00 11,812,793 7,048,293 413.1 15.0 428.6 36 11+79.00 11,812,793 7,048,293 413.1 15.0 428.6 36 11+79.00 11,812,884 7,048,359 413.1 15.0 428.6 36 11+79.00 11,812,884 7,048,359 413.1 15.0 428.6 36 11+79.00 11,812,895 7,048,304 411.2 15.0 426.6 41 12+97.00 11,812,895 7,048,304 411.0 15.0 426.6 41 13+38.00 11,812,895 7,048,394 411.0 15.0 426.6 41 13+38.00 11,812,895 7,048,315 411.0 15.0 424.4 24 13+88.00 11,812,999 7,048,044 409.1 15.0 424.4 24 14+58.00 11,812,999 7,048,044 409.1 15.0 424.1 48	12+44.00	11,812,120	7,048,818	420.7	15.0	435.7	49
13+90.00	12+93.00	11,812,157	7,048,785	420.2	15.0	435.2	49
14+39.00       11,812,267       7,048,688       418.7       15.0       433.7       49         14+88.00       11,812,304       7,048,656       418.1       15.0       433.1       49         15+37.00       11,812,341       7,048,624       417.6       15.0       432.6       49         15+86.00       11,812,347       7,048,591       417.0       15.0       432.0       48         16+34.00       11,812,414       7,048,599       416.7       15.0       431.7       24         16+58.00       11,812,423       7,048,511       416.8       15.0       431.2       39         16+59.00       11,812,482       7,048,485       415.1       15.0       430.1       39         17+70.00       11,812,511       7,048,485       415.1       15.0       430.1       39         17+70.00       11,812,511       7,048,485       415.1       15.0       430.1       39         18+15.00       11,812,511       7,048,483       414.9       15.0       429.9       39         18+39.00       11,812,537       7,048,433       414.6       15.0       429.6       48         18+87.00       11,812,634       7,048,362       413.7       15.0<	13+42.00	11,812,194	7,048,753	419.7	15.0	434.7	48
14+88.00 11,812,304 7,048,656 418.1 15.0 433.1 49  15+37.00 11,812,341 7,048,654 417.6 15.0 432.6 49  15+86.00 11,812,378 7,048,591 417.0 15.0 432.0 48  16+34.00 11,812,414 7,048,559 416.7 15.0 431.7 24  16+58.00 11,812,423 7,048,537 416.2 15.0 431.2 39  16+97.00 11,812,452 7,048,511 415.8 15.0 430.8 40  17+37.00 11,812,482 7,048,485 415.1 15.0 430.1 39  17+76.00 11,812,511 7,048,459 414.9 15.0 429.6 24  18+39.00 11,812,563 7,048,334 414.6 15.0 429.6 24  18+39.00 11,812,563 7,048,362 413.7 15.0 429.6 48  18+87.00 11,812,634 7,048,362 413.7 15.0 429.1 48  19+35.00 11,812,634 7,048,362 413.7 15.0 429.1 48  10+60.00 11,812,663 7,048,364 414.1 15.0 429.1 24  10+60.00 11,812,673 7,048,344 413.3 15.0 429.1 24  10+60.00 11,812,673 7,048,344 413.6 15.0 429.1 24  10+84.00 11,812,703 7,048,364 414.1 15.0 429.1 24  10+80.00 11,812,673 7,048,364 414.1 15.0 429.1 24  10+80.00 11,812,673 7,048,364 414.1 15.0 429.1 24  10+80.00 11,812,673 7,048,364 414.1 15.0 429.1 24  10+80.00 11,812,673 7,048,364 414.1 15.0 429.1 24  10+80.00 11,812,673 7,048,364 414.1 15.0 429.1 35  11+30.00 11,812,703 7,048,364 413.1 15.0 428.6 24  10+80.00 11,812,703 7,048,364 413.1 15.0 428.6 36  11+79.00 11,812,703 7,048,294 413.1 15.0 428.6 36  11+79.00 11,812,782 7,048,283 413.6 15.0 428.6 36  11+79.00 11,812,782 7,048,283 413.6 15.0 428.6 36  12+15.00 11,812,815 7,048,259 413.1 15.0 426.6 41  12+97.00 11,812,875 7,048,134 412.5 15.0 426.6 41  12+97.00 11,812,875 7,048,133 410.9 15.0 426.6 41  12+97.00 11,812,875 7,048,153 410.9 15.0 426.6 41  13+38.00 11,812,875 7,048,153 410.9 15.0 424.4 24  14+10.00 11,812,895 7,048,153 410.9 15.0 424.4 24  14+10.00 11,812,985 7,048,155 409.4 15.0 426.2 41  13+86.00 11,812,999 7,048,044 409.1 15.0 424.1 48	13+90.00	11,812,230	7,048,721	419.2	15.0	434.2	49
15+37.00 11,812,341 7,048,624 417.6 15.0 432.6 49  15+86.00 11,812,378 7,048,591 417.0 15.0 432.0 48  16+34.00 11,812,414 7,048,559 416.7 15.0 431.7 24  16+58.00 11,812,423 7,048,557 416.2 15.0 431.7 24  16+97.00 11,812,423 7,048,557 416.2 15.0 430.8 40  17+37.00 11,812,422 7,048,451 415.8 15.0 430.8 40  17+37.00 11,812,422 7,048,485 415.1 15.0 430.1 39  17+76.00 11,812,511 7,048,459 414.9 15.0 429.9 39  18+15.00 11,812,540 7,048,433 414.6 15.0 429.6 24  18+39.00 11,812,543 7,048,433 414.6 15.0 429.6 48  18+87.00 11,812,563 7,048,427 414.6 15.0 429.1 48  19+35.00 11,812,634 7,048,362 413.7 15.0 429.1 48  19+35.00 11,812,635 7,048,404 414.1 15.0 429.1 48  10+60.00 11,812,663 7,048,366 414.1 15.0 429.1 24  10+60.00 11,812,663 7,048,344 413.6 15.0 429.1 24  10+60.00 11,812,663 7,048,366 414.1 15.0 429.1 24  10+60.00 11,812,663 7,048,366 414.1 15.0 428.6 24  11+08.00 11,812,703 7,048,374 414.1 15.0 428.6 24  11+08.00 11,812,703 7,048,384 413.3 15.0 428.6 24  11+08.00 11,812,703 7,048,384 413.6 15.0 428.6 36  11+79.00 11,812,729 7,048,283 413.6 15.0 428.6 36  11+79.00 11,812,785 7,048,283 413.6 15.0 428.6 36  11+79.00 11,812,785 7,048,284 413.6 15.0 428.6 36  11+79.00 11,812,813 7,048,295 413.1 15.0 428.1 36  12+15.00 11,812,844 7,048,180 411.2 15.0 426.6 41  12+97.00 11,812,844 7,048,180 411.2 15.0 426.6 41  12+97.00 11,812,844 7,048,180 411.2 15.0 426.6 41  13+38.00 11,812,875 7,048,153 410.9 15.0 425.9 24  13+86.00 11,812,973 7,048,153 410.9 15.0 424.9 24  13+86.00 11,812,985 7,048,165 40.9 15.0 424.4 24  14+10.00 11,812,994 7,048,075 40.9 7 15.0 424.1 48	14+39.00	11,812,267	7,048,688	418.7	15.0	433.7	49
15+86.00 11,812,378 7,048,591 417.0 15.0 432.0 48  16+34.00 11,812,414 7,048,559 416.7 15.0 431.7 24  16+58.00 11,812,423 7,048,559 416.2 15.0 431.2 39  16+97.00 11,812,452 7,048,511 415.8 15.0 430.1 39  17+76.00 11,812,511 7,048,459 414.9 15.0 429.9 39  18+15.00 11,812,563 7,048,427 414.6 15.0 429.6 24  18+39.00 11,812,563 7,048,342 414.1 15.0 429.1 48  19+35.00 11,812,634 7,048,362 413.7 15.0 428.7 0  10+00.00 11,812,653 7,048,364 414.1 15.0 429.1 48  10+60.00 11,812,663 7,048,366 414.1 15.0 429.1 24  10+60.00 11,812,663 7,048,364 413.6 15.0 429.1 24  10+80.00 11,812,663 7,048,364 414.1 15.0 429.1 24  10+80.00 11,812,663 7,048,364 414.1 15.0 429.1 24  10+80.00 11,812,663 7,048,364 414.1 15.0 429.1 24  10+80.00 11,812,663 7,048,364 414.1 15.0 429.1 24  10+60.00 11,812,663 7,048,364 414.1 15.0 429.1 24  10+80.00 11,812,663 7,048,364 414.1 15.0 429.1 36  11+30.00 11,812,663 7,048,364 414.1 15.0 429.1 36  11+30.00 11,812,663 7,048,364 414.1 15.0 429.1 36  11+30.00 11,812,663 7,048,364 413.3 15.0 428.6 24  11+08.00 11,812,673 7,048,374 414.1 15.0 429.1 35  11+43.00 11,812,799 7,048,283 413.6 15.0 428.6 36  11+79.00 11,812,799 7,048,283 413.6 15.0 428.6 36  11+79.00 11,812,813 7,048,234 412.5 15.0 428.1 36  12+15.00 11,812,844 7,048,180 411.2 15.0 426.6 41  12+97.00 11,812,844 7,048,180 411.2 15.0 426.6 41  13+38.00 11,812,875 7,048,181 410.9 15.0 426.6 41  13+38.00 11,812,895 7,048,141 409.9 15.0 424.9 24  13+60.00 11,812,985 7,048,141 409.9 15.0 424.4 24  14+10.00 11,812,985 7,048,141 409.9 15.0 424.4 24  14+10.00 11,812,985 7,048,160 410.2 15.0 424.4 24  14+10.00 11,812,984 7,048,100 410.2 15.0 424.7 47  14+58.00 11,812,999 7,048,044 409.1 15.0 424.1	14+88.00	11,812,304	7,048,656	418.1	15.0	433.1	49
16+34.00         11,812,414         7,048,559         416.7         15.0         431.7         24           16+58.00         11,812,423         7,048,537         416.2         15.0         431.2         39           16+97.00         11,812,482         7,048,485         415.1         15.0         430.8         40           17+37.00         11,812,482         7,048,485         415.1         15.0         430.1         39           17+76.00         11,812,581         7,048,485         415.1         15.0         429.9         39           18+15.00         11,812,564         7,048,433         414.6         15.0         429.6         24           18+39.00         11,812,563         7,048,484         414.1         15.0         429.6         48           18+87.00         11,812,563         7,048,362         413.7         15.0         429.1         48           19+35.00         11,812,634         7,048,362         413.7         15.0         428.7         0           10+00.00         11,812,637         7,048,404         415.2         15.0         430.2         36           10+36.00         11,812,663         7,048,364         414.1         15.0         428.6	15+37.00	11,812,341	7,048,624	417.6	15.0	432.6	49
16+58.00 11,812,423 7,048,537 416.2 15.0 431.2 39 16+97.00 11,812,452 7,048,511 415.8 15.0 430.8 40 17+37.00 11,812,482 7,048,485 415.1 15.0 430.1 39 17+76.00 11,812,511 7,048,459 414.9 15.0 429.9 39 18+15.00 11,812,540 7,048,433 414.6 15.0 429.6 24 18+39.00 11,812,563 7,048,427 414.6 15.0 429.6 48 18+87.00 11,812,538 7,048,394 414.1 15.0 429.1 48 19+35.00 11,812,634 7,048,362 413.7 15.0 429.1 48 19+35.00 11,812,634 7,048,362 413.7 15.0 429.1 48 19+36.00 11,812,634 7,048,362 413.7 15.0 429.1 48 10+00.00 11,812,633 7,048,400 415.2 15.0 430.2 36 10+36.00 11,812,663 7,048,364 414.1 15.0 429.1 24 10+60.00 11,812,663 7,048,364 413.6 15.0 429.1 24 10+60.00 11,812,673 7,048,344 413.6 15.0 429.1 24 10+84.00 11,812,693 7,048,344 413.3 15.0 428.6 24 11+08.00 11,812,703 7,048,307 414.1 15.0 429.1 35 11+43.00 11,812,729 7,048,283 413.6 15.0 428.6 36 11+79.00 11,812,729 7,048,283 413.1 15.0 428.6 36 11+79.00 11,812,782 7,048,284 412.5 15.0 428.6 36 12+15.00 11,812,785 7,048,284 412.5 15.0 426.6 41 12+97.00 11,812,844 7,048,180 411.2 15.0 426.2 41 13+38.00 11,812,847 7,048,180 411.2 15.0 426.2 41 13+38.00 11,812,847 7,048,181 410.9 15.0 426.2 41 13+38.00 11,812,895 7,048,141 409.9 15.0 425.9 24 13+86.00 11,812,985 7,048,141 409.9 15.0 424.4 424 14+10.00 11,812,985 7,048,141 409.9 15.0 424.7 47 14+58.00 11,812,999 7,048,044 409.1 15.0 424.7 48	15+86.00	11,812,378	7,048,591	417.0	15.0	432.0	48
16+97.00	16+34.00	11,812,414	7,048,559	416.7	15.0	431.7	24
17+37.00         11,812,482         7,048,485         415.1         15.0         430.1         39           17+76.00         11,812,511         7,048,459         414.9         15.0         429.9         39           18+15.00         11,812,540         7,048,433         414.6         15.0         429.6         24           18+39.00         11,812,563         7,048,427         414.6         15.0         429.6         48           18+87.00         11,812,593         7,048,342         414.1         15.0         429.1         48           19+35.00         11,812,634         7,048,362         413.7         15.0         428.7         0           Wall B3 (Design Stationing 176+50 to 182+00)           10+00.00         11,812,663         7,048,400         415.2         15.0         430.2         36           10+36.00         11,812,663         7,048,344         413.6         15.0         428.6         24           10+60.00         11,812,663         7,048,344         413.6         15.0         428.6         24           10+60.00         11,812,668         7,048,344         413.3         15.0         428.3         24           11+80.00         11,812,795         <	16+58.00	11,812,423	7,048,537	416.2	15.0	431.2	39
17+76.00         11,812,511         7,048,459         414.9         15.0         429.9         39           18+15.00         11,812,540         7,048,433         414.6         15.0         429.6         24           18+39.00         11,812,563         7,048,427         414.6         15.0         429.6         48           18+87.00         11,812,598         7,048,394         414.1         15.0         429.1         48           19+35.00         11,812,634         7,048,362         413.7         15.0         428.7         0           Wall B3 (Design Stationing 176+50 to 182+00)           10+00.00         11,812,652         7,048,400         415.2         15.0         430.2         36           10+36.00         11,812,663         7,048,366         414.1         15.0         429.1         24           10+60.00         11,812,673         7,048,344         413.6         15.0         428.6         24           10+84.00         11,812,763         7,048,324         413.3         15.0         428.3         24           11+43.00         11,812,752         7,048,234         413.6         15.0         428.6         36           11+79.00         11,812,756         <	16+97.00	11,812,452	7,048,511	415.8	15.0	430.8	40
18+15.00       11,812,540       7,048,433       414.6       15.0       429.6       24         18+39.00       11,812,563       7,048,427       414.6       15.0       429.6       48         18+87.00       11,812,598       7,048,394       414.1       15.0       429.1       48         19+35.00       11,812,634       7,048,362       413.7       15.0       428.7       0         Wall B3 (Design Stationing 176+50 to 182+00)         Wall B3 (Design Stationing 176+50 to 182+00)         10+00.00       11,812,663       7,048,366       414.1       15.0       420.1       24         10+36.00       11,812,663       7,048,366       414.1       15.0       429.1       24         10+60.00       11,812,673       7,048,344       413.6       15.0       428.6       24         10+84.00       11,812,686       7,048,324       413.3       15.0       428.3       24         11+08.00       11,812,703       7,048,283       413.6       15.0       428.6       36         11+79.00       11,812,756       7,048,259       413.1       15.0       428.1       36         12+15.00       11,812,813       7,048,254       412.5 </td <td>17+37.00</td> <td>11,812,482</td> <td>7,048,485</td> <td>415.1</td> <td>15.0</td> <td>430.1</td> <td>39</td>	17+37.00	11,812,482	7,048,485	415.1	15.0	430.1	39
18+39.00       11,812,563       7,048,427       414.6       15.0       429.6       48         18+87.00       11,812,598       7,048,394       414.1       15.0       429.1       48         19+35.00       11,812,634       7,048,362       413.7       15.0       428.7       0         Wall B3 (Design Stationing 176+50 to 182+00)         Wall B3 (Design Stationing 176+50 to 182+00)         10+00.00       11,812,652       7,048,400       415.2       15.0       430.2       36         10+36.00       11,812,663       7,048,366       414.1       15.0       429.1       24         10+60.00       11,812,673       7,048,344       413.6       15.0       428.6       24         10+80.00       11,812,686       7,048,324       413.3       15.0       428.3       24         11+08.00       11,812,703       7,048,307       414.1       15.0       429.1       35         11+43.00       11,812,729       7,048,283       413.6       15.0       428.6       36         11+79.00       11,812,782       7,048,259       413.1       15.0       428.1       36         12+15.00       11,812,813       7,048,207       411.6 <t< td=""><td>17+76.00</td><td>11,812,511</td><td>7,048,459</td><td>414.9</td><td>15.0</td><td>429.9</td><td>39</td></t<>	17+76.00	11,812,511	7,048,459	414.9	15.0	429.9	39
18+87.00       11,812,598       7,048,394       414.1       15.0       429.1       48         19+35.00       11,812,634       7,048,362       413.7       15.0       428.7       0         Wall B3 (Design Stationing 176+50 to 182+00)         10+00.00       11,812,652       7,048,400       415.2       15.0       430.2       36         10+36.00       11,812,663       7,048,366       414.1       15.0       429.1       24         10+60.00       11,812,673       7,048,344       413.6       15.0       428.6       24         10+84.00       11,812,686       7,048,324       413.3       15.0       428.3       24         11+08.00       11,812,703       7,048,307       414.1       15.0       429.1       35         11+43.00       11,812,729       7,048,283       413.6       15.0       428.6       36         11+79.00       11,812,756       7,048,259       413.1       15.0       428.1       36         12+15.00       11,812,813       7,048,234       412.5       15.0       427.5       41         12+56.00       11,812,813       7,048,234       412.5       15.0       426.6       41         13+38.00 <td>18+15.00</td> <td>11,812,540</td> <td>7,048,433</td> <td>414.6</td> <td>15.0</td> <td>429.6</td> <td>24</td>	18+15.00	11,812,540	7,048,433	414.6	15.0	429.6	24
19+35.00     11,812,634     7,048,362     413.7     15.0     428.7     0       Wall B3 (Design Stationing 176+50 to 182+00)       10+00.00     11,812,652     7,048,400     415.2     15.0     430.2     36       10+36.00     11,812,663     7,048,366     414.1     15.0     429.1     24       10+60.00     11,812,673     7,048,344     413.6     15.0     428.6     24       10+84.00     11,812,686     7,048,324     413.3     15.0     428.3     24       11+08.00     11,812,703     7,048,307     414.1     15.0     429.1     35       11+43.00     11,812,729     7,048,283     413.6     15.0     428.6     36       11+79.00     11,812,756     7,048,259     413.1     15.0     428.6     36       12+15.00     11,812,782     7,048,234     412.5     15.0     427.5     41       12+56.00     11,812,813     7,048,207     411.6     15.0     426.6     41       12+97.00     11,812,844     7,048,180     411.2     15.0     426.2     41       13+38.00     11,812,875     7,048,141     409.9     15.0     424.9     24       13+86.00     11,812,993     7,048,125     409.	18+39.00	11,812,563	7,048,427	414.6	15.0	429.6	48
10+00.00	18+87.00	11,812,598	7,048,394	414.1	15.0	429.1	48
10+00.00       11,812,652       7,048,400       415.2       15.0       430.2       36         10+36.00       11,812,663       7,048,366       414.1       15.0       429.1       24         10+60.00       11,812,673       7,048,344       413.6       15.0       428.6       24         10+84.00       11,812,686       7,048,324       413.3       15.0       428.3       24         11+08.00       11,812,703       7,048,307       414.1       15.0       429.1       35         11+43.00       11,812,729       7,048,283       413.6       15.0       428.6       36         11+79.00       11,812,756       7,048,259       413.1       15.0       428.1       36         12+15.00       11,812,782       7,048,234       412.5       15.0       427.5       41         12+56.00       11,812,813       7,048,207       411.6       15.0       426.6       41         12+97.00       11,812,844       7,048,180       411.2       15.0       426.2       41         13+38.00       11,812,895       7,048,153       410.9       15.0       424.9       24         13+86.00       11,812,913       7,048,106       410.2       15.0<	19+35.00	11,812,634	7,048,362	413.7	15.0	428.7	0
10+36.00       11,812,663       7,048,366       414.1       15.0       429.1       24         10+60.00       11,812,673       7,048,344       413.6       15.0       428.6       24         10+84.00       11,812,686       7,048,324       413.3       15.0       428.3       24         11+08.00       11,812,703       7,048,307       414.1       15.0       429.1       35         11+43.00       11,812,729       7,048,283       413.6       15.0       428.6       36         11+79.00       11,812,756       7,048,259       413.1       15.0       428.1       36         12+15.00       11,812,782       7,048,234       412.5       15.0       427.5       41         12+56.00       11,812,813       7,048,207       411.6       15.0       426.6       41         12+97.00       11,812,844       7,048,180       411.2       15.0       426.2       41         13+38.00       11,812,875       7,048,153       410.9       15.0       425.9       24         13+86.00       11,812,913       7,048,125       409.4       15.0       424.4       24         14+58.00       11,812,964       7,048,075       409.7       15.0<				Wall B3	(Design Stationin	ng 176+50 to 182+00)	
10+60.00       11,812,673       7,048,344       413.6       15.0       428.6       24         10+84.00       11,812,686       7,048,324       413.3       15.0       428.3       24         11+08.00       11,812,703       7,048,307       414.1       15.0       429.1       35         11+43.00       11,812,729       7,048,283       413.6       15.0       428.6       36         11+79.00       11,812,756       7,048,259       413.1       15.0       428.1       36         12+15.00       11,812,782       7,048,234       412.5       15.0       427.5       41         12+56.00       11,812,813       7,048,207       411.6       15.0       426.6       41         12+97.00       11,812,844       7,048,180       411.2       15.0       426.2       41         13+38.00       11,812,875       7,048,153       410.9       15.0       425.9       24         13+86.00       11,812,913       7,048,125       409.4       15.0       424.4       24         14+10.00       11,812,928       7,048,106       410.2       15.0       425.2       48         14+58.00       11,812,999       7,048,044       409.7       15.0<	10+00.00	11,812,652	7,048,400	415.2	15.0	430.2	36
10+84.00       11,812,686       7,048,324       413.3       15.0       428.3       24         11+08.00       11,812,703       7,048,307       414.1       15.0       429.1       35         11+43.00       11,812,729       7,048,283       413.6       15.0       428.6       36         11+79.00       11,812,756       7,048,259       413.1       15.0       428.1       36         12+15.00       11,812,782       7,048,234       412.5       15.0       427.5       41         12+56.00       11,812,813       7,048,207       411.6       15.0       426.6       41         12+97.00       11,812,813       7,048,180       411.2       15.0       426.2       41         13+38.00       11,812,875       7,048,153       410.9       15.0       425.9       24         13+62.00       11,812,895       7,048,141       409.9       15.0       424.9       24         13+86.00       11,812,913       7,048,125       409.4       15.0       425.2       48         14+58.00       11,812,964       7,048,075       409.7       15.0       424.7       47         14+58.00       11,812,999       7,048,044       409.1       15.0<	10+36.00	11,812,663	7,048,366	414.1	15.0	429.1	24
11+08.00       11,812,703       7,048,307       414.1       15.0       429.1       35         11+43.00       11,812,729       7,048,283       413.6       15.0       428.6       36         11+79.00       11,812,756       7,048,259       413.1       15.0       428.1       36         12+15.00       11,812,782       7,048,234       412.5       15.0       427.5       41         12+56.00       11,812,813       7,048,207       411.6       15.0       426.6       41         12+97.00       11,812,844       7,048,180       411.2       15.0       426.2       41         13+38.00       11,812,875       7,048,153       410.9       15.0       425.9       24         13+86.00       11,812,995       7,048,141       409.9       15.0       424.9       24         14+10.00       11,812,928       7,048,106       410.2       15.0       425.2       48         14+58.00       11,812,964       7,048,075       409.7       15.0       424.7       47         14+58.00       11,812,999       7,048,044       409.1       15.0       424.1       48	10+60.00	11,812,673	7,048,344	413.6	15.0	428.6	24
11+43.00       11,812,729       7,048,283       413.6       15.0       428.6       36         11+79.00       11,812,756       7,048,259       413.1       15.0       428.1       36         12+15.00       11,812,782       7,048,234       412.5       15.0       427.5       41         12+56.00       11,812,813       7,048,207       411.6       15.0       426.6       41         12+97.00       11,812,844       7,048,180       411.2       15.0       426.2       41         13+38.00       11,812,875       7,048,153       410.9       15.0       425.9       24         13+62.00       11,812,895       7,048,141       409.9       15.0       424.9       24         13+86.00       11,812,913       7,048,125       409.4       15.0       424.4       24         14+10.00       11,812,928       7,048,106       410.2       15.0       425.2       48         14+58.00       11,812,964       7,048,075       409.7       15.0       424.7       47         14+58.00       11,812,999       7,048,044       409.1       15.0       424.1       48	10+84.00	11,812,686	7,048,324	413.3	15.0	428.3	24
11+79.00       11,812,756       7,048,259       413.1       15.0       428.1       36         12+15.00       11,812,782       7,048,234       412.5       15.0       427.5       41         12+56.00       11,812,813       7,048,207       411.6       15.0       426.6       41         12+97.00       11,812,844       7,048,180       411.2       15.0       426.2       41         13+38.00       11,812,875       7,048,153       410.9       15.0       425.9       24         13+62.00       11,812,895       7,048,141       409.9       15.0       424.9       24         13+86.00       11,812,913       7,048,125       409.4       15.0       424.4       24         14+10.00       11,812,928       7,048,106       410.2       15.0       425.2       48         14+58.00       11,812,964       7,048,075       409.7       15.0       424.7       47         14+58.00       11,812,999       7,048,044       409.1       15.0       424.1       48	11+08.00	11,812,703	7,048,307	414.1	15.0	429.1	35
11+79.00       11,812,756       7,048,259       413.1       15.0       428.1       36         12+15.00       11,812,782       7,048,234       412.5       15.0       427.5       41         12+56.00       11,812,813       7,048,207       411.6       15.0       426.6       41         12+97.00       11,812,844       7,048,180       411.2       15.0       426.2       41         13+38.00       11,812,875       7,048,153       410.9       15.0       425.9       24         13+62.00       11,812,895       7,048,141       409.9       15.0       424.9       24         13+86.00       11,812,913       7,048,125       409.4       15.0       424.4       24         14+10.00       11,812,928       7,048,106       410.2       15.0       425.2       48         14+58.00       11,812,964       7,048,075       409.7       15.0       424.7       47         14+58.00       11,812,999       7,048,044       409.1       15.0       424.1       48	11+43.00	11,812,729	7,048,283	413.6	15.0	428.6	36
12+56.00       11,812,813       7,048,207       411.6       15.0       426.6       41         12+97.00       11,812,844       7,048,180       411.2       15.0       426.2       41         13+38.00       11,812,875       7,048,153       410.9       15.0       425.9       24         13+62.00       11,812,895       7,048,141       409.9       15.0       424.9       24         13+86.00       11,812,913       7,048,125       409.4       15.0       424.4       24         14+10.00       11,812,928       7,048,106       410.2       15.0       425.2       48         14+58.00       11,812,964       7,048,075       409.7       15.0       424.7       47         14+58.00       11,812,999       7,048,044       409.1       15.0       424.1       48	11+79.00	11,812,756	7,048,259	413.1	15.0	428.1	36
12+97.00     11,812,844     7,048,180     411.2     15.0     426.2     41       13+38.00     11,812,875     7,048,153     410.9     15.0     425.9     24       13+62.00     11,812,895     7,048,141     409.9     15.0     424.9     24       13+86.00     11,812,913     7,048,125     409.4     15.0     424.4     24       14+10.00     11,812,928     7,048,106     410.2     15.0     425.2     48       14+58.00     11,812,964     7,048,075     409.7     15.0     424.7     47       14+58.00     11,812,999     7,048,044     409.1     15.0     424.1     48	12+15.00	11,812,782	7,048,234	412.5	15.0	427.5	41
12+97.00     11,812,844     7,048,180     411.2     15.0     426.2     41       13+38.00     11,812,875     7,048,153     410.9     15.0     425.9     24       13+62.00     11,812,895     7,048,141     409.9     15.0     424.9     24       13+86.00     11,812,913     7,048,125     409.4     15.0     424.4     24       14+10.00     11,812,928     7,048,106     410.2     15.0     425.2     48       14+58.00     11,812,964     7,048,075     409.7     15.0     424.7     47       14+58.00     11,812,999     7,048,044     409.1     15.0     424.1     48	12+56.00						41
13+38.00     11,812,875     7,048,153     410.9     15.0     425.9     24       13+62.00     11,812,895     7,048,141     409.9     15.0     424.9     24       13+86.00     11,812,913     7,048,125     409.4     15.0     424.4     24       14+10.00     11,812,928     7,048,106     410.2     15.0     425.2     48       14+58.00     11,812,964     7,048,075     409.7     15.0     424.7     47       14+58.00     11,812,999     7,048,044     409.1     15.0     424.1     48							41
13+62.00     11,812,895     7,048,141     409.9     15.0     424.9     24       13+86.00     11,812,913     7,048,125     409.4     15.0     424.4     24       14+10.00     11,812,928     7,048,106     410.2     15.0     425.2     48       14+58.00     11,812,964     7,048,075     409.7     15.0     424.7     47       14+58.00     11,812,999     7,048,044     409.1     15.0     424.1     48							24
13+86.00     11,812,913     7,048,125     409.4     15.0     424.4     24       14+10.00     11,812,928     7,048,106     410.2     15.0     425.2     48       14+58.00     11,812,964     7,048,075     409.7     15.0     424.7     47       14+58.00     11,812,999     7,048,044     409.1     15.0     424.1     48							
14+10.00     11,812,928     7,048,106     410.2     15.0     425.2     48       14+58.00     11,812,964     7,048,075     409.7     15.0     424.7     47       14+58.00     11,812,999     7,048,044     409.1     15.0     424.1     48							
14+58.00     11,812,964     7,048,075     409.7     15.0     424.7     47       14+58.00     11,812,999     7,048,044     409.1     15.0     424.1     48							
14+58.00 11,812,999 7,048,044 409.1 15.0 424.1 48							
							0

			Wall B4	(Design Stationir	ng 182+50 to 190+25)	
10+00.00	11,813,112	7,047,961	406.4	15.0	421.4	48
10+48.00	11,813,148	7,047,930	406.5	15.0	421.5	48
10+96.00	11,813,184	7,047,898	405.9	15.0	420.9	41
11+37.00	11,813,213	7,047,868	405.3	15.0	420.3	42
11+79.00	11,813,243	7,047,839	404.8	15.0	419.8	42
12+21.00	11,813,273	7,047,809	404.3	15.0	419.3	42
12+63.00	11,813,303	7,047,780	403.8	15.0	418.8	48
13+11.00	11,813,340	7,047,749	403.3	15.0	418.3	45
13+56.00	11,813,374	7,047,719	402.7	15.0	417.7	45
14+01.00	11,813,407	7,047,689	402.2	15.0	417.2	45
14+46.00	11,813,441	7,047,660	401.6	15.0	416.6	45
14+91.00	11,813,475	7,047,630	401.0	15.0	416.0	45
15+36.00	11,813,509	7,047,600	400.4	15.0	415.4	45
15+81.00	11,813,542	7,047,570	399.8	15.0	414.8	45
16+26.00	11,813,576	7,047,541	399.3	15.0	414.3	45
16+71.00	11,813,610	7,047,511	398.8	15.0	413.8	24
16+95.00	11,813,630	7,047,498	398.6	15.0	413.6	24
17+19.00	11,813,648	7,047,483	397.3	15.0	412.3	0
			Wall B5	(Design Stationir	ng 192+00 to 205+50)	
10+00.00	11,813,824	7,047,379	406.8	15.0	421.8	46
10+46.00	11,813,858	7,047,349	408.6	15.0	423.6	46
10+92.00	11,813,893	7,047,318	408.7	15.0	423.7	45
11+37.00	11,813,927	7,047,288	408.2	15.0	423.2	45
11+82.00	11,813,957	7,047,254	406.2	15.0	421.2	45
12+27.00	11,813,987	7,047,221	404.2	15.0	419.2	45
12+72.00	11,814,017	7,047,187	402.3	15.0	417.3	45
13+17.00	11,814,046	7,047,153	400.3	15.0	415.3	45
13+62.00	11,814,076	7,047,119	397.4	15.0	412.4	45
14+07.00	11,814,106	7,047,085	393.8	15.0	408.8	45
14+52.00	11,814,136	7,047,052	390.9	15.0	405.9	45
14+97.00	11,814,165	7,047,018	390.6	15.0	405.6	49
15+46.00	11,814,202	7,046,985	390.0	15.0	405.0	49
15+95.00	11,814,239	7,046,953	389.4	15.0	404.4	49
16+44.00	11,814,276	7,046,920	388.8	15.0	403.8	49
16+93.00	11,814,313	7,046,888	388.1	15.0	403.1	49
17+42.00	11,814,350	7,046,855	387.4	15.0	402.4	50
17+92.00	11,814,387	7,046,822	386.7	15.0	401.7	50
18+42.00	11,814,425	7,046,790	386.0	15.0	401.0	49
18+91.00	11,814,462	7,046,757	385.3	15.0	400.3	49
19+40.00	11,814,499	7,046,725	384.6	15.0	399.6	49
19+89.00	11,814,536	7,046,692	383.9	15.0	398.9	49
20+38.00	11,814,573	7,046,660	383.2	15.0	398.2	50
20+88.00	11,814,610	7,046,627	382.8	15.0	397.8	49
21+37.00	11,814,647	7,046,594	382.4	15.0	397.4	49
21+86.00	11,814,684	7,046,562	382.1	15.0	397.1	38
22+24.00	11,814,712	7,046,537	381.8	15.0	396.8	36
22+60.00	11,814,739	7,046,512	381.4	15.0	396.4	38
22+98.00	11,814,767	7,046,487	381.0	15.0	396.0	38
23+36.00	11,814,795	7,046,461	380.7	15.0	395.7	0

	Wall B6 (Design Stationing 204+50 to 215+50)									
10+00.00	11,814,749	7,046,545	370.3	15.0	385.3	39				
10+39.00	11,814,778	7,046,519	374.7	15.0	389.7	39				
10+78.00	11,814,807	7,046,492	379.9	15.0	394.9	39				
11+17.00	11,814,835	7,046,466	385.4	15.0	400.4	40				
11+57.00	11,814,864	7,046,439	390.7	15.0	405.7	48				
12+05.00	11,814,905	7,046,414	397.3	15.0	412.3	47				
12+52.00	11,814,938	7,046,380	398.4	15.0	413.4	48				
13+00.00	11,814,972	7,046,346	398.5	15.0	413.5	48				
13+48.00	11,815,006	7,046,311	396.3	15.0	411.3	48				
13+96.00	11,815,040	7,046,277	394.1	15.0	409.1	47				
14+43.00	11,815,073	7,046,243	392.9	15.0	407.9	48				
14+91.00	11,815,104	7,046,206	389.4	15.0	404.4	48				
15+39.00	11,815,135	7,046,169	386.6	15.0	401.6	48				
15+87.00	11,815,165	7,046,132	384.6	15.0	399.6	48				
16+35.00	11,815,196	7,046,096	381.8	15.0	396.8	48				
16+83.00	11,815,227	7,046,059	378.7	15.0	393.7	48				
17+31.00	11,815,258	7,046,022	377.6	15.0	392.6	48				
17+79.00	11,815,288	7,045,985	374.7	15.0	389.7	48				
18+27.00	11,815,319	7,045,948	371.8	15.0	386.8	48				
18+75.00	11,815,350	7,045,911	369.0	15.0	384.0	48				
19+23.00	11,815,381	7,045,874	369.1	15.0	384.1	38				
19+61.00	11,815,408	7,045,848	368.3	15.0	383.3	37				
19+98.00	11,815,434	7,045,821	367.3	15.0	382.3	38				
20+36.00	11,815,461	7,045,794	366.4	15.0	381.4	48				
20+84.00	11,815,504	7,045,772	364.3	15.0	379.3	0				
			Wall D1	(Design Stationir	ng 216+50 to 225+00)					
10+00.00	11,815,611	7,045,676	360.0	15.0	375.0	48				
10+48.00	11,815,647	7,045,644	359.9	15.0	374.9	48				
10+96.00	11,815,683	7,045,613	358.9	15.0	373.9	36				
11+32.00	11,815,711	7,045,590	358.3	15.0	373.3	36				
11+68.00	11,815,739	7,045,567	357.5	15.0	372.5	48				
12+16.00	11,815,776	7,045,537	356.3	15.0	371.3	48				
12+64.00	11,815,814	7,045,508	355.2	15.0	370.2	48				
13+12.00	11,815,852	7,045,479	354.2	15.0	369.2	48				
13+60.00	11,815,890	7,045,450	353.1	15.0	368.1	24				
13+84.00	11,815,907	7,045,432	353.7	15.0	368.7	48				
14+32.00	11,815,944	7,045,402	353.3	15.0	368.3	49				
14+81.00	11,815,982	7,045,372	352.8	15.0	367.8	48				
15+29.00	11,816,019	7,045,342	352.3	15.0	367.3	48				
15+77.00	11,816,056	7,045,312	351.9	15.0	366.9	48				
16+25.00	11,816,095	7,045,284	351.6	15.0	366.6	49				
16+74.00	11,816,135	7,045,256	351.4	15.0	366.4	48				
17+22.00	11,816,174	7,045,228	351.3	15.0	366.3	48				
17+70.00	11,816,213	7,045,200	351.1	15.0	366.1	48				
18+18.00	11,816,252	7,045,173	350.9	15.0	365.9	0				

CNE C - W	all C1 and C2	Acoustical P	rofile (Pro	jection NAD_198	33_StatePlane_Virginia	a_North US Feet)					
Station	X Coordinate	Y Coordinate	Base Elevation	Wall Height	Top Elevation	Segment Length					
	Wall C1 (Design Stationing 1193+00 to 1227+50)										
10+00.00	11,813,781	7,047,145	402.6	15.0	417.6	48					
10+48.00	11,813,814	7,047,111	405.0	15.0	420.0	48					
10+96.00	11,813,847	7,047,076	406.2	15.0	421.2	48					
11+44.00	11,813,883	7,047,044	406.2	15.0	421.2	48					
11+92.00	11,813,919	7,047,012	405.5	15.0	420.5	43					
12+35.00	11,813,952	7,046,984	404.6	15.0	419.6	44					
12+79.00	11,813,986	7,046,957	403.4	15.0	418.4	43					
13+22.00	11,814,019	7,046,929	402.3	15.0	417.3	43					
13+65.00	11,814,052	7,046,901	401.0	15.0	416.0	43					
14+08.00	11,814,085	7,046,873	399.8	15.0	414.8	36					
14+44.00	11,814,115	7,046,854	397.9	15.0	412.9	36					
14+80.00	11,814,145	7,046,834	395.4	15.0	410.4	36					
15+16.00	11,814,178	7,046,819	389.5	15.0	404.5	36					
15+52.00	11,814,211	7,046,804	387.8	15.0	402.8	48					
16+00.00	11,814,247	7,046,772	386.9	15.0	401.9	48					
16+48.00	11,814,283	7,046,741	386.2	15.0	401.2	48					
16+96.00	11,814,319	7,046,709	385.5	15.0	400.5	48					
17+44.00	11,814,355	7,046,677	384.8	15.0	399.8	48					
17+92.00	11,814,391	7,046,646	384.0	15.0	399.0	48					
18+40.00	11,814,427	7,046,614	383.3	15.0	398.3	48					
18+88.00	11,814,463	7,046,582	382.6	15.0	397.6	48					
19+36.00	11,814,499	7,046,551	381.9	15.0	396.9	48					
19+84.00	11,814,535	7,046,519	381.2	15.0	396.2	48					
20+32.00	11,814,571	7,046,487	380.5	15.0	395.5	48					
20+80.00	11,814,607	7,046,455	379.7	15.0	394.7	24					
21+04.00	11,814,625	7,046,440	379.2	15.0	394.2	24					
21+28.00	11,814,643	7,046,423	378.8	15.0	393.8	24					
21+52.00	11,814,661	7,046,407	378.5	15.0	393.5	23					
21+75.00	11,814,678	7,046,391	378.2	15.0	393.2	24					
21+99.00	11,814,696	7,046,375	377.9	15.0	392.9	24					
22+23.00	11,814,714	7,046,359	377.6	15.0	392.6	24					
22+47.00	11,814,731	7,046,342	377.4	15.0	392.4	24					
22+71.00	11,814,748	7,046,326	377.2	15.0	392.2	25					
22+96.00	11,814,766	7,046,309	377.1	15.0	392.1	24					
23+20.00	11,814,783	7,046,292	376.9	15.0	391.9	24					
23+44.00	11,814,800	7,046,275	376.8	15.0	391.8	24					
23+68.00	11,814,817	7,046,259	376.7	15.0	391.7	24					
23+92.00	11,814,834	7,046,242	376.6	15.0	391.6	24					
24+16.00	11,814,851	7,046,225	376.6	15.0	391.6	48					
24+64.00	11,814,885	7,046,191	376.4	15.0	391.4	48					
25+12.00	11,814,919	7,046,156	376.1	15.0	391.1	47					
25+59.00	11,814,952	7,046,122	375.8	15.0	390.8	48					
26+07.00	11,814,986	7,046,088	375.3	15.0	390.3	48					
26+55.00	11,815,020	7,046,054	374.8	15.0	389.8	48					
27+03.00	11,815,054	7,046,020	374.2	15.0	389.2	47					
27.05.00	11,010,004	7,010,020	5, 7.2	10.0	303.2	*1					

27+50.00	11,815,087	7,045,986	373.5	15.0	388.5	48
27+98.00	11,815,121	7,045,951	372.9	15.0	387.9	48
28+46.00	11,815,155	7,045,917	372.2	15.0	387.2	48
28+94.00	11,815,189	7,045,883	371.6	15.0	386.6	47
29+41.00	11,815,222	7,045,849	371.1	15.0	386.1	48
29+89.00	11,815,256	7,045,815	370.7	15.0	385.7	48
30+37.00	11,815,290	7,045,781	370.3	15.0	385.3	47
30+84.00	11,815,323	7,045,747	369.9	15.0	384.9	24
31+08.00	11,815,340	7,045,730	369.7	15.0	384.7	24
31+32.00	11,815,357	7,045,713	369.5	15.0	384.5	25
31+57.00	11,815,375	7,045,696	369.2	15.0	384.2	24
31+81.00	11,815,392	7,045,679	368.9	15.0	383.9	24
32+05.00	11,815,409	7,045,663	368.5	15.0	383.5	13
32+18.00	11,815,418	7,045,654	368.4	15.0	383.4	24
32+42.00	11,815,424	7,045,631	368.3	15.0	383.3	48
32+90.00	11,815,459	7,045,598	367.7	15.0	382.7	24
33+14.00	11,815,483	7,045,594	367.2	15.0	382.2	46
33+60.00	11,815,517	7,045,563	366.4	15.0	381.4	40
34+00.00	11,815,547	7,045,537	365.3	15.0	380.3	25
34+25.00	11,815,566	7,045,521	364.7	15.0	379.7	24
34+49.00	11,815,584	7,045,505	364.2	15.0	379.2	24
34+73.00	11,815,602	7,045,490	363.7	15.0	378.7	25
34+98.00	11,815,621	7,045,474	363.2	15.0	378.2	23
35+21.00	11,815,639	7,045,459	362.6	15.0	377.6	24
35+45.00	11,815,658	7,045,444	362.1	15.0	377.1	25
35+70.00	11,815,677	7,045,429	361.5	15.0	376.5	24
35+94.00	11,815,696	7,045,414	361.0	15.0	376.0	23
36+17.00	11,815,714	7,045,399	360.5	15.0	375.5	24
36+41.00	11,815,733	7,045,385	359.9	15.0	374.9	25
36+66.00	11,815,753	7,045,370	359.4	15.0	374.4	24
36+90.00	11,815,772	7,045,356	358.9	15.0	373.9	24
37+14.00	11,815,791	7,045,341	358.3	15.0	373.3	24
37+38.00	11,815,810	7,045,327	357.8	15.0	372.8	24
37+62.00	11,815,830	7,045,313	357.2	15.0	372.2	24
37+86.00	11,815,849	7,045,299	356.5	15.0	371.5	24
38+10.00	11,815,869	7,045,285	355.8	15.0	370.8	43
38+53.00	11,815,904	7,045,260	354.7	15.0	369.7	43
38+96.00	11,815,939	7,045,235	353.7	15.0	368.7	43
39+39.00	11,815,974	7,045,210	352.8	15.0	367.8	44
39+83.00	11,816,010	7,045,185	352.1	15.0	367.1	43
40+26.00	11,816,045	7,045,160	351.8	15.0	366.8	24
40+50.00	11,816,064	7,045,145	351.6	15.0	366.6	45
40+95.00	11,816,099	7,045,116	351.4	15.0	366.4	46
41+41.00	11,816,135	7,045,088	351.2	15.0	366.2	45
41+86.00	11,816,170	7,045,059	350.9	15.0	365.9	46
42+32.00	11,816,206	7,045,031	350.7	15.0	365.7	41
42+73.00	11,816,239	7,045,007	350.6	15.0	365.6	39
43+12.00	11,816,271	7,044,984	350.5	15.0	365.5	41
43+53.00	11,816,304	7,044,961	350.4	15.0	365.4	41
43+94.00	11,816,337	7,044,937	350.2	15.0	365.2	40
44+34.00	11,816,370	7,044,914	350.0	15.0	365.0	24
44+58.00	11,816,388	7,044,898	345.9	15.0	360.9	0
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			Wall C2	(Design Stationin	g 1228+50 to 1246+00)	
10+00.00	11,816,458	7,044,848	345.8	15.0	360.8	48
10+48.00	11,816,504	7,044,834	347.2	15.0	362.2	39
10+87.00	11,816,536	7,044,811	348.8	15.0	363.8	40
11+27.00	11,816,569	7,044,788	348.5	15.0	363.5	41
11+68.00	11,816,602	7,044,764	348.2	15.0	363.2	48
12+16.00	11,816,637	7,044,732	348.0	15.0	363.0	36
12+52.00	11,816,666	7,044,711	349.1	15.0	364.1	36
12+88.00	11,816,695	7,044,690	349.2	15.0	364.2	40
13+28.00	11,816,725	7,044,663	350.7	15.0	365.7	40
13+68.00	11,816,755	7,044,637	352.5	15.0	367.5	40
14+08.00	11,816,785	7,044,610	354.5	15.0	369.5	48
14+56.00	11,816,823	7,044,581	354.3	15.0	369.3	48
15+04.00	11,816,861	7,044,551	354.2	15.0	369.2	48
15+52.00	11,816,900	7,044,523	353.1	15.0	368.1	48
16+00.00	11,816,939	7,044,495	351.1	15.0	366.1	48
16+48.00	11,816,978	7,044,467	347.6	15.0	362.6	40
16+88.00	11,817,007	7,044,440	345.3	15.0	360.3	40
17+28.00	11,817,036	7,044,413	344.5	15.0	359.5	40
17+68.00	11,817,065	7,044,385	344.2	15.0	359.2	24
17+92.00	11,817,088	7,044,378	344.1	15.0	359.1	43
18+35.00	11,817,117	7,044,346	344.0	15.0	359.0	43
18+78.00	11,817,146	7,044,314	343.9	15.0	358.9	43
19+21.00	11,817,175	7,044,282	343.8	15.0	358.8	44
19+65.00	11,817,205	7,044,250	343.6	15.0	358.6	43
20+08.00	11,817,234	7,044,218	344.4	15.0	359.4	48
20+56.00	11,817,263	7,044,180	347.1	15.0	362.1	48
21+04.00	11,817,292	7,044,142	347.5	15.0	362.5	36
21+40.00	11,817,312	7,044,112	350.4	15.0	365.4	36
21+76.00	11,817,331	7,044,081	352.3	15.0	367.3	48
22+24.00	11,817,360	7,044,043	350.9	15.0	365.9	48
22+72.00	11,817,392	7,044,008	347.7	15.0	362.7	48
23+20.00	11,817,425	7,043,972	342.5	15.0	357.5	48
23+68.00	11,817,457	7,043,936	341.9	15.0	356.9	36
24+04.00	11,817,475	7,043,905	341.5	15.0	356.5	36
24+40.00	11,817,492	7,043,874	341.4	15.0	356.4	36
24+76.00	11,817,506	7,043,841	341.5	15.0	356.5	36
25+12.00	11,817,520	7,043,807	341.9	15.0	356.9	36
25+48.00	11,817,539	7,043,777	342.2	15.0	357.2	36
25+84.00	11,817,558	7,043,746	342.5	15.0	357.5	35
26+19.00	11,817,574	7,043,714	342.9	15.0	357.9	36
26+55.00	11,817,591	7,043,682	343.2	15.0	358.2	36
26+91.00	11,817,611	7,043,652	343.3	15.0	358.3	36
27+27.00	11,817,631	7,043,622	338.1	15.0	353.1	0

CNE D/E -	Walls E1-E4 an	nd D2 Acoust	ical Profile	(Projection NAI	D_1983_StatePlane_V	irginia_North US Feet)					
Station	X Coordinate	Y Coordinate	Base Elevation	Wall Height	Top Elevation	Segment Length					
	Wall E1 (Design Stationing 238+25 to 246+00)										
10+00.00	11,817,325	7,044,354	344.6	15.0	359.6	48					
10+48.00	11,817,357	7,044,318	347.3	15.0	362.3	48					
10+96.00	11,817,388	7,044,282	347.1	15.0	362.1	25					
11+21.00	11,817,401	7,044,261	348.0	15.0	363.0	48					
11+69.00	11,817,431	7,044,224	347.8	15.0	362.8	37					
12+06.00	11,817,454	7,044,195	347.7	15.0	362.7	36					
12+42.00	11,817,476	7,044,167	347.6	15.0	362.6	48					
12+90.00	11,817,501	7,044,126	347.3	15.0	362.3	48					
13+38.00	11,817,526	7,044,085	346.9	15.0	361.9	48					
13+86.00	11,817,552	7,044,045	346.7	15.0	361.7	48					
14+34.00	11,817,577	7,044,004	346.4	15.0	361.4	36					
14+70.00	11,817,596	7,043,973	346.3	15.0	361.3	36					
15+06.00	11,817,615	7,043,943	346.2	15.0	361.2	48					
15+54.00	11,817,640	7,043,902	346.1	15.0	361.1	24					
15+78.00	11,817,656	7,043,883	345.0	15.0	360.0	24					
16+02.00	11,817,668	7,043,862	344.8	15.0	359.8	24					
16+26.00	11,817,676	7,043,839	345.4	15.0	360.4	36					
16+62.00	11,817,694	7,043,808	345.1	15.0	360.1	35					
16+97.00	11,817,711	7,043,777	344.8	15.0	359.8	36					
17+33.00	11,817,733	7,043,748	344.6	15.0	359.6	36					
17+69.00	11,817,754	7,043,719	341.8	15.0	356.8	0					
			Wall E2	(Design Stationin	g 247+00 to 254+00)						
10+00.00	11,817,815.00	7,043,610.00	341	15.0	356.0	44					
10+44.00	11,817,837.00	7,043,571.50	342.95	15.0	358.0	44					
10+88.00	11,817,858.00	7,043,533.00	345.7	15.0	360.7	44					
11+32.00	11,817,880.00	7,043,495.00	347.19	15.0	362.2	44					
11+76.00	11,817,901.00	7,043,456.50	346.8	15.0	361.8	44					
12+20.00	11,817,923.00	7,043,418.00	343.95	15.0	359.0	44					
12+64.00	11,817,944.00		342.45	15.0	357.5	48					
13+12.00	11,817,966.00	7,043,337.00	342.37	15.0	357.4	48					
13+60.00	11,817,989.00	7,043,294.50	342.31	15.0	357.3	48					
14+08.00	11,818,011.00	7,043,252.00	342.25	15.0	357.3	44					
14+52.00	11,818,032.00	7,043,213.50	342.12	15.0	357.1	44					
14+96.00	11,818,054.00	7,043,175.00	341.99	15.0	357.0	43					
15+39.00	11,818,075.00	7,043,137.00	341.86	15.0	356.9	44					
15+83.00	11,818,097.00	7,043,098.50	341.66	15.0	356.7	44					
16+27.00	11,818,118.00	7,043,060.00	341.32	15.0	356.3	44					
16+71.00	11,818,140.00	7,043,022.00	340.89	15.0	355.9	24					
16+95.00	11,818,162.00	7,043,013.50	338.26	15.0	353.3	0					

	Wall E3 (Design Stationing 254+25 to 269+25)									
10+00.00	11,818,201	7,042,918	340.0	15.0	355.0	24				
10+24.00	11,818,213	7,042,897	337.5	15.0	352.5	24				
10+48.00	11,818,225	7,042,877	336.8	15.0	351.8	24				
10+72.00	11,818,238	7,042,856	336.2	15.0	351.2	24				
10+96.00	11,818,250	7,042,835	335.6	15.0	350.6	24				

11.20.00	11 010 202	7.042.045	225.0	15.0	250.0	24
11+20.00	11,818,262	7,042,815	335.0	15.0 15.0	350.0	24 24
11+44.00	11,818,275	7,042,794	334.3		349.3	
11+68.00	11,818,288	7,042,774	333.5	15.0	348.5	24
11+92.00	11,818,300	7,042,754	332.7	15.0	347.7	24
12+16.00	11,818,313	7,042,734	331.9	15.0	346.9	24
12+40.00	11,818,326	7,042,713	331.1	15.0	346.1	24
12+64.00	11,818,340	7,042,693	330.3	15.0	345.3	24
12+88.00	11,818,353	7,042,673	329.4	15.0	344.4	24
13+12.00	11,818,365	7,042,653	328.5	15.0	343.5	24
13+36.00	11,818,377	7,042,632	327.6	15.0	342.6	24
13+60.00	11,818,389	7,042,612	326.6	15.0	341.6	24
13+84.00	11,818,402	7,042,591	325.5	15.0	340.5	24
14+08.00	11,818,415	7,042,571	324.5	15.0	339.5	24
14+32.00	11,818,428	7,042,551	323.5	15.0	338.5	24
14+56.00	11,818,442	7,042,531	322.5	15.0	337.5	24
14+80.00	11,818,456	7,042,512	321.6	15.0	336.6	24
15+04.00	11,818,471	7,042,493	320.7	15.0	335.7	24
15+28.00	11,818,485	7,042,474	319.8	15.0	334.8	24
15+52.00	11,818,500	7,042,455	319.0	15.0	334.0	24
15+76.00	11,818,514	7,042,436	318.2	15.0	333.2	24
16+00.00	11,818,529	7,042,417	317.5	15.0	332.5	24
16+24.00	11,818,544	7,042,398	316.8	15.0	331.8	24
16+48.00	11,818,559	7,042,379	316.1	15.0	331.1	24
16+72.00	11,818,575	7,042,361	315.5	15.0	330.5	24
16+96.00	11,818,590	7,042,342	315.0	15.0	330.0	24
17+20.00	11,818,605	7,042,324	314.4	15.0	329.4	24
17+44.00	11,818,621	7,042,306	314.0	15.0	329.0	24
17+68.00	11,818,636	7,042,287	313.5	15.0	328.5	24
17+92.00	11,818,652	7,042,269	313.1	15.0	328.1	24
18+16.00	11,818,668	7,042,251	312.8	15.0	327.8	24
18+40.00	11,818,684	7,042,233	312.5	15.0	327.5	24
18+64.00	11,818,700	7,042,216	312.2	15.0	327.2	24
18+88.00	11,818,716	7,042,198	312.0	15.0	327.0	24
19+12.00	11,818,733	7,042,180	311.9	15.0	326.9	24
19+36.00	11,818,749	7,042,163	311.7	15.0	326.7	24
19+60.00	11,818,766	7,042,145	311.6	15.0	326.6	24
19+84.00	11,818,782	7,042,143	311.6	15.0	326.6	24
20+08.00	11,818,799	7,042,128	311.6	15.0	326.6	24
20+32.00	11,818,733	7,042,111	311.6	15.0	326.6	24
20+56.00	11,818,833	7,042,094	311.7	15.0	326.7	24
20+36.00	11,818,850	7,042,077	311.7	15.0	326.9	24
21+04.00	11,818,867	7,042,060	311.9	15.0	327.0	24
21+04.00	11,818,884				327.3	24
		7,042,026	312.3	15.0		
21+52.00	11,818,902	7,042,010	312.5	15.0	327.5	24
21+76.00	11,818,919	7,041,993	312.8	15.0	327.8	24
22+00.00	11,818,937	7,041,977	313.2	15.0	328.2	23
22+23.00	11,818,954	7,041,961	313.6	15.0	328.6	24
22+47.00	11,818,972	7,041,944	314.0	15.0	329.0	24
22+71.00	11,818,990	7,041,928	314.5	15.0	329.5	24
22+95.00	11,819,008	7,041,912	315.0	15.0	330.0	24
23+19.00	11,819,026	7,041,897	315.6	15.0	330.6	24
23+43.00	11,819,044	7,041,881	316.2	15.0	331.2	24
23+67.00	11,819,062	7,041,865	316.8	15.0	331.8	24
23+91.00	11,819,080	7,041,850	317.3	15.0	332.3	25
24+16.00	11,819,099	7,041,834	317.9	15.0	332.9	40
24+56.00	11,819,124	7,041,865	316.8	15.0	331.8	0

			Wall E4	(Design Stationin	g 270+75 to 277+50)	
10+00.00	11,819,231	7,041,781	324.7	15.0	339.7	38
10+38.00	11,819,209	7,041,750	322.8	15.0	337.8	29
10+67.00	11,819,233	7,041,734	324.1	15.0	339.1	30
10+97.00	11,819,258	7,041,717	325.5	15.0	340.5	30
11+27.00	11,819,283	7,041,701	327.0	15.0	342.0	29
11+56.00	11,819,307	7,041,685	328.4	15.0	343.4	45
12+01.00	11,819,345	7,041,661	330.4	15.0	345.4	44
12+45.00	11,819,382	7,041,638	332.3	15.0	347.3	45
12+90.00	11,819,420	7,041,614	334.0	15.0	349.0	44
13+34.00	11,819,457	7,041,591	335.2	15.0	350.2	45
13+79.00	11,819,495	7,041,567	336.4	15.0	351.4	24
14+03.00	11,819,517	7,041,558	338.5	15.0	353.5	24
14+27.00	11,819,537	7,041,546	339.1	15.0	354.1	24
14+51.00	11,819,555	7,041,530	338.1	15.0	353.1	41
14+92.00	11,819,590	7,041,508	338.9	15.0	353.9	40
15+32.00	11,819,624	7,041,487	339.6	15.0	354.6	40
15+72.00	11,819,658	7,041,465	340.2	15.0	355.2	40
16+12.00	11,819,692	7,041,444	340.7	15.0	355.7	50
16+62.00	11,819,740	7,041,458	349.2	15.0	364.2	49
17+11.00	11,819,787	7,041,473	346.4	15.0	361.4	0
			Wall D2	(Design Stationin	g 230+50 to 237+50)	
10+00.00	11,816,744	7,044,907	358.1	15.0	373.1	27
10+27.00	11,816,736	7,044,881	358.2	15.0	373.2	42
10+69.00	11,816,770	7,044,857	360.0	15.0	375.0	43
11+12.00	11,816,805	7,044,832	360.7	15.0	375.7	42
11+54.00	11,816,839	7,044,807	361.7	15.0	376.7	43
11+97.00	11,816,874	7,044,782	361.1	15.0	376.1	35
12+32.00	11,816,902	7,044,761	360.2	15.0	375.2	35
12+67.00	11,816,930	7,044,741	359.6	15.0	374.6	35
13+02.00	11,816,957	7,044,719	358.7	15.0	373.7	35
13+37.00	11,816,985	7,044,698	357.7	15.0	372.7	35
13+72.00	11,817,012	7,044,676	355.6	15.0	370.6	35
14+07.00	11,817,039	7,044,654	353.0	15.0	368.0	34
14+41.00	11,817,065	7,044,631	350.7	15.0	365.7	35
14+76.00	11,817,092	7,044,609	347.3	15.0	362.3	35
15+11.00	11,817,118	7,044,585	344.3	15.0	359.3	35
15+46.00	11,817,144	7,044,562	342.7	15.0	357.7	34
15+80.00	11,817,169	7,044,538	342.7	15.0	357.7	35
16+15.00	11,817,195	7,044,514	342.9	15.0	357.9	34
16+49.00	11,817,219	7,044,490	342.9	15.0	357.9	35
16+84.00	11,817,244	7,044,465	342.8	15.0	357.8	35
17+19.00	11,817,268	7,044,440	342.8	15.0	357.8	35
17+54.00	11,817,293	7,044,415	343.5	15.0	358.5	0

CNE D/E -	CNE D/E - Walls E1-E4 and D2 Acoustical Profile (Projection NAD_1983_StatePlane_Virginia_North US Feet)										
Station	X Coordinate	Y Coordinate	Base Elevation	Wall Height	Top Elevation	Segment Length					
	Wall E1 (Design Stationing 238+25 to 246+00)										
10+00.00	11,817,752	7,043,722	342.1	15.0	357.1	2					
10+02.00	11,817,751	7,043,724	342.2	15.0	357.2	30					
10+32.00	11,817,733	7,043,748	344.6	15.0	359.6	36					
10+68.00	11,817,711	7,043,777	344.8	15.0	359.8	35					
11+03.00	11,817,694	7,043,808	345.1	15.0	360.1	36					
11+39.00	11,817,676	7,043,839	345.4	15.0	360.4	24					
11+63.00	11,817,668	7,043,862	344.8	15.0	359.8	24					
11+87.00	11,817,656	7,043,883	345.0	15.0	360.0	24					
12+11.00	11,817,640	7,043,902	346.1	15.0	361.1	48					
12+59.00	11,817,615	7,043,943	346.2	15.0	361.2	36					
12+95.00	11,817,596	7,043,973	346.3	15.0	361.3	36					
13+31.00	11,817,577	7,044,004	346.4	15.0	361.4	48					
13+79.00	11,817,552	7,044,045	346.7	15.0	361.7	48					
14+27.00	11,817,526	7,044,085	346.9	15.0	361.9	48					
14+75.00	11,817,501	7,044,126	347.3	15.0	362.3	48					
15+23.00	11,817,476	7,044,167	347.6	15.0	362.6	36					
15+59.00	11,817,454	7,044,195	347.7	15.0	362.7	37					
15+96.00	11,817,431	7,044,224	347.8	15.0	362.8	48					
16+44.00	11,817,401	7,044,261	348.0	15.0	363.0	25					
16+69.00	11,817,388	7,044,282	347.1	15.0	362.1	48					
17+17.00	11,817,357	7,044,318	347.3	15.0	362.3	48					
17+65.00	11,817,325	7,044,354	344.6	15.0	359.6	0					
			Wall E2	(Design Stationin	g 247+00 to 254+00)						
10+00.00	11,818,162.00	7,043,013.50	338.26	15.0	353.3	24					
10+24.00	11,818,140.00	7,043,022.00	340.89	15.0	355.9	44					
10+68.00	11,818,118.00	7,043,060.00	341.32	15.0	356.3	44					
11+12.00	11,818,097.00	7,043,098.50	341.66	15.0	356.7	44					
11+56.00	11,818,075.00	7,043,137.00	341.86	15.0	356.9	43					
11+99.00	11,818,054.00	7,043,175.00	341.99	15.0	357.0	44					
12+43.00	11,818,032.00	7,043,213.50	342.12	15.0	357.1	44					
12+87.00	11,818,011.00	7,043,252.00	342.25	15.0	357.3	48					
13+35.00	11,817,989.00	7,043,294.50	342.31	15.0	357.3	48					
13+83.00	11,817,966.00	7,043,337.00	342.37	15.0	357.4	48					
14+31.00	11,817,944.00	7,043,379.50	342.45	15.0	357.5	44					
14+75.00	11,817,923.00	7,043,418.00	343.95	15.0	359.0	44					
15+19.00	11,817,901.00		346.8	15.0	361.8	44					
15+63.00	11,817,880.00		347.19	15.0	362.2	44					
16+07.00	11,817,858.00		345.7	15.0	360.7	44					
16+51.00	11,817,837.00		342.95	15.0	358.0	44					
16+95.00	11,817,815.00	7,043,610.00	341	15.0	356.0	0					

			Wall E3	(Design Stationin	g 254+25 to 269+25)	
10+00.00	11,818,201	7,042,918	340.0	15.0	355.0	24
10+24.00	11,818,213	7,042,897	337.5	15.0	352.5	24
10+48.00	11,818,225	7,042,877	336.8	15.0	351.8	24
10+72.00	11,818,238	7,042,856	336.2	15.0	351.2	24
10+96.00	11,818,250	7,042,835	335.6	15.0	350.6	24
11+20.00	11,818,262	7,042,815	335.0	15.0	350.0	24
11+44.00	11,818,275	7,042,794	334.3	15.0	349.3	24
11+68.00	11,818,288	7,042,774	333.5	15.0	348.5	24
11+92.00	11,818,300	7,042,754	332.7	15.0	347.7	24
12+16.00	11,818,313	7,042,734	331.9	15.0	346.9	24
12+40.00	11,818,326	7,042,713	331.1	15.0	346.1	24
12+64.00	11,818,340	7,042,693	330.3	15.0	345.3	24
12+88.00	11,818,353	7,042,673	329.4	15.0	344.4	24
13+12.00	11,818,365	7,042,653	328.5	15.0	343.5	24
13+36.00	11,818,377	7,042,632	327.6	15.0	342.6	24
13+60.00	11,818,389	7,042,612	326.6	15.0	341.6	24
13+84.00	11,818,402	7,042,591	325.5	15.0	340.5	24
14+08.00	11,818,415	7,042,571	324.5	15.0	339.5	24
14+32.00	11,818,428	7,042,551	323.5	15.0	338.5	24
14+56.00	11,818,442	7,042,531	322.5	15.0	337.5	24
14+80.00	11,818,456	7,042,512	321.6	15.0	336.6	24
15+04.00	11,818,471	7,042,493	320.7	15.0	335.7	24
15+28.00	11,818,485	7,042,474	319.8	15.0	334.8	24
15+52.00	11,818,500	7,042,455	319.0	15.0	334.0	24
15+76.00	11,818,514	7,042,436	318.2	15.0	333.2	24
16+00.00	11,818,529	7,042,417	317.5	15.0	332.5	24
16+24.00	11,818,544	7,042,398	316.8	15.0	331.8	24
16+48.00	11,818,559	7,042,379	316.1	15.0	331.1	24
16+72.00	11,818,575	7,042,361	315.5	15.0	330.5	24
16+96.00	11,818,590	7,042,342	315.0	15.0	330.0	24
17+20.00	11,818,605	7,042,324	314.4	15.0	329.4	24
17+44.00	11,818,621	7,042,306	314.0	15.0	329.0	24
17+68.00	11,818,636	7,042,387	313.5	15.0	328.5	24
17+92.00	11,818,652	7,042,269	313.1	15.0	328.1	24
18+16.00	11,818,668	7,042,251	312.8	15.0	327.8	24
18+40.00	11,818,684	7,042,233	312.5	15.0	327.5	24
18+64.00	11,818,700	7,042,216	312.2	15.0	327.2	24
18+88.00	11,818,716	7,042,198	312.0	15.0	327.0	24
19+12.00	11,818,733	7,042,180	311.9	15.0	326.9	24
19+36.00	11,818,749	7,042,163	311.7	15.0	326.7	24
19+60.00	11,818,766	7,042,145	311.6	15.0	326.6	24
19+84.00	11,818,782	7,042,128	311.6	15.0	326.6	24
20+08.00	11,818,799	7,042,111	311.6	15.0	326.6	24
20+32.00	11,818,816	7,042,094	311.6	15.0	326.6	24
20+56.00	11,818,833	7,042,077	311.7	15.0	326.7	24
20+80.00	11,818,850	7,042,060	311.9	15.0	326.9	24
21+04.00	11,818,867	7,042,043	312.0	15.0	327.0	24
21+28.00	11,818,884	7,042,026	312.3	15.0	327.3	24
21+52.00	11,818,902	7,042,010	312.5	15.0	327.5	24
21+76.00	11,818,919	7,042,010	312.8	15.0	327.8	24
22+00.00	11,818,937	7,041,977	313.2	15.0	328.2	23
22+23.00	11,818,954	7,041,961	313.6	15.0	328.6	24
22+47.00	11,818,972	7,041,944	314.0	15.0	329.0	24
22+71.00	11,818,990	7,041,928	314.5	15.0	329.5	24
22+95.00	11,819,008	7,041,912	315.0	15.0	330.0	24
23+19.00	11,819,026	7,041,897	315.6	15.0	330.6	24
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23+43.00	11,819,044	7,041,881	316.2	15.0	331.2	24
23+67.00	11,819,062	7,041,865	316.8	15.0	331.8	24
23+91.00	11,819,080	7,041,850	317.3	15.0	332.3	18
24+09.00	11,819,094	7,041,838	317.8	15.0	332.9	39
24+48.00	11,819,119	7,041,869	316.8	15.0	331.8	0

	Wall E4 (Design Stationing 270+75 to 277+50)									
10+00.00	11,819,787	7,041,473	346.4	15.0	361.4	49				
10+49.00	11,819,740	7,041,458	349.2	15.0	364.2	50				
10+99.00	11,819,692	7,041,444	340.7	15.0	355.7	40				
11+39.00	11,819,658	7,041,465	340.2	15.0	355.2	40				
11+79.00	11,819,624	7,041,487	339.6	15.0	354.6	40				
12+19.00	11,819,590	7,041,508	338.9	15.0	353.9	41				
12+60.00	11,819,555	7,041,530	338.1	15.0	353.1	24				
12+84.00	11,819,537	7,041,546	339.1	15.0	354.1	24				
13+08.00	11,819,517	7,041,558	338.5	15.0	353.5	24				
13+32.00	11,819,495	7,041,567	336.4	15.0	351.4	45				
13+77.00	11,819,457	7,041,591	335.2	15.0	350.2	44				
14+21.00	11,819,420	7,041,614	334.0	15.0	349.0	45				
14+66.00	11,819,382	7,041,638	332.3	15.0	347.3	44				
15+10.00	11,819,345	7,041,661	330.4	15.0	345.4	45				
15+55.00	11,819,307	7,041,685	328.4	15.0	343.4	29				
15+84.00	11,819,283	7,041,701	327.0	15.0	342.0	30				
16+14.00	11,819,258	7,041,717	325.5	15.0	340.5	30				
16+44.00	11,819,233	7,041,734	324.1	15.0	339.1	13				
16+57.00	11,819,222	7,041,741	323.5	15.0	338.5	37				
16+94.00	11,819,244	7,041,771	324.7	15.0	339.7	0				
			Wall D2	(Design Stationin	g 230+50 to 237+50)					
10+00.00	11,816,740	7,044,878	358.4	15.0	373.1	37				
10+37.00	11,816,770	7,044,857	360.0	15.0	373.2	43				
10+80.00	11,816,805	7,044,832	360.7	15.0	375.0	42				
11+22.00	11,816,839	7,044,807	361.7	15.0	375.7	43				
11+65.00	11,816,874	7,044,782	361.1	15.0	376.7	35				
12+00.00	11,816,902	7,044,761	360.2	15.0	376.1	35				
12+35.00	11,816,930	7,044,741	359.6	15.0	375.2	35				
12+70.00	11,816,957	7,044,719	358.7	15.0	374.6	35				
13+05.00	11,816,985	7,044,698	357.7	15.0	373.7	35				
13+40.00	11,817,012	7,044,676	355.6	15.0	372.7	35				
13+75.00	11,817,039	7,044,654	353.0	15.0	370.6	34				
14+09.00	11,817,065	7,044,631	350.7	15.0	368.0	35				
14+44.00	11,817,092	7,044,609	347.3	15.0	365.7	35				
14+79.00	11,817,118	7,044,585	344.3	15.0	362.3	35				
15+14.00	11,817,144	7,044,562	342.7	15.0	359.3	34				
15+48.00	11,817,169	7,044,538	342.7	15.0	357.7	35				
15+83.00	11,817,195	7,044,514	342.9	15.0	357.7	34				
16+17.00	11,817,219	7,044,490	342.9	15.0	357.9	35				
16+52.00	11,817,244	7,044,465	342.8	15.0	357.9	35				
16+87.00	11,817,268	7,044,440	342.8	15.0	357.8	35				
17+22.00	11,817,293	7,044,415	343.5	15.0	357.8	0				

CNE F - Walls F1, F1B, F1C, and F2 Acoustical Profile (Projection NAD_1983_StatePlane_Virginia_North US Feet)										
Station	X Coordinate	Y Coordinate	Base Elevation	Wall Height	Top Elevation	Segment Length				
	Wall F1 (Design Stationing 301+25 to 302+75)									
10+00.00	11,821,965	7,040,503	321.5	13.0	334.5	48				
10+48.00	11,822,010	7,040,487	321.1	13.0	334.1	48				
10+96.00	11,822,055	7,040,471	320.7	13.0	333.7	49				
11+45.00	11,822,101	7,040,455	320.3	13.0	333.3	0				
			Wall F1E	(Design Stationin	ng 303+00 to 303+25)					
10+00.00			320.08	13.0	333.1	24				
10+24.00	11,822,146.00	7,040,439.00	319.92	13.0	332.9	0				
				(Design Stationir	ng 303+50 to 304+75)					
10+00.00	11,822,166	7,040,432	319.8	13.0	332.8	37				
10+37.00	11,822,201	7,040,419	319.6	13.0	332.6	38				
10+75.00	11,822,237	7,040,407	319.7	13.0	332.7	38				
11+13.00	11,822,273	7,040,394	319.8	13.0	332.8	0				
			Wall F2	(Design Stationin	g 304+75 to 313+00)					
10+00.00	11,822,292	7,040,388	319.8	12.0	331.8	35				
10+35.00	11,822,325	7,040,376	319.9	12.0	331.9	36				
10+71.00	11,822,359	7,040,364	320.0	12.0	332.0	35				
11+06.00	11,822,392	7,040,352	320.1	12.0	332.1	49				
11+55.00	11,822,438	7,040,335	320.2	12.0	332.2	49				
12+04.00	11,822,484	7,040,318	319.9	12.0	331.9	50				
12+54.00	11,822,530	7,040,299	319.5	12.0	331.5	49				
13+03.00	11,822,575	7,040,280	318.9	12.0	330.9	49				
13+52.00	11,822,620	7,040,260	318.3	12.0	330.3	50				
14+02.00	11,822,665	7,040,239	317.5	12.0	329.5	49				
14+51.00	11,822,709	7,040,218	316.6	12.0	328.6	49				
15+00.00	11,822,753	7,040,196	315.7	12.0	327.7	50				
15+50.00	11,822,797	7,040,173	314.8	12.0	326.8	49				
15+99.00	11,822,840	7,040,149	313.9	12.0	325.9	49				
16+48.00	11,822,883	7,040,124	313.0	12.0	325.0	46				
16+94.00	11,822,928	7,040,115	307.8	12.0	319.8	46				
17+40.00	11,822,973	7,040,106	306.8	12.0	318.8	46				
17+86.00	11,823,018	7,040,097	306.5	12.0	318.5	30				
18+16.00	11,823,047	7,040,103	307.3	12.0	319.3	30				
18+46.00	11,823,076	7,040,109	309.5	12.0	321.5	0				

Station   X Coordinate   Evalution   Segment Length   Segment Length	CNE F - Wall F3 Acoustical Profile (Projection NAD_1983_StatePlane_Virginia_North US Feet)											
10+00.00	Station	X Coordinate			Wall Height	Top Elevation	Segment Length					
10+43.00		Wall F3 (Design Stationing 313+50 to 339+00)										
10+86.00	10+00.00	11,823,097	7,039,998	306.2	16.0	322.2	43					
11+29.00	10+43.00	11,823,132	7,039,973	308.3	16.0	324.3	43					
11+73.00 11,823,238 7,039,898 309.7 16.0 325.7 48 12+16.00 11,823,217 7,039,873 309.7 16.0 325.7 48 13+12.00 11,823,314 7,039,843 307.1 16.0 323.1 48 13+12.00 11,823,348 7,039,813 304.7 16.0 320.7 48 13+60.00 11,823,348 7,039,782 302.5 16.0 318.5 24 13+84.00 11,823,404 7,039,768 302.8 16.0 318.5 24 14+74.00 11,823,404 7,039,768 302.8 16.0 318.8 45 14+29.00 11,823,441 7,039,742 301.3 16.0 317.3 45 14+74.00 11,823,475 7,039,769 298.7 16.0 314.7 45 15+19.00 11,823,515 7,039,660 298.3 16.0 314.7 45 15+63.00 11,823,515 7,039,664 296.2 16.0 314.2 45 16+63.00 11,823,565 7,039,661 294.5 16.0 310.5 44 16+97.00 11,823,625 7,039,612 294.5 16.0 310.5 44 16+97.00 11,823,625 7,039,560 293.0 16.0 309.7 45 16+97.00 11,823,661 7,039,560 293.0 16.0 309.7 45 16+98.00 11,823,625 7,039,560 293.0 16.0 309.7 45 18+14.00 11,823,732 7,039,564 294.0 16.0 310.0 36 17+78.00 11,823,732 7,039,549 294.0 16.0 310.0 36 18+14.00 11,823,865 7,039,549 294.0 16.0 310.0 36 18+14.00 11,823,865 7,039,549 294.0 16.0 325.1 48 19+10.0 11,823,865 7,039,426 304.8 16.0 325.1 48 19+10.0 11,823,865 7,039,426 304.8 16.0 325.1 48 19+10.0 11,823,986 7,039,385 286.9 16.0 325.1 48 19+10.0 11,823,986 7,039,9350 286.9 16.0 325.1 48 19+10.0 11,823,986 7,039,9350 286.9 16.0 325.1 48 19+10.0 11,823,986 7,039,9350 286.9 16.0 320.8 49 19+20-00.0 11,823,986 7,039,9350 286.9 16.0 302.9 50 11,824,027 7,039,935 286.9 16.0 302.9 50 11,824,027 7,039,134 286.0 16.0 302.9 50 11,824,027 7,039,135 286.0 16.0 302.9 50 11,824,189 7,039,112 286.0 16.0 296.9 49 22+53.00 11,824,148 7,039,142 280.9 16.0 296.9 49 23+02.00 11,824,249 7,039,154 280.9 16.0 296.9 49 23+02.00 11,824,249 7,039,935 285.5 16.0 299.5 50 24+51.00 11,824,247 7,039,935 285.5 16.0 299.5 50 24+51.00 11,824,247 7,039,935 285.5 16.0 299.5 50 24+51.00 11,824,351 7,039,936 286.9 16.0 296.9 49 25+00.00 11,824,319 7,039,942 286.0 16.0 296.9 49 25+00.00 11,824,319 7,039,942 286.0 16.0 296.9 49 25+00.00 11,824,319 7,039,942 285.5 16.0 286.0 50 26+09.00 11,824,519 7,038,867 265.3 16.0 281.5 50 29+96.00 11,824,515 7,038,867 26	10+86.00	11,823,167	7,039,948	309.0	16.0	325.0	43					
12+16.00 11,823,273 7,039,873 309.7 16.0 325.7 48 12+64.00 11,823,310 7,039,843 307.1 16.0 323.1 48 13+60.00 11,823,348 7,039,813 304.7 16.0 320.7 48 13+60.01 11,823,348 7,039,813 304.7 16.0 320.7 48 13+60.01 11,823,348 7,039,782 302.5 16.0 318.5 24 13+84.00 11,823,444 7,039,742 301.3 16.0 318.8 45 14+74.00 11,823,478 7,039,716 298.7 16.0 314.7 45 15+19.00 11,823,515 7,039,690 298.3 16.0 314.3 44 15+63.00 11,823,515 7,039,664 296.2 16.0 314.3 44 16+63.00 11,823,588 7,039,688 295.3 16.0 311.3 45 16+63.00 11,823,561 7,039,566 293.7 16.0 310.5 44 16+97.00 11,823,661 7,039,586 293.7 16.0 310.5 44 17+42.00 11,823,661 7,039,586 293.7 16.0 309.0 36 17+78.00 11,823,732 7,039,549 294.0 16.0 310.0 366 17+78.00 11,823,785 7,039,549 294.0 16.0 310.0 36 18+14.00 11,823,786 7,039,537 299.8 16.0 315.8 49 18+63.00 11,823,865 7,039,482 310.1 16.0 325.1 49 19+11.00 11,823,885 7,039,482 310.1 16.0 325.1 49 19+10.00 11,823,885 7,039,482 310.1 16.0 325.1 49 19+10.00 11,823,885 7,039,482 310.1 16.0 325.1 49 19+60.00 11,823,986 7,039,537 299.8 16.0 325.1 49 19+60.00 11,823,986 7,039,359 295.5 16.0 325.1 48 19+60.00 11,823,986 7,039,359 295.5 16.0 325.1 48 19+60.00 11,823,986 7,039,358 285.2 16.0 300.2 55.0 49 19+60.00 11,823,986 7,039,358 285.2 16.0 300.2 55.0 50 11,824,007 7,039,357 286.0 16.0 300.0 49 12+54.00 11,823,986 7,039,358 285.2 16.0 300.2 49 12+54.00 11,824,007 7,039,357 286.0 16.0 300.0 49 12+54.00 11,824,007 7,039,358 285.2 16.0 300.3 49 12+54.00 11,824,007 7,039,358 285.2 16.0 300.3 49 12+54.00 11,824,189 7,039,269 284.3 16.0 295.5 50 13+54.00 11,824,210 7,039,183 281.7 16.0 295.5 50 13+54.00 11,824,310 7,039,183 281.7 16.0 295.5 50 13+54.00 11,824,327 7,039,183 281.7 16.0 295.5 50 13+54.00 11,824,327 7,039,183 281.7 16.0 295.5 50 13+54.00 11,824,327 7,039,183 281.7 16.0 295.5 50 13+54.00 11,824,327 7,039,900 277.5 16.0 295.5 50 14+54.00 11,824,335 7,039,886 26.0 16.0 295.0 50 14+54.00 11,824,335 7,039,886 26.0 16.0 295.0 50 14+54.00 11,824,335 7,039,886 26.0 16.0 295.0 50 14+54.00 11,824,335 7,038,896 26.0 16.0 280.0 4	11+29.00	11,823,202	7,039,923	307.8	16.0	323.8	44					
12+64.00         11,823,310         7,039,843         307.1         16.0         323.1         48           13+12.00         11,823,348         7,039,781         304.7         16.0         320.7         48           13+60.00         11,823,348         7,039,782         302.5         16.0         318.5         24           13+84.00         11,823,441         7,039,782         302.8         16.0         318.8         45           14+29.00         11,823,441         7,039,742         301.3         16.0         317.3         45           14+74.00         11,823,441         7,039,769         298.7         16.0         314.7         45           15+19.00         11,823,551         7,039,660         298.3         16.0         314.3         44           15+63.00         11,823,551         7,039,664         296.2         16.0         311.3         45           16+97.00         11,823,565         7,039,566         293.7         16.0         310.5         44           16+97.00         11,823,667         7,039,586         293.7         16.0         300.0         36           17-78.00         11,823,668         7,039,586         293.7         16.0         300.5	11+73.00	11,823,238	7,039,898	309.7	16.0	325.7	43					
13+12.00	12+16.00	11,823,273	7,039,873	309.7	16.0	325.7	48					
13+60.00       11,823,385       7,039,782       302.5       16.0       318.5       24         13+8-00       11,823,404       7,039,782       302.8       16.0       318.8       45         14+29.00       11,823,441       7,039,742       301.3       16.0       317.3       45         14+74.00       11,823,471       7,039,660       298.3       16.0       314.7       45         15+19.00       11,823,551       7,039,660       298.3       16.0       314.3       44         15+63.00       11,823,551       7,039,661       296.2       16.0       312.2       45         16+68.00       11,823,551       7,039,681       295.3       16.0       311.3       45         16+97.00       11,823,661       7,039,681       295.3       16.0       310.5       44         16+97.00       11,823,661       7,039,586       293.7       16.0       309.7       45         17-42.00       11,823,698       7,039,540       294.0       16.0       310.0       36         18+14.00       11,823,967       7,039,537       298.8       16.0       315.8       49         19+10.00       11,823,964       7,039,537       299.8       16.0 </td <td>12+64.00</td> <td>11,823,310</td> <td>7,039,843</td> <td>307.1</td> <td>16.0</td> <td>323.1</td> <td>48</td>	12+64.00	11,823,310	7,039,843	307.1	16.0	323.1	48					
13+84.00       11,823,404       7,039,768       302.8       16.0       318.8       45         14+29.00       11,823,441       7,039,742       301.3       16.0       317.3       45         14+74.00       11,823,481       7,039,769       298.7       16.0       314.7       45         15+19.00       11,823,551       7,039,669       298.3       16.0       314.3       44         15+63.00       11,823,585       7,039,664       296.2       16.0       312.2       45         16+93.00       11,823,682       7,039,661       294.5       16.0       310.5       44         16+97.00       11,823,682       7,039,612       294.5       16.0       300.5       44         16+97.00       11,823,661       7,039,586       293.7       16.0       309.7       45         17+8.00       11,823,766       7,039,537       299.8       16.0       310.0       36         18+14.00       11,823,885       7,039,549       294.0       16.0       315.8       49         19+10.00       11,823,885       7,039,549       299.8       16.0       323.9       48         19+10.00       11,823,885       7,039,482       310.1       16.0 </td <td>13+12.00</td> <td>11,823,348</td> <td>7,039,813</td> <td>304.7</td> <td>16.0</td> <td>320.7</td> <td>48</td>	13+12.00	11,823,348	7,039,813	304.7	16.0	320.7	48					
14+29.00       11,823,441       7,039,742       301.3       16.0       317.3       45         14+74.00       11,823,478       7,039,791       298.7       16.0       314.7       45         15+19.00       11,823,515       7,039,690       298.3       16.0       314.3       44         15+63.00       11,823,551       7,039,664       296.2       16.0       312.2       45         16+08.00       11,823,565       7,039,638       295.3       16.0       311.3       45         16+97.00       11,823,665       7,039,586       293.7       16.0       309.7       45         17+42.00       11,823,668       7,039,580       293.0       16.0       309.0       36         17+78.00       11,823,732       7,039,549       294.0       16.0       310.0       36         18+14.00       11,823,866       7,039,539       299.8       16.0       310.0       36         18+63.00       11,823,866       7,039,549       294.0       16.0       310.0       36         18+14.00       11,823,867       7,039,539       307.9       16.0       323.9       48         19+11.00       11,823,865       7,039,534       390.1       16.0<	13+60.00	11,823,385	7,039,782	302.5	16.0	318.5	24					
14+74.00       11,823,478       7,039,716       298.7       16.0       314.7       45         15+19.00       11,823,515       7,039,664       296.2       16.0       314.3       44         15+63.00       11,823,551       7,039,664       296.2       16.0       312.2       45         16+63.00       11,823,685       7,039,612       294.5       16.0       310.5       44         16+97.00       11,823,661       7,039,586       293.7       16.0       309.7       45         17+42.00       11,823,662       7,039,586       293.7       16.0       309.0       36         17+78.00       11,823,762       7,039,589       293.0       16.0       310.0       36         18+14.00       11,823,766       7,039,589       294.0       16.0       310.0       36         18+63.00       11,823,866       7,039,593       299.8       16.0       315.8       49         19+60.00       11,823,864       7,039,482       310.1       16.0       326.1       49         19+60.00       11,823,865       7,039,484       309.1       16.0       320.3       49         20+57.00       11,824,964       7,039,328       286.9       16.0<	13+84.00	11,823,404	7,039,768	302.8	16.0	318.8	45					
15+19.00 11,823,515 7,039,690 298.3 16.0 314.3 44 15+63.00 11,823,551 7,039,664 296.2 16.0 312.2 45 16+08.00 11,823,588 7,039,638 295.3 16.0 311.3 45 16+53.00 11,823,652 7,039,612 294.5 16.0 310.5 44 16+97.00 11,823,661 7,039,586 293.7 16.0 309.7 45 17+42.00 11,823,698 7,039,560 293.0 16.0 309.7 36 17+742.00 11,823,698 7,039,560 293.0 16.0 309.0 36 18+14.00 11,823,766 7,039,537 299.8 16.0 310.0 36 18+14.00 11,823,766 7,039,537 299.8 16.0 315.8 49 18+63.00 11,823,806 7,039,509 307.9 16.0 323.9 48 19+11.00 11,823,885 7,039,454 309.1 16.0 326.1 49 19+60.00 11,823,885 7,039,454 309.1 16.0 325.1 48 20+08.00 11,823,924 7,039,426 304.8 16.0 325.1 48 20+57.00 11,823,964 7,039,385 296.5 16.0 312.5 47 11+64.00 11,823,964 7,039,388 296.5 16.0 312.5 47 11+64.00 11,824,027 7,039,327 286.0 16.0 302.9 50 21+54.00 11,824,067 7,039,298 285.2 16.0 302.0 49 22+53.00 11,824,067 7,039,298 285.2 16.0 300.3 49 23+02.00 11,824,148 7,039,241 283.5 16.0 299.5 50 23+52.00 11,824,148 7,039,241 283.5 16.0 299.5 50 23+52.00 11,824,148 7,039,241 283.5 16.0 299.5 50 23+52.00 11,824,148 7,039,241 283.5 16.0 299.5 50 24+51.00 11,824,297 7,039,132 286.0 16.0 300.3 49 23+02.00 11,824,189 7,039,212 282.6 16.0 298.6 49 24+01.00 11,824,297 7,039,132 281.7 16.0 297.7 50 24+51.00 11,824,297 7,039,138 281.7 16.0 297.7 50 24+51.00 11,824,297 7,039,138 281.7 16.0 296.9 49 25+00.00 11,824,310 7,039,126 280.0 16.0 296.0 50 25+50.00 11,824,310 7,039,109 279.2 16.0 296.9 49 25+00.00 11,824,310 7,039,109 279.2 16.0 296.9 49 25+00.00 11,824,321 7,039,009 279.5 16.0 299.5 50 26+99.00 11,824,432 7,039,040 277.5 16.0 293.5 50 26+99.00 11,824,437 7,039,901 275.0 16.0 281.5 49 28+47.00 11,824,547 7,038,982 271.8 16.0 281.5 49 28+47.00 11,824,551 7,038,962 271.8 16.0 281.5 49 28+47.00 11,824,551 7,038,962 271.8 16.0 281.5 49 28+47.00 11,824,551 7,038,962 271.8 16.0 281.5 49 28+47.00 11,824,551 7,038,982 271.8 16.0 281.5 49 28+47.00 11,824,554 7,038,982 271.8 16.0 281.5 49 28+47.00 11,824,554 7,038,982 271.8 16.0 281.5 49 28+47.00 11,824,554 7,038,982 271.8 16.0 281.	14+29.00	11,823,441	7,039,742	301.3	16.0	317.3	45					
15+63.00 11,823,551 7,039,664 296.2 16.0 312.2 45 16+08.00 11,823,588 7,039,638 295.3 16.0 311.3 45 16+53.00 11,823,652 7,039,612 294.5 16.0 310.5 44 16+97.00 11,823,661 7,039,586 293.7 16.0 309.7 45 17+42.00 11,823,668 7,039,560 293.0 16.0 309.0 36 17+78.00 11,823,732 7,039,549 294.0 16.0 310.0 36 18+14.00 11,823,766 7,039,537 299.8 16.0 310.0 36 18+14.00 11,823,865 7,039,549 294.0 16.0 310.0 36 18+14.00 11,823,865 7,039,549 294.0 16.0 323.9 48 18+63.00 11,823,865 7,039,482 310.1 16.0 325.1 49 19+10.00 11,823,845 7,039,484 309.1 16.0 326.1 49 19+60.00 11,823,885 7,039,454 309.1 16.0 325.1 48 19-10.01 11,823,964 7,039,398 296.5 16.0 320.8 49 20+57.00 11,823,964 7,039,356 286.9 16.0 312.5 47 21+04.00 11,824,067 7,039,398 285.2 16.0 302.9 50 21+54.00 11,824,077 7,039,272 286.0 16.0 302.0 49 22+03.00 11,824,077 7,039,269 284.3 16.0 300.3 49 23+02.00 11,824,108 7,039,269 284.3 16.0 300.3 49 23+02.00 11,824,148 7,039,241 283.5 16.0 299.5 50 22+53.00 11,824,148 7,039,241 283.5 16.0 299.5 50 23+52.00 11,824,148 7,039,212 282.6 16.0 299.5 50 23+52.00 11,824,148 7,039,212 282.6 16.0 299.5 50 24+51.00 11,824,270 7,039,183 281.7 16.0 299.7 50 24+51.00 11,824,270 7,039,154 280.9 16.0 299.5 50 24+51.00 11,824,270 7,039,154 280.9 16.0 299.7 50 24+51.00 11,824,270 7,039,154 280.9 16.0 299.7 50 24+51.00 11,824,270 7,039,154 280.9 16.0 299.5 50 25+53.00 11,824,4189 7,039,212 282.6 16.0 299.5 50 24+51.00 11,824,270 7,039,154 280.9 16.0 299.7 50 24+51.00 11,824,270 7,039,154 280.9 16.0 299.7 50 24+51.00 11,824,270 7,039,154 280.9 16.0 299.7 50 24+51.00 11,824,473 7,039,000 277.5 16.0 294.3 49 26+49.00 11,824,473 7,039,001 275.0 16.0 298.5 50 27+98.00 11,824,473 7,039,001 275.0 16.0 298.5 50 28+97.00 11,824,454 7,038,953 265.5 16.0 281.5 49 28+40.00 11,824,473 7,039,001 275.0 16.0 298.5 50 28+97.00 11,824,594 7,038,895 265.5 16.0 281.5 49 28+40.00 11,824,547 7,038,88 266.0 16.0 280.0 49 28+40.00 11,824,547 7,038,88 266.0 16.0 280.0 49 28+40.00 11,824,547 7,038,888 266.0 16.0 280.0 49	14+74.00	11,823,478	7,039,716	298.7	16.0	314.7	45					
16+08.00         11,823,588         7,039,638         295.3         16.0         311.3         45           16+53.00         11,823,625         7,039,586         293.7         16.0         310.5         44           16+97.00         11,823,661         7,039,586         293.7         16.0         309.7         45           17+78.00         11,823,732         7,039,549         294.0         16.0         310.0         36           18+14.00         11,823,766         7,039,577         299.8         16.0         315.8         49           18+63.00         11,823,806         7,039,509         307.9         16.0         323.9         48           19+11.00         11,823,885         7,039,454         309.1         16.0         326.1         49           19+60.00         11,823,885         7,039,454         309.1         16.0         320.8         49           20+57.00         11,823,964         7,039,398         296.5         16.0         312.5         47           21+64.00         11,823,964         7,039,398         286.9         16.0         302.9         50           21+54.00         11,824,027         7,039,327         286.0         16.0         302.0	15+19.00	11,823,515	7,039,690	298.3	16.0	314.3	44					
16+53.00       11,823,625       7,039,612       294.5       16.0       310.5       44         16+97.00       11,823,698       7,039,586       293.7       16.0       309.7       45         17+42.00       11,823,698       7,039,560       293.0       16.0       309.0       36         17+78.00       11,823,766       7,039,549       294.0       16.0       310.0       36         18+14.00       11,823,766       7,039,537       299.8       16.0       315.8       49         18+63.00       11,823,805       7,039,599       307.9       16.0       323.9       48         19+11.00       11,823,845       7,039,482       310.1       16.0       326.1       49         19+60.00       11,823,885       7,039,426       304.8       16.0       325.1       48         20+08.00       11,823,984       7,039,398       296.5       16.0       312.5       47         21+04.00       11,823,986       7,039,398       296.5       16.0       302.9       50         21+54.00       11,824,067       7,039,298       285.2       16.0       302.0       49         22+03.00       11,824,188       7,039,298       285.2       16.0<	15+63.00	11,823,551	7,039,664	296.2	16.0	312.2	45					
16+97.00       11,823,661       7,039,586       293.7       16.0       309.7       45         17+42.00       11,823,698       7,039,560       293.0       16.0       309.0       36         17+78.00       11,823,732       7,039,549       294.0       16.0       310.0       36         18+14.00       11,823,866       7,039,537       299.8       16.0       315.8       49         18+63.00       11,823,865       7,039,482       310.1       16.0       326.1       49         19+60.00       11,823,885       7,039,482       310.1       16.0       325.1       48         20+08.00       11,823,984       7,039,426       304.8       16.0       325.1       48         20+08.00       11,823,984       7,039,382       296.5       16.0       322.8       49         20+57.00       11,823,986       7,039,356       286.9       16.0       302.9       50         21+94.00       11,824,027       7,039,327       286.0       16.0       302.0       49         22+93.00       11,824,027       7,039,282       285.2       16.0       301.2       50         22+95.00       11,824,189       7,039,212       282.6       16.0<	16+08.00	11,823,588	7,039,638	295.3	16.0	311.3	45					
17+42.00       11,823,698       7,039,560       293.0       16.0       309.0       36         17+78.00       11,823,732       7,039,549       294.0       16.0       310.0       36         18+14.00       11,823,766       7,039,537       299.8       16.0       315.8       49         18+63.00       11,823,806       7,039,509       307.9       16.0       323.9       48         19+11.00       11,823,845       7,039,482       310.1       16.0       326.1       49         19+60.00       11,823,885       7,039,426       304.8       16.0       325.1       48         20+08.00       11,823,994       7,039,426       304.8       16.0       320.8       49         20+57.00       11,823,996       7,039,398       296.5       16.0       302.8       49         21+54.00       11,824,027       7,039,327       286.0       16.0       302.0       49         22+53.00       11,824,067       7,039,298       285.2       16.0       301.2       50         22+53.00       11,824,108       7,039,269       284.3       16.0       300.3       49         23+52.00       11,824,189       7,039,212       282.6       16.0<	16+53.00	11,823,625	7,039,612	294.5	16.0	310.5	44					
17+78.00       11,823,732       7,039,549       294.0       16.0       310.0       36         18+14.00       11,823,766       7,039,537       299.8       16.0       315.8       49         18+63.00       11,823,806       7,039,599       307.9       16.0       323.9       48         19+11.00       11,823,845       7,039,482       310.1       16.0       326.1       49         19+60.00       11,823,985       7,039,484       309.1       16.0       325.1       48         20+08.00       11,823,924       7,039,426       304.8       16.0       320.8       49         20+57.00       11,823,964       7,039,398       296.5       16.0       302.9       50         21+54.00       11,824,027       7,039,327       286.0       16.0       302.9       50         21+54.00       11,824,067       7,039,228       285.2       16.0       301.2       50         22+53.00       11,824,108       7,039,269       284.3       16.0       300.3       49         23+52.00       11,824,148       7,039,212       282.6       16.0       299.5       50         23+50.00       11,824,219       7,039,134       280.9       16.0<	16+97.00	11,823,661	7,039,586	293.7	16.0	309.7	45					
18+14.00       11,823,766       7,039,537       299.8       16.0       315.8       49         18+63.00       11,823,806       7,039,509       307.9       16.0       323.9       48         19+11.00       11,823,845       7,039,482       310.1       16.0       326.1       49         19+60.00       11,823,885       7,039,454       309.1       16.0       325.1       48         20+08.00       11,823,964       7,039,426       304.8       16.0       320.8       49         20+57.00       11,823,986       7,039,398       296.5       16.0       312.5       47         21+04.00       11,824,067       7,039,356       286.9       16.0       302.9       50         21+54.00       11,824,067       7,039,298       285.2       16.0       301.2       50         22+53.00       11,824,108       7,039,298       284.3       16.0       300.3       49         23+52.00       11,824,148       7,039,241       283.5       16.0       299.5       50         23+52.00       11,824,219       7,039,183       281.7       16.0       297.7       50         24+51.00       11,824,310       7,039,154       280.9       16.0<	17+42.00	11,823,698	7,039,560	293.0	16.0	309.0	36					
18+63.00         11,823,806         7,039,509         307.9         16.0         323.9         48           19+11.00         11,823,845         7,039,482         310.1         16.0         326.1         49           19+60.00         11,823,885         7,039,454         309.1         16.0         325.1         48           20+08.00         11,823,924         7,039,426         304.8         16.0         320.8         49           20+57.00         11,823,986         7,039,398         296.5         16.0         312.5         47           21+04.00         11,823,986         7,039,356         286.9         16.0         302.9         50           21+54.00         11,824,027         7,039,327         286.0         16.0         302.0         49           22+03.00         11,824,108         7,039,298         285.2         16.0         301.2         50           22+53.00         11,824,108         7,039,298         284.3         16.0         300.3         49           23+02.00         11,824,108         7,039,241         283.5         16.0         299.5         50           23+52.00         11,824,189         7,039,3183         281.7         16.0         297.7	17+78.00	11,823,732	7,039,549	294.0	16.0	310.0	36					
19+11.00       11,823,845       7,039,482       310.1       16.0       326.1       49         19+60.00       11,823,885       7,039,454       309.1       16.0       325.1       48         20+08.00       11,823,924       7,039,426       304.8       16.0       320.8       49         20+57.00       11,823,964       7,039,398       296.5       16.0       312.5       47         21+04.00       11,823,986       7,039,327       286.0       16.0       302.9       50         21+54.00       11,824,027       7,039,232       286.0       16.0       302.0       49         22+30.00       11,824,108       7,039,298       285.2       16.0       301.2       50         22+53.00       11,824,108       7,039,294       284.3       16.0       300.3       49         23+52.00       11,824,189       7,039,212       282.6       16.0       299.5       50         23+52.00       11,824,229       7,039,183       281.7       16.0       297.7       50         24+51.00       11,824,310       7,039,154       280.9       16.0       296.9       49         25+50.00       11,824,331       7,039,097       279.2       16.0<	18+14.00	11,823,766	7,039,537	299.8	16.0	315.8	49					
19+60.00       11,823,885       7,039,454       309.1       16.0       325.1       48         20+08.00       11,823,924       7,039,426       304.8       16.0       320.8       49         20+57.00       11,823,964       7,039,398       296.5       16.0       312.5       47         21+04.00       11,824,027       7,039,327       286.0       16.0       302.9       50         21+54.00       11,824,067       7,039,298       285.2       16.0       301.2       50         22+03.00       11,824,067       7,039,298       285.2       16.0       300.3       49         22+53.00       11,824,108       7,039,269       284.3       16.0       300.3       49         23+02.00       11,824,148       7,039,241       283.5       16.0       299.5       50         23+52.00       11,824,189       7,039,212       282.6       16.0       298.6       49         24+01.00       11,824,279       7,039,183       281.7       16.0       297.7       50         24+50.00       11,824,310       7,039,126       280.9       16.0       296.9       49         25+00.00       11,824,351       7,039,046       278.3       16.0<	18+63.00	11,823,806	7,039,509	307.9	16.0	323.9	48					
20+08.00       11,823,924       7,039,426       304.8       16.0       320.8       49         20+57.00       11,823,964       7,039,398       296.5       16.0       312.5       47         21+04.00       11,823,986       7,039,356       286.9       16.0       302.9       50         21+54.00       11,824,067       7,039,237       286.0       16.0       302.0       49         22+53.00       11,824,108       7,039,298       285.2       16.0       301.2       50         22+53.00       11,824,108       7,039,296       284.3       16.0       300.3       49         23+02.00       11,824,148       7,039,241       283.5       16.0       299.5       50         23+52.00       11,824,189       7,039,212       282.6       16.0       298.6       49         24+51.00       11,824,229       7,039,183       281.7       16.0       297.7       50         24+51.00       11,824,310       7,039,154       280.9       16.0       296.9       49         25+00.00       11,824,351       7,039,068       278.3       16.0       295.2       50         26+00.00       11,824,332       7,039,068       278.3       16.0<	19+11.00	11,823,845	7,039,482	310.1	16.0	326.1	49					
20+57.00       11,823,964       7,039,398       296.5       16.0       312.5       47         21+04.00       11,823,986       7,039,356       286.9       16.0       302.9       50         21+54.00       11,824,027       7,039,327       286.0       16.0       302.0       49         22+03.00       11,824,067       7,039,298       285.2       16.0       301.2       50         22+53.00       11,824,108       7,039,269       284.3       16.0       300.3       49         23+02.00       11,824,148       7,039,241       283.5       16.0       299.5       50         23+52.00       11,824,189       7,039,212       282.6       16.0       298.6       49         24+01.00       11,824,229       7,039,183       281.7       16.0       297.7       50         24+51.00       11,824,270       7,039,154       280.9       16.0       296.9       49         25+00.00       11,824,310       7,039,097       279.2       16.0       295.2       50         26+00.00       11,824,332       7,039,068       278.3       16.0       293.5       50         26+99.00       11,824,433       7,039,040       277.5       16.0<	19+60.00	11,823,885	7,039,454	309.1	16.0	325.1	48					
21+04.00       11,823,986       7,039,356       286.9       16.0       302.9       50         21+54.00       11,824,027       7,039,327       286.0       16.0       302.0       49         22+03.00       11,824,067       7,039,298       285.2       16.0       301.2       50         22+53.00       11,824,108       7,039,269       284.3       16.0       300.3       49         23+02.00       11,824,148       7,039,241       283.5       16.0       299.5       50         23+52.00       11,824,189       7,039,212       282.6       16.0       298.6       49         24+01.00       11,824,229       7,039,183       281.7       16.0       297.7       50         24+51.00       11,824,270       7,039,154       280.9       16.0       296.9       49         25+00.00       11,824,310       7,039,126       280.0       16.0       296.0       50         25+50.00       11,824,351       7,039,097       279.2       16.0       295.2       50         26+00.00       11,824,332       7,039,040       277.5       16.0       293.5       50         26+99.00       11,824,433       7,039,040       277.5       16.0<	20+08.00	11,823,924	7,039,426	304.8	16.0	320.8	49					
21+54.00       11,824,027       7,039,327       286.0       16.0       302.0       49         22+03.00       11,824,067       7,039,298       285.2       16.0       301.2       50         22+53.00       11,824,108       7,039,269       284.3       16.0       300.3       49         23+02.00       11,824,148       7,039,241       283.5       16.0       299.5       50         23+52.00       11,824,189       7,039,212       282.6       16.0       298.6       49         24+01.00       11,824,229       7,039,183       281.7       16.0       297.7       50         24+51.00       11,824,270       7,039,154       280.9       16.0       296.9       49         25+00.00       11,824,310       7,039,126       280.0       16.0       296.0       50         25+50.00       11,824,351       7,039,097       279.2       16.0       295.2       50         26+00.00       11,824,432       7,039,068       278.3       16.0       294.3       49         26+49.00       11,824,432       7,039,040       277.5       16.0       293.5       50         26+99.00       11,824,513       7,038,982       271.8       16.0<	20+57.00	11,823,964	7,039,398	296.5	16.0	312.5	47					
21+54.00       11,824,027       7,039,327       286.0       16.0       302.0       49         22+03.00       11,824,067       7,039,298       285.2       16.0       301.2       50         22+53.00       11,824,108       7,039,269       284.3       16.0       300.3       49         23+02.00       11,824,148       7,039,241       283.5       16.0       299.5       50         23+52.00       11,824,189       7,039,212       282.6       16.0       298.6       49         24+01.00       11,824,229       7,039,183       281.7       16.0       297.7       50         24+51.00       11,824,270       7,039,154       280.9       16.0       296.9       49         25+00.00       11,824,310       7,039,126       280.0       16.0       296.0       50         25+50.00       11,824,351       7,039,097       279.2       16.0       295.2       50         26+00.00       11,824,432       7,039,068       278.3       16.0       294.3       49         26+49.00       11,824,432       7,039,040       277.5       16.0       293.5       50         26+99.00       11,824,513       7,038,982       271.8       16.0<				286.9	16.0	302.9	50					
22+03.00       11,824,067       7,039,298       285.2       16.0       301.2       50         22+53.00       11,824,108       7,039,269       284.3       16.0       300.3       49         23+02.00       11,824,148       7,039,241       283.5       16.0       299.5       50         23+52.00       11,824,189       7,039,212       282.6       16.0       298.6       49         24+01.00       11,824,229       7,039,183       281.7       16.0       297.7       50         24+51.00       11,824,270       7,039,154       280.9       16.0       296.9       49         25+00.00       11,824,310       7,039,126       280.0       16.0       296.0       50         25+50.00       11,824,351       7,039,097       279.2       16.0       295.2       50         26+00.00       11,824,392       7,039,068       278.3       16.0       294.3       49         26+49.00       11,824,432       7,039,040       277.5       16.0       293.5       50         26+99.00       11,824,473       7,039,011       275.0       16.0       291.0       49         27+98.00       11,824,513       7,038,982       271.8       16.0<	21+54.00		7,039,327	286.0	16.0	302.0	49					
22+53.00       11,824,108       7,039,269       284.3       16.0       300.3       49         23+02.00       11,824,148       7,039,241       283.5       16.0       299.5       50         23+52.00       11,824,189       7,039,212       282.6       16.0       298.6       49         24+01.00       11,824,229       7,039,183       281.7       16.0       297.7       50         24+51.00       11,824,270       7,039,154       280.9       16.0       296.9       49         25+00.00       11,824,310       7,039,126       280.0       16.0       296.0       50         25+50.00       11,824,351       7,039,097       279.2       16.0       295.2       50         26+00.00       11,824,351       7,039,068       278.3       16.0       294.3       49         26+49.00       11,824,432       7,039,040       277.5       16.0       293.5       50         26+99.00       11,824,473       7,039,011       275.0       16.0       291.0       49         27+48.00       11,824,513       7,038,982       271.8       16.0       287.8       50         28+90.0       11,824,594       7,038,953       265.5       16.0 </td <td>22+03.00</td> <td></td> <td></td> <td>285.2</td> <td>16.0</td> <td>301.2</td> <td>50</td>	22+03.00			285.2	16.0	301.2	50					
23+02.00       11,824,148       7,039,241       283.5       16.0       299.5       50         23+52.00       11,824,189       7,039,212       282.6       16.0       298.6       49         24+01.00       11,824,229       7,039,183       281.7       16.0       297.7       50         24+51.00       11,824,270       7,039,154       280.9       16.0       296.9       49         25+00.00       11,824,310       7,039,126       280.0       16.0       296.0       50         25+50.00       11,824,351       7,039,097       279.2       16.0       295.2       50         26+00.00       11,824,392       7,039,068       278.3       16.0       294.3       49         26+49.00       11,824,432       7,039,040       277.5       16.0       293.5       50         26+99.00       11,824,473       7,039,011       275.0       16.0       291.0       49         27+48.00       11,824,513       7,038,982       271.8       16.0       287.8       50         27+98.00       11,824,594       7,038,953       265.5       16.0       281.5       49         28+97.00       11,824,635       7,038,867       265.3       16.0<				284.3	16.0	300.3	49					
23+52.00       11,824,189       7,039,212       282.6       16.0       298.6       49         24+01.00       11,824,229       7,039,183       281.7       16.0       297.7       50         24+51.00       11,824,270       7,039,154       280.9       16.0       296.9       49         25+00.00       11,824,310       7,039,126       280.0       16.0       296.0       50         25+50.00       11,824,351       7,039,097       279.2       16.0       295.2       50         26+00.00       11,824,392       7,039,068       278.3       16.0       294.3       49         26+49.00       11,824,432       7,039,040       277.5       16.0       293.5       50         26+99.00       11,824,473       7,039,011       275.0       16.0       291.0       49         27+48.00       11,824,513       7,038,982       271.8       16.0       287.8       50         27+98.00       11,824,554       7,038,953       265.5       16.0       279.2       50         28+97.00       11,824,635       7,038,896       264.0       16.0       280.0       49         29+46.00       11,824,675       7,038,887       265.3       16.0<				283.5	16.0	299.5	50					
24+01.00       11,824,229       7,039,183       281.7       16.0       297.7       50         24+51.00       11,824,270       7,039,154       280.9       16.0       296.9       49         25+00.00       11,824,310       7,039,126       280.0       16.0       296.0       50         25+50.00       11,824,351       7,039,097       279.2       16.0       295.2       50         26+00.00       11,824,392       7,039,068       278.3       16.0       294.3       49         26+49.00       11,824,432       7,039,040       277.5       16.0       293.5       50         26+99.00       11,824,473       7,039,011       275.0       16.0       291.0       49         27+48.00       11,824,513       7,038,982       271.8       16.0       287.8       50         27+98.00       11,824,554       7,038,953       265.5       16.0       281.5       49         28+97.00       11,824,635       7,038,986       264.0       16.0       280.0       49         29+46.00       11,824,675       7,038,867       265.3       16.0       281.3       50         29+96.00       11,824,716       7,038,838       269.0       16.0<					16.0							
24+51.00       11,824,270       7,039,154       280.9       16.0       296.9       49         25+00.00       11,824,310       7,039,126       280.0       16.0       296.0       50         25+50.00       11,824,351       7,039,097       279.2       16.0       295.2       50         26+00.00       11,824,392       7,039,068       278.3       16.0       294.3       49         26+49.00       11,824,432       7,039,040       277.5       16.0       293.5       50         26+99.00       11,824,473       7,039,011       275.0       16.0       291.0       49         27+48.00       11,824,513       7,038,982       271.8       16.0       287.8       50         27+98.00       11,824,554       7,038,953       265.5       16.0       281.5       49         28+97.00       11,824,635       7,038,986       264.0       16.0       280.0       49         29+46.00       11,824,675       7,038,887       265.3       16.0       281.3       50         29+96.00       11,824,716       7,038,838       269.0       16.0       285.0       49		11,824,229			16.0							
25+00.00       11,824,310       7,039,126       280.0       16.0       296.0       50         25+50.00       11,824,351       7,039,097       279.2       16.0       295.2       50         26+00.00       11,824,392       7,039,068       278.3       16.0       294.3       49         26+49.00       11,824,432       7,039,040       277.5       16.0       293.5       50         26+99.00       11,824,473       7,039,011       275.0       16.0       291.0       49         27+48.00       11,824,513       7,038,982       271.8       16.0       287.8       50         27+98.00       11,824,554       7,038,953       265.5       16.0       281.5       49         28+47.00       11,824,634       7,038,925       263.2       16.0       279.2       50         28+97.00       11,824,635       7,038,866       264.0       16.0       280.0       49         29+46.00       11,824,675       7,038,867       265.3       16.0       285.0       49         29+96.00       11,824,716       7,038,838       269.0       16.0       285.0       49	24+51.00			280.9	16.0	296.9	49					
25+50.00       11,824,351       7,039,097       279.2       16.0       295.2       50         26+00.00       11,824,392       7,039,068       278.3       16.0       294.3       49         26+49.00       11,824,432       7,039,040       277.5       16.0       293.5       50         26+99.00       11,824,473       7,039,011       275.0       16.0       291.0       49         27+48.00       11,824,513       7,038,982       271.8       16.0       287.8       50         27+98.00       11,824,554       7,038,953       265.5       16.0       281.5       49         28+47.00       11,824,594       7,038,953       263.2       16.0       279.2       50         28+97.00       11,824,635       7,038,896       264.0       16.0       280.0       49         29+46.00       11,824,675       7,038,867       265.3       16.0       281.3       50         29+96.00       11,824,716       7,038,838       269.0       16.0       285.0       49	25+00.00			280.0		296.0						
26+00.00       11,824,392       7,039,068       278.3       16.0       294.3       49         26+49.00       11,824,432       7,039,040       277.5       16.0       293.5       50         26+99.00       11,824,473       7,039,011       275.0       16.0       291.0       49         27+48.00       11,824,513       7,038,982       271.8       16.0       287.8       50         27+98.00       11,824,554       7,038,953       265.5       16.0       281.5       49         28+47.00       11,824,594       7,038,925       263.2       16.0       279.2       50         28+97.00       11,824,635       7,038,896       264.0       16.0       280.0       49         29+46.00       11,824,675       7,038,887       265.3       16.0       281.3       50         29+96.00       11,824,716       7,038,838       269.0       16.0       285.0       49												
26+49.00       11,824,432       7,039,040       277.5       16.0       293.5       50         26+99.00       11,824,473       7,039,011       275.0       16.0       291.0       49         27+48.00       11,824,513       7,038,982       271.8       16.0       287.8       50         27+98.00       11,824,554       7,038,953       265.5       16.0       281.5       49         28+47.00       11,824,594       7,038,925       263.2       16.0       279.2       50         28+97.00       11,824,635       7,038,896       264.0       16.0       280.0       49         29+46.00       11,824,675       7,038,867       265.3       16.0       281.3       50         29+96.00       11,824,716       7,038,838       269.0       16.0       285.0       49												
26+99.00       11,824,473       7,039,011       275.0       16.0       291.0       49         27+48.00       11,824,513       7,038,982       271.8       16.0       287.8       50         27+98.00       11,824,554       7,038,953       265.5       16.0       281.5       49         28+47.00       11,824,594       7,038,925       263.2       16.0       279.2       50         28+97.00       11,824,635       7,038,896       264.0       16.0       280.0       49         29+46.00       11,824,675       7,038,867       265.3       16.0       281.3       50         29+96.00       11,824,716       7,038,838       269.0       16.0       285.0       49												
27+48.00       11,824,513       7,038,982       271.8       16.0       287.8       50         27+98.00       11,824,554       7,038,953       265.5       16.0       281.5       49         28+47.00       11,824,594       7,038,925       263.2       16.0       279.2       50         28+97.00       11,824,635       7,038,896       264.0       16.0       280.0       49         29+46.00       11,824,675       7,038,867       265.3       16.0       281.3       50         29+96.00       11,824,716       7,038,838       269.0       16.0       285.0       49												
27+98.00     11,824,554     7,038,953     265.5     16.0     281.5     49       28+47.00     11,824,594     7,038,925     263.2     16.0     279.2     50       28+97.00     11,824,635     7,038,896     264.0     16.0     280.0     49       29+46.00     11,824,675     7,038,867     265.3     16.0     281.3     50       29+96.00     11,824,716     7,038,838     269.0     16.0     285.0     49												
28+47.00     11,824,594     7,038,925     263.2     16.0     279.2     50       28+97.00     11,824,635     7,038,896     264.0     16.0     280.0     49       29+46.00     11,824,675     7,038,867     265.3     16.0     281.3     50       29+96.00     11,824,716     7,038,838     269.0     16.0     285.0     49												
28+97.00     11,824,635     7,038,896     264.0     16.0     280.0     49       29+46.00     11,824,675     7,038,867     265.3     16.0     281.3     50       29+96.00     11,824,716     7,038,838     269.0     16.0     285.0     49												
29+46.00     11,824,675     7,038,867     265.3     16.0     281.3     50       29+96.00     11,824,716     7,038,838     269.0     16.0     285.0     49												
29+96.00 11,824,716 7,038,838 269.0 16.0 285.0 49												
	30+45.00	11,824,756	7,038,810	270.6	16.0	286.6	50					

30+95.00	11,824,797	7,038,781	269.8	16.0	285.8	49
31+44.00	11,824,837	7,038,752	268.9	16.0	284.9	50
31+94.00	11,824,878	7,038,724	268.1	16.0	284.1	49
32+43.00	11,824,918	7,038,695	268.6	16.0	284.6	50
32+93.00	11,824,959	7,038,666	267.7	16.0	283.7	49
33+42.00	11,824,999	7,038,637	269.7	16.0	285.7	50
33+92.00	11,825,040	7,038,609	268.7	16.0	284.7	49
34+41.00	11,825,080	7,038,580	268.0	16.0	284.0	50
34+91.00	11,825,121	7,038,551	265.9	16.0	281.9	49
35+40.00	11,825,161	7,038,522	260.1	16.0	276.1	0

CNE G - Walls G1_G6 Acoustical Profile (Projection NAD_1983_StatePlane_Virginia_North US Feet)									
Station	X Coordinate	Y Coordinate	Base Elevation	Wall Height	Top Elevation	Segment Length			
Wall G1 (Design Stationing 1280+75 to 1312+50)									
	11,819,955.00		345.39	18.0	363.4	24			
	11,819,979.00		345.15	18.0	363.2	24			
	11,820,002.00		344.96	18.0	363.0	25			
	11,820,024.00		344.83	18.0	362.8	24			
	11,820,045.00		344.7	18.0	362.7	24			
	11,820,066.00		344.55	18.0	362.6	25			
	11,820,088.00		344.37	18.0	362.4	24			
	11,820,109.00		344.17	18.0	362.2	24			
11+94.00	11,820,131.00	7,040,995.00	343.95	18.0	362.0	23			
12+17.00	11,820,152.00	7,040,985.00	343.7	18.0	361.7	24			
12+41.00	11,820,174.00	7,040,974.50	343.43	18.0	361.4	24			
12+65.00	11,820,196.00	7,040,965.00	343.13	18.0	361.1	24			
12+89.00	11,820,218.00	7,040,955.00	342.82	18.0	360.8	24			
13+13.00	11,820,240.00	7,040,945.50	342.51	18.0	360.5	24			
13+37.00	11,820,262.00	7,040,936.00	342.2	18.0	360.2	24			
13+61.00	11,820,284.00	7,040,927.00	341.89	18.0	359.9	24			
13+85.00	11,820,306.00	7,040,918.00	341.58	18.0	359.6	25			
14+10.00	11,820,329.00	7,040,909.50	341.15	18.0	359.2	24			
14+34.00	11,820,351.00	7,040,900.50	340.68	18.0	358.7	24			
14+58.00	11,820,374.00	7,040,892.50	340.21	18.0	358.2	24			
14+82.00	11,820,396.00	7,040,884.00	339.74	18.0	357.7	49			
15+31.00	11,820,442.00	7,040,868.00	338.79	18.0	356.8	48			
15+79.00	11,820,487.00	7,040,852.00	337.83	18.0	355.8	48			
16+27.00	11,820,532.00	7,040,836.00	336.88	18.0	354.9	48			
16+75.00	11,820,577.00	7,040,820.00	335.92	18.0	353.9	49			
17+24.00	11,820,623.00	7,040,804.00	334.96	18.0	353.0	48			
17+72.00	11,820,668.00	7,040,788.00	334.04	18.0	352.0	48			
18+20.00	11,820,713.00	7,040,772.00	333.46	18.0	351.5	48			
18+68.00	11,820,758.00	7,040,756.00	332.95	18.0	351.0	49			
19+17.00	11,820,804.00	7,040,740.00	332.49	18.0	350.5	48			
19+65.00	11,820,849.00	7,040,724.00	332.04	18.0	350.0	48			
20+13.00	11,820,894.00	7,040,708.00	331.6	18.0	349.6	48			
	11,820,939.00		331.16	18.0	349.2	49			
	11,820,985.00		330.71	18.0	348.7	48			
	11,821,030.00		330.27	18.0	348.3	48			
	11,821,075.00		329.83	18.0	347.8	48			
	11,821,120.00		329.38	18.0	347.4	24			
	11,821,143.00		329.16	18.0	347.2	24			
	11,821,166.00		328.94	18.0	346.9	23			
	11,821,188.00		328.72	18.0	346.7	24			
	11,821,211.00		328.5	18.0	346.5	24			
	11,821,234.00		328.28	18.0	346.3	23			
	11,821,256.00		328.06	18.0	346.1	24			
	11,821,279.00		327.83	18.0	345.8	24			
	11,821,302.00		327.61	18.0	345.6	24			
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					2.2.	
	11,821,325.00		327.39	18.0	345.4	23
	11,821,347.00		327.17	18.0	345.2	24
	11,821,370.00		326.95	18.0	345.0	24
	11,821,393.00		326.73	18.0	344.7	24
25+63.00	11,821,416.00	7,040,527.50	326.51	18.0	344.5	24
25+87.00	11,821,439.00	7,040,520.00	326.29	18.0	344.3	23
26+10.00	11,821,461.00	7,040,512.50	326.07	18.0	344.1	24
26+34.00	11,821,484.00	7,040,505.50	325.85	18.0	343.9	24
26+58.00	11,821,507.00	7,040,498.00	325.63	18.0	343.6	24
26+82.00	11,821,530.00	7,040,491.00	325.4	18.0	343.4	24
27+06.00	11,821,553.00	7,040,483.50	325.18	18.0	343.2	24
27+30.00	11,821,576.00	7,040,476.50	324.96	18.0	343.0	24
27+54.00	11,821,599.00	7,040,469.50	324.74	18.0	342.7	24
27+78.00	11,821,622.00	7,040,462.50	324.52	18.0	342.5	24
28+02.00	11,821,645.00	7,040,455.50	324.3	18.0	342.3	24
28+26.00	11,821,668.00	7,040,448.50	324.08	18.0	342.1	24
28+50.00	11,821,691.00	7,040,441.50	323.85	18.0	341.9	23
28+73.00			323.63	18.0	341.6	24
28+97.00			323.41	18.0	341.4	24
29+21.00			323.18	18.0	341.2	24
29+45.00			322.96	18.0	341.0	24
29+69.00			322.74	18.0	340.7	24
$\overline{}$	11,821,828.00		322.52	18.0	340.5	24
	11,821,851.00		322.29	18.0	340.3	24
	11,821,874.00		322.07	18.0	340.1	23
	11,821,896.00		321.85	18.0	339.9	24
	11,821,919.00		321.62	18.0	339.6	24
	11,821,942.00		321.02	18.0	339.4	24
	11,821,965.00		321.18	18.0	339.2	23
	11,821,987.00		320.96	18.0	339.0	24
	11,822,010.00		320.73	18.0	338.7	24
	11,822,033.00		320.73	18.0	338.5	23
	11,822,055.00		320.29	18.0	338.3	25
			319.86	18.0	337.9	23
32+33.00	11,822,078.00 11,822,097.00		319.86		335.3	25
				18.0	333.8	
33+03.00			315.83	18.0		49
	11,822,143.00		316.39	18.0	334.4	49
	11,822,190.00		319.44	18.0	337.4	24
	11,822,213.00		318.48	18.0	336.5	24
	11,822,237.00		318.64	18.0	336.6	24
	11,822,260.00		318.86	18.0	336.9	48
	11,822,305.00		317.59	18.0	335.6	48
	11,822,350.00		316.83	18.0	334.8	24
	11,822,373.00		316.44	18.0	334.4	25
	11,822,396.00		316.05	18.0	334.1	24
	11,822,418.00		315.63	18.0	333.6	24
	11,822,440.00		315.28	18.0	333.3	25
	11,822,463.00		314.97	18.0	333.0	24
	11,822,485.00		314.64	18.0	332.6	24
	11,822,507.00		314.29	18.0	332.3	24
	11,822,529.00		313.91	18.0	331.9	24
	11,822,551.00		313.51	18.0	331.5	24
38+11.00	11,822,573.00	7,040,127.50	313.08	18.0	331.1	23
38+34.00	11,822,594.00	7,040,117.50	312.65	18.0	330.7	24
38+58.00	11,822,616.00	7,040,107.50	312.23	18.0	330.2	24
38+82.00	11,822,638.00	7,040,097.00	311.81	18.0	329.8	24
39+06.00	11,822,656.00	7,040,081.00	311.5	18.0	329.5	24

39+30.00	11,822,677.00	7,040,070.00	311.07	18.0	329.1	24
39+54.00	11,822,698.00	7,040,059.00	310.64	18.0	328.6	25
39+79.00	11,822,720.00	7,040,048.00	310.21	18.0	328.2	24
40+03.00	11,822,741.00	7,040,036.50	309.78	18.0	327.8	24
40+27.00	11,822,762.00	7,040,025.00	309.36	18.0	327.4	24
40+51.00	11,822,783.00	7,040,013.00	308.93	18.0	326.9	23
40+74.00	11,822,803.00	7,040,001.00	308.5	18.0	326.5	24
40+98.00	11,822,824.00	7,039,989.00	308.07	18.0	326.1	24
41+22.00	11,822,845.00	7,039,976.50	307.64	18.0	325.6	24
41+46.00	11,822,865.00	7,039,964.00	307.21	18.0	325.2	24
41+70.00	11,822,886.00	7,039,951.50	306.78	18.0	324.8	24
41+94.00	11,822,906.00	7,039,938.50	306.57	18.0	324.6	0

			Wall G2 (	Design Stationing	1313+75 to 1318+75)	
10+00.00	11,823,012.00	7,039,873.00	301.8	18.0	319.8	18
10+42.00	11,823,046.00	7,039,848.50	304.82	18.0	322.8	18
10+85.00	11,823,081.00	7,039,824.00	304.27	18.0	322.3	18
11+27.00	11,823,115.00	7,039,800.00	303.6	18.0	321.6	18
11+69.00	11,823,149.00	7,039,775.50	302.93	18.0	320.9	18
12+17.00	11,823,186.00	7,039,745.50	302.13	18.0	320.1	18
12+66.00	11,823,224.00	7,039,715.00	301.31	18.0	319.3	18
12+89.00	11,823,241.00	7,039,699.00	300.94	18.0	318.9	18
13+13.00	11,823,259.00	7,039,682.50	300.2	18.0	318.2	25
13+36.00	11,823,252.00	7,039,658.50	300.57	18.0	317.9	25
13+84.00	11,823,245.00	7,039,634.50	300.93	18.0	317.1	25
14+23.00	11,823,238.00	7,039,610.50	301.3	18.0	316.5	25
	11,823,231.00		301.66	18.0	315.8	25
	11,823,223.00		302.03	18.0	312.4	25
	11,823,216.00		302.4	18.0	309.1	15
15+86.00	11,823,212.00	7,039,524.00	302.62	18.0	305.7	0
			Wall G3 (	Design Stationing	1320+25 to 1323+25)	
	11,823,548.00		293.06	18.0	311.1	45
10+45.00	11,823,585.00	7,039,465.50	291.71	18.0	309.7	44
10+89.00	11,823,621.00	7,039,439.50	290.35	18.0	308.4	45
	11,823,658.00		289.06	18.0	307.1	44
11+78.00	11,823,694.00		287.9	18.0	305.9	44
12+22.00	11,823,730.00	7,039,362.50	286.87	18.0	304.9	45
	11,823,767.00		285.97	18.0	304.0	44
13+11.00	11,823,803.00	7,039,310.50	283.68	18.0	301.7	0
					1323+75 to 1328+75)	
	11,823,840.00		282.7	18.0	300.7	48
	11,823,885.00		283.85	18.0	301.9	48
	11,823,924.00		283.02	18.0	301.0	48
	11,823,963.00		282.2	18.0	300.2	48
11+92.00			281.37	18.0	299.4	48
12+40.00	, ,		280.54	18.0	298.5	49
12+89.00			279.72	18.0	297.7	48
	11,824,120.00		278.89	18.0	296.9	48
	11,824,159.00		278.07	18.0	296.1	48
	11,824,198.00		277.24	18.0	295.2	48
14+81.00	11,824,237.00	7,039,017.50	270.37	18.0	288.4	0

			Wall G5 (	Design Stationing	1329+00 to 1334+00)	
10+00.00	11,824,658.00	7,038,699.00	260.03	18.0	278.0	48
10+48.00	11,824,619.00	7,038,727.00	267.37	18.0	285.4	49
10+97.00	11,824,579.00	7,038,754.50	268.2	18.0	286.2	48
11+45.00	11,824,540.00	7,038,782.50	269.02	18.0	287.0	48
11+93.00	11,824,501.00	7,038,810.00	269.85	18.0	287.9	48
12+41.00	11,824,462.00	7,038,838.00	270.61	18.0	288.6	48
12+89.00	11,824,424.00	7,038,868.00	271.54	18.0	289.5	48
13+37.00	11,824,387.00	7,038,898.00	272.42	18.0	290.4	48
13+85.00	11,824,350.00	7,038,928.00	273.3	18.0	291.3	48
14+33.00	11,824,312.00	7,038,958.00	274.21	18.0	292.2	24
14+57.00	11,824,293.00	7,038,972.50	274.64	18.0	292.6	48
15+05.00	11,824,254.00	7,039,000.00	268.77	18.0	286.8	0
			Wall G6 (	Design Stationing	1334+50 to 1338+75)	
10+00.00	11,824,723.00	7,038,654.00	261.77	18.0	279.8	48
10+48.00	11,824,769.00	7,038,640.50	264.46	18.0	282.5	48
10+96.00	11,824,808.00	7,038,613.00	264.39	18.0	282.4	48
11+44.00	11,824,847.00	7,038,585.00	263.56	18.0	281.6	48
11+92.00	11,824,886.00	7,038,557.50	262.67	18.0	280.7	48
12+40.00	11,824,925.00	7,038,529.50	261.65	18.0	279.7	48
12+88.00	11,824,964.00	7,038,502.00	260.52	18.0	278.5	49
13+37.00	11,825,004.00	7,038,474.00	259.27	18.0	277.3	48
13+85.00	11,825,043.00	7,038,446.50	254.79	18.0	272.8	0

		Υ	Base			
tation	X Coordinate	Coordinate	Elevation	Wall Height	Top Elevation	Segment Length
			Wall G10	(Design Stationir	ng 1372+00 to 1374+75)	
0+00.00	11,828,006	7,036,882	215.4	17.0	232.4	38
0+38.00	11,828,040	7,036,865	216.9	17.0	233.9	37
0+75.00	11,828,073	7,036,848	218.4	17.0	235.4	38
1+13.00	11,828,107	7,036,831	219.8	17.0	236.8	37
1+50.00	11,828,140	7,036,814	221.2	17.0	238.2	40
1+90.00	11,828,177	7,036,798	223.0	17.0	240.0	40
2+30.00	11,828,214	7,036,783	224.6	17.0	241.6	40
2+70.00	11,828,251	7,036,767	223.8	17.0	240.8	0
			Wall G10	B (Design Stationi	ng 1375+50 to 1376+75)	
0+00.00	11,828,315	7,036,742	229.9	17.0	261.9	23
0+23.00	11,828,338	7,036,739	230.3	17.0	262.7	25
.0+48.00	11,828,361	7,036,731	231.2	17.0	265.4	45
.0+93.00	11,828,402	7,036,713	242.0	17.0	266.0	45
1+38.00	11,828,443	7,036,696	244.4	17.0	266.4	18
1+56.00	11,828,450	7,036,679	244.0	17.0	267.0	0
	, ,	, ,	Wall G11	(Design Stationir	ng 1377+75 to 1384+75)	
0+00.00	11,828,479	7,036,668	244.9	17.0	261.9	15
0+15.00	11,828,493	7,036,674	245.7	17.0	262.7	25
0+40.00	11,828,516	7,036,664	248.4	17.0	265.4	23
0+63.00	11,828,537	7,036,654	249.0	17.0	266.0	24
.0+87.00	11,828,559	7,036,643	249.4	17.0	266.4	24
1+11.00	11,828,580	7,036,632	250.0	17.0	267.0	25
1+36.00	11,828,602	7,036,621	250.3	17.0	267.3	24
1+60.00	11,828,623	7,036,610	251.4	17.0	268.4	24
1+84.00	11,828,644	7,036,598	251.5	17.0	268.5	23
2+07.00	11,828,664	7,036,586	252.5	17.0	269.5	24
2+31.00	11,828,685	7,036,573	253.6	17.0	270.6	24
2+55.00	11,828,705	7,036,561	255.7	17.0	272.7	24
2+79.00	11,828,725	7,036,548	256.6	17.0	273.6	24
3+03.00		7,036,534	257.3	17.0	274.3	24
	11,828,765	7,036,521	258.9	17.0	275.9	24
3+51.00		7,036,507	260.3	17.0	277.3	24
3+75.00	11,828,804	7,036,493	261.5	17.0	278.5	24
3+99.00	11,828,823	7,036,478	262.1	17.0	279.1	24
4+23.00	11,828,842	7,036,464	263.0	17.0	280.0	25
4+48.00	11,828,861	7,036,448	263.6	17.0	280.6	23
4+71.00	11,828,879	7,036,433	264.1	18.0	282.1	25
4+96.00	11,828,898	7,036,418	264.2	18.0	282.2	24
5+20.00	11,828,916	7,036,402	265.2	18.0	283.2	23
5+43.00	11,828,933	7,036,386	266.1	18.0	284.1	42
5+85.00	11,828,964	7,036,357	268.7	18.0	286.7	42
6+27.00	11,828,904	7,036,337	270.3	18.0	288.3	42
6+69.00	11,829,026	7,036,329	270.3	18.0	290.1	41
7+10.00	11,829,020	7,036,301	269.8	18.0	287.8	0
, . 10.00	11,023,037	1,030,213			ng 1384+75 to 1396+00)	

10+00.00	11,829,086	7,036,247	265.4	18.0	283.4	50
10+50.00	11,829,123	7,036,213	275.2	18.0	293.2	50
11+00.00	11,829,160	7,036,179	275.9	18.0	293.9	50
11+50.00	11,829,197	7,036,146	276.9	18.0	294.9	50
12+00.00	11,829,234	7,036,112	277.4	18.0	295.4	50
12+50.00	11,829,271	7,036,079	278.1	18.0	296.1	49
12+99.00	11,829,307	7,036,045	278.2	18.0	296.2	50
13+49.00	11,829,344	7,036,012	277.4	18.0	295.4	50
13+99.00	11,829,381	7,035,978	276.4	18.0	294.4	50
14+49.00	11,829,418	7,035,945	274.6	18.0	292.6	50
14+99.00	11,829,455	7,035,911	275.0	18.0	293.0	50
15+49.00	11,829,492	7,035,878	275.2	18.0	293.2	50
15+99.00	11,829,529	7,035,844	274.9	17.0	291.9	50
16+49.00	11,829,566	7,035,810	273.6	17.0	290.6	23
16+72.00	11,829,583	7,035,794	271.9	17.0	288.9	48
17+20.00	11,829,617	7,035,760	271.6	17.0	288.6	48
17+68.00	11,829,650	7,035,725	271.9	17.0	288.9	48
18+16.00	11,829,684	7,035,691	271.4	17.0	288.4	47
18+63.00	11,829,719	7,035,659	269.8	17.0	286.8	48
19+11.00	11,829,755	7,035,626	268.2	17.0	285.2	47
19+58.00	11,829,790	7,035,594	265.7	17.0	282.7	48
20+06.00	11,829,826	7,035,562	260.3	17.0	277.3	48
20+54.00	11,829,861	7,035,529	259.2	17.0	276.2	48
21+02.00	11,829,897	7,035,497	256.9	17.0	273.9	0
			Wall G13	(Design Stationii	ng 1396+75 to 1400+75)	
10+00.00	11,829,959	7,035,439	255.3	17.0	272.3	23
10+23.00	11,829,976	7,035,423	254.3	17.0	271.3	33
10+56.00	11,830,004	7,035,405	257.0	17.0	274.0	33
10+89.00	11,830,032	7,035,387	256.6	17.0	273.6	50
11+39.00	11,830,067	7,035,351	256.4	17.0	273.4	50
11+89.00	11,830,102	7,035,315	256.4	17.0	273.4	50
12+39.00	11,830,137	7,035,280	256.6	16.0	272.6	24
12+63.00	11,830,151	7,035,261	256.1	16.0	272.1	24
12+87.00	11,830,169	7,035,245	256.4	15.0	271.4	24
13+11.00	11,830,189	7,035,232	257.2	14.0	271.2	36
13+47.00	11,830,216	7,035,207	257.7	13.0	270.7	36
13+83.00	11,830,243	7,035,183	251.7	13.0	264.7	0
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CNE H - W	alls H2-H11 A	coustical Prof	ile (Project	ion NAD_1983_	StatePlane_Virginia_N	lorth US Feet)
Station	X Coordinate	Y Coordinate	Base Elevation	Wall Height	Top Elevation	Segment Length
			Wall H2	(Design Stationin	g 408+00 to 414+75)	
10+00.00	11,830,918.00	7,034,774.00	287.71	15.0	302.7	16
10+16.00	11,830,930.00	7,034,763.50	295.28	15.0	310.3	40
10+56.00	11,830,958.00	7,034,735.50	295.46	15.0	310.5	40
10+96.00	11,830,986.00	7,034,707.00	297.02	15.0	312.0	16
11+12.00	11,830,997.00	7,034,718.50	303.68	15.0	318.7	35
11+47.00	11,831,026.00	7,034,699.50	305.89	15.0	320.9	34
11+81.00	11,831,054.00	7,034,681.00	308.31	15.0	323.3	34
12+15.00	11,831,082.00	7,034,662.00	310.18	15.0	325.2	44
12+59.00	11,831,110.00	7,034,628.50	310.71	15.0	325.7	43
13+02.00	11,831,137.00	7,034,595.00	311.92	15.0	326.9	43
13+45.00	11,831,164.00	7,034,562.00	313.26	15.0	328.3	43
13+88.00	11,831,191.00	7,034,528.50	312.37	15.0	327.4	43
14+31.00	11,831,218.00	7,034,495.00	311.85	15.0	326.9	46
14+77.00	11,831,253.00	7,034,464.50	311.99	15.0	327.0	46
15+23.00	11,831,287.00	7,034,434.00	312.34	15.0	327.3	46
15+69.00	11,831,321.00	7,034,403.50	313.04	15.0	328.0	47
16+16.00	11,831,356.00	7,034,372.50	315.01	15.0	330.0	47
16+63.00	11,831,403.00	7,034,366.00	313.72	15.0	328.7	0

			Wall H3-4	l (Design Stationi	ng 415+75 to 430+00)	
10+00.00	11,831,489.00	7,034,271.50	315.32	16.0	331.3	23
10+23.00	11,831,502.00	7,034,252.00	319.19	16.0	335.2	36
10+59.00	11,831,529.00	7,034,228.00	320.38	16.0	336.4	36
10+95.00	11,831,555.00	7,034,203.50	321.54	16.0	337.5	24
11+19.00	11,831,576.00	7,034,191.00	321.63	16.0	337.6	24
11+43.00	11,831,594.00	7,034,175.00	322.14	16.0	338.1	24
11+67.00	11,831,609.00	7,034,156.00	323.74	16.0	339.7	36
12+03.00	11,831,636.00	7,034,132.00	324.77	16.0	340.8	36
12+39.00	11,831,663.00	7,034,108.50	325.76	16.0	341.8	45
12+84.00	11,831,695.00	7,034,077.50	326.96	16.0	343.0	24
13+08.00	11,831,715.00	7,034,064.00	326.93	16.0	342.9	24
13+32.00	11,831,732.00	7,034,047.50	327.54	16.0	343.5	24
13+56.00	11,831,746.00	7,034,028.00	328.76	16.0	344.8	29
13+85.00	11,831,767.00	7,034,008.00	329.44	16.0	345.4	24
14+09.00	11,831,785.00	7,033,992.00	330.01	16.0	346.0	47
14+56.00	11,831,821.00	7,033,961.50	331.07	16.0	347.1	48
15+04.00	11,831,858.00	7,033,930.50	331.98	16.0	348.0	48
15+52.00	11,831,895.00	7,033,899.50	332.8	16.0	348.8	40
15+92.00	11,831,926.00	7,033,874.50	333.44	16.0	349.4	40
16+32.00	11,831,957.00	7,033,849.00	334.01	16.0	350.0	40
16+72.00	11,831,988.00	7,033,823.50	333.21	16.0	349.2	47
17+19.00	11,832,025.00	7,033,794.00	333.59	16.0	349.6	47
17+66.00	11,832,062.00	7,033,764.50	335.56	16.0	351.6	47
18+13.00	11,832,099.00	7,033,735.00	335.96	16.0	352.0	48
18+61.00	11,832,136.00	7,033,705.00	336.29	16.0	352.3	47
19+08.00	11,832,173.00	7,033,675.50	336.54	16.0	352.5	0

19+08.00	11,832,210.00	7,033,646.00	336.72	16.0	352.7	47
19+55.00	11,832,247.00	7,033,616.50	336.84	16.0	352.8	48
20+03.00	11,832,284.00	7,033,586.50	328.73	16.0	344.7	47
20+50.00	11,832,321.00	7,033,557.00	336.81	16.0	352.8	47
20+97.00	11,832,358.00	7,033,527.50	336.71	16.0	352.7	48
21+45.00	11,832,395.00	7,033,497.50	336.6	16.0	352.6	43
21+88.00	11,832,428.00	7,033,470.50	336.5	16.0	352.5	43
22+31.00	11,832,462.00	7,033,443.50	336.4	16.0	352.4	43
22+74.00	11,832,495.00	7,033,416.00	336.31	16.0	352.3	43
23+17.00	11,832,529.00	7,033,389.00	336.22	16.0	352.2	44
23+61.00	11,832,563.00	7,033,361.50	336.19	16.0	352.2	0
			Wall H5	(Design Stationin	g 430+50 to 434+00)	
10+00.00	11,832,608.00	7,033,323.50	336.28	16.0	352.3	25
10+25.00	11,832,627.00	7,033,308.00	336.35	16.0	352.4	23
10+48.00	11,832,645.00	7,033,293.00	336.44	16.0	352.4	25
10+73.00	11,832,664.00	7,033,277.50	336.56	16.0	352.6	23
10+96.00	11,832,682.00	7,033,262.50	336.69	16.0	352.7	25
11+21.00	11,832,701.00	7,033,247.00	336.82	16.0	352.8	43
11+64.00	11,832,734.00	7,033,219.50	337.05	16.0	353.1	43
12+07.00	11,832,767.00	7,033,192.00	337.29	16.0	353.3	44
12+51.00	11,832,801.00	7,033,164.50	337.52	16.0	353.5	43
12+94.00	11,832,834.00	7,033,136.50	337.76	16.0	353.8	43
13+37.00	11,832,867.00	7,033,109.00	337.99	16.0	354.0	0
			Wall H6	(Design Stationin	g 434+50 to 436+25)	
10+00.00	11,832,914.00	7,033,070.50	338.32	16.0	354.3	42
10+47.00	11,832,946.00	7,033,043.50	338.55	16.0	354.6	42
10+95.00	11,832,979.00	7,033,017.00	338.77	16.0	354.8	42
11+42.00	11,833,011.00	7,032,990.00	339	16.0	355.0	42
11+90.00	11,833,043.00	7,032,963.00	339.23	16.0	355.2	0

			Wall H7	(Design Stationin	g 437+25 to 438+00)	
10+00.00	11,833,142.00	7,032,904.00	339.19	16.0	355.2	24
10+24.00	11,833,154.00	7,032,883.00	339.26	16.0	355.3	48
10+72.00	11,833,191.00	7,032,852.50	338.87	16.0	354.9	0
			Wall H8	(Design Stationin	g 438+50 to 440+00)	
10+00.00	11,833,213.00	7,032,834.00	338.28	16.0	354.3	25
10+25.00	11,833,232.00	7,032,818.50	340.22	16.0	356.2	24
10+49.00	11,833,251.00	7,032,803.50	340.35	16.0	356.4	36
10+85.00	11,833,279.00	7,032,781.00	340.54	16.0	356.5	36
11+21.00	11,833,307.00	7,032,758.50	340.74	16.0	356.7	36
11+57.00	11,833,335.00	7,032,736.00	339.05	16.0	355.1	0
			Wall H9	(Design Stationin	g 440+25 to 441+00)	
10+00.00	11,833,365.00	7,032,712.00	339.35	16.0	355.4	30
10+30.00	11,833,388.00	7,032,693.50	341.44	16.0	357.4	30
10+60.00	11,833,411.00	7,032,674.50	340.06	16.0	356.1	0
			Wall H10	(Design Stationin	ng 441+25 to 443+00)	
10+00.00	11,833,442.00	7,032,650.00	340.22	16.0	356.2	36
10+36.00	11,833,470.00	7,032,627.50	342.89	16.0	358.9	36
10+72.00	11,833,498.00	7,032,605.00	343.58	16.0	359.6	24
10+96.00	11,833,517.00	7,032,590.00	344.08	16.0	360.1	24
11+20.00	11,833,536.00	7,032,575.00	344.64	16.0	360.6	24
11+44.00	11,833,555.00	7,032,560.50	345.23	16.0	361.2	12
11+56.00	11,833,564.00	7,032,553.00	343.74	16.0	359.7	0

			Wall H11	(Design Stationin	ng 443+50 to 452+75)	
10+00.00	11,833,600.00	7,032,525.50	345.08	16.0	361.1	24
10+24.00	11,833,619.00	7,032,510.50	347.58	16.0	363.6	24
10+48.00	11,833,638.00	7,032,496.00	348.36	16.0	364.4	24
10+72.00	11,833,657.00	7,032,481.50	349.19	16.0	365.2	24
10+96.00	11,833,676.00	7,032,466.50	350.04	16.0	366.0	24
11+20.00	11,833,695.00	7,032,452.00	350.93	16.0	366.9	24
11+44.00	11,833,714.00	7,032,437.50	351.82	16.0	367.8	49
11+93.00	11,833,751.00	7,032,406.00	353.56	16.0	369.6	48
12+41.00	11,833,787.00	7,032,375.00	355.26	16.0	371.3	49
12+90.00	11,833,824.00	7,032,343.50	356.81	16.0	372.8	24
13+14.00	11,833,843.00	7,032,329.50	357.51	16.0	373.5	24
13+38.00	11,833,862.00	7,032,315.00	358.16	16.0	374.2	24
13+62.00	11,833,881.00	7,032,301.00	358.78	16.0	374.8	25
13+87.00	11,833,901.00	7,032,286.50	359.36	16.0	375.4	24
14+11.00	11,833,920.00	7,032,272.50	359.89	16.0	375.9	25
14+36.00	11,833,940.00	7,032,258.00	360.39	16.0	376.4	24
14+60.00	11,833,959.00	7,032,244.00	360.86	16.0	376.9	24
14+84.00	11,833,978.00	7,032,230.00	361.28	16.0	377.3	24
15+08.00	11,833,998.00	7,032,216.00	361.66	16.0	377.7	24
15+32.00	11,834,017.00	7,032,202.00	362.01	16.0	378.0	24
15+56.00	11,834,037.00	7,032,188.00	362.32	16.0	378.3	24
15+80.00	11,834,057.00	7,032,174.50	362.59	16.0	378.6	43
16+23.00	11,834,092.00	7,032,149.00	363.13	16.0	379.1	44
16+67.00	11,834,128.00	7,032,123.50	368.02	16.0	384.0	44
17+11.00	11,834,164.00	7,032,098.00	370.49	16.0	386.5	44
17+55.00	11,834,200.00	7,032,072.50	372.2	16.0	388.2	44
17+99.00	11,834,236.00	7,032,047.00	374.13	16.0	390.1	44
18+43.00	11,834,272.00	7,032,021.50	375.15	16.0	391.2	24
18+67.00	11,834,295.00	7,032,014.50	376.12	16.0	392.1	23
18+90.00	11,834,317.00	7,032,008.00	377.26	16.0	393.3	35
19+25.00	11,834,349.00	7,032,021.00	377.24	16.0	393.2	0

Station         X Coordinate         Y Coordinate Elevation         Wall I2 (Design Stationing 1426+00 to 1434+25)           10+00.00         11,832,776.00         7,032,989.50         337.41         13.0         350.4         2           10+02.00         11,832,774.00         7,032,990.50         337.4         13.0         350.4         10           10+12.00         11,832,767.00         7,032,997.00         337.34         13.0         350.3         10           10+22.00         11,832,759.00         7,033,003.50         337.29         13.0         350.3         10           10+32.00         11,832,751.00         7,033,010.00         337.23         13.0         350.2         10           10+42.00         11,832,744.00         7,033,016.50         337.18         13.0         350.2         10           10+52.00         11,832,736.00         7,033,029.00         337.01         13.0         350.1         10           10+62.00         11,832,728.00         7,033,029.00         337.01         13.0         350.0         10           10+72.00         11,832,778.00         7,033,029.00         336.99         13.0         350.0         10           10+82.00         11,832,750.00         7,033,048.50         336.8	
10+00.00       11,832,776.00       7,032,989.50       337.41       13.0       350.4       2         10+02.00       11,832,774.00       7,032,990.50       337.4       13.0       350.4       10         10+12.00       11,832,767.00       7,032,997.00       337.34       13.0       350.3       10         10+22.00       11,832,759.00       7,033,003.50       337.29       13.0       350.3       10         10+32.00       11,832,751.00       7,033,010.00       337.23       13.0       350.2       10         10+42.00       11,832,736.00       7,033,016.50       337.18       13.0       350.2       10         10+52.00       11,832,736.00       7,033,022.50       337.12       13.0       350.1       10         10+62.00       11,832,728.00       7,033,029.00       337.06       13.0       350.1       10         10+72.00       11,832,731.00       7,033,035.50       337.01       13.0       350.0       10         10+82.00       11,832,713.00       7,033,048.50       336.95       13.0       350.0       10         10+92.00       11,832,698.00       7,033,065.00       336.84       13.0       349.8       10         11+20.00       11	
10+02.00         11,832,774.00         7,032,990.50         337.4         13.0         350.4         10           10+12.00         11,832,767.00         7,032,997.00         337.34         13.0         350.3         10           10+22.00         11,832,759.00         7,033,003.50         337.29         13.0         350.3         10           10+32.00         11,832,751.00         7,033,010.00         337.23         13.0         350.2         10           10+42.00         11,832,736.00         7,033,016.50         337.18         13.0         350.2         10           10+52.00         11,832,736.00         7,033,022.50         337.12         13.0         350.1         10           10+62.00         11,832,728.00         7,033,029.00         337.06         13.0         350.1         10           10+72.00         11,832,731.00         7,033,035.50         337.01         13.0         350.0         10           10+82.00         11,832,755.00         7,033,048.50         336.89         13.0         349.9         10           11+20.00         11,832,698.00         7,033,065.00         336.84         13.0         349.8         10           11+22.00         11,832,690.00         7,033,067.50	
10+12.00       11,832,767.00       7,032,997.00       337.34       13.0       350.3       10         10+22.00       11,832,759.00       7,033,003.50       337.29       13.0       350.3       10         10+32.00       11,832,751.00       7,033,010.00       337.23       13.0       350.2       10         10+42.00       11,832,744.00       7,033,016.50       337.18       13.0       350.2       10         10+52.00       11,832,736.00       7,033,022.50       337.12       13.0       350.1       10         10+62.00       11,832,728.00       7,033,022.00       337.06       13.0       350.1       10         10+72.00       11,832,721.00       7,033,035.50       337.01       13.0       350.0       10         10+82.00       11,832,713.00       7,033,042.00       336.95       13.0       350.0       10         10+92.00       11,832,705.00       7,033,048.50       336.89       13.0       349.9       10         11+02.00       11,832,698.00       7,033,061.50       336.79       13.0       349.8       10         11+22.00       11,832,665.00       7,033,067.50       336.76       13.0       349.8       10         11+22.00	
10+22.00       11,832,759.00       7,033,003.50       337.29       13.0       350.3       10         10+32.00       11,832,751.00       7,033,010.00       337.23       13.0       350.2       10         10+42.00       11,832,744.00       7,033,016.50       337.18       13.0       350.2       10         10+52.00       11,832,736.00       7,033,022.50       337.12       13.0       350.1       10         10+62.00       11,832,728.00       7,033,029.00       337.06       13.0       350.1       10         10+72.00       11,832,721.00       7,033,035.50       337.01       13.0       350.0       10         10+82.00       11,832,713.00       7,033,042.00       336.95       13.0       350.0       10         10+92.00       11,832,705.00       7,033,048.50       336.89       13.0       349.9       10         11+02.00       11,832,698.00       7,033,061.50       336.84       13.0       349.8       10         11+22.00       11,832,662.00       7,033,067.50       336.76       13.0       349.8       10         11+32.00       11,832,667.00       7,033,080.50       336.7       13.0       349.7       10         11+52.00       1	
10+32.00       11,832,751.00       7,033,010.00       337.23       13.0       350.2       10         10+42.00       11,832,744.00       7,033,016.50       337.18       13.0       350.2       10         10+52.00       11,832,736.00       7,033,022.50       337.12       13.0       350.1       10         10+62.00       11,832,728.00       7,033,029.00       337.06       13.0       350.1       10         10+72.00       11,832,721.00       7,033,035.50       337.01       13.0       350.0       10         10+82.00       11,832,713.00       7,033,042.00       336.95       13.0       350.0       10         10+92.00       11,832,705.00       7,033,048.50       336.89       13.0       349.9       10         11+02.00       11,832,698.00       7,033,055.00       336.84       13.0       349.8       10         11+22.00       11,832,682.00       7,033,067.50       336.76       13.0       349.8       10         11+32.00       11,832,667.00       7,033,087.00       336.73       13.0       349.7       10         11+52.00       11,832,659.00       7,033,087.00       336.66       13.0       349.6       10         11+72.00	
10+42.00       11,832,744.00       7,033,016.50       337.18       13.0       350.2       10         10+52.00       11,832,736.00       7,033,022.50       337.12       13.0       350.1       10         10+62.00       11,832,728.00       7,033,029.00       337.06       13.0       350.1       10         10+72.00       11,832,721.00       7,033,035.50       337.01       13.0       350.0       10         10+82.00       11,832,713.00       7,033,042.00       336.95       13.0       350.0       10         10+92.00       11,832,705.00       7,033,048.50       336.89       13.0       349.9       10         11+02.00       11,832,698.00       7,033,055.00       336.84       13.0       349.8       10         11+12.00       11,832,690.00       7,033,061.50       336.79       13.0       349.8       10         11+22.00       11,832,667.00       7,033,074.00       336.73       13.0       349.7       10         11+22.00       11,832,667.00       7,033,087.00       336.66       13.0       349.7       10         11+22.00       11,832,652.00       7,033,093.50       336.66       13.0       349.6       10         11+22.00	
10+52.00       11,832,736.00       7,033,022.50       337.12       13.0       350.1       10         10+62.00       11,832,728.00       7,033,029.00       337.06       13.0       350.1       10         10+72.00       11,832,721.00       7,033,035.50       337.01       13.0       350.0       10         10+82.00       11,832,713.00       7,033,042.00       336.95       13.0       350.0       10         10+92.00       11,832,705.00       7,033,048.50       336.89       13.0       349.9       10         11+02.00       11,832,698.00       7,033,055.00       336.84       13.0       349.8       10         11+12.00       11,832,690.00       7,033,061.50       336.79       13.0       349.8       10         11+22.00       11,832,682.00       7,033,074.00       336.76       13.0       349.8       10         11+32.00       11,832,667.00       7,033,087.00       336.73       13.0       349.7       10         11+52.00       11,832,659.00       7,033,087.00       336.66       13.0       349.7       10         11+62.00       11,832,652.00       7,033,093.50       336.63       13.0       349.6       10         11+82.00	
10+62.00       11,832,728.00       7,033,029.00       337.06       13.0       350.1       10         10+72.00       11,832,721.00       7,033,035.50       337.01       13.0       350.0       10         10+82.00       11,832,713.00       7,033,042.00       336.95       13.0       350.0       10         10+92.00       11,832,705.00       7,033,048.50       336.89       13.0       349.9       10         11+02.00       11,832,698.00       7,033,055.00       336.84       13.0       349.8       10         11+12.00       11,832,690.00       7,033,061.50       336.79       13.0       349.8       10         11+22.00       11,832,682.00       7,033,067.50       336.76       13.0       349.8       10         11+32.00       11,832,675.00       7,033,087.00       336.73       13.0       349.7       10         11+42.00       11,832,667.00       7,033,087.00       336.66       13.0       349.7       10         11+52.00       11,832,652.00       7,033,093.50       336.63       13.0       349.6       10         11+72.00       11,832,644.00       7,033,100.00       336.6       13.0       349.6       10         11+82.00       1	
10+72.00       11,832,721.00       7,033,035.50       337.01       13.0       350.0       10         10+82.00       11,832,713.00       7,033,042.00       336.95       13.0       350.0       10         10+92.00       11,832,705.00       7,033,048.50       336.89       13.0       349.9       10         11+02.00       11,832,698.00       7,033,055.00       336.84       13.0       349.8       10         11+12.00       11,832,690.00       7,033,061.50       336.79       13.0       349.8       10         11+22.00       11,832,682.00       7,033,067.50       336.76       13.0       349.8       10         11+32.00       11,832,675.00       7,033,074.00       336.73       13.0       349.7       10         11+42.00       11,832,667.00       7,033,087.00       336.66       13.0       349.7       10         11+52.00       11,832,659.00       7,033,093.50       336.63       13.0       349.7       10         11+62.00       11,832,652.00       7,033,093.50       336.63       13.0       349.6       10         11+82.00       11,832,636.00       7,033,100.00       336.6       13.0       349.6       10         11+82.00       1	
10+82.00       11,832,713.00       7,033,042.00       336.95       13.0       350.0       10         10+92.00       11,832,705.00       7,033,048.50       336.89       13.0       349.9       10         11+02.00       11,832,698.00       7,033,055.00       336.84       13.0       349.8       10         11+12.00       11,832,690.00       7,033,061.50       336.79       13.0       349.8       10         11+22.00       11,832,682.00       7,033,067.50       336.76       13.0       349.8       10         11+32.00       11,832,675.00       7,033,074.00       336.73       13.0       349.7       10         11+42.00       11,832,667.00       7,033,080.50       336.7       13.0       349.7       10         11+52.00       11,832,659.00       7,033,087.00       336.66       13.0       349.7       10         11+62.00       11,832,652.00       7,033,093.50       336.63       13.0       349.6       10         11+72.00       11,832,644.00       7,033,100.00       336.6       13.0       349.6       10         11+82.00       11,832,636.00       7,033,106.00       336.57       13.0       349.6       10	
10+92.00       11,832,705.00       7,033,048.50       336.89       13.0       349.9       10         11+02.00       11,832,698.00       7,033,055.00       336.84       13.0       349.8       10         11+12.00       11,832,690.00       7,033,061.50       336.79       13.0       349.8       10         11+22.00       11,832,682.00       7,033,067.50       336.76       13.0       349.8       10         11+32.00       11,832,675.00       7,033,074.00       336.73       13.0       349.7       10         11+42.00       11,832,667.00       7,033,080.50       336.7       13.0       349.7       10         11+52.00       11,832,659.00       7,033,087.00       336.66       13.0       349.7       10         11+62.00       11,832,652.00       7,033,093.50       336.63       13.0       349.6       10         11+72.00       11,832,644.00       7,033,100.00       336.6       13.0       349.6       10         11+82.00       11,832,636.00       7,033,106.00       336.57       13.0       349.6       10	
11+02.00       11,832,698.00       7,033,055.00       336.84       13.0       349.8       10         11+12.00       11,832,690.00       7,033,061.50       336.79       13.0       349.8       10         11+22.00       11,832,682.00       7,033,067.50       336.76       13.0       349.8       10         11+32.00       11,832,675.00       7,033,074.00       336.73       13.0       349.7       10         11+42.00       11,832,667.00       7,033,080.50       336.7       13.0       349.7       10         11+52.00       11,832,659.00       7,033,087.00       336.66       13.0       349.7       10         11+62.00       11,832,652.00       7,033,093.50       336.63       13.0       349.6       10         11+72.00       11,832,644.00       7,033,100.00       336.6       13.0       349.6       10         11+82.00       11,832,636.00       7,033,106.00       336.57       13.0       349.6       10	
11+12.00       11,832,690.00       7,033,061.50       336.79       13.0       349.8       10         11+22.00       11,832,682.00       7,033,067.50       336.76       13.0       349.8       10         11+32.00       11,832,675.00       7,033,074.00       336.73       13.0       349.7       10         11+42.00       11,832,667.00       7,033,080.50       336.7       13.0       349.7       10         11+52.00       11,832,659.00       7,033,087.00       336.66       13.0       349.7       10         11+62.00       11,832,652.00       7,033,093.50       336.63       13.0       349.6       10         11+72.00       11,832,644.00       7,033,100.00       336.6       13.0       349.6       10         11+82.00       11,832,636.00       7,033,106.00       336.57       13.0       349.6       10	
11+22.00     11,832,682.00     7,033,067.50     336.76     13.0     349.8     10       11+32.00     11,832,675.00     7,033,074.00     336.73     13.0     349.7     10       11+42.00     11,832,667.00     7,033,080.50     336.7     13.0     349.7     10       11+52.00     11,832,659.00     7,033,087.00     336.66     13.0     349.7     10       11+62.00     11,832,652.00     7,033,093.50     336.63     13.0     349.6     10       11+72.00     11,832,644.00     7,033,100.00     336.6     13.0     349.6     10       11+82.00     11,832,636.00     7,033,106.00     336.57     13.0     349.6     10	
11+32.00     11,832,675.00     7,033,074.00     336.73     13.0     349.7     10       11+42.00     11,832,667.00     7,033,080.50     336.7     13.0     349.7     10       11+52.00     11,832,659.00     7,033,087.00     336.66     13.0     349.7     10       11+62.00     11,832,652.00     7,033,093.50     336.63     13.0     349.6     10       11+72.00     11,832,644.00     7,033,100.00     336.6     13.0     349.6     10       11+82.00     11,832,636.00     7,033,106.00     336.57     13.0     349.6     10	
11+42.00     11,832,667.00     7,033,080.50     336.7     13.0     349.7     10       11+52.00     11,832,659.00     7,033,087.00     336.66     13.0     349.7     10       11+62.00     11,832,652.00     7,033,093.50     336.63     13.0     349.6     10       11+72.00     11,832,644.00     7,033,100.00     336.6     13.0     349.6     10       11+82.00     11,832,636.00     7,033,106.00     336.57     13.0     349.6     10	
11+52.00     11,832,659.00     7,033,087.00     336.66     13.0     349.7     10       11+62.00     11,832,652.00     7,033,093.50     336.63     13.0     349.6     10       11+72.00     11,832,644.00     7,033,100.00     336.6     13.0     349.6     10       11+82.00     11,832,636.00     7,033,106.00     336.57     13.0     349.6     10	
11+62.00     11,832,652.00     7,033,093.50     336.63     13.0     349.6     10       11+72.00     11,832,644.00     7,033,100.00     336.6     13.0     349.6     10       11+82.00     11,832,636.00     7,033,106.00     336.57     13.0     349.6     10	
11+72.00     11,832,644.00     7,033,100.00     336.6     13.0     349.6     10       11+82.00     11,832,636.00     7,033,106.00     336.57     13.0     349.6     10	
11+82.00 11,832,636.00 7,033,106.00 336.57 13.0 349.6 10	
11+92.00 11.832.629.00 7.033.112.50 336.53 13.0 349.5	
Wall E2 (De 11,832,621.00 7,033,119.00 336.5 13.0 349.5 10	
12+12.00 11,832,613.00 7,033,125.50 336.47 13.0 349.5 10	
12+22.00 11,832,606.00 7,033,132.00 336.44 13.0 349.4 10	
12+32.00 11,832,598.00 7,033,138.50 336.41 13.0 349.4 10	
12+42.00 11,832,590.00 7,033,145.00 336.39 13.0 349.4 9	-
12+51.00 11,832,583.00 7,033,151.00 336.37 13.0 349.4 10	
12+61.00 11,832,575.00 7,033,157.50 336.35 13.0 349.4 10	
12+71.00 11,832,567.00 7,033,164.00 336.34 13.0 349.3 10	
12+81.00 11,832,560.00 7,033,170.50 336.32 13.0 349.3 10	
12+91.00 11,832,552.00 7,033,177.00 336.31 13.0 349.3 9	
13+00.00 11,832,545.00 7,033,183.00 336.31 13.0 349.3 24	
13+24.00 11,832,550.00 7,033,206.00 335.87 13.0 348.9 10	
13+34.00 11,832,543.00 7,033,212.50 335.85 13.0 348.9 10	
13+44.00 11,832,535.00 7,033,218.50 335.82 13.0 348.8 10	
13+54.00 11,832,527.00 7,033,225.00 335.81 13.0 348.8 10	
13+64.00 11,832,520.00 7,033,231.50 335.79 13.0 348.8 10	
13+74.00 11,832,512.00 7,033,237.50 335.78 13.0 348.8 10	
13+84.00 11,832,504.00 7,033,244.00 335.77 13.0 348.8 10	
13+94.00 11,832,496.00 7,033,250.50 335.76 13.0 348.8 9	
14+03.00 11,832,489.00 7,033,256.50 335.76 13.0 348.8 10	
14+13.00 11,832,481.00 7,033,263.00 335.76 13.0 348.8 10	
14+23.00 11,832,473.00 7,033,269.50 335.76 13.0 348.8 99	
15+22.00 11,832,396.00 7,033,332.50 335.93 13.0 348.9 10	
15+32.00 11,832,388.00 7,033,338.50 335.96 13.0 349.0 0	

15+42.00	11,832,380.00	7,033,345.00	335.99	13.0	349.0	10
15+52.00	11,832,373.00	7,033,351.50	336.02	13.0	349.0	10
15+62.00	11,832,365.00	7,033,357.50	336.05	13.0	349.1	10
15+72.00	11,832,357.00	7,033,364.00	336.08	13.0	349.1	5
15+77.00	11,832,353.00	7,033,367.00	336.09	13.0	349.1	5
15+82.00	11,832,349.00	7,033,370.00	336.11	13.0	349.1	10
15+92.00	11,832,341.00	7,033,376.50	336.14	13.0	349.1	9
16+01.00	11,832,334.00	7,033,382.50	336.17	13.0	349.2	10
16+11.00	11,832,326.00	7,033,389.00	336.2	13.0	349.2	10
16+21.00	11,832,318.00	7,033,395.00	336.23	13.0	349.2	10
16+31.00	11,832,310.00	7,033,401.50	336.26	13.0	349.3	9
16+40.00	11,832,303.00	7,033,407.50	336.29	13.0	349.3	10
16+50.00	11,832,295.00	7,033,414.00	336.32	13.0	349.3	10
16+60.00	11,832,287.00	7,033,420.00	336.35	13.0	349.4	10
16+70.00	11,832,279.00	7,033,426.50	336.38	13.0	349.4	10
16+80.00	11,832,271.00	7,033,432.50	336.41	13.0	349.4	10
16+90.00	11,832,264.00	7,033,439.00	336.43	13.0	349.4	10
17+00.00	11,832,256.00	7,033,445.00	336.46	13.0	349.5	10
17+10.00	11,832,248.00	7,033,451.50	336.48	13.0	349.5	10
17+20.00	11,832,240.00	7,033,457.50	336.49	13.0	349.5	10
17+30.00	11,832,232.00	7,033,464.00	336.51	13.0	349.5	9
17+39.00	11,832,225.00	7,033,470.00	336.52	13.0	349.5	10
17+49.00	11,832,217.00	7,033,476.50	336.52	13.0	349.5	10
17+59.00	11,832,209.00	7,033,482.50	336.53	13.0	349.5	10
17+69.00	11,832,201.00	7,033,489.00	336.53	13.0	349.5	10
17+79.00	11,832,193.00	7,033,495.00	336.52	13.0	349.5	10
17+89.00	11,832,186.00	7,033,501.50	336.52	13.0	349.5	10
17+99.00	11,832,178.00	7,033,507.50	336.51	13.0	349.5	10
18+09.00	11,832,170.00	7,033,514.00	336.5	13.0	349.5	10
18+19.00	11,832,162.00	7,033,520.00	336.48	13.0	349.5	10
18+29.00	11,832,154.00	7,033,526.50	336.46	18.0	354.5	0

CNE I - Walls I4-I6 Acoustical Profile (Projection NAD_1983_StatePlane_Virginia_North US Feet)							
Station	X Coordinate	Y Coordinate	Base Elevation	Wall Height	Top Elevation	Segment Length	
Wall I4 (Design Stationing 1437+75 to 1441+75)							
10+00.00	11,833,072.00	7,032,760.00	340.89	16.0	356.9	45	
10+45.00	11,833,107.00	7,032,731.00	340.46	16.0	356.5	45	
10+90.00	11,833,142.00	7,032,702.00	340.7	16.0	356.7	45	
11+35.00	11,833,177.00	7,032,673.00	340.96	16.0	357.0	44	
11+79.00	11,833,211.00	7,032,644.50	341.11	16.0	357.1	45	
12+24.00	11,833,246.00	7,032,615.50	341.27	16.0	357.3	45	
12+69.00	11,833,281.00	7,032,586.50	341.44	16.0	357.4	45	
13+14.00	11,833,316.00	7,032,557.50	341.74	16.0	357.7	45	
13+59.00	11,833,351.00	7,032,528.50	342.27	16.0	358.3	45	
14+04.00	11,833,386.00	7,032,499.50	342.99	16.0	359.0	0	
			Wall 15 (I	Design Stationing	1442+00 to 1443+75)		
10+00.00	11,833,406.00	7,032,480.00	343.56	16.0	359.6	38	
10+38.00	11,833,436.00	7,032,456.50	344.34	16.0	360.3	37	
10+75.00	11,833,465.00	7,032,433.00	345.23	16.0	361.2	38	
11+13.00	11,833,495.00	7,032,409.00	345.62	16.0	361.6	23	
11+36.00	11,833,513.00	7,032,394.00	346.49	16.0	362.5	0	
			Wall 16 (I	Design Stationing	1444+25 to 1449+25)		
10+00.00	11,833,576.00	7,032,347.00	347.99	16.0	364.0	48	
10+48.00	11,833,614.00	7,032,317.00	350.13	16.0	366.1	48	
10+96.00	11,833,651.00	7,032,287.00	353.38	16.0	369.4	48	
11+44.00	11,833,688.00	7,032,257.00	356.99	16.0	373.0	48	
11+92.00	11,833,726.00	7,032,227.00	360.26	16.0	376.3	24	
12+16.00	11,833,748.00	7,032,236.50	356.26	16.0	372.3	50	
12+66.00	11,833,788.00	7,032,207.00	357.71	16.0	373.7	50	
13+16.00	11,833,828.00	7,032,177.50	359.01	16.0	375.0	51	
13+67.00	11,833,869.00	7,032,148.00	360.14	16.0	376.1	41	
14+08.00	11,833,901.00	7,032,122.00	360.9	16.0	376.9	40	
14+48.00	11,833,932.00	7,032,096.50	361.55	16.0	377.6	48	
14+96.00	11,833,948.00	7,032,051.00	362.51	16.0	378.5	0	

CNEs JK - Walls JK Acoustical Profile (Projection NAD_1983_StatePlane_Virginia_North US Feet)								
Station	X Coordinate	Y Coordinate	Base Elevation	Wall Height	Top Elevation	Segment Length		
	Wall J2 (Design Stationing 1454+00 to 1458+75)							
10+00.00	11,834,391.00	7,031,776.00	361.73	16.0	377.7	48		
10+48.00	11,834,430.00	7,031,748.00	361.42	16.0	377.4	48		
	11,834,469.00		361.14	16.0	377.1	48		
11+44.00	11,834,508.00	7,031,692.50	361.02	16.0	377.0	49		
	11,834,548.00		360.81	16.0	376.8	48		
12+41.00	11,834,587.00	7,031,637.00	360.74	16.0	376.7	24		
$\overline{}$	11,834,606.00		360.74	16.0	376.7	24		
	11,834,624.00		360.72	16.0	376.7	25		
	11,834,643.00		360.73	16.0	376.7	24		
$\overline{}$	11,834,661.00		360.77	16.0	376.8	23		
-	11,834,678.00		360.98	16.0	377.0	24		
	11,834,696.00		361.28	16.0	377.3	24		
$\overline{}$	11,834,713.00		361.61	16.0	377.6	24		
-	11,834,730.00		362	16.0	378.0	24		
14+57.00	11,834,747.00	7,031,493.00	365.88	16.0	381.9	0		
					1459+50 to 1461+00)			
	11,834,789.00		367.25	16.0	383.3	24		
	11,834,806.00		364.45	16.0	380.5	24		
	11,834,823.00		365.13	16.0	381.1	24		
	11,834,840.00		365.79	16.0	381.8	24		
	11,834,856.00		366.41	16.0	382.4	24		
	11,834,873.00		367.09	16.0	383.1	24		
	11,834,889.00		369.79	16.0	385.8	23		
11+67.00	11,834,904.00	7,031,337.00	369.84	16.0	385.8	0		
					1462+00 to 1470+75)			
10+00.00	11,834,975	7,031,263	370.7	16.0	386.7	49		
10+49.00	11,835,006	7,031,225	373.1	16.0	389.1	48		
10+97.00	11,835,036	7,031,187	373.7	16.0	389.7	48		
11+45.00	11,835,066	7,031,149	374.3	16.0	390.3	48		
11+93.00	11,835,096	7,031,111	374.7	16.0	390.7	49		
12+42.00	11,835,127	7,031,073	375.0	16.0	391.0	48		
12+90.00	11,835,157	7,031,035	375.2	16.0	391.2	48		
13+38.00	11,835,187	7,030,997	375.3	16.0	391.3	48		
13+86.00	11,835,217	7,030,960	375.3	16.0	391.3	48		
14+34.00	11,835,247	7,030,922	375.1	16.0	391.1	49		
14+83.00	11,835,278	7,030,884	374.9	16.0	390.9	48		
15+31.00	11,835,308	7,030,846	374.5	16.0	390.5	48		
15+79.00	11,835,338	7,030,808	373.9	16.0	389.9	38		
16+17.00	11,835,360	7,030,777	373.5	16.0	389.5	37		
16+54.00	11,835,381	7,030,746	373.1	16.0	389.1	38		
16+92.00	11,835,403	7,030,716	372.6	16.0	388.6	38		
17+30.00	11,835,425	7,030,685	371.3	16.0	387.3	35		
17+65.00	11,835,447	7,030,657	371.8	16.0	387.8	35		
18+00.00	11,835,469	7,030,630	371.4	16.0	387.4	35		
18+35.00	11,835,490	7,030,602	366.2	16.0	382.2	0		

			Wall K2 (	Design Stationing	1471+00 to 1474+25)	
10+00.00	11,835,522	7,030,563	366.4	16.0	382.4	48
10+48.00	11,835,552	7,030,525	368.9	16.0	384.9	48
10+96.00	11,835,582	7,030,487	369.4	16.0	385.4	48
11+44.00	11,835,612	7,030,449	368.9	16.0	384.9	48
11+92.00	11,835,642	7,030,412	368.4	16.0	384.4	49
12+41.00	11,835,673	7,030,374	367.7	16.0	383.7	48
12+89.00	11,835,703	7,030,336	363.0	16.0	379.0	24
13+13.00	11,835,707	7,030,312	361.3	16.0	377.3	0
			Wall K3 (	Design Stationing	1475+00 to 1482+00)	
10+00.00	11,835,768	7,030,270	366.1	16.0	382.1	47
10+47.00	11,835,797	7,030,232	366.0	16.0	382.0	48
10+95.00	11,835,827	7,030,195	365.4	16.0	381.4	48
11+43.00	11,835,857	7,030,157	364.9	16.0	380.9	48
11+91.00	11,835,887	7,030,120	364.4	16.0	380.4	48
12+39.00	11,835,917	7,030,083	363.9	16.0	379.9	47
12+86.00	11,835,946	7,030,045	363.4	16.0	379.4	48
13+34.00	11,835,976	7,030,008	362.9	16.0	378.9	48
13+82.00	11,836,006	7,029,970	362.4	16.0	378.4	48
14+30.00	11,836,036	7,029,933	362.0	16.0	378.0	48
14+78.00	11,836,066	7,029,896	361.6	16.0	377.6	48
15+26.00	11,836,096	7,029,858	361.3	16.0	377.3	47
15+73.00	11,836,125	7,029,821	361.1	16.0	377.1	48
16+21.00	11,836,155	7,029,783	361.0	16.0	377.0	48
16+69.00	11,836,185	7,029,746	360.9	16.0	376.9	48
17+17.00	11,836,215	7,029,708	360.9	16.0	376.9	0
			Wall K4 (	Design Stationing	1482+25 to 1488+50)	
10+00.00	11,836,228	7,029,691	360.9	16.0	376.9	46
10+46.00	11,836,257	7,029,655	361.0	16.0	377.0	46
10+92.00	11,836,286	7,029,619	361.2	16.0	377.2	46
11+38.00	11,836,314	7,029,582	361.4	16.0	377.4	46
11+84.00	11,836,343	7,029,546	361.7	16.0	377.7	46
12+30.00	11,836,372	7,029,510	362.0	16.0	378.0	46
12+76.00	11,836,401	7,029,474	362.3	16.0	378.3	47
13+23.00	11,836,430	7,029,438	362.6	16.0	378.6	46
13+69.00	11,836,458	7,029,402	362.9	16.0	378.9	46
14+15.00	11,836,487	7,029,366	363.2	16.0	379.2	46
14+61.00	11,836,516	7,029,330	363.5	16.0	379.5	47
15+08.00	11,836,545	7,029,293	363.8	16.0	379.8	46
15+54.00	11,836,573	7,029,257	364.1	16.0	380.1	46
16+00.00	11,836,602	7,029,221	364.4	16.0	380.4	0

CNE N - W	CNE N - Walls N1-N3 Acoustical Profile (Projection NAD_1983_StatePlane_Virginia_North US Feet)						
Station	X Coordinate	Y Coordinate	Base Elevation	Wall Height	Top Elevation	Segment Length	
			Wall N1 (	Design Stationing	1508+00 to 1509+75)		
10+00.00	11,837,784.00	7,027,642.00	350.93	12.0	362.9	43	
10+43.00	11,837,811.00	7,027,608.00	352.31	12.0	364.3	43	
10+86.00	11,837,838.00	7,027,574.00	353.78	12.0	365.8	44	
11+30.00	11,837,865.00	7,027,539.50	355.27	12.0	367.3	44	
11+74.00	11,837,893.00	7,027,505.50	356.94	12.0	368.9	0	
			Wall N2 (	Design Stationing	1511+50 to 1517+50)		
10+00.00	11,838,041.00	7,027,407.50	361.71	15.0	376.7	47	
10+47.00	11,838,070.00	7,027,370.50	364.37	15.0	379.4	46	
10+93.00	11,838,098.00	7,027,334.00	366.26	15.0	381.3	47	
11+40.00	11,838,127.00	7,027,297.50	368.15	15.0	383.2	46	
11+86.00	11,838,155.00	7,027,261.00	370.05	15.0	385.1	47	
12+33.00	11,838,184.00	7,027,224.00	371.95	15.0	387.0	47	
	11,838,213.00		373.85	15.0	388.9	46	
	11,838,241.00		375.75	15.0	390.8	47	
13+73.00	11,838,270.00	7,027,114.00	377.65	15.0	392.7	24	
	11,838,284.00		378.61	15.0	393.6	48	
	11,838,309.00		380.45	15.0	395.5	48	
	11,838,334.00		382.28	15.0	397.3	40	
	11,838,359.00		383.91	15.0	398.9	40	
	11,838,383.00		385.54	15.0	400.5	40	
	11,838,408.00		390.05	15.0	405.1	0	
				Design Stationing	1518+25 to 1526+75)		
10+00.00	11,838,462.00	7,026,849.00	388.13	15.0	403.1	42	
	11,838,487.00		391.84	15.0	406.8	42	
	11,838,513.00		392.79	15.0	407.8	42	
	11,838,538.00		393.42	15.0	408.4	42	
	11,838,563.00		393.87	15.0	408.9	45	
	11,838,591.00		394.35	15.0	409.4	45	
	11,838,618.00		394.65	15.0	409.7	45	
	11,838,646.00		394.77	15.0	409.8	44	
	11,838,673.00		394.71	15.0	409.7	45	
	11,838,701.00		394.47	15.0	409.5	45	
	11,838,728.00		394.07	15.0	409.1	47	
	11,838,758.00		393.04	15.0	408.0	0	
	11,838,758.00		393.04	15.0	408.0	67	
	11,838,801.00		391.15	15.0	406.2	109	
	11,838,868.00		390.66	15.0	405.7	109	
	11,838,935.00		390.11	15.0	405.1	22	
	11,838,949.00		390.08	15.0	405.1	0	
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APPENDIX D - HB 2577 DOCUMENTATION



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October 14, 2019

### **MEMORANDUM**

**TO:** LJ Muchenje PE, Noise Abatement

**FROM:** Bill Kaufell Skelly and Loy, Noise Consultant

**SUBJECT:** Route 7 Corridor Improvements Project, UPC 52328

The 2009 General Assembly passed Chapter 120 (HB 2577, as amended by HB2025), which amends the Code of Virginia by adding in Article 15 of Chapter 1 of Title 33.1 a section numbered 33.1-223.2:21, relating to highway noise abatement.

House Bill 2025 States: Requires that whenever the Commonwealth Transportation Board or the Department plan for or undertake any highway construction or improvement project and such project includes or may include the requirement for the mitigation of traffic noise impacts, first consideration should be given to the use of noise reducing design and low noise pavement materials and techniques in lieu of construction of noise walls or sound barriers. Vegetative screening, such as the planting of appropriate conifers, in such a design would be utilized to act as a visual screen if visual screening is required.

In an effort to honor the intent of HB 2025 we are asking for your input (per <u>Chapter VI of Materials Division's Manual of Instruction</u> and <u>Section 2B-3 Determination of Roadway Design</u> of the VDOT Road Design manual (pages 2B-5 and 2B-6)). As part of the Noise Technical Report and technical files, we are seeking your professional opinion by providing comments for the project noted above. Please distribute this memorandum to the appropriate District staff and combine all responses into one response.

Should you have any questions, please contact me at (804) 371-6768. Thank you for your time and consideration regarding this request.

Additional Locations: Pittsburgh, PA State College, PA Morgantown, WV Hagerstown, MD Hunt Valley, MD

Comment: Is noise reducing design feasible in lieu of construction of noise walls or sound

barriers? For example, the roadway alignment can be shifted away from noise sensitive receptors or the roadway can be placed in deep cut (Location & Design to

address)

Response: The horizontal alignment for this project was developed with the intent of limiting the right of way impacts to the properties fronting Route 7 while preserving the

existing median for safety. The current design, developed through alternative studies and public input, provides the best solution to meet these goals. Shifting the horizontal alignment to the outside or inside will create undesirable impacts such as additional right-of-way/easement acquisitions, and potential median width

reductions or eliminations and, in turn, leading to decreased safety.

The vertical alignment for this project was developed with the intent of holding the existing grade as much as possible. The current design holds closely to the existing grade and provides room for milling/overlaying operations and cross slope correction. Placing the roadway in deep cut is not feasible given that it would require total pavement reconstruction through the corridor as well as triggering substantial utility relocation impacts.

Comment: Can the project support the use of low noise pavement in lieu of construction of

noise walls or sound barriers? (Materials Division to address)

Response: The Virginia Department of Transportation is not authorized by the Federal

Highway Administration to use "quiet pavement" at this time as a form of noise mitigation. Upon completion of the Quiet Pavement Pilot Program and approval from FHWA, the use of "quiet pavement" will be given additional consideration.

Comment: Can landscaping be utilized to act as a visual screen if visual screening is required?

(Location & Design to address)

Response: Landscaping can be used as a visual screen if required. The landscaping must be

placed outside of the clear zone, must not decrease driver sight distance, and must

not require additional right-of-way.

Note: Please provide the name of each responder.

APPENDIX E - WARRANTED, FEASIBLE, AND REASONABLE WORKSHEETS

# VDOT Highway Traffic Noise Abatement Warranted, Feasible, and Reasonable Worksheet Note: Not all questions apply depending on the design phase which may cause differing answers between preliminary and final design phase. Answers to the questions may change depending on the design phase of the project. Date: Date: 11/1/19 Project No. and UPC: State Project No. 007-029-128, B610, C502, P102, R202 Federal Project No. STP-5A01(745) and STP-5A01(790) UPC 52328

County: Fairfax

District: Route 7

Barrier System ID: Barrier System A1

Community Name and/or CNE# CNE A

Noise Abatement Category(s) B, C, and D

Design phase: Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was	
u.	issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
	_	Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	1
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	1
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	100%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	9,597 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	1
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	4
d.	Total number of benefited receptors.	5
e.	Surface Area per benefited receptor unit. (ft²/BR)	1,919 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	No
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
a.	Length of the proposed noise barrier. (ft)	600 ft
b.	Height range of the proposed noise barrier. (ft)	16-16 ft
c.	Average height of the proposed noise barrier. (ft)	16.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$403,074
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise	
	barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) REASONABLE?	No
Additional Reasons for Decision:	

# VDOT Highway Traffic Noise Abatement Warranted, Feasible, and Reasonable Worksheet Note: Not all questions apply depending on the design phase which may cause differing answers between preliminary and final design phase. Answers to the questions may change depending on the design phase of the project. Date: Date: 11/1/19 Project No. and UPC: State Project No. 007-029-128, B610, C502, P102, R202 Federal Project No. STP-5A01(745) and STP-5A01(790) UPC 52328

County: Fairfax

District: Route 7

Barrier System ID: Barrier System A2

Community Name and/or CNE# CNE A

Noise Abatement Category(s)

Design phase: Final design

	Warranted	1
1 a.	Community Documentation (if applicable)	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
Ъ.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	1
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	1
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	100%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	20,117 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	1
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	12
d.	Total number of benefited receptors.	13
e.	Surface Area per benefited receptor unit. (ft²/BR)	1,547 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	Yes
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
a.	Length of the proposed noise barrier. (ft)	1,286 ft
b.	Height range of the proposed noise barrier. (ft)	13-18 ft
c.	Average height of the proposed noise barrier. (ft)	16.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$844,914
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) REASONABLE?	Yes
Additional Reasons for Decision:	

1 3	
Date:	11/1/19
Project No. and UPC:	State Project No. 007-029-128, B610, C502, P102, R202
	Federal Project No. STP-5A01(745) and STP-5A01(790)
	UPC 52328
County:	Fairfax
District:	Route 7
Barrier System ID:	Barrier System B1-B6 and D1
Community Name and/or CNE#	CNEs B and D
Noise Abatement Category(s)	B, C, D, and E
Design phase:	Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was	
	issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	19
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	19
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	100%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	83,891 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	19
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	49
d.	Total number of benefited receptors.	68
e.	Surface Area per benefited receptor unit. (ft²/BR)	1,234 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	Yes
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
	Length of the proposed noise barrier. (ft)	5,593 ft
b.	Height range of the proposed noise barrier. (ft)	15-15
c.	Average height of the proposed noise barrier. (ft)	15.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$3,523,422
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) REASONABLE?	Yes
Additional Reasons for Decision:	

Date:	11/1/19
Project No. and UPC:	State Project No. 007-029-128, B610, C502, P102, R202
	Federal Project No. STP-5A01(745) and STP-5A01(790)
	UPC 52328
County:	Fairfax
District:	Route 7
Barrier System ID:	Barrier System C1 and C2
Community Name and/or CNE#	CNE C
Noise Abatement Category(s)	В
Design phase:	Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	21
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	21
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	100%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	77,096 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	21
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	47
d.	Total number of benefited receptors.	68
e.	Surface Area per benefited receptor unit. (ft²/BR)	1,134 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	Yes
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
a.	Length of the proposed noise barrier. (ft)	5,140 ft
b.	Height range of the proposed noise barrier. (ft)	15-15
c.	Average height of the proposed noise barrier. (ft)	15.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$3,238,032
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	37
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) REASONABLE?	Yes
Additional Reasons for Decision:	

Date: Project No. and UPC:	1/12/22 State Project No. 007-029-128, B610, C502, P102, R202 Federal Project No. STP-5A01(745) and STP-5A01(790)
	UPC 52328
County:	Fairfax
District:	Route 7
Barrier System ID:	Barrier System D2 and E1-E4
Community Name and/or CNE#	CNEs D and E
Noise Abatement Category(s)	В
Design phase:	Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was	
	issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	18
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	18
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	100%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	64,888 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	18
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	24
d.	Total number of benefited receptors.	42
e.	Surface Area per benefited receptor unit. (ft²/BR)	1,545 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	Yes
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
a.	Length of the proposed noise barrier. (ft)	4,326 ft
b.	Height range of the proposed noise barrier. (ft)	15-15
c.	Average height of the proposed noise barrier. (ft)	15.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$2,725,296
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Yes
Yes
Yes

Date: Project No. and UPC:	11/1/19 State Project No. 007-029-128, B610, C502, P102, R202 Federal Project No. STP-5A01(745) and STP-5A01(790) UPC 52328
County:	Fairfax
District:	Route 7
Barrier System ID:	Barrier System F1, F1B, F1C and F2
Community Name and/or CNE#	CNE F
Noise Abatement Category(s)	B and C
Design phase:	Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	8
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	7
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	88%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	14,658 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	7
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	3
d.	Total number of benefited receptors.	10
e.	Surface Area per benefited receptor unit. (ft²/BR)	1,466 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	Yes
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
a.	Length of the proposed noise barrier. (ft)	1,127 ft
b.	Height range of the proposed noise barrier. (ft)	13-13
c.	Average height of the proposed noise barrier. (ft)	13.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$615,636
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Yes
Yes
Yes

	e: ject No. and UPC:	R202 1(790)
County: Fairfax	ınty:	
District: Route 7	trict:	
Barrier System ID: Barrier F3	rier System ID:	
Community Name and/or CNE# CNE F	nmunity Name and/or CNE#	
Noise Abatement Category(s) B	se Abatement Category(s)	
Design phase: Final design	ign phase:	

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2 a.	Criteria requiring consideration of noise abatement Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	12
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	12
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	100%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	40,735 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	12
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	14
d.	Total number of benefited receptors.	26
e.	Surface Area per benefited receptor unit. (ft²/BR)	1,567 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	Yes
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
a.	Length of the proposed noise barrier. (ft)	2,546 ft
b.	Height range of the proposed noise barrier. (ft)	16-16
c.	Average height of the proposed noise barrier. (ft)	16.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$1,710,870
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) REASONABLE?	Yes
Additional Reasons for Decision:	

1 0	
Date:	11/1/19
Project No. and UPC:	State Project No. 007-029-128, B610, C502, P102, R202
	Federal Project No. STP-5A01(745) and STP-5A01(790)
	UPC 52328
County:	Fairfax
District:	Route 7
Barrier System ID:	Barrier System F4-F4B
Community Name and/or CNE#	CNE F
Noise Abatement Category(s)	B, C
Design phase:	Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	6
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	6
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	100%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	Yes
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	35,352 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	6
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	16
d.	Total number of benefited receptors.	22
e.	Surface Area per benefited receptor unit. (ft²/BR)	1,607 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	No
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
1	Length of the proposed noise barrier. (ft)	2,210 ft
b.	Height range of the proposed noise barrier. (ft)	16-16 ft
c.	Average height of the proposed noise barrier. (ft)	16.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$1,484,784
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	No
Is the Noise Barrier(s) REASONABLE?	No
Additional Reasons for Decision:	
Barriers impact the 100 year floodplain in this area resulting in safety issues by restricting flow	v during high
water events. Therefore it is not recommended that the barriers be built.	

Date:	11/1/19
Project No. and UPC:	State Project No. 007-029-128, B610, C502, P102, R202
	Federal Project No. STP-5A01(745) and STP-5A01(790)
	UPC 52328
County:	Fairfax
District:	Route 7
Barrier System ID:	Barrier System F5-F9
Community Name and/or CNE#	CNE F
Noise Abatement Category(s)	В
Design phase:	Final design
<del>-</del>	-

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	8
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	8
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	100%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	54,789 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	8
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	17
d.	Total number of benefited receptors.	25
e.	Surface Area per benefited receptor unit. (ft²/BR)	2,192 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	No
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
a.	Length of the proposed noise barrier. (ft)	2,489 ft
b.	Height range of the proposed noise barrier. (ft)	22-22 ft
c.	Average height of the proposed noise barrier. (ft)	22.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$2,301,138
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) REASONABLE?	No
Additional Reasons for Decision:	

### CNE F - BARRIER F5 - F8 HEIGHT EVALUATION

										2040 Loudest	t Hour Predict	ted Future Noi	ise Levels	Leq(h)	in dBA									
	# of Dwelling		F5-F	8 30'	F5-F	8 28'	F5-F8	3 26'	F5-F	8 24'	F5-F	8 22'	F5-F8 20'		F5-F9 18'		F5-F8 16'		F5-F6	8 14'	F5-F6	8 12'	F5-F	8 10'
Receptor Number	Units	No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)		Insertion Loss (IL)*	With Barrier (dBA)	Insertion Loss (IL)* (dBA)																
CNE F Barrier Syste	em F5 - F8				1	. ,		. ,	l	. ,						, ,	1	,		, ,		,	1	. ,
F-100	1	69 67	64	5	64	5	64	5	64	5	64	5	64	5	64	5	64	5	65	5	65	4	65	4
F-101 F-102	1	65	62 61	4	62 61	4	62 61	5 4	62 61	5	62 61	4	62 61	5	62 61	4	62 61	4	62 62	5	63 62	4	63 62	4
F-103	1	63	60	3	60	3	60	3	60	3	60	3	60	3	60	3	60	3	60	3	60	3	60	3
F-104 F-105	1	56 56	53 52	3	53 52	3	53 52	4	53 52	3	53 52	3	54 52	3 4	54 52	2	54 52	2	54 53	3	54 53	2	54 53	2
F-105 F-106	1	61	57	5	57	5	52	5	52	4	57	4	52	4	57	4	57	4	58	4	58	3	58	3
F-107	1	62	57	4	57	4	58	4	58	4	58	4	58	4	58	4	58	4	58	3	59	3	59	3
F-108 F-109	1	45 60	43 54	3	43 55	2	43 55	2	43 55	2	43 55	2	43 55	2	44 55	2	44 56	2	43 56	2	43 56	2	43 56	2
F-110	1	56	50	6	50	5	51	5	51	5	51	5	51	4	52	4	52	4	52	4	52	3	52	3
F-111	1	54	49	5	49	5	50	4	50	4	50	4	50	4	50	4	51	3	51	3	51	3	51	3
F-112 F-113	1	53 52	48 48	4	48 48	4	48 48	4	49 48	4	49 49	4	49 49	4	49 49	3	49 49	3	50 49	3	50 50	3	50 50	3
F-114	1	51	48	3	48	3	48	3	48	3	48	3	48	3	48	3	49	2	49	2	49	2	49	2
F-115	1	50	46	3	46	3	47	3	47	3	47	3	47	3	47	3	47	2	48	2	48	2	48	2
F-116	1	72	64 58	8 13	64 59	8 12	65	8 12	65 59	8 12	65 60	8 12	65	7	65	7	65	7	65	7	66	6	66	6
F-117 F-118	1	71 61	55	13 6	59	6	59 55	6	59	12 5	56	12 5	60 56	11 5	60 56	11 4	61 57	10	62 57	4	62 58	9	62 58	9
F-119	1	59	53	6	53	5	53	5	54	5	54	5	54	4	54	4	55	4	55	3	56	3	56	3
F-120	1	55	50	5	50	5	50	4	51	4	51	4	51	4	51	4	51	3	52	3	52	3	52	3
F-121 F-122	1	52 52	49 48	3	49 48	3	49 48	3 4	49 48	3	49 48	3	49 48	3 4	49 48	3	49 48	3	50 49	3	50 49	2	50 49	2
F-123	1	74	66	8	66	8	66	8	66	8	66	8	66	8	66	8	66	8	67	8	67	7	67	7
F-124	1	73	63	10	63	10	63	10	63	10	64	10	64	10	64	10	64	9	65	9	65	8	67	7
F-125 F-126	1	73 60	67 52	5 8	67 52	5 8	67 52	7	68 53	7	68 53	7	68 53	7	68 54	5	68 54	5	68 54	5 6	68 55	4	69 56	4
F-127	1	56	52	5	52	5	52	5	52	4	52	4	52	4	52	4	53	4	53	3	53	3	54	2
F-128	1	53	48	5	48	5	48	5	48	5	48	4	48	4	49	4	49	4	49	4	49	3	50	3
F-129 F-130	1	54 55	48 49	6	48	6	48 49	6	49 49	6	49 50	6	49 50	5	49 50	5	50 51	5	50 51	4 5	50 51	4	51 52	3 4
F-131	1	56	51	5	51	5	51	5	51	5	51	5	52	4	52	4	52	4	52	4	53	3	53	3
F-132	1	65	56	9	56	9	57	9	57	9	57	8	57	8	58	8	58	7	58	7	59	7	60	6
F-133 F-134	1	65 56	58 54	6	58 54	6	59 54	6 3	59 54	6	59 54	6	59 54	6 2	59 54	6	59 54	5	60 54	5	60 54	5	60 54	2
F-135	1	58	55	2	55	2	55	2	55	2	55	2	55	2	56	2	56	2	56	2	56	2	56	2
F-136	1	61	60	1	60	1	60	1	60	1	60	1	60	1	60	1	60	1	60	1	60	1	60	1
F-137 F-138	1	58 57	58 57	0	58 58	0	58 58	0	58 58	0	58 58	0	58 58	0	58 58	0	58 58	0	58 58	0	58 58	0	58 58	0
F-138	1	57	57	0	57	0	58	0	58	0	58	0	57	0	58	0	58	0	58	0	58	0	58	0
F-140	1	66	66	0	66	0	66	0	66	0	66	0	66	0	66	0	66	0	66	0	66	0	66	0
F-141	1	54	54	0	54	0	54	0	54	0	54	0	54	0	54	0	54	0	54	0	54	0	54	0
F-142 F-143	1	55 53	54 51	2	54 52	2	54 52	2	54 52	2	54 52	2	54 52	2	54 52	2	54 52	2	54 52	2	54 52	1	54 52	1
F-144	1	54	51	2	52	2	52	2	52	2	52	2	52	2	52	2	52	2	52	2	52	2	52	2
F-145	1	52	49	3	49	3	49	3	49	3	49	3	49	3	50	3	50	3	50	2	50	2	50	2
F-146 F-147	1	51 53	47 53	3	48 53	3 1	48 53	3	48 53	2	49 53	0												
F-148	1	55	55	0	55	0	55	0	55	0	55	0	55	0	55	0	55	0	55	0	55	0	55	0
F-149	1	56	56	1	56	1	56	1	56	1	56	1	56	1	56	1	56	1	56	1	56	1	56	1
F-150 F-151	1	55 59	54 58	0	54 58	0	54 59	0	54 59	0	54 59	0	54 59	0	54 59	0	55 59	0	55 59	0	55 59	0	55 59	0
F-152	1	58	58	0	58	0	58	0	58	0	58	0	58	0	58	0	58	0	58	0	58	0	58	0
F-153	1	54	53	1	53	1	53	1	53	1	53	1	53	1	53	1	53	1	53	1	53	1	53	1
F-154 F-155	1	56 54	56 54	0	56 54	0	56 54	0	56 54	0	56 54	0	56 54	0	56 54	0	56 54	0	56 54	0	56 54	0	56 54	0
F-155	1	53	53	0	53	0	54	0	54	0	54	0	53	0	54	0	54	0	54	0	53	0	53	0
F-157	1	53	52	1	52	1	52	1	52	1	52	1	52	1	52	1	52	0	52	0	52	0	52	0
F-158 F-159	1	55 52	54 52	0	54 52	0	54 52	0	54 52	0	54 52	0	54 52	0	54 52	0	54 52	0	54 52	0	54 52	0	54 52	0
F-159 F-160	1	52 52	52	0	52	0	52 52	0	52 52	0	52	0	52 52	0	52	0	52	0	52	0	52	0	52	0
F-161	1	51	51	0	51	0	51	0	51	0	51	0	51	0	51	0	51	0	51	0	51	0	51	0
F-162	1 1	53	53	0	53	0	53	0	53	0	53	0	53	0	53	0	53 55	0	53	0	53	0	53 55	0
F-163 F-164	1	55 57	55 57	0	55 57	0	55 57	0	55 57	0	55 57	0	55 57	0	55 57	0	55	0	55 57	0	55 57	0	55 57	0
Total Number of Imp	acted Units			8		8		8		8		8		8	- "	8		8		8		8		8
mpacted Receptors	Receiving ≥ 5 dB(A)			7		7		7	l	7		7		7		7		7		7		4		4
ercent of Impacted s the Barrier Feacible	Receptors Receivin e Based unon 5 dR/	g ≥ 5 dB(A) Insertion Loss A) Reduction Criteria (Yes/No):	?	88% Yes		88% Yes		88% Yes	l	88% Yes		50% Yes		50% Yes										
		II Receptors ≥5 dB[A] Insertio		23		22		20	1	18		17	1	14		12		12		11	1	7	1	5
		on Loss of 7 dB(A) or more.		4		4		4	l	4		4		4		4		4		4		4		4
		least one Impacted Receptor ( VDOT acoustical specifications	res/No)?	Yes Yes		Yes Yes		Yes Yes	1	Yes Yes		Yes Yes	1	Yes Yes		Yes Yes		Yes Yes		Yes Yes	1	Yes Yes	1	Yes Yes
Socs wan penolin a	ccording to FFIWAY		f Optimized Design		1	48020		44589	l	41159		37730	<b>†</b>	34300		30869	t -	27440	1	24010	1	20579	1	17150
		Square Footage/B	enefitted Receptor	2237		2183		2229	1	2287		2219	1	2450		2572		2287		2183	1	2940	1	3430
*	Insertion Loss (III)	ound levels may be different o	Reasonable:	No No	1	No	<u> </u>	No	<u> </u>	No		No	L	No		No	<u> </u>	No	1	No	1	No	1	No
66	Insertion Loss (IL) s Indicates noise imp		ide to rounding																					
	Indicates at least a																							

### CNE F - BARRIER F5 - F9 HEIGHT EVALUATION

									20.4	n Loudont II	our Predicted	i Euturo Naia	Lovels	Leq(h)	in dRA									
	# of Dwelling			F9 30'		9 28'	F5-F	0.001		9 24'		9 22'	F5-F			9 18'		9 16'	F5-F	2.44	F5-F	F5-F9 10		
eptor Number	Units	No Barrier	With Barrier	Insertion Loss	With Barrier	Insertion Loss (IL)*	With Barrier	Insertion Loss (IL)*	With Barrier	Insertion Loss (IL)*	With Barrier	Insertion Loss (IL)*	With Barrier	Insertion Loss (IL)*	With Barrier	Insertion Loss (IL)*	With Barrier	Insertion Loss (IL)*	With Barrier	Insertion Loss (IL)*	With Barrier	Insertion Loss (IL)*	With Barrier	Inse
			(dBA)	(IL)* (dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(d
F-100	m F5 - F9	60	64		64	5	64	5	64	,	64	5	64	5	64	-	64		65	5	65	5	66	
F-100	1	67	62	5	62	5	62	5	62	5	62	5	62	5	62	5	62	5	62	5	62	5	64	
F-102	1	65	61	4	61	4	61	4	61	4	61	4	61	4	61	4	61	4	62	4	62	4	62	+
F-103	1	63	60	3	60	3	60	3	60	3	60	3	60	3	60	3	60	3	60	3	60	3	61	$\top$
F-104	1	56	53	3	53	3	53	3	53	3	53	3	54	3	54	2	54	2	54	2	54	2	54	1
F-105	1	56	52	4	52	4	52	4	52	4	52	4	52	4	52	3	52	3	53	3	53	3	53	T
F-106	1	61	57	5	57	5	57	5	57	4	57	4	57	4	57	4	57	4	58	4	58	4	58	T
F-107	1	62	57	4	57	4	58	4	58	4	58	4	58	4	58	4	58	4	58	3	58	3	59	
F-108	1	45	42	3	43	3	43	3	43	2	43	2	43	2	43	2	43	2	43	2	43	2	43	
F-109	1	60	54	5	55	5	55	5	55	5	55	5	55	4	55	4	56	4	56	4	56	4	56	+-
F-110 F-111	1	56 54	50 49	6	50 49	5	51 49	5	51 50	5	51 50	5	51 50	5	52 50	4	52 51	3	52 51	4	52 51	3	53 51	+
F-111 F-112	1	54	49	5	49	4	49	4	49	4	49	4	49	4	49	3	49	3	50	3	50	3	50	+
F-112	1	52	48	4	48	4	48	4	49	4	49	4	48	4	49	3	49	3	49	3	49	3	50	+
F-114	1	51	47	4	47	4	47	4	47	4	48	3	48	3	48	3	49	3	49	3	48	3	49	+
F-115	1	50	46	4	46	4	46	3	46	3	46	3	47	3	47	3	47	3	47	2	47	2	48	+
F-116	1	72	64	8	64	8	65	8	65	8	65	8	65	7	65	7	65	7	65	7	65	7	67	
F-117	1	71	58	13	59	12	59	12	59	12	60	12	60	11	60	11	61	10	62	10	62	10	63	1
-118	1	61	55	6	55	6	55	6	55	5	56	5	56	5	56	4	57	4	57	4	57	4	58	T
-119	1	59	53	6	53	6	53	5	54	5	54	5	54	5	54	4	55	4	55	3	55	3	56	+
-120	1	55	50	5	50	5	50	5	51	4	51	4	51	4	51	4	51	3	52	3	52	3	52	$\top$
-121	1	52	48	4	48	4	48	4	48	4	49	3	49	3	49	3	49	3	49	3	49	3	50	I
-122	1	52	47	5	47	5	47	5	47	5	47	4	47	4	48	4	48	4	48	4	48	4	49	ፗ
-123	1	74	66	8	66	8	66	8	66	8	66	8	66	8	66	8	66	8	67	8	67	8	67	4
-124	1	73	63	10	63	10	63	10	63	10	63	10	64	10	64	10	64	9	65	9	65	9	67	4
-125	11	73	67	5	67	5	67	5	68	5	68	5	68	5	68	5	68	5	68	5	68	5	69	4
-126 -127	1	60 56	52 51	8	52 51	- 8 - 5	52 51	- 8 - 5	52 51	8	53 51	7 5	53 52	7 5	53 52	7	54 52	6	54 52	6	54 52	6 4	56 54	+
-127	1	53	47	6	47	6	47	6	47	5	47	5	48	5	48	4	48	5	48	4	48	4	49	+
-128	1	54	47	8	47	7	47	7	47	7	48	7	48	6	48		49	5	49	5	49	- 4 - c	50	+
-130	1	55	47	8	48	8	48	7	48	7	49	7	49	7	49	6	50	6	50	5	50	5	52	+
-131	1	56	49	7	50	6	50	6	50	6	50	6	51	5	51	5	51	5	52	4	52	4	53	+
-132	1	65	55	10	56	10	56	10	56	9	56	9	57	9	57	8	58	8	58	7	58	7	59	+
-133	1	65	57	8	57	8	57	8	57	7	58	7	58	7	58	7	58	6	59	6	59	6	60	+
-134	1	56	51	5	51	5	51	5	52	5	52	4	52	4	52	4	52	4	53	3	53	3	53	+
F-135	1	58	53	5	53	5	53	5	53	5	53	5	53	4	54	4	54	4	54	3	54	3	55	T
F-136	1	61	57	4	57	4	57	4	57	4	57	4	57	4	58	3	58	3	58	3	58	3	59	
F-137	1	58	54	5	54	4	54	4	54	4	55	4	55	4	55	3	55	3	56	3	56	3	56	Т
F-138	1	57	54	4	54	4	54	3	54	3	54	3	55	3	55	3	55	2	55	2	55	2	56	Щ
F-139	1	57	53	4	53	4	53	4	54	4	54	4	54	3	54	3	54	3	54	3	54	3	55	Щ
F-140	1	66	60	6	60	6	60	6	60	6	60	6	60	6	61	5	61	5	61	5	61	5	62	_
F-141	1	54	50	4	51	4	51	4	51	4	51	4	51	4	51	3	51	3	51	3	51	3	52	+
-142 -143	1	55 53	51 49	4	51 49	4	52 49	3 4	52 49	3 4	52 49	3 4	52 49	3	52 50	3	52 50	3	52 50	3	52 50	3	53 51	+
-143	1	53	49	4	49	4	49 50	4	49 50	4	49 50	4	50	4	50	4	50	3	50	3	50	3	51	+
-144	1	52	49	6	49	6	47	6	47	5	47	5	47	5	47	4	48	5	48	4	48	4	49	+
-146	1	51	45	6	45	5	46	5	46	5	46	5	46	5	46	5	46	4	47	4	47	4	47	+
-147	1	53	49	4	49	4	49	4	49	4	49	4	50	4	50	4	50	4	50	3	50	3	51	+
-148	1	55	51	4	51	4	51	4	51	4	51	4	52	4	52	3	52	3	52	3	52	3	53	+
-149	1	56	51	5	51	5	52	5	52	5	52	5	52	4	52	4	52	4	53	4	53	4	54	T
-150	1	55	51	4	51	4	51	4	51	4	51	4	51	4	52	4	52	4	52	3	52	3	53	Т
-151	1	59	55	3	55	3	55	3	55	3	56	3	56	3	56	3	56	3	56	3	56	3	57	I
-152	1	58	55	3	55	3	55	3	55	3	55	3	55	3	55	3	56	3	56	2	56	2	56	
-153	1	54	50	4	50	4	50	4	50	4	50	4	50	4	50	4	50	4	51	3	51	3	52	4
-154	11	56	53	2	54	2	54	2	54	2	54	2	54	2	54	2	54	2	54	2	54	2	54	+
-155	1	54	52	2	52	2	52	2	52	2	52	2	52	2	52	2	52	2	53	2	53	2	53	+
-156 -157	1	53	51	3	51	2	51	2	51	2	51	2	51	2	51	2	51	2	51	2	51	2	52	+
-157 -158	1	53 55	50 53	2	50 53	2	50 53	2	50 53	2	51 53	2	51 53	2	51 53	2	51 53	2	51 53	2	51 53	1	51 54	+
-158 -159	1	52	53	1	53	1	53	1	53	1	53	1	53	1	53	1	53	1	53	0	53	0	54	+
-160	1	52	51	1	51	1	51	1	51	1	51	1	51	1	51	1	51	1	51	1	51	1	51	+
-161	1	51	50	1	50	1	50	1	50	1	50	1	50	1	50	1	50	1	50	1	50	1	51	+
-162	1	53	53	1	53	1	53	1	53	1	53	1	53	1	53	1	53	1	53	0	53	0	53	+
-163	1	55	54	1	54	1	54	1	54	1	54	1	54	0	54	0	54	0	55	0	55	0	55	T
-164	1	57	57	0	57	0	57	0	57	0	57	0	57	0	57	0	57	0	57	0	57	0	57	T
mber of Impa	cted Units			8		8		8		8		8		8		8		8		8		8		_
	teceiving ≥ 5 dB(A)			8	l	8	l	8	l	8		8		8		8		8		8		8	ı	
		g ≥ 5 dB(A) Insertion Loss		100%	l	100%		100%		100%		100%		100%		100%		100%		100%		100%	ı	
		A) Reduction Criteria (Yes/No)?		Yes	l	Yes	l	Yes	l	Yes		Yes		Yes		Yes		Yes		Yes		Yes	ı	
		I Receptors ≥ 5 dB[A] Insertion	n Loss)	33	l	30	l	29	l	26	1	25	l	21	l	17	l	16	1	13	1	13	ı	
		in Loss of 7 dB(A) or more.	44. 13	4	l	4		4		4		4		4		4		4		4		4	ı	
		east one Impacted Receptor (Y	es/No)?	Yes	l	Yes		Yes		Yes		Yes		Yes		Yes		Yes		Yes		Yes	ı	
iii perform ac	cording to FHWA/\	DOT acoustical specifications	O-Mariana D	Yes	-	Yes	-	Yes	-	Yes		Yes		Yes		Yes		Yes		Yes	-	Yes		_
		Square Footage of			l	69732 2324		64750 2233		59769 2299		54789 2192		49808 2372		44827 2637		39847 2490		34866 2682		29884 2299	ı	
		Square Footage/Bo	enefitted Recepto Reasonable		l	2324 No		2233 No		2299 No		2192 No		2372 No		2637 No	l	2490 No	1	2682 No	1	2299 No	ı	

CNE F - BARRIER F6 - F8 HEIGHT EVALUATION

									2040 Lo	udest Hour	Predicted F	uture Noise	Levels	Leq(h)	) in dBA									
	# of Dwelling		F6.	F8 30'	F6-F	8 28'	F6-F	8 26'	F6-F	8 24'	F6-F	8 22'	F6-F	8 20'	F6.F	8 18'	F6-F8 16'		F6-F8 14'		F6-F	8 12'	F6-F8	8 10'
Receptor Number	Units		With	Insertion	With	Insertion	With	Insertion	With	Insertion	With	Insertion	With	Insertion	With	Insertion	With	Insertion	With	Insertion	With	Insertion	With	Insertio
		No Barrier	Barrier (dBA)	Loss (IL)* (dBA)	Barrier (dBA)	Loss (IL)* (dBA)	Barrier (dBA)	Loss (IL)* (dBA)	Barrier (dBA)	Loss (IL)* (dBA)	Barrier (dBA)	Loss (IL)* (dBA)	Barrier (dBA)	Loss (IL)* (dBA)	Barrier (dBA)	Loss (IL)* (dBA)	Barrier (dBA)	Loss (IL)* (dBA)	Barrier (dBA)	Loss (IL)* (dBA)	Barrier (dBA)	Loss (IL)* (dBA)	Barrier (dBA)	Loss (IL (dBA)
CNE F Barrier Syste	m F6 - F8		1		!				!								!							
F-100 F-101	1	69	68	1	68	1	68	1	68	1	68	0	68	1	68 67	1	68	1	68	1	68	1	68	0
F-101 F-102	1	67 65	67 65	0	67 65	0	67 65	0	67 65	0	65	0	67 65	0	65	0	65	0	67 65	0	67 65	0	67	0
F-103	1	63	62	0	62	0	62	0	62	0	63	0	63	0	63	0	63	0	63	0	63	0	63	0
F-104	1	56	54	2	54	2	54	2	54	2	54	2	54	2	54	2	54	2	54	2	54	2	55	1
F-105	1	56	54	2	54	2	54	2	54	2	54	2	54	2	54	2	54	2	54	2	54	2	54	2
F-106 F-107	1	61 62	60 60	2	60 60	2	60 60	2	60 60	2	60	2 2	60 60	1 2	60	2	60 60	1 2	60	2	60 60	1 1	60 60	1
F-108	1	45	43	2	43	2	44	2	44	2	44	2	44	2	44	1	44	1	44	2	43	2	43	2
F-109	1	60	56	4	56	4	56	3	56	3	56	3	57	3	57	3	57	3	57	3	57	3	57	2
F-110	1	56	52	4	52	4	52	4	52	4	52	4	52	3	53	3	53	3	53	3	53	2	54	2
F-111 F-112	1	54 53	50 49	4	50 49	4	50 49	4	51 49	3	51 49	3	51 50	3	51 50	3	51 50	3	51 50	3	52 50	2	52 51	2
F-112 F-113	1	53	49	3	49	3	49	3	49	3	49	3	49	3	49	3	50	2	50	2	50	2	50	2
F-114	1	51	48	3	48	3	48	3	48	3	48	3	49	2	49	2	49	2	49	2	49	2	50	1
F-115	1	50	47	3	47	3	47	3	47	3	47	2	47	2	47	2	48	2	48	2	48	2	48	1
F-116	1	72 71	66	6	66	6	66	6	66	6	66	6	66	6	66	6	66	6	67	6	67	5	67	5
F-117 F-118	1	71 61	60 55	11	60 56	11	60 56	11	61 56	11	61 56	10 4	61 57	10	61 57	10 4	62 57	9	62 58	9	63 58	8	64 58	7
F-119	1	59	53	5	56	5	54	5	56	5	56 54	4	54	4	55	4	55	4	55	3	56	3	56	3
F-120	1	55	50	5	50	4	51	4	51	4	51	4	51	4	51	4	52	3	52	3	52	3	53	2
F-121	1	52	49	3	49	3	49	3	49	3	49	3	49	3	49	3	50	2	50	2	50	2	50	2
F-122	1	52	48	4	48	4	48	4	48	4	48	4	48	4	48	3	49	3	49	3	49	3	49	2
F-123 F-124	1	74 73	66	8 10	66	8 10	66	8 10	66 63	10	66 64	8 10	66 64	8 10	66 64	8 10	66 64	8	67 65	9	67 65	7 8	67 67	7
F-124 F-125	1	73	67	5	67	5	67	5	68	5	68	5	68	5	68	5	68	5	68	5	68	4	69	4
F-126	1	60	52	8	52	8	52	7	53	7	53	7	53	7	54	6	54	6	54	6	55	5	56	4
F-127	1	56	52	5	52	5	52	4	52	4	52	4	52	4	52	4	53	4	53	3	54	3	54	2
F-128	1	53	48	5	48	4	48	4	48	4	48	4	49	4	49	4	49	4	49	4	49	3	50	3
F-129 F-130	1	54 55	48 49	6	48 49	6	48 49	6	49 50	6	49 50	5 6	49 50	5 6	49 50	5	50 51	5	50 51	4 5	50 51	4	51 52	3
F-131	1	56	51	5	51	5	51	5	51	5	51	5	52	4	52	4	52	4	52	4	53	3	53	3
F-132	1	65	56	9	56	9	57	9	57	9	57	8	57	8	58	8	58	7	58	7	59	7	60	6
F-133	1	65	58	6	58	6	59	6	59	6	59	6	59	6	59	6	59	5	60	5	60	5	60	4
F-134	1	56	54	3	54	3	54	3	54	2	54	2	54	2	54	2	54	2	54	2	54	2	54	2
F-135 F-136	1	58 61	55 60	2	55 60	2	55 60	2	55 60	2	55 60	2	55 60	2	56 60	2								
F-137	1	58	58	1	58	1	58	1	58	1	58	1	58	1	58	0	58	0	58	0	58	0	58	0
F-138	1	57	57	0	58	0	58	0	58	0	58	0	58	0	58	0	58	0	58	0	58	0	58	0
F-139	1	57	57	0	57	0	57	0	57	0	57	0	57	0	57	0	57	0	57	0	57	0	57	0
F-140	1	66	66	0	66	0	66	0	66	0	66	0	66	0	66	0	66	0	66	0	66	0	66	0
F-141 F-142	1	54 55	54 54	0	54 54	0	54 54	0	54 54	0	54 54	0	54 54	0	54 54	0	54 54	0	54 54	0	54 54	0	54 54	0
F-143	1	53	52	2	52	2	52	2	52	2	52	2	52	2	52	2	52	2	52	2	52	1	52	1
F-144	1	54	51	2	52	2	52	2	52	2	52	2	52	2	52	2	52	2	52	2	52	2	52	2
F-145	1	52	49	3	49	3	49	3	49	3	49	3	49	3	50	3	50	3	50	2	50	2	50	2
F-146 F-147	1	51	48	3	48	3	48	3	48	3	48	3	48	3	48	3	48	3	48	2	48	2	49	2
F-147 F-148	1	53 55	53 55	0	53 55	0	53 55	0	53 55	0	53 55	0	53 55	0	53 55	0	53 55	0	53 55	0	53 55	0	53 55	0
F-149	1	56	56	1	56	1	56	1	56	1	56	1	56	1	56	1	56	1	56	1	56	1	56	1
F-150	1	55	54	1	54	1	54	1	54	1	54	1	54	1	54	1	55	1	55	1	55	1	55	1
F-151	1	59	58	0	58	0	59	0	59	0	59	0	59	0	59	0	59	0	59	0	59	0	59	0
F-152 F-153	1	58 54	58 53	0	58 53	0	58 53	0	58 53	0	58 53	0	58 53	0	58 53	0	58 53	0	58 53	0	58 53	0	58 53	0
F-154	1	56	56	0	56	0	56	0	56	0	56	0	56	0	56	0	56	0	56	0	56	0	56	0
F-155	1	54	54	0	54	0	54	0	54	0	54	0	54	0	54	0	54	0	54	0	54	0	54	0
F-156	1	53	53	0	53	0	53	0	53	0	53	0	53	0	53	0	53	0	53	0	53	0	53	0
F-157 F-158	1	53	52	0	52	0	52	0	52	1	52 54	1	52	0	52	0	52	0	52 54	0	52	0	52 54	0
F-158 F-159	1	55 52	54 52	0	54 52	0	54 52	0	54 52	0	54 52	0	54 52	0	54 52	0	54 52	0	54 52	0	54 52	0	54 52	0
F-160	1	52	52	0	52	0	52	0	52	0	52	0	52	0	52	0	52	0	52	0	52	0	52	0
F-161	1	51	51	0	51	0	51	0	51	0	51	0	51	0	51	0	51	0	51	0	51	0	51	0
F-162	1	53	53	0	53	0	53	0	53	0	53	0	53	0	53	0	53	0	53	0	53	0	53	0
F-163 F-164	1	55 57	55 57	0	55 57	0	55 57	0	55 57	0	55 57	0	55 57	0	55 57	0	55 57	0	55 57	0	55 57	0	55 57	0
F-164 otal Number of Impa	acted Units	16	5/	8	5/	8	5/	8	5/	8	3/	8	5/	8	3/	8	5/	8	5/	8	5/	8	5/	8
mpacted Receptors F		Insertion Loss		5		5		5		5		5		5		5		5		5		4		4
Percent of Impacted I	Receptors Receiving	g ≥ 5 dB(A) Insertion Loss		63%		63%		63%		63%		63%		63%		63%		63%		63%		50%		50%
		A) Reduction Criteria (Yes/No)?		Yes		Yes		Yes		Yes		Yes		Yes		Yes		Yes		Yes		Yes		Yes
		II Receptors $\geq 5 dB[A]$ Insertion on Loss of 7 dB(A) or more.	n Loss)	16 4		14		13		13		11		10		10		10		9		7		5
	eceiving an insertio		es/No)?	4 Yes	l	3 Yes		3 Yes		3 Yes		3 Yes												
	oss goal met for at I				1		1	Yes	I	Yes		Yes		Yes		Yes	ı				1		l	
7 dB(A) Insertion Lo		/DOT acoustical specifications		Yes		Yes				162		162		163		Yes		Yes		Yes		Yes		Yes
7 dB(A) Insertion Lo		/DOT acoustical specifications Square Footage of Opt		38449		35886		33322		30759		28196		25633		23069		20506		17943		15379		12816
7 dB(A) Insertion Lo		/DOT acoustical specifications	tted Receptor	38449 2403		35886 2563		33322 2563		30759 2366		28196 2563		25633 2563		23069 2307		20506 2051		17943 1994		15379 2197		12816 2563
s 7 dB(A) Insertion Lo Does Wall perform ac	ccording to FHWA/	/DOT acoustical specifications Square Footage of Opt Square Footage/Benefi	tted Receptor Reasonable?	38449 2403 No		35886		33322		30759		28196		25633		23069		20506		17943		15379		12816
s 7 dB(A) Insertion Lo Does Wall perform ac	ccording to FHWA/	/DOT acoustical specifications Square Footage of Opt Square Footage/Benefi ound levels may be different d	tted Receptor Reasonable?	38449 2403 No		35886 2563		33322 2563		30759 2366		28196 2563		25633 2563		23069 2307		20506 2051		17943 1994		15379 2197		12816 2563

### CNE F - BARRIER F6 - F9 HEIGHT EVALUATION

												HEIGHT EVAL												
												Predicted Future			in dBA									
Receptor Number	# of Dwelling Units		F6-F	9 30'	F6-F	9 28'	F6-F	9 26'	F6-	F9 24'	F6-F	9 22'	F6-F	9 20'	F6-F	9 18'	F6-I	F9 16'	F6-I	F9 14'	F6-F	F9 12'	F6-	F9 10'
		No Barrier	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	With Barrier (dBA)	Insertion Loss (IL)* (dBA)	With Barrier (dBA)	Insertion Loss (IL)* (dBA)
CNE F Barrier Syste	m F6 - F9																							
F-100 F-101	1	69 67	68	0	68 67	0	68 67	0	68 67	1	68 67	0	68 67	0	68	0	68 67	0	68 67	0	68 67	0	68 67	0
F-102	1	65	65	0	65	0	65	0	65	0	65	0	65	0	65	0	65	0	65	0	65	0	65	0
F-103	1	63	62	0	62	0	62	0	62	0	62	0	63	0	63	0	63	0	63	0	63	0	63	0
F-104 F-105	1 1	56 56	54 54	2	54 54	2	54 54	2	54 54	2	54 54	2	54 54	2	54 54	2	54 54	2	54 54	2	54 54	2	55 54	2
F-105	1	61	60	2	60	2	60	2	60	2	60	2	60	1	60	1	60	1	60	1	60	1	60	1
F-107	1	62	60	2	60	2	60	2	60	2	60	2	60	2	60	2	60	2	60	2	60	1	60	1
F-108	1	45	43	2	43	2	43	2	43	2	44	2	44	2	44	2	44	2	43	2	43	2	43	2
F-109 F-110	1	60 56	56 52	4	56 52	4	56 52	3	56 52	3 4	56 52	3 4	57 52	3	57 53	3	57 53	3	57 53	3	57 53	3	57 54	2
F-111	1	54	50	4	50	4	50	4	50	4	51	3	51	3	51	3	51	3	51	3	52	2	52	2
F-112	1	53	49	4	49	4	49	4	49	4	49	3	49	3	50	3	50	3	50	3	50	2	51	2
F-113	11	52	48	4	48	4	48	4	49	3	49	3	49	3	49	3	49	3	50	2	50	2	50	2
F-114 F-115	1	51 50	47 46	4	48 46	3	48 47	2	48 47	3 2	49 48	2	49 48	2 2	49 48	2								
F-116	1	72	66	6	66	6	66	6	66	6	66	6	66	6	66	6	66	6	67	6	67	5	67	5
F-117	1	71	60	11	60	11	60	11	61	11	61	10	61	10	61	10	62	9	62	9	63	8	64	7
F-118 F-119	1 1	61	55	5	56	5	56	5	56	5	56	4	57	4	57	4	57	4	58	3	58	3	58	2
F-119 F-120	1 1	59 55	53 50	5	53 50	5	54 51	5	54 51	5	54 51	5	54 51	4	55 51	4	55 52	3	55 52	3	56 52	3	56 53	3 2
F-121	1	52	48	4	48	4	48	4	49	3	49	3	49	3	49	3	49	3	49	3	50	2	50	2
F-122	1	52	47	5	47	5	47	5	47	4	47	4	48	4	48	4	48	4	48	3	49	3	49	3
F-123 F-124	1 1	74 73	66	10	66	8 10	66	8	66	10	66	8 10	66 64	8 10	66	10	66	8	65	8	67 65	7 8	67 67	7
F-124 F-125	1	73	67	10	67	10 5	67	5	68	5	68	10 5	68	10	68	5	68	5	68	5	68	4	69	4
F-126	1	60	52	8	52	8	52	8	52	8	53	7	53 52	7	53	7	54	6	54	6	55	5	56 54	4
F-127	1	56	51	5	51	5	51	5	51	5	51	5		5	52	4	52	4	52	4	53	3		2
F-128 F-129	1	53 54	47 47	6 7	47 47	5	47 47	5 7	47 47	5	48 48	5 7	48 48	5	48 48	5 6	48 49	4 5	49 49	4	49 50	4	49 50	3
F-130	1	55	48	8	48	8	48	7	48	7	49	7	49	6	49	6	50	6	50	5	51	5	52	4
F-131	1	56	49	7	50	6	50	6	50	6	50	6	51	5	51	5	51	5	52	4	52	4	53	3
F-132	1	65	55	10	56	10	56	10	56	9	56	9	57	9	57	8	58	8	58	7	59	7	59	6
F-133 F-134	1	65 56	57 51	8	57 51	8	57 51	8	57 52	7	58 52	4	58 52	7	58 52	4	58 52	6	59 53	6	59 53	6	60 53	3
F-135	1	58	53	5	53	5	53	5	53	5	53	5	53	4	54	4	54	4	54	3	55	3	55	3
F-136	1	61	57	4	57	4	57	4	57	4	57	4	57	4	58	3	58	3	58	3	59	2	59	2
F-137 F-138	1 1	58 57	54 54	5	54 54	4	54 54	4	54 54	3	55 54	4	55 55	4	55 55	3	55 55	3	56	3	56 56	2 2	56 56	2
F-138	1	57	53	4	53	4	53	4	54	4	54	4	54	3	54	3	54	3	55 54	3	55	3	55	2
F-140	1	66	60	6	60	6	60	6	60	6	60	6	60	6	61	5	61	5	61	5	61	5	62	4
F-141	1	54	50	4	51	4	51	4	51	4	51	4	51	4	51	3	51	3	51	3	52	3	52	2
F-142 F-143	1 1	55 53	51 49	4 5	51 49	4 5	52 49	4	52 49	3	52 49	3	52 49	3	52 50	3	52 50	3	52 50	3	53 50	3	53 51	3
F-144	1	54	49	4	50	4	50	4	50	4	50	4	50	4	50	4	50	3	50	3	51	3	51	3
F-145	1	52	47	6	47	6	47	6	47	5	47	5	47	5	48	5	48	4	48	4	49	4	49	3
F-146 F-147	1 1	51	45	5	45	5	46	5	46	5	46	5	46	5	46	4	47	4	47	3	47	4	48	3
F-147 F-148	1	53 55	49 51	4	49 51	4	49 51	4	49 51	4	49 51	4	50 52	4	50 52	4	50 52	3	50 52	3	50 52	3	51 53	3
F-149	1	56	51	5	51	5	52	5	52	5	52	5	52	4	52	4	52	4	53	4	53	3	54	3
F-150	1	55	51	4	51	4	51	4	51	4	51	4	51	4	52	4	52	4	52	3	52	3	53	2
F-151 F-152	1 1	59 58	55 55	3	55 55	3	55 55	3	55 55	3	56 55	3	56 55	3	56 55	3	56 56	3	56 56	3	56 56	2	57 56	2
F-153	1	54	50	4	50	4	50	4	50	4	50	4	50	4	50	4	50	4	51	3	51	3	52	2
F-154	1	56	53	2	54	2	54	2	54	2	54	2	54	2	54	2	54	2	54	2	54	1	54	1
F-155 F-156	1	54 53	52 51	3	52 51	2	52 51	2	52 51	2	52 51	2 2	52 51	2	52 51	2	52 51	2	53 51	2	53 52	2	53 52	1
F-157	1	53	50	2	50	2	50	2	50	2	51	2	51	2	51	2	51	2	51	2	51	2	51	1
F-158	1	55	53	2	53	2	53	2	53	2	53	2	53	1	53	1	53	1	53	1	54	1	54	1
F-159 F-160	1	52 52	52	1	52	1	52	1	52	1	52	1	52	1	52	1	52	1	52	0	52	0	52	0
F-160 F-161	1 1	52 51	51 50	1	51 50	1	51 50	1	51 50	1	51 50	1	51 50	1	51 50	1	51 50	1	51 50	1	51 50	1	51 51	1
F-162	1	53	53	1	53	1	53	1	53	1	53	1	53	1	53	1	53	1	53	0	53	0	53	0
F-163	1	55	54	1	54	1	54	1	54	1	54	1	54	0	54	0	54	0	55	0	55	0	55	0
F-164 Total Number of Imp	1 acted Units	57	57	0	57	0	57	0	57	0	57	0	57	0	57	0	57	0	57	0	57	0	57	0
Impacted Receptors I		Insertion Loss		6	1	6	1	6	l	6	1	6		6		6		6	1	6	1	5		4
Percent of Impacted	Receptors Receivin	g ≥ 5 dB(A) Insertion Loss		75%	1	75%		75%	l	75%	l	75%		75%		75%		75%		75%	l	63%		50%
		A) Reduction Criteria (Yes/No)?		Yes	l	Yes		Yes	l	Yes	l	Yes		Yes		Yes		Yes		Yes	l	Yes		Yes
		II Receptors ≥ 5 dB[A] Insertio on Loss of 7 dB(A) or more.	n Loss)	25 4	1	24 3		22 3	l	22 3	l	19 3		16 3		14 3		13 3		11 3	l	9		6
		on coss of 7 ав(A) of more. least one Impacted Receptor (Y	'es/No)?	Yes	l	Yes		Yes	l	Yes	l	Yes		Yes		Yes		Yes		Yes	l	Yes		Yes
		VDOT acoustical specifications		Yes		Yes		Yes		Yes		Yes		Yes		Yes		Yes		Yes		Yes		Yes
		Square Footage o				57598		53483		49369		45255		41141		37027		32913		28799		24684		20570
		Square Footage/B	enefitted Receptor Reasonable?		l	2400 No		2431 No	l	2244 No	l	2382 No		2571 No		2645 No		2532 No		2618 No	l	2743 No		3428 No
	Insertion Loss (IL) s	sound levels may be different d		140			1	140		140					1	140		110	1	140		140		
66	Indicates noise imp	pact (NAC only)																						
5	Indicates at least a	5 dBA benefit																						

Date: 1/12/22	
ž ,	007-029-128, B610, C502, P102, R202
•	o. STP-5A01(745) and STP-5A01(790)
UPC 52328	
County: Fairfax	
District: Route 7	
Barrier System ID: Barrier System G	1-G6
Community Name and/or CNE# CNE G	
Noise Abatement Category(s)  B, C and D	
Design phase: Final design	

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	24
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	24
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	100%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	96,303 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	24
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	54
d.	Total number of benefited receptors.	78
e.	Surface Area per benefited receptor unit. (ft²/BR)	1,235 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	Yes
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
a.	Length of the proposed noise barrier. (ft)	5,350 ft
b.	Height range of the proposed noise barrier. (ft)	18-18 ft
c.	Average height of the proposed noise barrier. (ft)	18.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$4,044,726
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) REASONABLE?	Yes
Additional Reasons for Decision:	

Date: Project No. and UPC:	11/1/19 State Project No. 007-029-128, B610, C502, P102, R202 Federal Project No. STP-5A01(745) and STP-5A01(790) UPC 52328
County:	Fairfax
District:	Route 7
Barrier System ID:	Barrier System G8-G9
Community Name and/or CNE#	CNE G
Noise Abatement Category(s)	B, C
Design phase:	Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	16
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	15
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	94%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	Yes
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	26,678 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	15
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	13
d.	Total number of benefited receptors.	28
e.	Surface Area per benefited receptor unit. (ft²/BR)	953 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	Yes
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
	Length of the proposed noise barrier. (ft)	1,906 ft
b.	Height range of the proposed noise barrier. (ft)	14-14 ft
c.	Average height of the proposed noise barrier. (ft)	14.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$1,120,476
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Is the Noise Barrier(s) WARRANTED?  Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) FEASIRI E?	
is the Noise Daniel(s) i Exsided:	No
Is the Noise Barrier(s) REASONABLE?	Yes
Additional Reasons for Decision:	dymin a high
Barriers impact the 100 year floodplain in this area resulting in safety issues by restricting flowater events. Therefore it is not recommended that the barriers be built.	ow during nigh

Date: Project No. and UPC:	1/12/22  State Project No. 007-029-128, B610, C502, P102, R202  Federal Project No. STP-5A01(745) and STP-5A01(790)  UPC 52328
County:	Fairfax
District:	Route 7
Barrier System ID:	Barrier System G10-G13
Community Name and/or CNE#	CNE G
Noise Abatement Category(s)	В
Design phase:	Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	20
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	20
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	100%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	44,649 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	20
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	10
d.	Total number of benefited receptors.	30
e.	Surface Area per benefited receptor unit. (ft²/BR)	1,488 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	Yes
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
a.	Length of the proposed noise barrier. (ft)	2,591 ft
b.	Height range of the proposed noise barrier. (ft)	13-18
c.	Average height of the proposed noise barrier. (ft)	17.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$1,875,258
f.	Barrier Material	NA
3	Community Desires Related to the Barrier	
	Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) REASONABLE?	Yes
Additional Reasons for Decision:	

Date: Project No. and UPC:	11/1/19 State Project No. 007-029-128, B610, C502, P102, R202 Federal Project No. STP-5A01(745) and STP-5A01(790) UPC 52328
County:	Fairfax
District:	Route 7
Barrier System ID:	Barrier System G14-G16
Community Name and/or CNE#	CNE G
Noise Abatement Category(s)	B, C, and D
Design phase:	Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	3
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	3
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	100%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	12,831 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	3
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	1
d.	Total number of benefited receptors.	4
e.	Surface Area per benefited receptor unit. (ft²/BR)	3,208 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	No
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	No
2	Additional Noise Barrier Details	
a.	Length of the proposed noise barrier. (ft)	801 ft
b.	Height range of the proposed noise barrier. (ft)	16-16 ft
c.	Average height of the proposed noise barrier. (ft)	16.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$538,902
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be	
	reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) REASONABLE?	No
Additional Reasons for Decision:	

Date: Project No. and UPC:	1/12/22 State Project No. 007-029-128, B610, C502, P102, R202 Federal Project No. STP-5A01(745) and STP-5A01(790) UPC 52328
County:	Fairfax
District:	Route 7
Barrier System ID:	Barrier System H2-H11
Community Name and/or CNE#	CNE H
Noise Abatement Category(s)	B, C and D
Design phase:	Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	20
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	18
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	90%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	61,772 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	18
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	24
d.	Total number of benefited receptors.	42
e.	Surface Area per benefited receptor unit. (ft²/BR)	1,471 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	Yes
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
	Length of the proposed noise barrier. (ft)	3,901 ft
b.	Height range of the proposed noise barrier. (ft)	15-16 ft
c.	Average height of the proposed noise barrier. (ft)	16.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$2,594,424
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Yes
Yes
Yes

Date:	11/1/19
Project No. and UPC:	State Project No. 007-029-128, B610, C502, P102, R202
	Federal Project No. STP-5A01(745) and STP-5A01(790)
	UPC 52328
County:	Fairfax
District:	Route 7
Barrier System ID:	Barrier I2
Community Name and/or CNE#	CNE I
Noise Abatement Category(s)	В
Design phase:	Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was	
	issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	5
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	5
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	100%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	10,852 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	5
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	2
d.	Total number of benefited receptors.	7
e.	Surface Area per benefited receptor unit. (ft²/BR)	1,550 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	Yes
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
a.	Length of the proposed noise barrier. (ft)	835 ft
b.	Height range of the proposed noise barrier. (ft)	13-13
c.	Average height of the proposed noise barrier. (ft)	13.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$455,784
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) REASONABLE?	Yes
Additional Reasons for Decision:	

Project No. and UPC: State Project No. 007-029-128, B610, C502, P102, R202 Federal Project No. STP-5A01(745) and STP-5A01(790) UPC 52328	
County: Fairfax	
District: Route 7	_
Barrier System ID: Barrier System I4-I6	
Community Name and/or CNE# CNE I	
Noise Abatement Category(s) B	
Design phase: Final design	

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was	
	issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	8
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	8
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	100%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	16,654 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	8
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	4
d.	Total number of benefited receptors.	12
e.	Surface Area per benefited receptor unit. (ft²/BR)	1,388 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	Yes
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
a.	Length of the proposed noise barrier. (ft)	1,041 ft
b.	Height range of the proposed noise barrier. (ft)	16-16
c.	Average height of the proposed noise barrier. (ft)	16.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$699,468
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not	
	desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) REASONABLE?	Yes
Additional Reasons for Decision:	

Date: Project No. and UPC:	11/1/19 State Project No. 007-029-128, B610, C502, P102, R202 Federal Project No. STP-5A01(745) and STP-5A01(790) UPC 52328
County:	Fairfax
District:	Route 7
Barrier System ID:	Barrier System J2-J3,K1-K4
Community Name and/or CNE#	CNE J, and K
Noise Abatement Category(s)	B, C, E, D
Design phase:	Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was	
	issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	-
1	Impacted receptor units	
a.	Number of impacted receptor units:	15
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	14
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	93%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	49,494 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	14
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	27
d.	Total number of benefited receptors.	41
e.	Surface Area per benefited receptor unit. (ft²/BR)	1,207 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	Yes
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
a.	Length of the proposed noise barrier. (ft)	3,094 ft
b.	Height range of the proposed noise barrier. (ft)	16-16
c.	Average height of the proposed noise barrier. (ft)	16.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$2,078,748
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) REASONABLE?	Yes
Additional Reasons for Decision:	

Date: Project No. and UPC:	11/1/19 State Project No. 007-029-128, B610, C502, P102, R202 Federal Project No. STP-5A01(745) and STP-5A01(790) UPC 52328
County:	Fairfax
District:	Route 7
Barrier System ID:	Barrier System L1-L5
Community Name and/or CNE#	CNE L
Noise Abatement Category(s)	В
Design phase:	Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	4
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	3
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	75%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	11,693 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	3
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	1
d.	Total number of benefited receptors.	4
e.	Surface Area per benefited receptor unit. (ft²/BR)	2,923 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	No
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
a.	Length of the proposed noise barrier. (ft)	974 ft
b.	Height range of the proposed noise barrier. (ft)	11-13
c.	Average height of the proposed noise barrier. (ft)	12.2 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$491,106
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the	
	reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) REASONABLE?	No
Additional Reasons for Decision:	

County: Fairfax  District: Route 7  Barrier System ID: Barrier System L6-L8  Community Name and/or CNE# CNE L	Date: Project No. and UPC:	11/1/19 State Project No. 007-029-128, B610, C502, P102, R202 Federal Project No. STP-5A01(745) and STP-5A01(790) UPC 52328
Barrier System ID: Barrier System L6-L8	County:	Fairfax
	District:	Route 7
Community Name and/or CNE# CNE L	Barrier System ID:	Barrier System L6-L8
	Community Name and/or CNE#	CNE L
Noise Abatement Category(s) B, C and D	Noise Abatement Category(s)	B, C and D
Design phase: Final design	Design phase:	Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	2
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	2
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	100%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	9,703 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	2
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	2
d.	Total number of benefited receptors.	4
e.	Surface Area per benefited receptor unit. (ft²/BR)	2,426 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	No
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
a.	Length of the proposed noise barrier. (ft)	852 ft
b.	Height range of the proposed noise barrier. (ft)	10-12
c.	Average height of the proposed noise barrier. (ft)	11.5 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$407,526
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) REASONABLE?	No
Additional Reasons for Decision:	

Date: Project No. and UPC:	11/1/19 State Project No. 007-029-128, B610, C502, P102, R202 Federal Project No. STP-5A01(745) and STP-5A01(790) UPC 52328
County:	Fairfax
District:	Route 7
Barrier System ID:	Barrier System N1-N3
Community Name and/or CNE#	CNE N
Noise Abatement Category(s)	B and D
Design phase:	Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	10
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	9
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	90%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	23,132 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	9
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	6
d.	Total number of benefited receptors.	15
e.	Surface Area per benefited receptor unit. (ft²/BR)	1,542 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	Yes
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
	Length of the proposed noise barrier. (ft)	1,577 ft
b.	Height range of the proposed noise barrier. (ft)	12-15
c.	Average height of the proposed noise barrier. (ft)	14.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$971,544
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) REASONABLE?	Yes
Additional Reasons for Decision: Existing Barrier (UPC 82135) is Included in the Square Footage and length	

# Note: Not all questions apply depending on the design phase which may cause differing answers between preliminary and final design phase. Answers to the questions may change depending on the design phase of the project. Date: Date: Project No. and UPC: State Project No. 007-029-128, B610, C502, P102, R202 Federal Project No. STP-5A01(745) and STP-5A01(790) UPC 52328

County: Fairfax
District: Route 7

Barrier System ID: Barrier System N4

Community Name and/or CNE# CNE N

Noise Abatement Category(s) B

Design phase: Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was	
	issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
	_	No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
	<u>-</u>	Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	1
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	1
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	100%
d.	Is the percentage 50 or greater?	Yes
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	5,427 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	1
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	0
d.	Total number of benefited receptors.	1
e.	Surface Area per benefited receptor unit. (ft²/BR)	5,427 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	No
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	Yes
2	Additional Noise Barrier Details	
a.	Length of the proposed noise barrier. (ft)	301 ft
b.	Height range of the proposed noise barrier. (ft)	18
c.	Average height of the proposed noise barrier. (ft)	18.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$227,934
f.	Barrier Material	NA
3	Community Desires Related to the Barrier	
	Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	Yes
Is the Noise Barrier(s) REASONABLE?	No
Additional Reasons for Decision:	

Date:	11/1/19
Project No. and UPC:	State Project No. 007-029-128, B610, C502, P102, R202
	Federal Project No. STP-5A01(745) and STP-5A01(790)
	UPC 52328
	-
County:	Fairfax
District:	Route 7
Barrier System ID:	Barrier System Existing Wall
Community Name and/or CNE#	CNE N
Noise Abatement Category(s)	В
Design phase:	Final design

	Warranted	
1 a.	Community Documentation (if applicable) Date community was permitted. (Per 23CFR 772 this is the date the building permit was	
	issued).	NA
b.	Date of approval for the Categorical Exclusion (CE), Record of Decision (ROD), or Finding of No Significant Impact (FONSI):	NA
c.	Does the date in 1.a precede the date in 1.b? If yes, proceed to Warranted Item 2. If no, consideration of noise abatement is not warranted. Proceed to "Decision" block and answer "no" to warranted question. As the reason for this decision, state that "Community was permitted after the date of approval of CE, ROD, or FONSI, as appropriate."	
		No
2	Criteria requiring consideration of noise abatement	
a.	Project causes design year noise levels to approach or exceed the Noise Abatement Criteria?	
		Yes
b.	Project causes a substantial noise increase of 10 dB(A) or more?	No

	Feasibility	
1	Impacted receptor units	
a.	Number of impacted receptor units:	10
b.	Number of impacted receptor units receiving 5 dB(A) or more insertion loss (IL):	0
c.	Percentage of impacted receptor units receiving 5 dB(A) or more IL	0%
d.	Is the percentage 50 or greater?	No
2	Will placement of the noise barrier cause engineering or safety conflicts, e.g drainage issues or site distance issues?	No
3	Will placement of the noise barrier restrict access to vehicular or pedestrian travel?	No
4	Will placement of the noise barrier conflict with existing utility locations?	No

	Reasonableness	
1	Surface Area (Square foot)-Benefit Factors	
a.	Surface Area (Total square foot) of the proposed noise barrier. (ft <sup>2</sup> )	4,607 SF
b.	Impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	0
c.	Non-impacted noise sensitive receptor(s) receiving 5 dB(A) IL or more.	1
d.	Total number of benefited receptors.	1
e.	Surface Area per benefited receptor unit. (ft²/BR)	4,607 SF/BR
f.	Is (1e) less than or equal to the maximum square feet per benefited receptor (MaxSF/BR) value of 1600?	No
g.	Does the barrier provide an IL of at least 7 dB(A) for at least one impacted receptor in the design year?	No
2	Additional Noise Barrier Details	
	Length of the proposed noise barrier. (ft)	307 ft
b.	Height range of the proposed noise barrier. (ft)	15
c.	Average height of the proposed noise barrier. (ft)	15.0 ft
d.	Cost per square foot. (\$/ft <sup>2</sup> )	\$42/SF
e.	Total Barrier Cost (\$)	\$193,494
f.	Barrier Material	NA
3	Community Desires Related to the Barrier  Do at least 50 percent of the benefited receptor unit owner(s) and renters desire the noise barrier? If yes, continue to "decision" block. If no, the barrier can be considered not to be reasonable. Proceed to "decision" block and answer "no" to reasonableness question. As the reason for this decision, state that "The majority of the impacted receptor unit owners do not desire the barrier."	

Decision	
Is the Noise Barrier(s) WARRANTED?	Yes
Is the Noise Barrier(s) FEASIBLE?	No
Is the Noise Barrier(s) REASONABLE?	No
Additional Reasons for Decision: Existing Barrier is not considered Feasible for the impacts within CNE N due to the Route 7	
project. Therefore modification to the existing barrier is warranted and will be studied as a res	sult

APPENDIX F - TNM FILES

TNM Files for this project can be downloaded at the following address:

 $\underline{https://terracon.sharefile.com/d-s4c019e31a7804ff6a9031b799941ed35}$ 

# APPENDIX G -NOISE REPORT GUIDANCE AND ACCOUNTABILITY CHECKLIST

# VIRGINIA DEPARTMENT OF TRANSPORTATION NOISE REPORT GUIDANCE AND ACCOUNTABILITY CHECKLIST

**VERSION 3.0** 

This checklist is not an inclusive document that accounts for all projects. However this guidance checklist outlines the most common items that will be reviewed during VDOT's review process. This checklist follows guidance set forth in VDOT's Highway Traffic Noise Manual.

Checked Items are Required Preliminary Final Design

UPC:
Completed By:

Date:

106689/109790 Skelly and Loy/W Kaufell 11/05/2019 N/A D This Item has been verified by the document writer
This item is "Not/Applicable" to this project
This Item is Project Dependent

#### 1.0 TITLE PAGE

- 1.1 X V Report is Appropriately Named, with Correct Project Limits, Project Number(s), UPC(s) (Universal Project Code), and Submission Date
- **1.2 X** ✓ Person Performing the Noise Analysis is Prequalified in the State of Virginia

### 2.0 TABLE OF CONTENTS (TOC)

2.1 X - Items listed in TOC are Accurately Numbered, Including the Report Sections, Tables, Figures, Graphics, and Appendices

#### 3.0 EXECUTIVE SUMMARY

- 3.1 X Brief Project Description provided with Project Location Information
- 3.2 X Summary of the Number (and sound level ranges) of Impacts for Existing, No-Build (if applicable), and the Future Design Year
- 3.3 X Noise Abatement Summary and Barrier Analyses Summary (If Future Design Year Impacts are Predicted)
- 3.4 X ✓ "Conversely..." Statement Added
- **3.5 X** ✓ ✓ Construction Noise Summary
- 2. Discussion of Futher Noise Abatement Considerations during Final Design eg. Rail noise, Aviation noise, Reflected Noise from Existing or Proposed Barriers / Retaining Walls, Commitments for further evaluation based on new design information, Alternatives to proposed noise barrier placement. . .

### 4.0 INTRODUCTION

4.1 X Discussion of the Project Description of the Proposed Project. Should include the Project Limits, Number of Proposed Lanes and/or Proposed

Checked	nary	sign	UPC:	106689/109790	×	This Item has been verified by the document writer
Items are	imir	De	Completed By:	Skelly and Loy/W Kaufell	N/A	This item is "Not/Applicable" to this project
Required	Prel	Final	Date:	10/10/2018	D	This Item is Project Dependent
		F				

iviodification, Lane volutins etc . . .

4.2 X - Discussion of the History of the Project, Background, Future Design Year, Specific Pertanent Project Details, Including the Preferred Alternative and other Road Improvements.

Checked Items are Required		Preliminary	Final Design	UPC: Completed By: Date:	106689/109790 Skelly and Loy/W Kaufell 10/10/2018	N/A D	This Item has been verified by the document writer This item is "Not/Applicable" to this project This Item is Project Dependent				
4.3											
4.4	X	D	D	- Additional NEPA docur	mentation (If Necessary - Documents to sup	oport an older ROD	or Date of Public Knowledge)				
5.0	MET	HOD	OLO	GY							
5.1	X	✓	✓	- FHWA and State Police	y Discussion and Compliance Regulations						
5.2	X	✓	✓	- Sound Level Metrics D	efined						
5.3	X	<b>√</b>		- NAC Defined							
5.4	X	<b>√</b>		- Definiton of Noise Imp							
5.5		✓	✓	- Analysis Proceedure D	efined						
5.6	X	✓	✓	- TNM Model Version D	efined and Program Overview Description ខ្	given					
	Sour	ce of I	Mode	l Inputs Documented							
5.7	X	✓	✓	- Discussion of the Sour	ce of Design Files / Typical Sections/ Profile	s / Cross Sections, o	or Study Corridor Limits if Engineering is not Available				
5.8	X	✓	✓	- Discussion of Traffic Vo	olumes / Speeds / Truck %'s						
5.9	X	✓	✓	- Document the Source	of Survey Information						
5.10	X	<b>X</b> D - Additional Data (Existng or Proposed Retaining Walls, Existing Noise Barriers or Berms, GIS Layers and/or Supplemental Elevation Data)									
6.0	EXISTING NOISE ENVIRONMENT										
6.1	NOISE MONITORING										
6.1.1	X - Noise Monitoring Methodology is Clearly Defined										
6.1.2	X	✓	<ul> <li>✓ - The Date(s) of Monitoring are Documented</li> </ul>								
6.1.3	X	✓	✓	- Type of Meter is Noted and Pertainent Calibration Information is Included							

Checked	nary	sign	UPC:	106689/109790	*	This Item has been verified by the document writer
Items are	imir	l De	Completed By:	Skelly and Loy/W Kaufell	N/A	This item is "Not/Applicable" to this project
Required	Pre	Fina	Date:	10/10/2018	D	This Item is Project Dependent

**6.1.4 X** ✓ · Number of Sites (Short-term or Long-term) are Identified and Located on Figure

Checked Items are Required		Preliminary	Final Design	UPC: Completed By: Date:	106689/109790 Skelly and Loy/W Kaufell 10/10/2018	N/A D	This Item has been verified by the document writer This item is "Not/Applicable" to this project This Item is Project Dependent				
6.1.5	X	X - Documentation of Noise Monitoring Data Sheets and other monitoring factors such sampling interval, weather									
6.1.6	X	✓	✓	- Table and Discussion of	of Ambient Noise Monitoring Results and	Required Sample Text	Regarding Monitoring				
6.1.7	X	✓	✓	- Table and Discussion o	of Noise Validation Results						
6.2	UND	EVELC	PED	LANDS AND PERMITTI	ED DEVELOPMENTS						
6.2.1	X	✓	✓	- "Undeveloped Lands a	and Permitted Developments" Sample Tex	kt Added					
6.2.2	X	✓	✓	- Documentation of the	Coordination Dates and Contact Informa	tion for the Undevelo	ped Lands and Permitted Developments Search				
6.3	СОМ	MON	NOIS	SE ENVIRONMENT (CN	E) DETERMINATION						
6.3.1	X	✓	✓	- Are all Noise Sensitive	Receptors within at least 500 feet of the	Proposed Edge of Pav	rement Considered for Evaluation?				
6.3.2	X	✓	✓	- Discussion of Existing	Land Uses for each CNE						
6.3.3	X	✓	✓	- Are all non noise sensi	itive land uses addressed in the report (re	easons why they are no	ot noise sensitive)?				
6.3.4	X	✓	✓	- CNE's Boundaries Loca	ated on Figure						
6.4	WOR	RST NO	DISE I	HOUR							
6.4.1	X	✓	✓	- The Worst Noise Hour	selected needs to be the same for ALL ro	padways. Review to er	nsure this is accurate.				
6.4.2	X - Discussion of the Selection of the Worst Noise Hour										
6.4.3	X	X - Was 24-Hour (Long Term Monitoring) Utilized to Determine the Worst Noise Hour									
6.4.4	<b>X</b> D - State if Multiple Sets of TNM runs were Created / Modeled to Determine the Worst Noise Hour (or were there dual worst noise hours)										

Checked	74.0	ıaı y sign	UPC:	106689/109790	*	This Item has been verified by the document writer
Items are	: <u>:</u>	l De	Completed By:	Skelly and Loy/W Kaufell	N/A	This item is "Not/Applicable" to this project
Required	2	ina	Date:	10/10/2018	D	This Item is Project Dependent
		4				

**6.4.5 X D D** - Were other Factors Considered for the Selection of the Worst Noise Hour

### 6.5 RECEPTOR IDENTIFICATION AND NAC CATEGORIZATION

If NAC A's are present, is the Criteria met and the Items Listed Below are Discussed:

6.5.1 D Serenity and Quiet - The site under consideration meets the serenity and quiet criterion if the current Leq noise level does not approach or exceed the Activity Category A Noise Abatement Criterion (NAC) during any period when serving its intended purpose.

			-								
Checked		Preliminary	Final Design	UPC:	106689/109790		×	This Item has been verified by the document writer			
Items are		imi	II De	Completed By:	Skelly and Loy/W Kaufell		N/A	This item is "Not/Applicable" to this project			
Required		Pre	Fina	Date:	10/10/2018		D	This Item is Project Dependent			
6.5.2		D	D	Public Need - The site	under consideration provides an importa	nt benefit o	of the publi	c visiting or using the site due to its historical, religious,			
				cultural, or natural sign	nificance						
6.5.3		D	D	Intended Purpose - Is t	he Preservation of Serenity and Quiet Es	sential to Co	ontinue to	Serve its Intended Purpose			
6.5.4		D	D	- Frequent Human Use -	· Can the public can access the site during	g all times w	hen it is av	vailable and able to serve its intended purpose?			
6.5.5		D	D		ng Documentation Included						
0.5.5											
	If NA	C B's	are pi	resent, is the Criteria r	net and the Items Listed Below are D	iscussed:					
6.5.5	X	D	D	- Are the Number of Red	ceptors Equal to or Representative to a N	lumber of D	welling Un	its			
6.5.6	X	D	D	- Are there Multi-floor F	Residential Units and do they have Outdo	or Use Area	ıs				
6.5.7	X	D	D	- Are Outdoor Use Area	s (Balconies) Identified and Discussed						
	If NA	C C's	are pi	esent. is the Criteria n	net and the Items Listed Below are D	iscussed:					
6 5 0			•								
6.5.8	X	D	D	- Are the Outdoor Use A	reas Documented for Each of the Identif	ied Recepto	ors				
6.5.9	X	D	D	- Was the "Grid system"	Used and Shown on Figures for Recreati	onal Areas,	Trails, Cam	npgrounds, Cemeteries, etc			
	If NA	C D's	are p	resent, is the Criteria r	net and the Item Listed Below is Disc	cussed:					
6.5.10	X	D	D	- Discuss the Building M	aterials and Interior Reduction Factor for	r each Ident	ified Recep	otor			
	If NA	C E's	are pr	esent, is the Criteria n	ent, is the Criteria met and the Item Listed Below is Discussed:						
6.5.11	X	D	D	- Are Outdoor Use Area	s Identified and Discussed						
6.5.12	X	D	D	- If "No", Text Should be	e Provided that the Land Use was Identific	ed but not E	Evaluated d	lue to the Lack of Outdoor Use			
	Histo	ric Pr	opert	ies							
6.5.13		D	D	- Discuss if any Section 2	106 (Historic) Properties were Identified						
6.5.14		D	D	- Discuss if any Section 4	4(f) Properties were Identified						
0.5.17		_	_	= 12 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2							

Checked Items are Required		Preliminary	Final Design	UPC: Completed By: Date:	106689/109790 Skelly and Loy/W Kaufell 10/10/2018	N/A D	This Item has been verified by the document writer This item is "Not/Applicable" to this project This Item is Project Dependent		
6.5.15		D	D	- If Section 4(f) Properti	es are Identified, Does it Constitute a "Cons	tructive Use" Dete	rmination		

### 6.6 MODELED EXISTING ENVIRONMENT

- **6.6.1 X** ✓ **D** Are Existing and Future Design Years Stated
- **6.6.2 X D** Are Existing Noise Barriers Present within the Proposed Project Area
- **6.6.3 X D D** If Existing Noise Barriers are Present, Does the Project Involve In-Kind Barrier Replacement
- **6.6.4 X** ✓ ✓ Discussion of the Overall Numbers of Existing Condition Impacts and Sound Level Ranges (all CNEs)
- **6.6.5 X** ✓ Discussion of the Determination and Identification of Noise Impacts (by CNE under Existing Condition)
- **6.6.6 X** ✓ **D** Existing Noise Environment discussion

### 7.0 FUTURE NOISE ENVIRONMENT

### 7.1 MODELED FUTURE ENVIRONMENT

- **7.1.1 X ✓** Is there Documentation why a No-Build Condition evaluation was/wasn't warranted?
- 7.1.2 | X | D D Discussion of the Overall Numbers of No-Build Condition Impacts and Sound Level Ranges (all CNEs)
- 7.1.3 | X | D D Discussion of the Determination and Identification of Noise Impacts (by CNE under No-Build Condition)
- 7.1.4 X Discussion of the Overall Numbers of Build Condition Impacts and Sound Level Ranges (all CNEs)
- 7.1.5 X V Discussion of the Determination and Identification of Noise Impacts (by CNE under Build Condition)
- **7.1.6 X V D** Comparison of existing and future total noise levels for all identified receptors
- **7.1.7 X ✓** Future Noise Environment Discussion
- **7.1.8** | **X** | ✓ ✓ Table of Predicted Noise Levels (By CNE)

### 7.2 NOISE ABATEMENT DETERMINATION

7.2.1 X - Alternative Abatement Measures Discussion

Checked	ıary	sign	UPC:	106689/109790		×	This Item has been verified by the document writer
Items are	imir	l De	<b>Completed By:</b>	Skelly and Loy/W Kaufell		N/A	This item is "Not/Applicable" to this project
Required	rel	ina	Date:	10/10/2018		D	This Item is Project Dependent
	4	ш			•		

Checked	nary	sign	UPC:	106689/109790	×	This Item has been verified by the document writer
Items are	imi	l De	Completed By:	Skelly and Loy/W Kaufell	N/A	This item is "Not/Applicable" to this project
Required	Pre	Final	Date:	10/10/2018	D	This Item is Project Dependent

**7.2.2 X** ✓ • Was VDOT's Single Receptor Methodology Utilized?

#### **WARRANTED CRITERIA**

- **7.2.3 X** ✓ ✓ Is Warranted Criteria Defined?
- **7.2.3.1 X** ✓ ✓ NAC Impact Definition ("Approach or Exceed") Provided
- **7.2.3.2 X** ✓ Substantial Increase Impact Definiton Provided
- 7.2.3.3 X · · · Has the NAC for Each Evaluated Land Use Category been Defined

#### **FEASIBILITY CRITERIA**

- **7.2.4 X** ✓ Is Feasibility Defined?
- 7.2.4.1 X Included definition regarding "Are at least 50% of the impacted receptors predicted to experience at least a 5dB(A) benefit?"
- **7.2.4.2 X** ✓ Included definition regarding "Is the barrier able to be constructed?"

#### **REASONABLENESS CRITERIA**

- **7.2.5 X** ✓ ✓ Is Reasonableness Defined?
- **7.2.5.1 X** ✓ · Included definition regarding "Noise Reduction Design Goals"
- **7.2.5.2** ★ Included definition regarding "Cost-effectiveness"
- **7.2.5.3 X ✓** Included definition regarding "The Viewpoints of the Benefited Receptors"

#### NOISE BARRIER EVALUATION

- 7.2.6 X Barrier Documentation should Include: Discussion of Total Number of Impacts, Benefitted Impacts, Additional Benefits, Total Benefits, Feasibility, Reasonablity, Barrier Length, Range of Panel Heights, Barrier Location, Ground or Structure Mounted, Barrier Systems, etc. . .
- 7.2.7 X Reason for Barrier Placement, Barrier Termini, Barrier Location etc. . .

Checked	nary	sign	UPC:	106689/109790		×	This Item has been verified by the document writer
Items are	imir	l De	Completed By:	Skelly and Loy/W Kaufell		N/A	This item is "Not/Applicable" to this project
Required	Preli	Final	Date:	10/10/2018	•	D	This Item is Project Dependent

7.2.8 X ✓ - All Evaluated Barrriers shown on Figures
 7.2.9 X - Barriers were Optimized to Maximize Benefits while Minimizing Cost (Diminishing Returns)

Checked Items are Required		Preliminary	Final Design	UPC: Completed By: Date:	106689/109790 Skelly and Loy/W Kaufell 10/10/2018	N/A D	This Item has been verified by the document writer This item is "Not/Applicable" to this project This Item is Project Dependent			
7.2.10	Table was included that shows the Barrier name, Insertion Loss, Panel Height Range, Total Length, Total Surface Area, Total Benefits, Total sq.ft. / no. of benefits, Cost (for Planning Purposes Only)									
7.2.11	X	X - Table that shows the Sound Levels, Barrier Insertion Loss for each Receptor included in the Barrier Analysis								
7.2.12	X	D 🗸 - Table that shows the Approximate Stationing, Northing, Easting, Bottom and Top of barrier, Panel Heights by Segment								
7.2.13	X	D	D	- Does the Barrier (Systo	em) Work Independently or is it Depender	nt on Another Barrier	(Existing or Proposed)			
8.0	CON	CONSTRUCTION NOISE								
8.1	X	✓	✓	- Construction Noise Dis	scussion					
9.0	PUB	PUBLIC INVOLVEMENT PROCESS								
9.1	NOIS	E CO	МРАТ	IBLE CONTOURS						
9.1.1	X	✓	✓	- 66 dBA Contour Discus	ssion and Shown on Figure(s)					
9.1.2	X	D	D	- Discussion of Public In	volvement Efforts (including Community I	nformation Meetings	s, Individual Meetings, and Special Coordination)			
9.2	VOTI	NG PI	ROCE	EDURES						
9.2.1		✓	✓	- Voting Process Define	d?					
9.2.2			✓	- How many / when we	re Certified Letters Sent?					
9.2.3			✓	- What were the Voting	Results Related to Desire for a Barrier?					
9.2.4			✓	- Summary of Barrier Su	rvey Results and Comments?					
9.2.5		✓ - How many Surveys were Unresponsive or Undeliverable?								
9.2.6	✓ - Voting Graphic showing the Results of the Barrier Survey?									
9.2.7	✓ - Were there any Special Abatement Commitments / Acoustic Profiles/ Aesthetics Considerations									

Checked Items are Required	Preliminary	Final Design	UPC: Completed By: Date:	106689/109790 Skelly and Loy/W Kaufell 10/10/2018		X N/A D	This Item has been verified by the document writer This item is "Not/Applicable" to this project This Item is Project Dependent	
9.2.8	✓ - Is this an Addendum Report with Revised Impact / Barrier Results							

Design **Preliminary** UPC: 106689/109790 X This Item has been verified by the document writer Checked N/A Items are **Completed By:** Skelly and Loy/W Kaufell This item is "Not/Applicable" to this project Final Required 10/10/2018 D This Item is Project Dependent Date: 10.0 **OTHER CONSIDERATIONS** 10.1 - Absorptive or Reflective Noise Barriers Proposed? D 10.2 - Was Reflection Noise Considered? D 10.3 - Was Structure Noise Considered? D 10.4 - Was Rail or Aviation Noise Considered? 11.0 **APPENDICES** 11.1 - List of References - List of Preparers / Reviewers 11.2 - Traffic Data 11.3 11.4 Noise Monitoring Field Logs Warranted, Feasible, Reasonable, Worksheets 11.5 Alternative Mitigation Measures Response Form from Project Manager 11.6 11.7 Other Site Sketches of Monitored Locations, Noise Meter Printouts, Noise Meter Calibration Reports, Pertinent Correspondance 11.8 - TNM Certification Certificates - Noise Report Guidance and Accountability Form 11.9 12.0 **TNM RUNS** 

Report, However a Copy of the Printed Modeling Information shall be Supplied Upon Request

12.1

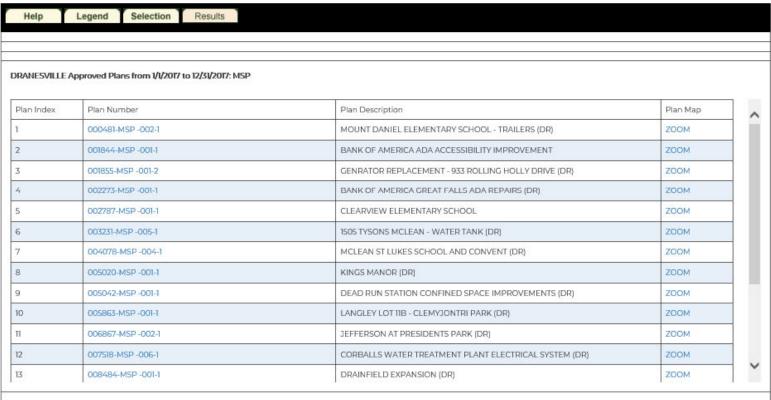
Actual TNM Runs (Electronic Files) must be Submitted for Review with Report, TNM Output Tables are Not Required for Inclusion into the

Checked	ıary	sign	UPC:	106689/109790	×	This Item has been verified by the document writer
Items are	imir	l De	Completed By:	Skelly and Loy/W Kaufell	N/A	This item is "Not/Applicable" to this project
Required	rel	ina	Date:	10/10/2018	D	This Item is Project Dependent
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### 13.0 GENERAL

**13.1 X** ✓ • Figures were Developed in Accordance with VDOT's Noise Report Development and Guidance Document

APPENDIX H - FAIRFAX COUNTY PERMITTED LANDS AS OF ROD



McKee Beshers
Wildlife MGT Area

Wheaton
Glenmont

Sterling
Sterling
Sugarland Run

Potomac

Reston

VIRGINIA

Bethesda

Arlington

Arlington

Arlington

Arlington

Arlington

Arlington

Arlington

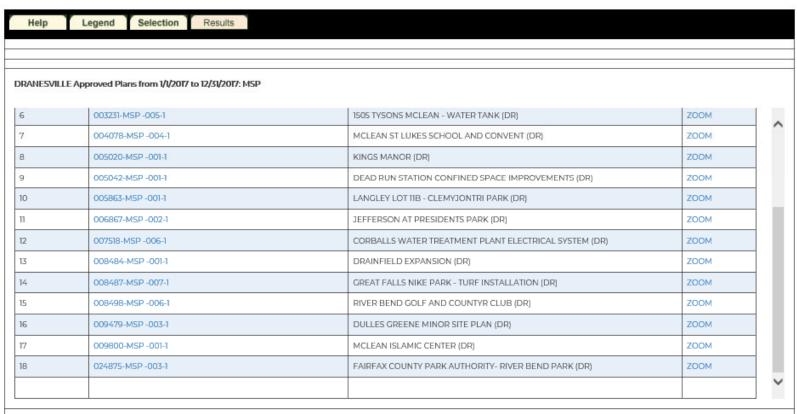
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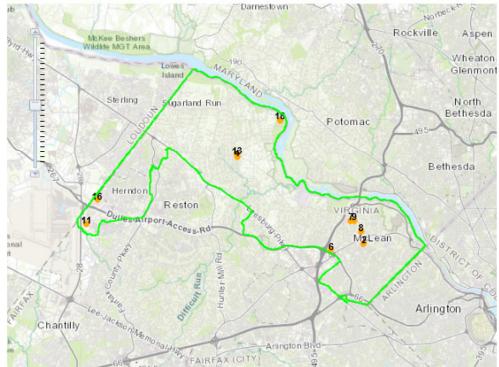
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**GOVERNMENT** 

# Search By Magisterial District

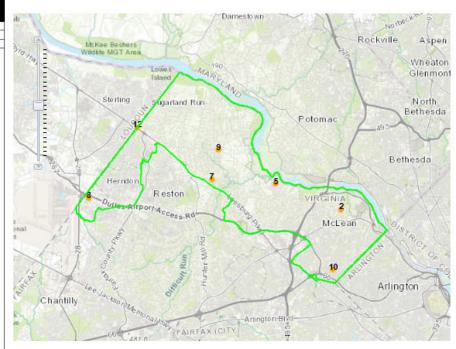




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Plan Index	Plan Number	Plan Description	Plan Map
1	000481-SP -002-2	MOUNT DANIEL ELEMENTARY SCHOOL (DR)	ZOOM
2	000525-SP -001-2	LANGLEY HIGH SCHOOL - RENOVATION + ADDITION (DR)	ZOOM
3	001504-SP -006-2	ARROWBROOK CENTRE LANDBAYS BI & CI (DR)	ZOOM
4	003728-SP-003-2	FLEETWOOD RESIDENTIAL [DR]	ZOOM
5	005158-SP -008-2	MADEIRA SCHOOL OVAL RENOVATION (DR)	ZOOM
6	005518-SP -041-2	WOODLAND PARK WEST TOWNS AND CONDOMINIUMS [DR]	ZOOM
7	005860-SP -002-3	FOLEY/ WALKER ROAD (DR)	ZOOM
8	006848-SP -013-2	DULLES STATION PARCEL 5A	ZOOM
9	021868-SP -001-2	TD BANK - 9901 GEORGETOWN PIKE (DR)	ZOOM
10	025205-SP -001-2	HAYCOCK ELEMENTARY SCHOOL (DR)	ZOOM
11	025351-SP -001-2	HERNDON HIGH SCHOOL (DR)	ZOOM
12	025379-SP -001-2	POPEYES AT LEESBURG (DR)	ZOOM



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PRANESVILLE	Approved Plans from 1/1/2017 to 12/31/2017: S	E	
Plan Index	Plan Number	Plan Description	Plan Map
1	SE 2013-DR-001	DRIVE-IN FINANCIAL INSTITUTION IN THE C-8 DISTRICT WITH	ZOOM
2	SE 2014-DR-033	USES IN FLOODPLAIN	ZOOM
3	SE 2014-DR-043	TO PERMIT OFFICE	ZOOM
4	SE 2014-DR-052	RESIDENTIAL CLUSTER SUBDIVISION	ZOOM
5	SE 2014-DR-057	CLUSTER SUBDIVISION	ZOOM
6	SE 2015-DR-005	HOME CHILD CARE FACILITY	ZOOM
7	SE 2015-DR-016	ELECTRICALL-POWERED REGIONAL RAIL TRANSIT FACILITIES	ZOOM
8	SE 2015-DR-028	ELECTRICALLY POWERED REGIONAL RAIL TRANSIT FACILITIES	ZOOM
9	SE 2017-DR-002	WAIVER OF CERTAIN SIGN REGULATIONS TO PERMIT AN INCREAS	ZOOM
10	SE 2017-DR-003	DRIVE-IN FINANCIAL INSTITUTION AND WAIVER OF MINIMUM L	ZOOM



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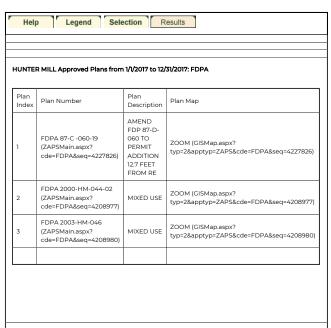


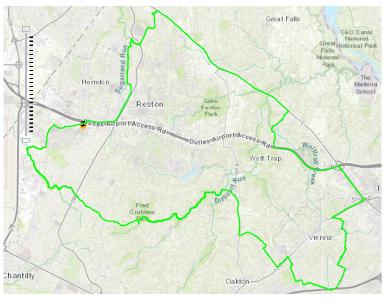
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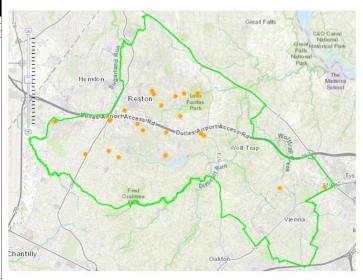
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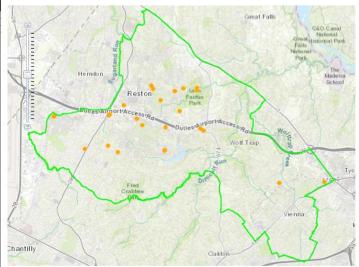
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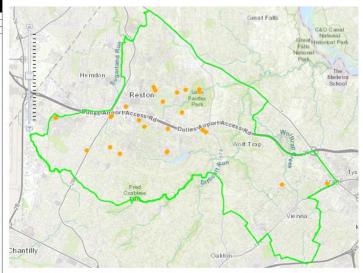
HUNTER MILL I	n Process Plans from 1/1/2017 to 12/31/2017: MSP		
		Two services	12
Plan Index	Plan Number	Plan Description	Plan Map
1	000491-MSP -001-2	ISLAND WALK RENOVATION/MODERNIZATION	ZOOM
2	001463-MSP -004-1	VERIZON WIRELESS SOUTH LAKES HS (HM)	ZOOM
3	001463-MSP -005-2	SOUTH LAKES HIGH SCHOOL (HM)	ZOOM
4	001463-MSP -007-1	LANGSTON HUGHES MIDDLE SCHOOL (HM)	ZOOM
5	002075-MSP -001-1	UNITARIAN UNIVERSALIST CHURCH IN RESTON (HM)	ZOOM
6	002615-MSP -005-1	RESTON BLK 6 SEC 913 - 11493 SUNSET HILLS RENOV (HM)	ZOOM
7	003129-MSP -001-1	SYSTEM RELIABILITY IMPROVMENTS FOX MILL PUMP STATION	ZOOM
8	003292-MSP -004-1	LAKE FAIRFAX BUSINESS CENTER BUILDING 6 (HM)	ZOOM
9	003741-MSP -005-1	GODDARD AT TYSONS (HM)	ZOOM
10	003899-MSP -001-1	PARKRIDGE CENTER	ZOOM
n	003899-MSP -003-1	PARKRIDGE II SITE IMPROVEMENTS RESTON SEC 910 (HM)	ZOOM
12	003900-MSP-004-3	CAMPUS COMMONS (HM)	ZOOM
13	004053-MSP -004-2	FCPA LAKE FAIRFAX GROUPED ADA SHELTER B (HM)	ZOOM



	1111		
IUNTER MI	LL. In Process Plans from 1/1/2017 to 12/31/2017: MSP		
14	004278-MSP -003-I	TYCON COURTHOUSE DEVELOPMENT (HM)	ZOOM
15	004486-MSP-001-1	LAKE FAIRFAX PARK PICNIC SHELTERS	ZOOM
16	004599-MSP -004-1	LOCKHEED MARTIN (HM)	ZOOM
17	004599-MSP -006-1	RESTON, SEC. 904 (HM)	ZOOM
18	004847-MSP -001-1	KIDDIE ACADEMY (HM)	ZOOM
19	004890-MSP-006-2	RESTON SEC 912 BLK I (HM)	ZOOM
20	005226-MSP -001-2	LAKE ANNE ELEMENTARY SCHOOL RENOVATION (HM)	ZOOM
21	005482-MSP-003-1	RESTON METRO CENTER (HM)	ZOOM
22	005482-MSP -004-1	RESTON CROSSING (HM)	ZOOM
23	005482-MSP-005-1	2003 EDMUND HALLEY DR (HM)	ZOOM
24	005731-MSP -006-1	MEADOWLARK GARDENS PARKING (HM)	ZOOM
25	005734-MSP-001-2	RESTON FIRE STATION 25 TEMP STATION [HM]	ZOOM
26	006246-MSP -001-2	WOLFTRAP ELEMENTARY SCHOOL	ZOOM
27	006734-MSP -001-1	RESTON SEC 40, BLOCK IC (HM)	ZOOM



HUNTER MI	LL. In Process Plans from 1/1/2017 to 12/31/2017: MSP		
24	005731-MSP -006-1	MEADOWLARK GARDENS PARKING (HM)	ZOOM
25	005734-MSP -001-2	RESTON FIRE STATION 25 TEMP STATION (HM)	ZOOM
26	006246-MSP -001-2	WOLFTRAP ELEMENTARY SCHOOL	ZOOM
27	006734-MSP -001-1	RESTON SEC 40, BLOCK IC (HM)	ZOOM
28	007693-MSP -004-2	VILLAGE CENTER AT DULLES (HM)	ZOOM
29	007693-MSP -006-1	VILLAGE CENTER AT DULLES (HM)	ZOOM
30	007805-MSP -001-1	SHEEHY AUTOMOTIVE (HM)	ZOOM
31	008501-MSP -002-2	RENOVATION OF TYSONS TOWERS (HM)	ZOOM
32	009058-MSP -002-2	CARTER LAKE APARTMENTS (HM)	ZOOM
33	009348-MSP -001-1	RESTON, SEC, 93, BLK 2 [HM]	ZOOM
34	015795-MSP -001-2	RESTON SECTION 15 BLOCK 1 FAIRWAY POOL AND CLUBHSE (HM)	ZOOM
35	018335-MSP -002-2	RESTON ANIMAL HOSPITAL (HM)	ZOOM
36	018955-MSP -002-1	RN DRIVING RANGE (HM)	ZOOM

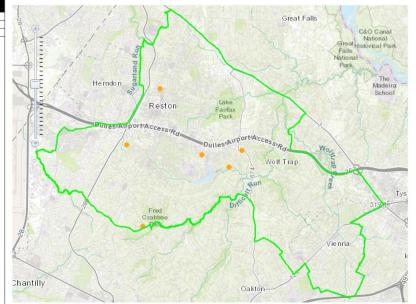


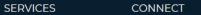


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# Search By Magisterial District

IUNTER MILL	In Process Plans from 1/1/2017 to 12/31/2017	:SP	
Plan Index	Plan Number	Plan Description	Plan Map
1	SP 2003-HM-026	HOME CHILD CARE FACILITY	ZOOM
2	SP 2004-HM-039	HOME PROFESSIONAL OFFICE	ZOOM
3	SP 2006-HM-069	TO PERMIT MODIFICATIONS TO THE LIMITATIONS ON THE KEEPI	ZOOM
4	SP 2009-HM-056	MODIFICATION TO THE LIMITATIONS ON THE KEEPING OF ANIMA	ZOOM
5	SP 2014-HM-152	HOME CHILD CARE FACILITY	ZOOM
6	SP 2015-HM-078	HOME CHILD CARE FACILITY	ZOOM
7	SP 2016-HM-108	REDUCTION IN CERTAIN YARD REQUIRMENTS TO PERMIT CONSTRU	ZOOM
8	SP 2017-HM-002	REDUCTION OF CERTAIN YARD REQUIREMENTS TO PERMIT CONSTR	ZOOM
9	SP 2017-HM-006	HOME CHILD CARE FACILITY	ZOOM
10	SP 2017-HM-017	REDUCTION IN MINIMUM YARD REQUIREMENTS BASED ON AN ERRO	ZOOM
11	SP 2017-HM-022	HOME CHILD CARE FACILTY	ZOOM
12	SP 2017-HM-032	ACCESSORY DWELLING UNIT	ZOOM
13	SP 2017-HM-081	REDUCTION OF CERTAIN YARD REQUIREMENTS TO PERMIT CONSTR	ZOOM

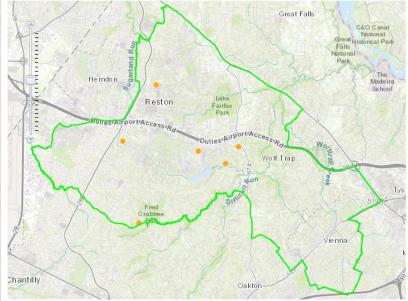




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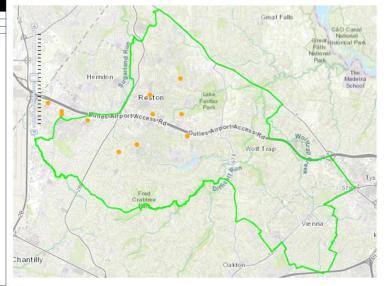
# Search By Magisterial District

IUNIERM	IILL In Process Plans from 1/1/2017 to 12/31/201	; 2h	
3	SP 2006-HM-069	TO PERMIT MODIFICATIONS TO THE LIMITATIONS ON THE KEEPI	ZOOM
4	SP 2009-HM-056	MODIFICATION TO THE LIMITATIONS ON THE KEEPING OF ANIMA	ZOOM
5	SP 2014-HM-152	HOME CHILD CARE FACILITY	ZOOM
6	SP 2015-HM-078	HOME CHILD CARE FACILITY	ZOOM
7	SP 2016-HM-108	REDUCTION IN CERTAIN YARD REQUIRMENTS TO PERMIT CONSTRU	ZOOM
8	SP 2017-HM-002	REDUCTION OF CERTAIN YARD REQUIREMENTS TO PERMIT CONSTR	ZOOM
9	SP 2017-HM-006	HOME CHILD CARE FACILITY	zоом
10	SP 2017-HM-017	REDUCTION IN MINIMUM YARD REQUIREMENTS BASED ON AN ERRO	ZOOM
11	SP 2017-HM-022	HOME CHILD CARE FACILTY	ZOOM
12	SP 2017-HM-032	ACCESSORY DWELLING UNIT	ZOOM
13	SP 2017-HM-081	REDUCTION OF CERTAIN YARD REQUIREMENTS TO PERMIT CONSTR	ZOOM
14	SP 2017-HM-112	REDUCTION IN MINIMUM YARD REQUIREMENTS BASED ON ERROR I	ZOOM
15	SP 2017-HM-113	HOME CHILD CARE FACILITY	ZOOM



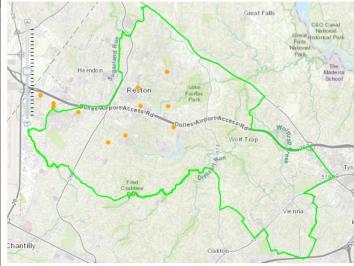


	n Process Plans from 1/1/2017 to 12/31/2017: SP P		
Plan Index	Plan Number	Plan Description	Plan Map
1	000365-SP -002-3	COLTS NECK BLOCK 1, SECTION 30, RESTON [HM]	ZOOM
2	000786-SP -013-2	SUNRISE SQUARE FORMALLY TI690 SUNRISE VALLEY DRIVE [HM]	ZOOM
3	000786-SP -014-1	SUNRISE VALLEY (HM)	ZOOM
4	000826-SP -OTI-2	RESTON EASTGATE (HM)	ZOOM
5	001504-SP -003-2	ARROWBROOK CENTRE PHASE 1 (HM)	ZOOM
6	001504-SP -004-2	ARROWBROOK CENTRE TRAIL SITE PLAN (HM)	ZOOM
7	002608-SP -003-2	RESTON SEC 87-1 REDEVELOPMENT (HM)	ZOOM
8	003488-SP -007-2	LINCOLN AT WIEHLE STATION	ZOOM
9	003729-SP -005-2	LOFTS AT RESTON STATION (HM)	ZOOM
10	003900-SP -023-2	SUNRISE OAK PROFESSIONAL CENTER (HM)	ZOOM
11	004599-SP -015-3	SUNRISE TECHNOLOGY PARK - CORESITE VA3 (HM)	ZOOM
12	004847-SP -005-3	PINECREST RESEARCH CENTER (HM)	ZOOM
13	005518-SP -030-1	TECHPOINTE WOODLAND PARK	ZOOM

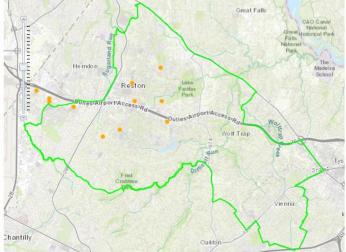




IUNTER MI	LL. In Process Plans from 1/1/2017 to 12/31/2017: SP F		
			P
14	005518-SP -043-2	WOODLAND PARK EAST INFRASTRUCTURE PLAN (HM)	ZOOM
15	005518-SP -044-2	WOODLAND PARK EAST BLK A (HM)	ZOOM
16	005518-SP -045-2	WOODLAND PARK EAST BLOCK B (HM)	ZOOM
17	005518-SP -046-1	WOODLAND PARK EAST BLCKS C AND D INFRASTRUCTURE [HM]	ZOOM
18	005518-SP -047-1	WOODLAND PARK EAST BLOCK C (HM)	ZOOM
19	005518-SP -048-1	FAIRFIELD AT WOODLAND PARK EAST BLOCK D (HM)	ZOOM
20	005518-SP -049-1	WOODLAND PARK EAST-URBAN RECREATION PARK (HM)	ZOOM
21	006039-SP -009-2	RESTON HOSPITAL CAMPUS (HM)	ZOOM
22	006092-SP -002-2	MARTIN LUTHER KING JR CHRISTIAN CHURCH [HM]	ZOOM
23	006279-SP -005-1	TYSONS WEST RETAIL [HM]	ZOOM
24	006848-SP -012-2	DULLES STATION - DULLES CORNER, BLDG D (HM)	ZOOM
25	007281-SP -003-2	RESTON SECTION 905 BLOCK 7 PRCL E2 & N2	ZOOM
26	007693-SP -045-1	FLORIS - CONSERVATORY FOR FINE ARTS (HM)	ZOOM
27	007693-SP -046-1	NORTHWEST COUNTY FLEMENTARY SCHOOL (HM)	ZOOM









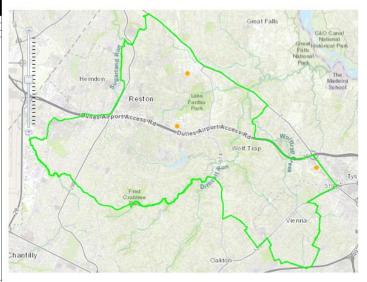


RESIDENTS

HUNTER MILL I	n Process Plans from 1/1/2017 to 12/31/2017: SE		
Plan Index	Plan Number	Plan Description	Plan Map
1	SE 2002-HM-009	TO PERMIT A PRIVATE SCHOOL OF GENERAL EDUCATION AND CHI	ZOOM
2	SE 2011-HM-010	HOME CHILD CARE FACILITY	ZOOM
3	SE 2014-HM-034	INCREASE IN FAR IN THE PTC DISTRICT TO PERMIT OFFICE AN	ZOOM
4	SE 2016-HM-020	ELECTRICALLY POWERED REGIONAL RAIL TRANSIT FACILITIES	ZOOM
5	SE 2016-HM-024	ASSISTED LIVING FACILITY	ZOOM
6	SE 2017-HM-010	RETAIL SALES ESTABLISHMENT IN AN INDUSTRIAL DISTRICT	ZOOM
7	SE 2017-HM-016	HOTEL AND INCREASE IN FAR	ZOOM
8	SE 2017-HM-030	INCREASE IN FAR	ZOOM
9	SE 2017-HM-031	WAIVER OF CERTAIN SIGN REGULATIONS	ZOOM

BUSINESS

GOVERNMENT

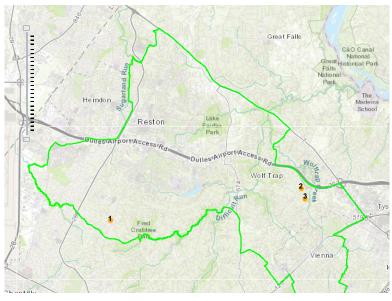


(/)

### Search By Magisterial District







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# MAP Detail



LDSnet Overview--[007339-SD -003-3]

Wednesday, October 30, 2019



Map Types:

ESRI Topopgraphic

#### New Tax Map#(s)

Grid No	Quad No	Double Circle No	Single Cir <b>(/)</b> e No	Lot No	Lot Suffix	Partial Indicator
012	1	21			В	YES
012	1	21		0004		YES
012	1	21		0002		YES
012	1	21		0005		YES
012	1	21			А	YES
012	1	21		0003		YES
012	1	21		0001		YES

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Support ADA Accessibility (https://www.fairfaxcounty.gov/topics/accessibility/)

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[that ps://www.Defæildaproceunt topics/languagetranslation/)

(http://www.tairfaxcountyeda.org/) Download Mobile App

Thit has the work of the private of

Commonwealth of Virginia (https://www.virginia.gov/)

USA.gov (https://www.usa.gov/)

LDInet Overview-[D07339-5D-003-5]

Please be advised that an approved plan does not indicate construction is ready to commence. Typically, a Land Disturbance Permit must be issued prior to a Pre-Construction Meeting. Please check the Outstanding Items to see if Approval Conditions must be met.

Select a Query:	
Distribution Status	
Handling Status	
Processing Status	
Fee Information	
Site Specific Options	
Related Submission	
Submission Sub-Type	
View GIS Map	
Bonds and Agreements	
Review Comment	
Let a man be	

Status	Outstanding Item	Porticipant
Site-Location	Related Submission	Submission ID

Wednesday, October 30, 2019

#### mintellustion renton

AND					
Dist Point	Dist Purpose	Assignee	Status	Date Sent	Action
PLAN CONTROL PROCESSING DP	ACCEPTANCE		DP FINAL	04/28/2014	PASS
PLAN CONTROL PROCESSING DP	INFORMATION ONLY		DP FINAL	11/18/2014	N/A
ADDRESS REVIEW DP	REVIEW		DP FINAL	04/29/2014	APPROVE
BOND ESTIMATE REVIEW DP	REVIEW	EWH03	DP FINAL	04/29/2014	APPROVE
BOND/PERMIT PACKAGE REVIEW DP	REVIEW	HFARA1	PENDING		
BOS DP	REVIEW		PENDING		
CONSERVATION DEPOSIT ESTIMATE REVIEW DP	REVIEW	EWHII3	DP FINAL	04/30/2014	APPROVE
FIRE MARSHAL DP	REVIEW		DPFINAL	06/25/2008	APPROVE
FUTURE CONSTRUCTION ESTIMATE REVIEW DP	REVIEW	HFARAT	PENDING		
GEO TECH REVIEW DP	REVIEW		PENDING		
HEALTH DEPARTMENT DP	REVIEW		DP FINAL	09/02/2008	APPROVE
INSPECTION FEE DP	REVIEW	AFRANK	DP FINAL	08/22/2014	APPROVE
INSPECTION FEE DP	REVIEW	EWHII3	DP FINAL	04/30/2014	APPROVE
OSDS DECISION DP	REVIEW	MBAIG1	DP FINAL	10/30/2014	APPROVE
PRO RATA SHARE DP	REVIEW	EWH03	DP FINAL	04/30/2014	APPROVE
PROFFER REVIEW DP	REVIEW		DP FINAL	07/21/2014	APPROVE
PROJECT APPROVAL DP	REVIEW	LCUNNI	DP FINAL	07/21/2014	REVIEW COMPLETE
SITE PERMITS PROCESSING DP	REVIEW		DISTRIBUTED	11/18/2014	
SITE REVIEW BR CHIEF DP	REVIEW	GMCLAU	DP FINAL	06/12/2014	APPROVE
SITE REVIEW DP	REVIEW	CMAVR2	DP FINAL	04/28/2014	APPROVE
SITE REVIEW DP	REVIEW	CMAVR2	DP FINAL	06/30/2014	APPROVE
STORM WATER MANAGEMENT BRICH DP	REVIEW		PENDING		
STORM WATER MANAGEMENT DP	REVIEW	ASANT2	PENDING		
STREET LIGHTS DP	REVIEW	LRATCH	DP FINAL	01/15/2008	APPROVE
URBAN FORESTRY DP	REVIEW	CHERWI	DP FINAL	01/15/2008	APPROVE
VDOT DISTRICT REVIEW DP	REVIEW		DP FINAL	03/03/2008	APPROVE
WA FAIRFAX WATER DP	REVIEW		DP FINAL	01/18/2008	APPROVE
WASTEWATER PLANNING AND MONITORING DIVISION	REVIEW	KCHILT	DP FINAL	04/29/2014	REVIEW NOT RORD

#### Life Cycle Status:

ıcs	Date Achieved
PROJECT COMPLETED	08/30/2018
REVISED	01/27/2016
REVISED	06/16/2015
REVISED	02/27/2015
APPROVED	11/07/2014
DISTRIBUTED TO BONDING	07/03/2014
DISTRIBUTED	04/28/2014
ACCEPTED	04/28/2014
SUBMITTED	04/28/2014
RECEIVED	04/28/2014

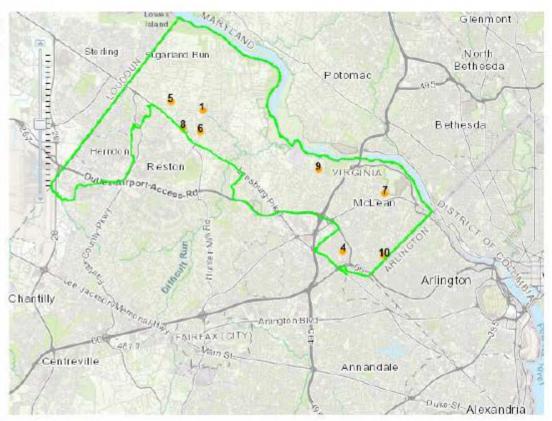
#### DRANES/ILLE Approved Plans from 1/1/2017 to 12/31/2017: SP P

Plan Index	Plan Number	Plan Description	Plan Map
1	000481-SP-002-7	MOUNT DANIEL ELEMENTARY SCHOOL (DR)	ZOOM
2	000525-SP-001-2	LANGLEY HIGH SCHOOL - RENOVATION + ADDITION (DR)	200M
3	D01504-5P-406-2	AFROWBROOK CENTRE LANDBAYS BL& CI (DR)	ZOOM
4	D03778-SP-003-2	FLEETWOOD RESIDENTIAL [DR]	ZOOM
5	D0515B-SP -008-2	MADEIRA SCHOOL OVAL RENOVATION (DR)	ZOOM
6	0055IB.SP -041-2	WOODLAND PARK WEST TOWNS AND CONDOMINIUMS [DR]	ZOOM
7	005860-SP-002-3	FOLEY/WALKER POAD (DR)	ZOOM
8	D06848-SP-D13-2	DULLES STATION PARCEL SA	ZOOM
9	021868-SP-001-2	TD BANK - 9001 GEORGETOWN PIKE (DR)	ZOOM
10	025205 SP :001-2	HAYCOCK ELEMENTARY SCHOOL (DR)	ZOOM
π	025351.SP -001-2	HERNDON HIGH SCHOOL (DR)	ZOOM
12	025379-SP-001-2	POPEYES ATLEESBURG (DR)	ZOOM



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	97.30 7.00			
DANESVILLE	Approved Plans from 1/1/2017 to 12/31/2017	:SD		
Plan Index	Plan Number	Plan Description	Plan Map	,
1	001089-5D -001-2	AULAKH SUBDIVISION (DR)	ZOOM	
2	001237-SD -001-2	MEHR FARMS (DR)	ZOOM	
3	001809-5D -002-2	JAMES A THOMPSON PROPERTY (DR)	ZDOM	
4	004344-SD-002-1	MID PIKE - 7150 PENGUIN PLACE LOT 16 (DR)	ZOOM	
5	004605-SD -001-2	OSBORNE PROPERTY (OR)	ZOOM	
6	005024-SD-001-2	1039 SPRINGVALE ROAD [DR]	ZOOM	
7	005863-SD -001-1	TIOI CHAIN BRIDGE ROAD (DR)	ZDOM	
8	007339-SD -003-3	MARKELL PROPERTY (DR)	ZOOM	
9	008868-SD -001-2	BULL NECK (DR)	ZOOM	
10	009176-SD -002-2	FRANKLIN PARK BLOCK 5 LOTS 57A & 58E (DR)	ZOOM	
11	025427-5D -001-2	SUMMER HILL PROPERTY	ZOOM	
12	025856-SD -001-2	RIVERMONT (DR)	ZOOM	





# **APPENDIX J**

ROUTE 7 WIDENING RESTONE AVENUE TO JARRET DRIVE UPC 99478 STATE PROJECT No. 007-029-942 and 007-029-225 FEDERAL PROJECT No.: STP-5A01(745) and STP-5A01(790) CONTRACT IS No. C00099478DB98

Project Number Barrier Name Barrier A2  (Include Permitted Developments)  NAC CATEGORY  NAC CATEGORY  Representative Responses Sent  Total Number of Representative Votes  Impacted and Benefited B 1 5 Not Impacted and Benefited C 1 5 Impacted and Benefited C 1 5 Impacted and Benefited D 0 0 0 Impacted and Benefited E 0 0 0 Impacted and Benefited D 0 0 0 Impacted Impacted D 0 0 0 0 0 Impacted Impacted D 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	UPC	10	6917 and 99478				
Total Number of Representative Responses Sent	Project Number			9-942	1st Mailin	g Summary	
Impacted and Benefited   B			Barrier A2				
Indicated Permitted Developments   NAC CATEGORY   Representative Responses   Sent   Sent   Representative Votes							
Not Impacted and Benefited	nclude Permitted Deve	:lopments)	NAC CATEGO	ORY	Representative Responses		
Impacted and Benefited C 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Impacted and Bene	efited	В		1	5	
Not Impacted and Benefited  Impacted and Benefited  D  O  O  Not Impacted and Benefited  D  O  O  O  Not Impacted and Benefited  E  O  O  O  O  O  O  O  O  O  O  O  O	Not Impacted and Be	nefited	В		13	36	5
Impacted and Benefited D O O O O O O O O O O O O O O O O O O	Impacted and Bene	efited	С		1	5	
Not Impacted and Benefited E 0 0 0 Impacted and Benefited E 0 0 0 Not Impacted and Benefited E 0 0 0  Potential Maximum Number of Weighted Votes 46  Number of Weighted Votes Cast YES NO Total 34 0 34  % of "Yes" % of "No" Votes (All Votes (All Votes (All Votes) Votes 73.9 0.0 26.1  % of "Yes" % of "No" Votes (Respondents (Respondents ) ) 100.0 0.0	Not Impacted and Be	nefited	С		0	0	
Impacted and Benefited E 0 0 0  Not Impacted and Benefited E 0 0 0  Potential Maximum Number of Weighted Votes 46  Number of Weighted Votes Cast YES NO Total 34 0 34  % of "Yes" % of "No" % of Votes (All Votes (All Votes (All Votes) Votes) Votes Yotes (Respondents	Impacted and Bene	efited	D		0	0	
Not Impacted and Benefited E 0 0  Potential Maximum Number of Weighted Votes 46  Number of Weighted Votes Cast 46  Number of Weighted Votes Cast 75 Total Outstanding Votes 75 Page 75			D		0	0	
Potential Maximum Number of Weighted Votes  46  Number of Weighted Votes Cast  YES NO Total 34 0 34  Wof "Yes" Wof "No" Wotes (All Votes (All Votes) Votes) Votes  73.9 0.0 26.1  Results in the box below should only be considered when all of the responses have been tallied					0		
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34 0 34  % of "Yes" % of "No" Votes (All Votes (All Votes) Votes)  73.9 0.0 26.1  Results in the box below should only be considered when all of the responses have been tallied  (Respondents (Respondents ) ) 100.0 0.0							
% of "Yes"  % of "No"  Votes (All Votes (All Votes)  Votes)  Votes  73.9					12	73.91	73
The Barrier Is Recommended for Construction	Votes) 73.9  % of "Yes" Votes (Respondents )	Votes) 0.0  % of "No" Votes (Respondents )	Votes 26.1	Results in t			n all of the
				т	he Barrier Is Recommended	for Construction	1

1100		20017 1001	70		
UPC		06917 and 994			
Project Number		9-225 and 0007		1st Mailin	g Summary
Barrier Name	Bar	rier B1-B5B and	d D1		
(Include Permitted Devel	opments)	NAC CA	TEGORY	Total Number of Representative Responses Sent	Total Maxiumum Number of Representative Votes
Impacted and Bene	fited		3	18	85
Not Impacted and Ber	nefited	l l	3	38	111
Impacted and Bene	fited	(	C	2	10
Not Impacted and Ber	nefited	(	<u> </u>	10	30
Impacted and Bene	fited	]	)	0	0
Not Impacted and Ber	nefited	[	)	1	1
Impacted and Bene	fited	ı	Ξ	0	0
Not Impacted and Ber	nefited			0	0
Number	237 of Weighted V	otes Cast		Number of Total	% Total Votes Cast / % Total
YES	NO	Total		Outstanding Votes	Actual Votes
130	14	144		93	<b>60.76</b> 60
130	14	144		33	00.70
% of "Yes" Votes (All Votes) 54.9	% of "No" Votes (All Votes) 5.9	% of Outstanding Votes 39.2			
% of "Yes"	% of "No"		Results in t	the box below should only be	considered when all of the
Votes	Votes			responses have been	tallied
(Respondents ) 90.3	(Respondents ) 9.7				
			1	he Barrier Is Recommended	for Construction
Versic	on 1.2				

UPC		1(	06917 and 9947	78		
Project Nui	mher		9-225 and 0007		1st Mailin	g Summary
Barrier Na			arrier C1 and C		130 Widning	5 Juninary
Barrier	arric		arrier er and e			
(Include Perr	mitted Deve	lopments)	NAC CA	TEGORY	Total Number of Representative Responses Sent	Total Maxiumum Number of Representative Votes
Impacte	ed and Bene	fited	E	3	23	105
	cted and Be		E	3	46	138
Impacte	ed and Bene	fited	(	2	0	0
Not Impa	cted and Be	nefited	(	2	0	0
Impacte	ed and Bene	fited		)	0	0
	cted and Be		]	)	0	0
Impacte	ed and Bene	fited	[		0	0
	cted and Be		E		0	0
	Number	Votes 243 of Weighted V	otes Cast		Number of Total	% Total Votes Cast / % Total
	YES	NO	Total		Outstanding Votes	Actual Votes
	202	6	208		35	<b>85.60</b> 85
	202	Ü	200			65.66
	% of "Yes" Votes (All Votes) 83.1	% of "No" Votes (All Votes) 2.5	% of Outstanding Votes 14.4			
9	% of "Yes" Votes	% of "No" Votes		Results in t	he box below should only be responses have been	
(Ri		(Respondents )			responses have been	Cancu
				Т	he Barrier Is Recommended	for Construction
	Versio	on 1.2				

UP	^	1(	06917 and 994	70		
Project N			9-225 and 0007		1st Mailin	g Summary
Barrier			rier D2 and E1		1st iviallin	g Summary
Barrier	Name	Ddl	Her DZ and E1	-E4		
(Include Pe	rmitted Deve	lopments)	NAC CA	TEGORY	Total Number of Representative Responses Sent	Total Maxiumum Number of Representative Votes
Impac	ted and Bene	fited	F	В	19	90
	acted and Be			В	27	75
	ted and Bene		(	 C	0	0
Not Imp	acted and Be	nefited	(		0	0
Impac	ted and Bene	fited	]	)	0	0
Not Imp	acted and Be	nefited	ו	D	0	0
Impac	ted and Bene	fited	E	E	0	0
Not Imp	acted and Be	nefited	E	E	0	0
<u> </u>   r		Votes 165			Number of Total	% Total Votos Cast / % Tatal
	YES	of Weighted V	otes Cast Total		Outstanding Votes	% Total Votes Cast / % Total Actual Votes
1 h	119	3	122		43	<b>73.94</b> 73
<u>-</u>	110	9				76.61
	% of "Yes" Votes (All Votes) 72.1	% of "No" Votes (All Votes) 1.8	% of Outstanding Votes 26.1			
	% of "Yes" Votes	% of "No" Votes		Results in t	he box below should only be responses have been	
		(Respondents ) 2.5				
				T	he Barrier Is Recommended	for Construction
	Versio	on 1.2				

Project Numb Barrier Nam Include Permit Impacted Not Impacted	ie	Barrie	-225 and 0007 r F1, F1B, F1C a		1st Mailin	g Summary	
Barrier Nam  Include Permit  Impacted  Not Impacted	ie		r F1, F1B, F1C a	and F2			
Impacted Not Impacte	ted Develo	opments)					
Impacted Not Impacte	ted Develo	opments)					
Not Impacte			NAC CAT	TEGORY	Total Number of Representative Responses Sent	Total Maxiumu Representa	
	and Benef	fited	Е	3	4	20	0
Impacted	d and Ben	refited	E	3	3	9	
	and Benef		(	C	3	1.	5
Not Impacte			(	0	0	C	)
Impacted				)	0	C	
Not Impacte				)	0	C	)
Impacted			E	<u> </u>	0	C	)
Not Impacte	d and Ben	refited	E	<u> </u>	0	C	)
	Number o	of Weighted Vo	otes Cast  Total		Number of Total Outstanding Votes	% Total Votes Actual	
	24	0	24		20	54.55	54
% c	tes (All /otes) 54.5 of "Yes" /otes	Votes (All Votes) 0.0  % of "No" Votes (Respondents	Outstanding Votes 45.5	Results in t	the box below should only be responses have been		en all of the
1	100.0	0.0		,	The Barrier Is Recommended	for Construction	n

UPC		10	UPC 106917 and 99478						
Project Nu	ımber	0007-029	9-225 and 0007-029-942		1st Mailin	g Summary			
Barrier N	lame		Barrier F3						
(Include Per	mitted Devel	opments)	NAC CAT	ΓEGORY	Total Number of Representative Responses Sent		um Number of ative Votes		
Impacted and Benefited		В		12	$\epsilon$	50			
	acted and Ber		E	3	15	4	12		
	ted and Bene		(		0		0		
Not Impa	acted and Ber	nefited	(	<u> </u>	0		0		
	ed and Bene				0		0		
	acted and Ber				0		0		
	ted and Bene		E		0		0		
Not Impa	acted and Ber	nefited	E		0		0		
		of Weighted Vo			Number of Total Outstanding Votes		Cast / % Total		
	YES	NO	Total						
	96	0	96		6	94.12	94		
-	% of "Yes" Votes (All Votes) 94.1  % of "Yes" Votes Respondents ) 100.0	% of "No" Votes (All Votes)  0.0  % of "No" Votes (Respondents )  0.0	% of Outstanding Votes 5.9	Results in t	the box below should only be responses have beer		en all of the		
				,	he Barrier Is Recommended	for Constructio	on		
	Versio	on 1.2							

			-		
UPC		06917 and 9947			
Project Number	0007-029	9-225 and 0007	-029-942	1st Mailin	g Summary
Barrier Name		Barrier G1-G6			
(Include Permitted Deve	lopments)	NAC CAT	regory	Total Number of Representative Responses Sent	Total Maxiumum Number of Representative Votes
Impacted and Benefited		В	1	24	115
Not Impacted and Be		В		58	162
Impacted and Bene		C		0	0
Not Impacted and Be		0		1	3
Impacted and Bene				0	0
Not Impacted and Be				1	1
Impacted and Bene		E		0	0
Not Impacted and Be		E		0	0
	Votes 281	r of Weighted			
Number YES	of Weighted V NO	otes Cast Total		Number of Total Outstanding Votes	% Total Votes Cast / % Total Actual Votes
188	5	193		88	<b>68.68</b> 68
% of "Yes" Votes (All Votes) 66.9  % of "Yes" Votes (Respondents ) 97.4	% of "No" Votes (All Votes)  1.8  % of "No" Votes (Respondents )  2.6	% of Outstanding Votes 31.3		the box below should only be responses have been The Barrier Is Recommended	tallied
Versi	on 1.2				

UPC		1(	06917 and 9947	78		
Project Num	her		9-225 and 0007		1st Mailin	g Summary
Barrier Nan			Barrier G10-G13		±3¢ iviaiiii;	5 Junimary
Burrier War	iic .		differ G10 G1.			
(Include Permi	itted Devel	opments)	NAC CA	TEGORY	Total Number of Representative Responses Sent	Total Maxiumum Number of Representative Votes
Impacted	Impacted and Benefited E		3	23	100	
Not Impact				3	13	30
	and Bene		(	 C	0	0
Not Impact			(	 C	0	0
	l and Bene		[	)	0	0
Not Impact				)	0	0
	l and Bene		[		0	0
Not Impact			E		0	0
	Number	Votes 130 of Weighted V	otes Cast		Number of Total	% Total Votes Cast / % Total
<u> </u>	YES	NO	Total		Outstanding Votes	Actual Votes
	109	3	10tai		18	<b>86.15</b> 86
	103	3	112		10	00.13
Vo	of "Yes" otes (All Votes) 83.8	% of "No" Votes (All Votes) 2.3	% of Outstanding Votes 13.8			
	of "Yes"	% of "No"		Results in t	he box below should only be	
	Votes	Votes			responses have been	tallied
(Res	97.3	(Respondents ) 2.7				
				Т	he Barrier Is Recommended	for Construction
	Versio	on 1.2				

UPC	106917 and 99478
Project Number	0007-029-225 and 0007-029-942
Barrier Name	Barrier H2-H11

### 2nd Mailing Summary

(Include Permitted Developments)	NAC CATEGORY	Total Number of Representative Responses Sent	Total Maxiumum Number of Representative Votes
Impacted and Benefited	В	16	70
Not Impacted and Benefited	В	29	78
Impacted and Benefited	С	6	30
Not Impacted and Benefited	С	0	0
Impacted and Benefited	D	0	0
Not Impacted and Benefited	D	1	1
Impacted and Benefited	E	0	0
Not Impacted and Benefited	E	0	0

Potential Maximum Number of
Weighted Votes

Number of Weighted Votes Cast						
YES NO Total						
106 8 114						

% of "Yes"	% of "No"	% of
Votes (All	Votes (All	Outstandi
Votes)	Votes)	ng Votes
59.2	4.5	36.3

% of "Yes"	% of "No"
Votes	Votes
(Responde	(Responde
nts)	nts)
93.0	7.0

Number of Total
Outstanding Votes

65

Number of Total
Total Votes Cast / %
Total Actual Votes

65

63.69
63

Results in the box below should only be considered when all of the responses have been tallied

The Barrier Is Recommended for Construction

Version 1.2

UPC		06917 and 994				
Project Number	0007-02	9-225 and 0007	'-029-942	1st Mailin	g Summary	
Barrier Name		Barrier I2				
(Include Permitted	(Include Permitted Developments) NAC CAT			Total Number of Representative Responses Sent	Total Maxiumum N	
Impacted and	Renefited		3	5	25	
Not Impacted and			3	3	6	
Impacted and			 C	0	0	
Not Impacted an			 C	0	0	
Impacted and		ı	)	0	0	
Not Impacted an	d Benefited	1	)	0	0	
Impacted and	Benefited	I	E	0	0	
Not Impacted an	d Benefited		=	0	0	
Num	Votes 31  The properties of Weighted Votes	lotes Cart		Number of Total	% Total Votes Casi	t / % Total
YES	NO	Total		Outstanding Votes	% Total Votes Cast Actual Vot	
22	0	22		9	70.97	70
% of "You Votes ( Vote	All Votes (All Votes)  0.0  es" % of "No" Votes ents (Respondents)	% of Outstanding Votes 29.0	Results in t	he box below should only be responses have been		ll of the
			T	he Barrier Is Recommended	for Construction	
	ersion 1.2					

UPC		10	UPC 106917 and 99478				
Project Numbe	er	0007-029	9-225 and 0007-029-942		1st Mailing Summary		
Barrier Name			Barrier 14-16				
(Include Permitte	ed Devel	opments)	NAC CA	ΓEGORY	Total Number of Representative Responses Sent		um Number of ative Votes
Impacted and Benefited		E	3	9	4	40	
Not Impacted	and Ber	nefited	E	3	5		12
Impacted a			(		0		0
Not Impacted			(	<u> </u>	0		0
Impacted a					0		0
Not Impacted					0		0
Impacted a			E		0		0
Not Impacted	and Ber	nefited	E		0		0
		52 of Weighted Vo			Number of Total Outstanding Votes		Cast / % Total
	'ES	NO	Total				
	40	0	40		12	76.92	76
Vote Vo 70 % of Vo (Respo	"Yes" es (All ites) 6.9 "Yes" otes ondents ) 00.0	% of "No" Votes (All Votes)  0.0  % of "No" Votes (Respondents )  0.0	% of Outstanding Votes 23.1	Results in	the box below should only be responses have beer		nen all of the
				,	The Barrier Is Recommended	for Construction	on
	Versio	on 1.2					

UPC	106917 and 99478
Project Number	0007-029-225 and 0007-029-942
Barrier Name	Barrier J2-J3 and K1-K4

### 2nd Mailing Summary

(Include Permitted Developments)	NAC CATEGORY	Total Number of Representative Responses Sent	Total Maxiumum Number of Representative Votes
Impacted and Benefited	В	6	30
Not Impacted and Benefited	В	18	48
Impacted and Benefited	С	8	40
Not Impacted and Benefited	С	8	24
Impacted and Benefited	D	0	0
Not Impacted and Benefited	D	2	2
Impacted and Benefited	E	0	0
Not Impacted and Benefited	E	0	0

Potential Maximum Number of Weighted Votes

144

Number of Weighted Votes Cast					
YES	NO	Total			
41	20	61			

% of "Yes"	% of "No"	% of	
Votes (All	Votes (All	Outstandi	
Votes)	Votes)	ng Votes	
28.5	13.9	57.6	

% of "Yes"	% of "No"	
Votes	Votes	
(Responde	(Responde	
nts)	nts)	
67.2	32.8	

Number of Total % Total Votes Cast / % Total Actual Votes 83 42.36 42

Results in the box below should only be considered when all of the responses have been tallied

The Barrier Is Recommended for Construction

Version 1.2

UPC		1(	06017 and 004	70		
Project Num				1st Mailing Summary		
Barrier Nar		0007-029-225 and 0007- Barrier N1-N3		-029-942	1st Mailing Summary	
Dairiei Nai	ille		Dairiei N1-N3			
(Include Permitted Developments)		NAC CATEGORY		Total Number of Representative Responses Sent	Total Maxiumum Number of Representative Votes	
Impacted	Impacted and Benefited		F	3	9	45
Not Impact				3	7	18
	d and Bene		(		0	0
Not Impact				<u> </u>	0	0
	d and Bene			)	0	0
Not Impact			D		0	0
	d and Bene		E		0	0
Not Impact			E		0	0
	Number	Votes 63 of Weighted V	otes Cast		Number of Total	% Total Votes Cast / % Total
	YES	NO	Total		Outstanding Votes	Actual Votes
	46	3	49		14	<b>77.78</b> 77
	of "Yes" lotes (All Votes) 73.0 of "Yes" Votes spondents )	% of "No" Votes (All Votes)  4.8  % of "No" Votes (Respondents )  6.1	% of Outstanding Votes 22.2		he box below should only be responses have been the Barrier Is Recommended	tallied
	Versic	on 1.2				

# **APPENDIX K**

ROUTE 7 WIDENING RESTONE AVENUE TO JARRET DRIVE UPC 99478 STATE PROJECT No. 007-029-942 and 007-029-225 FEDERAL PROJECT No.: STP-5A01(745) and STP-5A01(790) CONTRACT IS No. C00099478DB98



### Route 7 Corridor Improvements Project & Brown's Chapel Cemetery (Parcel 085)

Jennifer Thomas < jennifer.thomas@shirleycontracting.com>

Fri, Jun 12, 2020 at 3:51 PM

Reply-To: jennifer.thomas@shirleycontracting.com

To: virginia.rita@gmail.com

Cc: Jeffrey Austin <a href="mailto:com">jaustin@shirleycontracting.com">jaustin@shirleycontracting.com</a>, "Kuntz, Steven" <skuntz@dewberry.com</a>, Md Rahman <md.rahman@vdot.virginia.gov</a>, Charles Pruitt <charles.pruitt@vdot.virginia.gov</a>, Richard Gutridge <mi>richard.gutridge@vdot.virginia.gov</a>, Ryan Marrah <ryan.marrah@shirleycontracting.com</a>

Mr. and Mrs. Rita:

Per my conversation with Mr. Rita today, attached is a marked-up copy of the plan sheet for the area near Brown's Chapel Cemetery that shows the locations of the noise barriers along the parcel, as well as the widths of the grass areas between the roadway and the shared use path, and between the shared use paths and the noise barriers. Also shown are the widths of the entrances that will be reconstructed as part of the improvements along Route 7.

If you have any questions, please feel free to contact me at any time. Thanks!

Best regards,

Jennifer

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Jennifer A. Thomas | Public Relations Specialist SHIRLEY CONTRACTING COMPANY, LLC

45240 Business Court, Suite 100 | Dulles, VA | 20166 p. 571-447-7742

jennifer.thomas@shirleycontracting.com

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Route 7 Corridor Improvements Project Hotline: 833-777-7411

Route 7 Corridor Improvements Project Web Site: ConnectRoute7.org



346 - BROWNS CHAPEL CEMETERY PLAN SHEETS.pdf 1252K



### Route 7 Corridor Improvements Project: Proposed Noise Barrier Question

Jennifer Thomas < jennifer.thomas@shirleycontracting.com>

Mon, Feb 10, 2020 at 5:11 PM

Reply-To: jennifer.thomas@shirleycontracting.com

To: jerrycmailey@comcast.net

Cc: Md Rahman <md.rahman@vdot.virginia.gov>, Charles Pruitt <charles.pruitt@vdot.virginia.gov>, Richard Gutridge <richard.gutridge@vdot.virginia.gov>, "Kuntz, Steven" <skuntz@dewberry.com>, Jeffrey Austin <jaustin@shirleycontracting.com>, "Muchenje, Lovejoy 'LJ' P.E. (VDOT)" <Lovejoy.Muchenje@vdot.virginia.gov>

Mr. Mailey:

Thank you for sending in your noise barrier response form to the Route 7 Corridor Improvements Project team. Please see the answer (below in red) to the question that you submitted with the form:

1. Will the end of the barrier at Reston Parkway taper downwards or end abruptly at the height of the barrier? To maximize the noise mitigation that the proposed noise barriers provide, the barriers will not taper down towards the ground at the ends.

If you have any additional questions, please feel free to contact me.

Thanks so much!

Best regards,

Jennifer

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Jennifer A. Thomas | Public Relations Specialist SHIRLEY CONTRACTING COMPANY, LLC 45240 Business Court, Suite 100 | Dulles, VA | 20166 p. 571-447-7742 jennifer.thomas@shirleycontracting.com shirleycontracting.com

Route 7 Corridor Improvements Project Hotline: 833-777-7411



### Route 7 Corridor Improvements Project: Dogwood Pattern on Noise Barriers

**Jennifer Thomas** <jennifer.thomas@shirleycontracting.com> Reply-To: jennifer.thomas@shirleycontracting.com

Mon, Feb 10, 2020 at 5:27 PM

To: John Baione <ibaione748@gmail.com>

To: John Baione < jbaione / 48@gmail.com>

Cc: "Muchenje, Lovejoy 'LJ' P.E. (VDOT)" <Lovejoy.Muchenje@vdot.virginia.gov>, Md Rahman <md.rahman@vdot.virginia.gov>, Charles Pruitt <charles.pruitt@vdot.virginia.gov>, Richard Gutridge <ri>crichard.gutridge@vdot.virginia.gov>, "Kuntz, Steven" <skuntz@dewberry.com>, Jeffrey Austin <jaustin@shirleycontracting.com>

Mr. Baione:

Thank you for sending your noise barrier response form to the Route 7 Corridor Improvements Project team. Please see the response (below in red) to the question that you submitted with the form:

1. "Why is the decorative side facing traffic & not the property owners."

Due to the need for sound absorption on the road side of the barriers and the way the noise barriers must be constructed, the dogwood finish at the top of the panels will be placed on the road side.

The depth variations of the combined dogwood/ashlar stone pattern that contribute to sound absorption require that the panels be cast on a horizontal plane with the road side of the panels face down to allow the weight of the concrete to fully fill in the road side of the form's deeper grooves/valleys and higher peaks.

As the concrete settles into the road side of the forms, the residential side of the panel is then smoothed out and stamped with the stone pattern. The dogwood pattern has deeper grooves than stamping will permit. The result is that the road side of the panel has deeper grooves/valleys and higher peaks than the residential side, and it is this depth that contributes to the noise absorption qualities of the road side of the panel.

If you have any additional questions, please feel free to contact me.

Thanks so much!

Best regards,

Jennifer

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Jennifer A. Thomas | Public Relations Specialist SHIRLEY CONTRACTING COMPANY, LLC 45240 Business Court, Suite 100 | Dulles, VA | 20166 p. 571-447-7742 jennifer.thomas@shirleycontracting.com

shirleycontracting.com

Route 7 Corridor Improvements Project Hotline: 833-777-7411



### **Route 7 Corridor Improvements Project Noise Barriers**

Jennifer Thomas < jennifer.thomas@shirleycontracting.com>

Wed, Mar 4, 2020 at 2:03 PM

Reply-To: jennifer.thomas@shirleycontracting.com

To: dataservinc@hotmail.com

Cc: "Muchenje, Lovejoy 'LJ' P.E. (VDOT)" <Lovejoy.Muchenje@vdot.virginia.gov>, Jeffrey Austin

<jaustin@shirleycontracting.com>, "Kuntz, Steven" <skuntz@dewberry.com>, Md Rahman <md.rahman@vdot.virginia.gov>,

Charles Pruitt <charles.pruitt@vdot.virginia.gov>, Richard Gutridge <richard.gutridge@vdot.virginia.gov>

Mr. Parsons:

Thank you for sending in your noise barrier response form with the attached letter.

A Final Noise Report was completed as part of the Route 7 Corridor Improvements Project. The report was completed per the Federal Noise Regulation and VDOT's Noise Policy. Your property is represented by site B-62 in the Final Noise Report. According to the results of the analysis, the future noise levels (with the project in place) are predicted to be 68 decibels. VDOT's noise abatement criteria is set at 66 decibels. Since the predicted future noise levels at your property are above VDOT's noise abatement criteria, a noise barrier was evaluated and found to be warranted. The evaluated barrier system 'Barrier System B1-B5, D1' was also shown to be feasible and reasonable. Per the VDOT's noise policy, a barrier is considered feasible if its shown to provide a minimum of 5 decibel of noise reduction to the majority of the impacted sites. In addition, a barrier is considered reasonable if the ratio of the total area of the barrier (Square Feet) and the total number of benefitted properties (i.e. those sites receiving at least 5 decibels of noise reduction from the proposed noise barrier) is shown to be 1,600 or less. The reasonable number for 'Barrier System B1-B5, D1' was shown to be 1,234.

The barrier in front of your property was evaluated as a system since the barriers are interdependent. In other words, the individual Barrier B5B was shown to provide noise mitigation to sites behind both Barrier D1 and Barrier B5. Similarly, Barrier B5 was shown to provide noise mitigation to sites behind Barrier B5B and Barrier B4. Barrier B4 was shown to provide mitigation to sites behind Barrier B5 and Barrier B3. Because of the unique nature of the Route 7 project, this pattern of interdependency was shown all the way to Barrier 1. Because 'Barrier System B1-B5, D1' is a barrier system, it was evaluated as such.

The ultimate decision on whether the proposed barrier is constructed or not will be determined based on votes received from the benefitted property owners and tenants--that is, those property owners/tenants whose parcels are expected to receive a noise reduction of at least 5 decibels by the proposed noise barrier/barrier system. At the conclusion of the voting process, the votes are tallied. If the majority of respondents are shown to be in favor of the barrier, then the barrier is constructed. Depending on the outcome of the voting process, *partial mitigation* may be considered. Partial mitigation is essentially where one barrier segment (instead of the entire barrier system) is constructed. For example, if the majority are in favor of the barrier, but those not in favor of the barrier are at one end of the barrier, then the Design-Build team may perform further analysis to determine if the remaining portion of the barrier would still be feasible and reasonable as defined by Federal Highway Administration and VDOT noise abatement policies. We are still in the process of collecting the voting results. If the voting results reveal a cluster of "No" votes at one end of the Barrier B1-B5, D1 system, partial mitigation may be evaluated.

If you have any additional questions about the Route 7 project, please feel free to contact me at any time.

Best regards,

Jennifer

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Jennifer A. Thomas | Public Relations Specialist SHIRLEY CONTRACTING COMPANY, LLC 45240 Business Court, Suite 100 | Dulles, VA | 20166 p. 571-447-7742 jennifer.thomas@shirleycontracting.com shirleycontracting.com

Route 7 Corridor Improvements Project Hotline: 833-777-7411





### Route 7 Corridor Improvements Project: Dogwood Pattern on Noise Barriers

Jennifer Thomas < jennifer.thomas@shirleycontracting.com>

Mon, Feb 10, 2020 at 5:20 PM

Reply-To: jennifer.thomas@shirleycontracting.com

To: nicholsanddiamonds@cox.net

Cc: "Muchenje, Lovejoy 'LJ' P.E. (VDOT)" <Lovejoy.Muchenje@vdot.virginia.gov>, Jeffrey Austin

<jaustin@shirleycontracting.com>, "Kuntz, Steven" <skuntz@dewberry.com>, Md Rahman <md.rahman@vdot.virginia.gov>,
Charles Pruitt <charles.pruitt@vdot.virginia.gov>, Richard Gutridge <richard.gutridge@vdot.virginia.gov>

Ms. Nichols:

Thank you for sending your noise barrier response form to the Route 7 Corridor Improvements Project team. Please see the response (below in red) to the comment that you submitted with the form:

1. "The dogwood pattern on the noise barrier should be on the homeowner's side, since the homeowner has to look at the barrier, forever! Better yet, put the dogwood pattern on <u>both</u> sides of the barrier."

Due to the need for sound absorption on the road side of the barriers and the way the noise barriers must be constructed, the dogwood finish at the top of the panels will be placed on the road side.

The depth variations of the combined dogwood/ashlar stone pattern that contribute to sound absorption require that the panels be cast on a horizontal plane with the road side of the panels face down to allow the weight of the concrete to fully fill in the road side of the form's deeper grooves/valleys and higher peaks.

As the concrete settles into the road side of the forms, the residential side of the panel is then smoothed out and stamped with the stone pattern. The dogwood pattern has deeper grooves than stamping will permit. The result is that the road side of the panel has deeper grooves/valleys and higher peaks than the residential side, and it is this depth that contributes to the noise absorption qualities of the road side of the panel.

If you have any additional questions, please feel free to contact me.

Thanks so much!

Best regards,

Jennifer

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Jennifer A. Thomas | Public Relations Specialist SHIRLEY CONTRACTING COMPANY, LLC 45240 Business Court, Suite 100 | Dulles, VA | 20166 p. 571-447-7742 jennifer.thomas@shirleycontracting.com shirleycontracting.com

Route 7 Corridor Improvements Project Hotline: 833-777-7411



### Route 7 Corridor Improvements Project: Proposed Noise Barrier N1

**Jennifer Thomas** <jennifer.thomas@shirleycontracting.com> Reply-To: jennifer.thomas@shirleycontracting.com

Mon, Feb 10, 2020 at 3:56 PM

To: khaled.amro@gmail.com

Cc: Jeffrey Austin <jaustin@shirleycontracting.com>, "Kuntz, Steven" <skuntz@dewberry.com>, Md Rahman <md.rahman@vdot.virginia.gov>, Charles Pruitt <charles.pruitt@vdot.virginia.gov>, Richard Gutridge <richard.gutridge@vdot.virginia.gov>, "Muchenje, Lovejoy 'LJ' P.E. (VDOT)" <Lovejoy.Muchenje@vdot.virginia.gov>

#### Mr. Amro:

In response to your question about the location of proposed noise barrier N1 that was submitted with your noise barrier form, the placement of the barrier at this location is governed by sight distance. If proposed barrier N1 were placed between the service road and Route 7, vehicles making a right turn from EB Route 7 to Laurel Hill Road and vehicles on the service road would not be able to see each other. Therefore, for safety reasons, the proposed noise barrier was placed at its current location.

If you have any further questions, please feel free to contact me.

Thanks so much!

Best regards,

Jennifer

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Jennifer A. Thomas | Public Relations Specialist SHIRLEY CONTRACTING COMPANY, LLC 45240 Business Court, Suite 100 | Dulles, VA | 20166 p. 571-447-7742 jennifer.thomas@shirleycontracting.com shirleycontracting.com

Route 7 Corridor Improvements Project Hotline: 833-777-7411



### Route 7 Corridor Improvements Project Questions: 1280 Middleton Court

Jennifer Thomas < jennifer.thomas@shirleycontracting.com>

Wed, Feb 19, 2020 at 5:25 PM

Reply-To: jennifer.thomas@shirleycontracting.com

To: lmanziano@gmail.com

Cc: Jeffrey Austin <jaustin@shirleycontracting.com>, "Kuntz, Steven" <skuntz@dewberry.com>, Md Rahman <md.rahman@vdot.virginia.gov>, Charles Pruitt <charles.pruitt@vdot.virginia.gov>, Richard Gutridge <richard.gutridge@vdot.virginia.gov>, "Muchenje, Lovejoy 'LJ' P.E. (VDOT)" <Lovejoy.Muchenje@vdot.virginia.gov>, Ryan Marrah <ryan.marrah@shirleycontracting.com>

In response to your questions that were written in the Comments section on the noise wall voting response form that you mailed to us, areas of VDOT right-of-way and temporary and permanent easements that are disturbed for the construction of the project will be graded and seeded with VDOT-approved grass seed.

Detailed information on existing and projected noise levels are documented in the project's Final Noise Analysis. The existing (2018) loudest-hour noise level at 1280 Middleton Court, identified as receptor G-168 in Table 7 of the Final Noise Analysis, is estimated at 63 decibels. The projected loudest-hour noise level in 2040 without a noise wall at this location is 68 decibels, and the projected loudest-hour noise level in 2040 with a noise wall at this location is 59 decibels (see Table 22, Final Noise Analysis).

If you have any additional questions, please feel free to contact me.

Thanks so much!

Best regards,

Jennifer

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Jennifer A. Thomas | Public Relations Specialist
SHIRLEY CONTRACTING COMPANY, LLC
45240 Business Court, Suite 100 | Dulles, VA | 20166
p. 571-447-7742
jennifer.thomas@shirleycontracting.com
shirleycontracting.com

**Route 7 Corridor Improvements Project Hotline: 833-777-7411** 



### **Question on Noise Barrier Response**

**Jennifer Thomas** <jennifer.thomas@shirleycontracting.com> To: selbassioni@cox.net

Thu, Feb 6, 2020 at 2:25 PM

In response to the question you submitted with your noise barrier response form (see attached), the package that you received from VDOT should have included a map that showed the limits of noise barriers I4-I6. If you did not receive a map showing the noise wall locations, please let me know and I'll send it to you via email.

Thanks so much!

Best regards,

**Jennifer** 

---

Jennifer A. Thomas | Public Relations Specialist SHIRLEY CONTRACTING COMPANY, LLC 45240 Business Court, Suite 100 | Dulles, VA | 20166 p. 571-447-7742

jennifer.thomas@shirleycontracting.com shirleycontracting.com

Route 7 Corridor Improvements Project Hotline: 833-777-7411

Route 7 Corridor Improvements Project Web Site: ConnectRoute7.org

SKM\_C364e20020613490.pdf



### **Route 7 Corridor Improvements Project Questions**

Jennifer Thomas < jennifer.thomas@shirleycontracting.com>

Fri, Feb 7, 2020 at 9:31 AM

To: wfhom@yahoo.com

Cc: Jeffrey Austin <jaustin@shirleycontracting.com>, Md Rahman <md.rahman@vdot.virginia.gov>, Charles Pruitt <charles.pruitt@vdot.virginia.gov>, Richard Gutridge <richard.gutridge@vdot.virginia.gov>, "Chellappa, Smitha L." <Smitha.Chellappa@fairfaxcounty.gov>, "Kuntz, Steven" <skuntz@dewberry.com>

Mr. Hom:

In response to the questions you submitted with the Route 7 Corridor Improvements Potential Noise Barrier Public Input Survey Questionnaire, lighting on the project will be replaced "in kind"--that is, any existing street lights that must be moved to accommodate the construction will be replaced with LED lights that provide equivalent illumination. These lighting replacements are intended to provide roadway lighting and will not provide lighting specifically to illuminate areas behind the proposed noise barriers. Requests for additional lighting in specific areas may be submitted to the Fairfax County Department of Public Works and Environmental Services (https://www.fairfaxcounty.gov/publicworks/).

Prior to the start of construction, there was a wide paved shoulder adjacent to the westbound lanes of Route 7 between Amanda Drive and the deceleration lane for Great Passage Boulevard, but this was not marked as or intended to be used as an acceleration lane. Acceleration lanes are not typically provided on roadways such as Route 7 since they don't provide enough length to accommodate full acceleration adjacent to the thru-lanes, and create speed differentials which are undesirable. This is partially due to the short distance between intersections, and because of this there are no plans for an acceleration lane in this area as part of the proposed improvements. The optimization of the traffic signal at Baron Cameron Avenue and the additional thru-lane for traffic in this area may result in reduced congestion per-lane and additional gaps in traffic to accommodate entering vehicles from Amanda Drive, improving the right-turn maneuver to westbound Route 7.

If you have any additional questions, please feel free to contact me at any time.

Thanks so much!

Best regards,

**Jennifer** 

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Jennifer A. Thomas | Public Relations Specialist SHIRLEY CONTRACTING COMPANY, LLC 45240 Business Court, Suite 100 | Dulles, VA | 20166 p. 571-447-7742

jennifer.thomas@shirleycontracting.com shirleycontracting.com

Route 7 Corridor Improvements Project Hotline: 833-777-7411



## **Route 7 Corridor Improvements Project: Wooden Fence**

**Jennifer Thomas** <jennifer.thomas@shirleycontracting.com> To: fybwlb@aol.com

Fri, Feb 7, 2020 at 3:35 PM

Mr. Bekenstein:

In response to the question you submitted with your noise barrier questionnaire form regarding the wooden fence between the parcels on Water Pointe Lane and Route 7, the project will not be impacting this fence.

If you have any additional questions, please feel free to contact me at any time.

Thanks so much!

Best regards,

Jennifer

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